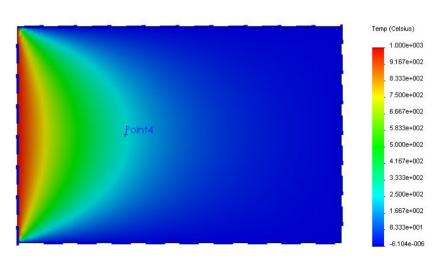
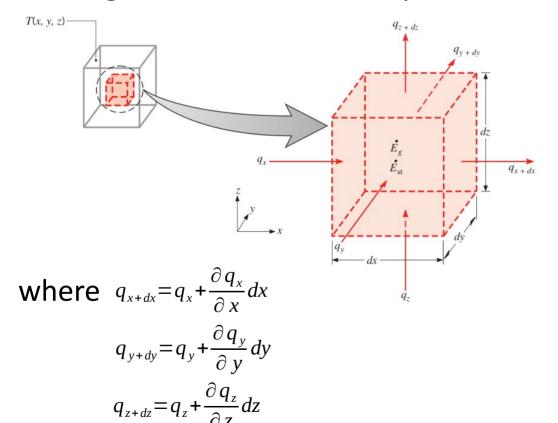


- Goal is to describe the temperature in any particular point within a substance.
- This is known as the temperature distribution.
- Once the distribution is known, the conduction heat flux may be determined at any particular point.
- First lets consider a homogeneous substance that is described using Cartesian coordinates.
- The temperature distribution would then be



Looking at a differential sized portion of the material



- The \dot{E}_g term refers to the rate of thermal energy generation (e.g. resistance heating).
- The \dot{E}_{st} term refers to the energy storage ability of the material; this is related to the thermal capacity of the substance.

- 1st Law may then be applied.
- Then some math is done.
- Which yields

$$\frac{\partial}{\partial x} \left(k \frac{\partial T}{\partial x} \right) + \frac{\partial}{\partial y} \left(k \frac{\partial T}{\partial y} \right) + \frac{\partial}{\partial z} \left(k \frac{\partial T}{\partial z} \right) + \dot{q} = \rho c_p \frac{\partial T}{\partial t}$$

- This is known as the heat diffusion equation for Cartesian coordinates.
- It is a partial differential equation.
- It governs the temperature distribution within a material.

Some Simplified Forms

• If the thermal conductivity k is constant

$$\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} + \frac{\dot{q}}{k} = \frac{1}{\alpha} \frac{\partial T}{\partial t}$$

• If the system is steady state

$$\frac{\partial}{\partial x} \left(k \frac{\partial T}{\partial x} \right) + \frac{\partial}{\partial y} \left(k \frac{\partial T}{\partial y} \right) + \frac{\partial}{\partial z} \left(k \frac{\partial T}{\partial z} \right) + \dot{q} = 0$$

If the heat transfer is 1D

$$\frac{\partial}{\partial x} (k \frac{\partial T}{\partial x}) + \dot{q} = \rho c_p \frac{\partial T}{\partial t}$$

$$\frac{\partial}{\partial y} (k \frac{\partial T}{\partial y}) + \dot{q} = \rho c_p \frac{\partial T}{\partial t}$$

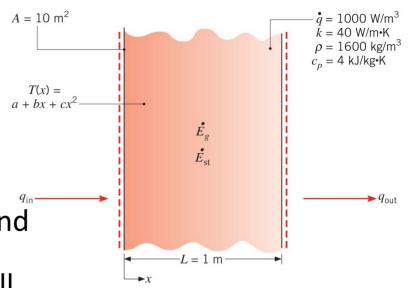
$$\frac{\partial}{\partial z} (k \frac{\partial T}{\partial z}) + \dot{q} = \rho c_p \frac{\partial T}{\partial t}$$

Example 1

The temperature distribution across a wall $1 m_{a+bx+cx^2}^{T(x)}$ thick at a certain instant of time is given as

$$T(x)=a+bx+cx^2$$

where T is in ${}^{\circ}C$ and x is in meters, while a, b, and c are as shown to the right. A uniform heat generation of $q = 1000 \ W/m^3$, is present in the wall of area $10 \ m^2$ having properties as shown. Determine the rate of heat transfer entering and leaving the wall at $x=0 \ m$ and $x=1 \ m$, respectively. Determine the rate of change of energy storage in the wall. Determine the time rate of temperature change at x=0, 0.25, and $0.5 \ m$.



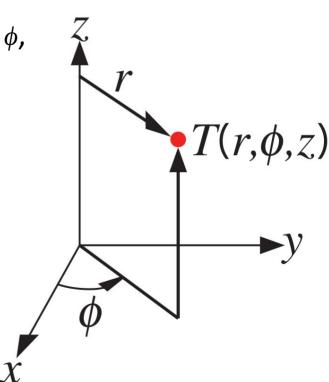
$$a=900 °C$$

$$b=-300 \frac{°C}{m}$$

$$c=-50 \frac{°C}{2}$$

Cylindrical Coordinate System

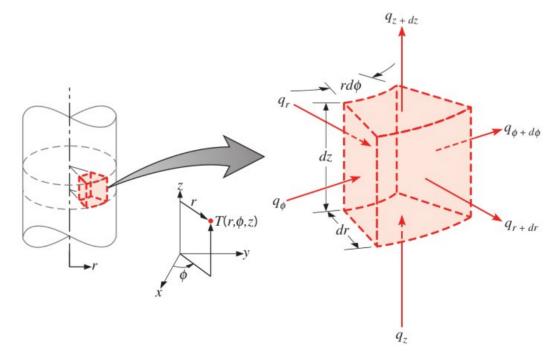
- An alternative coordinate system
- Instead of x, y, and z like when using Cartesian coordinates, cylindrical coordinate system use r, ϕ , and z.
- r is a radius.
- ϕ is an angle.
- z is a height.
- The advantage is when cylindrical objects are analyzed.



Heat Diffusion Equation for Cylindrical Systems

 Using the cylindrical coordinate system, a similar approach may be used to derive the heat diffusion equation

$$\frac{1}{r}\frac{\partial}{\partial r}\left(kr\frac{\partial T}{\partial r}\right) + \frac{1}{r^2}\frac{\partial}{\partial \phi}\left(k\frac{\partial T}{\partial \phi}\right) + \frac{\partial}{\partial z}\left(k\frac{\partial T}{\partial z}\right) + \dot{q} = \rho c_p \frac{\partial T}{\partial t}$$



Some Simplified Forms

• If the thermal conductivity k is constant

$$\frac{1}{r}\frac{\partial}{\partial r}\left(r\frac{\partial T}{\partial r}\right) + \frac{1}{r^2}\frac{\partial^2 T}{\partial \phi^2} + \frac{\partial^2 T}{\partial z^2} + \frac{\dot{q}}{k} = \frac{1}{\alpha}\frac{\partial T}{\partial t}$$

If the system is steady state

$$\frac{1}{r}\frac{\partial}{\partial r}\left(kr\frac{\partial T}{\partial r}\right) + \frac{1}{r^2}\frac{\partial}{\partial \phi}\left(k\frac{\partial T}{\partial \phi}\right) + \frac{\partial}{\partial z}\left(k\frac{\partial T}{\partial z}\right) + \dot{q} = 0$$

If the heat transfer is 1D

$$\frac{1}{r} \frac{\partial}{\partial r} (kr \frac{\partial T}{\partial r}) + \dot{q} = \rho c_p \frac{\partial T}{\partial t}$$

$$\frac{1}{r^2} \frac{\partial}{\partial \phi} (k \frac{\partial T}{\partial \phi}) + \dot{q} = \rho c_p \frac{\partial T}{\partial t}$$

$$\frac{\partial}{\partial z} (k \frac{\partial T}{\partial z}) + \dot{q} = \rho c_p \frac{\partial T}{\partial t}$$

Example 2

Uniform internal heat generation of 5×10^7 W/m³ is occurring in a cylindrical nuclear reactor fuel rod of 50 mm diameter, and under steady state conditions the temperature distribution is of the form

$$T(r)=a+br^2$$

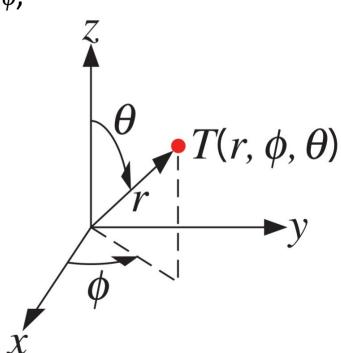
where T is in ${}^{\circ}C$ and r in meters, while a and b are as indicate below. The fuel rod properties are shown below.

- (a) What is the rate of heat transfer per unit length of the rod at $r=0 \ mm$ (the center line) and at $r=25 \ mm$ (the surface)?
- (b) If the reactor power level is suddenly increased to 10^8 W/m³, what is the initial time rate of temperature change at the center line and rod surface?

$$a = 800 \,^{\circ}C$$
 $b = -4.167 \times 10^{5} \,^{\circ}C \over m^{2}$ $k = 30 \, \frac{W}{m \, K}$ $\rho = 1100 \, \frac{kg}{m^{3}}$ $c_{p} = 800 \, \frac{J}{kg \, K}$

Spherical Coordinate System

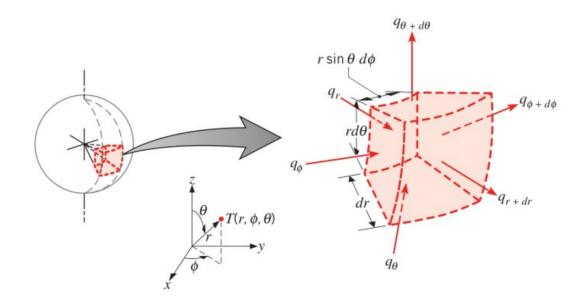
- Another alternative coordinate system
- Instead of x, y, and z like when using Cartesian coordinates, cylindrical coordinate system use r, ϕ , and θ .
- r is a radius.
- ϕ is an angle within the x-y plane.
- θ is an angle from the z axis.
- The advantage is when spherical objects are analyzed.



Heat Diffusion Equation for Spherical Systems

 Using the spherical coordinate system, a similar approach may be used to derive the heat diffusion equation

$$\frac{1}{r^2} \frac{\partial}{\partial r} (k r^2 \frac{\partial T}{\partial r}) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial}{\partial \phi} (k \frac{\partial T}{\partial \phi}) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} (k \sin \theta \frac{\partial T}{\partial \theta}) + \dot{q} = \rho c_p \frac{\partial T}{\partial t}$$



Some Simplified Forms

• If the thermal conductivity k is constant

$$\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial T}{\partial r} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 T}{\partial \phi^2} + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial T}{\partial \theta} \right) + \frac{\dot{q}}{k} = \frac{1}{\alpha} \frac{\partial T}{\partial t}$$

If the system is steady state

$$\frac{1}{r^2} \frac{\partial}{\partial r} (kr^2 \frac{\partial T}{\partial r}) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial}{\partial \phi} (k \frac{\partial T}{\partial \phi}) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} (k \sin \theta \frac{\partial T}{\partial \theta}) + \dot{q} = 0$$

• If the heat transfer is 1D

$$\frac{1}{r^{2}} \frac{\partial}{\partial r} (kr^{2} \frac{\partial T}{\partial r}) + \dot{q} = \rho c_{p} \frac{\partial T}{\partial t}$$

$$\frac{1}{r^{2} \sin^{2} \theta} \frac{\partial}{\partial \phi} (k \frac{\partial T}{\partial \phi}) + \dot{q} = \rho c_{p} \frac{\partial T}{\partial t}$$

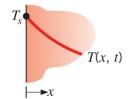
$$\frac{1}{r^{2} \sin \theta} \frac{\partial}{\partial \theta} (k \sin \theta \frac{\partial T}{\partial \theta}) + \dot{q} = \rho c_{p} \frac{\partial T}{\partial t}$$

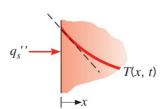
Boundary and Initial Conditions

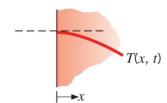
- Boundary and initial conditions are constraints placed on a system that dictate how a particular location (as in the case of boundary conditions) or instant of time (as in the case of initial conditions) behaves.
- There are several common boundary conditions:
 - Constant surface temperature $T(0,t)=T_s$

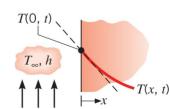
 - Constant surface temperature

 Constant surface heat flux $-k \frac{\partial T}{\partial x}\Big|_{x=0} = q_s''$ Adiabatic surface $\frac{\partial T}{\partial x}\Big|_{x=0} = 0$ Convection surface condition $-k \frac{\partial T}{\partial x}\Big|_{x=0} = h(T_{\infty} T(0, t))$









Example 3

A long copper bar of rectangular cross section, whose width w is much greater than its thickness L, is maintained in contact with a heat sink at its lower surface, and the temperature throughout the bar is approximately equal to that of the sink, T_{o} . Suddenly, an electric current is passed through the bar and a stream of air of temperature T_{∞} is passed over the top surface, while the bottom surface continues to be maintained at T_{o} . Determine the boundary and initial conditions that could be used to solve this arrangement for the temperature distribution as a function of both position and time. Copper bar (k, α) T(x, y, z, t)

Heat sink T_o