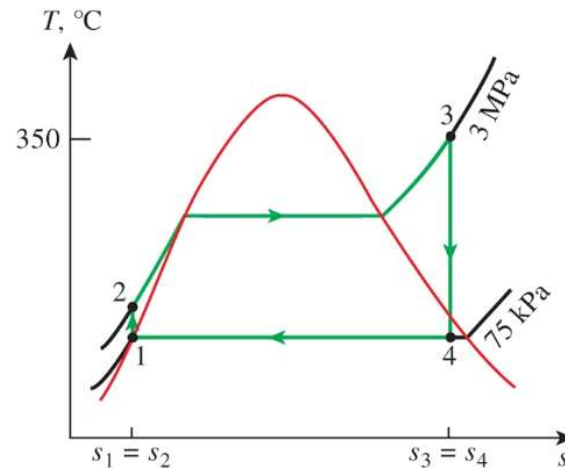
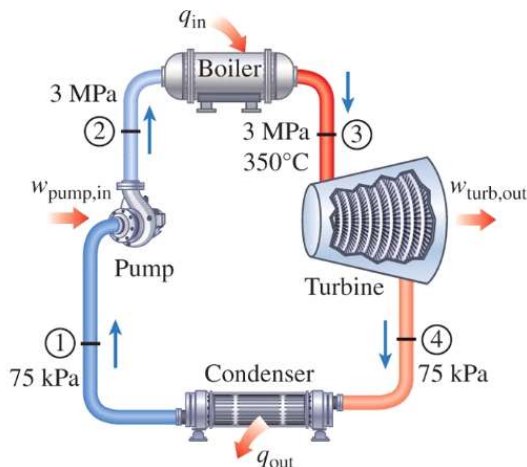


**Given:**  $\text{kJ} := 1000\text{J}$

Consider a steam power plant operating on the simple ideal Rankine cycle. Steam enters the turbine at 3 MPa and 350°C and is condensed in the condenser at a pressure of 75 kPa.

$$P_3 := 3\text{ MPa} \quad T_3 := 350\text{ }^{\circ}\text{C} \quad P_4 := 75\text{ kPa}$$



**Required:**

Determine the thermal efficiency.

**Solution:**

At state 1, the pressure will be the same as state 4 and a saturated liquid.

$$P_1 := P_4 = 75\text{ kPa} \quad x_1 := 0$$

Going to Table A-5 @  $P_1 = 75\text{ kPa}$  &  $x_1 = 0$  shows

$$h_1 := 384.44 \frac{\text{kJ}}{\text{kg}} \quad \nu_1 := 0.001037 \frac{\text{m}^3}{\text{kg}} \quad T_1 := 91.76\text{ }^{\circ}\text{C}$$

At state 2, the pressure will be the same as state 3 and will have the same entropy as state 1.

$$P_2 := P_3 = 3\text{ MPa}$$

The specific work of the pump when using an incompressible fluid may then be determined by

$$w_p := \nu_1 \cdot (P_2 - P_1) = 3.033 \frac{\text{kJ}}{\text{kg}}$$

It is also known that the specific work of the pump is given by

$$w_p = h_2 - h_1$$

The specific enthalpy at state 2 may then be found by

$$h_2 := w_p + h_1 = 387.473 \frac{\text{kJ}}{\text{kg}}$$

Going to Table A-4 @  $T_3 = 350\text{ }^{\circ}\text{C}$  &  $P_3 = 3000\text{ kPa}$  shows that the state is superheated.

**Solution (contd.):**

Going to Table A-6 @  $T_3 = 350^\circ\text{C}$  &  $P_3 = 3\text{ MPa}$  shows

$$h_3 := 3116.1 \frac{\text{kJ}}{\text{kg}} \quad s_3 := 6.7450 \frac{\text{kJ}}{\text{kg}\cdot\text{K}}$$

At state 4, the entropy will be the same as state 3.

$$s_4 := s_3 = 6.745 \frac{\text{kJ}}{\text{kg}\cdot\text{K}}$$

Going to Table A-5 @  $P_4 = 75\text{ kPa}$  &  $s_4 = 6.745 \frac{\text{kJ}}{\text{kg}\cdot\text{K}}$  shows the state is in the two phase region.

$$s_f := 1.2132 \frac{\text{kJ}}{\text{kg}\cdot\text{K}} \quad s_g := 7.4558 \frac{\text{kJ}}{\text{kg}\cdot\text{K}} \quad h_f := 384.44 \frac{\text{kJ}}{\text{kg}} \quad h_g := 2662.4 \frac{\text{kJ}}{\text{kg}}$$

$$x_4 := \frac{s_4 - s_f}{s_g - s_f} = 0.886 \quad h_4 := h_f + x_4 \cdot (h_g - h_f) = 2403.0 \frac{\text{kJ}}{\text{kg}}$$

The specific heat rejected by the cycle is then

$$q_{\text{out}} := h_4 - h_1 = 2018.6 \frac{\text{kJ}}{\text{kg}}$$

The specific heat added to the cycle is then

$$q_{\text{in}} := h_3 - h_2 = 2728.6 \frac{\text{kJ}}{\text{kg}}$$

The thermal efficiency of the cycle is then given by

$$\eta_{\text{th}} := 1 - \frac{q_{\text{out}}}{q_{\text{in}}} = 26.0\%$$

Alternatively, the thermal efficiency of the cycle could have been found by calculating the specific work of the turbine. This is shown below.

$$w_t := h_3 - h_4 = 713.075 \frac{\text{kJ}}{\text{kg}}$$

The net work is then

$$w_{\text{net}} := w_t - w_p = 710.042 \frac{\text{kJ}}{\text{kg}}$$

The thermal efficiency may then be found by

$$\eta_{\text{th}} := \frac{w_{\text{net}}}{q_{\text{in}}} = 26.0\%$$

The Carnot efficiency may also be calculated.

$$\eta_{\text{th,rev}} := 1 - \frac{T_1}{T_3} = 41.4\%$$