#### GLOBAL MODEL - CMI - SD150414 - AUTRE FLUIDE

# **Equations**

function 
$$\Delta P_a \left( \dot{Q}, \, \rho_v, \, \mu_v, \, A_v, \, d_v, \, l_a, \, h_{lv}, \, Re \right)$$
 (1)

If 
$$Re < 2300$$
 then (2)

$$\Delta P_a = \frac{32 \cdot \mu_v \cdot \dot{Q} \cdot l_a}{\rho_v \cdot A_v \cdot h_{lv} \cdot d_v^2} \tag{3}$$

else (4)

$$\Delta P_a = \left(\frac{0.3164}{Re^{0.25}}\right) \cdot \frac{\dot{Q}^2 \cdot l_a}{2 \cdot \rho_v \cdot A_v^2 \cdot h_{lv}^2 \cdot d_v} \tag{5}$$

endif (6)

end (7)

 $Subprogram Caloduc \left(Pipe Mat\$, \ Fluid\$, \ ORCFluid\$, \ d_i, \ d_o, \ L_e, \ L_c, \ L_a, \ u_f, \ \dot{M}_f, \ \rho_f, \ T_{in,f}, \ P_f, \ P_{atm}, \ T_{ev,wf}, \ h_{f,c}: \dot{Q}_{cv,wf}, \ h_{f,c}: \dot$ 

#### Rayons

$$r_o = D_o/2 \tag{9}$$

$$r_i = D_i/2 \tag{10}$$

## 1. Evaporateur

## 1.1 Conduction paroi

$$T_{p,e} = \frac{T_{we,in} + T_{we,out}}{2} \tag{11}$$

$$\lambda_e = k \left( PipeMat\$, \ \mathsf{T} = T_{p,e} \right) \tag{12}$$

## 1.2 Evaporation (h<sub>e</sub>)

Imura correlation

$$h_e = 0.32 \cdot \left( \frac{\rho_{l,e}^{0.65} \cdot k_{l,e}^{0.3} \cdot Cp_{l,e}^{0.7} \cdot g\#^{0.2} \cdot q_e^{0.4}}{\rho_{v,e}^{0.25} \cdot h_{lv,e}^{0.4} \cdot \mu_{l,e}^{0.1}} \right) \cdot \left( P_{sat,e} / P_{atm} \right)^{0.3}$$

$$(13)$$

$$q_e = \frac{\dot{Q}_e}{2 \cdot \pi \cdot L_e \cdot r_i} \tag{14}$$

$$T_{sat,e} = T_{sat} \left( Fluid\$, \ P = P_{sat,e} \right) \tag{15}$$

$$\rho_{l,e} = \rho \left( Fluid\$, \ \mathbf{P} = P_{sat,e}, \ \mathbf{X} = 0 \right) \tag{16}$$

$$k_{l,e} = k \left( Fluid\$, \ \mathbf{P} = P_{sat,e}, \ \mathbf{X} = 0 \right) \tag{17}$$

$$cp_{l,e} = c_p \left( Fluid\$, \ \mathbf{P} = P_{sat,e}, \ \mathbf{X} = 0 \right)$$
 (18)

$$\rho_{v,e} = \rho \left( Fluid\$, \ \mathbf{P} = P_{sat,e}, \ \mathbf{X} = 1 \right) \tag{19}$$

$$h_{lv,e} = h(Fluid\$, P = P_{sat,e}, X = 1) - h(Fluid\$, P = P_{sat,e}, X = 0)$$
 (20)

$$\mu_{l,e} = \mu \left( Fluid\$, \ \mathbf{P} = P_{sat,e}, \ \mathbf{X} = 0 \right) \tag{21}$$

$$\mu_{v,e} = \mu \left( Fluid\$, \ \mathbf{P} = P_{sat,e}, \ \mathbf{X} = 1 \right) \tag{22}$$

## 1.3 Convection et Rayonnement fumées (h<sub>f</sub>)

#### Convection

## Rayonnement idéal

$$h_{f,r} = sigma\# \cdot \frac{(T_{in,f} + 273.15)^4 - (T_{we,out} + 273.15)^4}{T_{in,f} - T_{we,out}}$$
(23)

#### Somme

$$h_f = h_{f,r} + h_{f,c} \tag{24}$$

#### 1.4 Global

$$\dot{Q}_e = \frac{2 \cdot \pi \cdot L_e \cdot \lambda_e}{\ln \left( r_o / r_i \right)} \cdot \left( T_{we,out} - T_{we,in} \right) \tag{25}$$

$$\dot{Q}_e = 2 \cdot \pi \cdot L_e \cdot r_i \cdot h_e \cdot (T_{we,in} - T_{sat,e}) \tag{26}$$

$$\dot{Q}_e = 2 \cdot \pi \cdot L_e \cdot r_o \cdot h_f \cdot (T_{in,f} - T_{we,out}) \tag{27}$$

$$\dot{M}_v = \dot{Q}_e / h_{lv,e} \tag{28}$$

## 2 Pertes de charge vapeur

VDI

$$A_v = 0.9 \cdot \left(\pi \cdot r_i^2\right) \tag{29}$$

$$A_v = \pi \cdot \frac{d_v^2}{4} \tag{30}$$

$$Re_a = \frac{\dot{Q}_e \cdot d_v}{\mu_{v.c} \cdot A_v \cdot h_{lv.c}} \tag{31}$$

$$\Delta P_a = \Delta P_a \left( \dot{Q}_c, \, \rho_{v,c}, \, \mu_{v,c}, \, A_v, \, d_v, \, l_a, \, h_{lv,c}, \, Re_a \right) \tag{32}$$

$$Re_{r,c} = \frac{\dot{Q}_c \cdot d_v/2}{\mu_{v,c} \cdot A_c \cdot h_{lv,c}} \tag{33}$$

$$A_c = 2 \cdot \pi \cdot L_c \cdot r_i \tag{34}$$

$$\Delta P_{c} = \frac{\Delta P_{a} \left( \dot{Q}_{c}, \ \rho_{v,c}, \ \mu_{v,c}, \ A_{v}, \ d_{v}, \ l_{c}, \ h_{lv,c}, \ Re_{a} \right)}{2} \tag{35}$$

$$Re_{r,e} = \frac{\dot{Q}_e \cdot d_v/2}{\mu_{v,e} \cdot A_e \cdot h_{lv,e}} \tag{36}$$

$$A_e = 2 \cdot \pi \cdot L_e \cdot r_i \tag{37}$$

$$\Delta P_e = \frac{\Delta P_a \left( \dot{Q}_e, \, \rho_{v,e}, \, \mu_{v,e}, \, A_v, \, d_v, \, l_e, \, h_{lv,e}, \, Re_a \right)}{2} \tag{38}$$

$$\Delta P_{ev,cd} = \frac{\Delta P_a + \Delta P_c + \Delta P_e}{100000} \tag{39}$$

$$P_{sat,c} = P_{sat,e} - \Delta P_{ev,cd} \tag{40}$$

#### 3. Condenseur

## 3.1 Conduction paroi

$$T_{p,c} = \frac{T_{wc,in} + T_{wc,out}}{2} \tag{41}$$

$$\lambda_c = k \left( PipeMat\$, \ T = \frac{T_{wc,in} + T_{wc,out}}{2} \right)$$
 (42)

#### 3.2 Condensation

#### Rohsenow, Wen and Guo correlation

$$h_N = 0.943 \cdot k_{l,c} / L_c \cdot \left( \frac{L_c^3 \cdot \rho_{l,c} \cdot (\rho_{l,c} - \rho_{v,c}) \cdot g\#}{\mu_{l,c} \cdot k_{l,c} \cdot (T_{sat,c} - T_{wc,in})} \cdot \left( h_{lv,c} + 0.68 \cdot cp_{l,c} \cdot (T_{sat,c} - T_{wc,in}) \right) \right)^{0.25}$$

$$(43)$$

$$P_{sat,c} = P_{sat} \left( Fluid\$, T = T_{sat,c} \right) \tag{44}$$

$$k_{l,c} = k \left( Fluid\$, P = P_{sat,c}, X = 0 \right) \tag{45}$$

$$h_{lv,c} = h(Fluid\$, P = P_{sat,c}, X = 1) - h(Fluid\$, P = P_{sat,c}, X = 0)$$
 (46)

$$cp_{l,c} = c_p \left( Fluid\$, \ P = P_{sat,c}, \ X = 0 \right) \tag{47}$$

$$\mu_{l,c} = \mu \left( Fluid\$, \ \mathbf{P} = P_{sat,c}, \ \mathbf{X} = 0 \right) \tag{48}$$

$$\mu_{v,c} = \mu \left( Fluid\$, \ P = P_{sat,c}, \ X = 1 \right)$$
 (49)

$$\rho_{v,c} = \rho \left( Fluid\$, \ \mathbf{P} = P_{sat,c}, \ \mathbf{X} = 1 \right) \tag{50}$$

$$\rho_{l,c} = \rho \left( Fluid\$, \ \mathbf{P} = P_{sat,c}, \ \mathbf{X} = 0 \right) \tag{51}$$

$$h_c = 1.51 \cdot h_N \cdot (P_{sat,c}/P_{crit})^{0.15}$$
 (52)

$$P_{crit} = P_{crit} (Water)$$
 (53)

#### 3.3 ORC evaporateur

## Cooper

$$h_{wf} = 55 \cdot M M_{wf}^{-0.5} \cdot q_c^{0.67} \cdot p_{r,wf}^{0.12} \cdot \left(-\log 10(p_{r,wf})\right)^{-0.55}$$
(54)

$$p_{r,wf} = \frac{P_{ev,wf}}{P_{crit}\left(ORCFluid\$\right)} \tag{55}$$

$$MM_{wf} = MW(ORCFluid\$)$$
 (56)

$$P_{ev,wf} = P_{sat} \left( ORCFluid\$, T = T_{ev,wf} \right)$$
(57)

3.4 Global

$$\dot{Q}_c = \dot{Q}_e \tag{58}$$

$$\dot{Q}_c = 2 \cdot \pi \cdot L_c \cdot r_o \cdot h_{wf} \cdot (T_{wc,out} - T_{ev,wf}) \tag{59}$$

$$\dot{Q}_c = \frac{2 \cdot \pi \cdot L_c \cdot \lambda_c}{\ln\left(r_o/r_i\right)} \cdot \left(T_{wc,in} - T_{wc,out}\right) \tag{60}$$

$$\dot{Q}_c = 2 \cdot \pi \cdot L_c \cdot r_i \cdot h_c \cdot (T_{sat,c} - T_{wc,in}) \tag{61}$$

$$q_c = \frac{\dot{Q}_c}{2 \cdot \pi \cdot L_c \cdot r_i} \tag{62}$$

#### 4 Limites de fonctionnement

#### 4.1 Limite d'entrainement

Habituellement la plus contraignante dans le cas d'un thermosyphon diphasique

$$\dot{Q}_{limit,ent} = 3.2 \cdot h_{lv,e} \cdot A_v \cdot \left(\rho_{v,e}^{-0.25} + \rho_{l,e}^{-0.25}\right)^{-2} \cdot \left(\sigma_{eau} \cdot g \# \cdot (\rho_{l,e} - \rho_{v,e})\right)^{0.25}$$
(63)

$$\sigma_{eau} = \gamma \left( Water, \ T = T_{sat,e} \right) \tag{64}$$

4.2 Limite d'ébullition

$$\dot{Q}_{limit,ebu} = (\pi \cdot d_v \cdot l_e) \cdot 0.149 \cdot \rho_{v,e} \cdot h_{lv,e} \cdot \left(\frac{\sigma_{eau} \cdot (\rho_{l,e} - \rho_{v,e}) \cdot g\#}{\rho_{v,e}^2}\right)^{0.25}$$

$$(65)$$

4.3 Limite sonique

$$\dot{Q}_{limit,son} = 0.474 \cdot A_v \cdot h_{lv,e} \cdot \left( \rho_{v,e} \cdot P_{sat,e} \cdot \left| 100000 \frac{\text{Pa}}{\text{bar}} \right| \right)^{0.5}$$
(66)

$$\dot{Q}_{cal} = \dot{Q}_c \tag{67}$$

end (68)

#### 1. Inputs et paramètres

1.1 Caractéristiques géométriques

$$A_f = 11.56 \text{ [m}^2\text{]}$$
 Aire du conduit de fumée (69)

1.2 Matériau et fluide

$$PipeMat\$ = \text{`Carbon\_steel'}$$
 (70)

$$Fluid\$ = \text{`Water'}$$
 (71)

1.3 Fluides secondaires

Point de fonctionnement du 11/09/2014 à 15:34:31

$$\rho_{f,N} = 1.242 \text{ [kg/m}^3]$$
 (72)

$$ORCFluid\$ = \text{`n-pentane'}$$
 (73)

1.4 Constantes

$$P_{atm} = 1 \text{ [bar]} \tag{74}$$

1.5 Echangeur caloduc

\$Constant nbr\_cal#=160

\$Constant nbr\_rangee#=20

$$nbr_{total,cal} = nbr_{cal\#} \tag{75}$$

$$nbr_{rangee,cal} = nbr_{rangee\#}$$
 (76)

$$nbr_{ligne,cal} = nbr_{cal\#}/nbr_{rangee\#}$$

$$\tag{77}$$

$$D_{ech} = 3.4 \text{ [m]}$$

#### 1.6 ORC

### 2 Echange thermique caloduc

Coefficient de convection moyen

 $\mathsf{call} \;\; External_{Flow,Inline,Bank} \big( \text{`Air'} \;, \; T_{in,f}, \; T_{out,f}, \; T_{we,moy}, \; 1, \; u_{f,1}, \; nbr_{cal\#}/nbr_{rangee\#}, \; D_o, \; S_T, \; S_L : h_{f,c}, \; \Delta p_f, \; Nusselt_f : left for the sum of the sum$ 

# Discrétisation spatiale

$$T_{f,1} = T_{in,f}$$
 (80)

duplicate 
$$i = 1, nbr_{cal\#}/nbr_{rangee\#}$$
 (81)

 $\textbf{call } \textit{Caloduc} \left( \textit{PipeMat\$}, \textit{Fluid\$}, \textit{ORCFluid\$}, \textit{d}_i, \textit{d}_o, \textit{L}_e, \textit{L}_c, \textit{L}_a, \textit{u}_{f,i}, \dot{\textit{M}}_f, \textit{\rho}_{f,i}, \textit{T}_{f,i}, \textit{P}_f, \textit{P}_{atm}, \textit{T}_{ev,wf}, \textit{h}_{f,c} : \dot{Q}_{cal,i}, \dot$ 

$$\rho_{f,i} = \rho_{f,N} \cdot \frac{273.15}{T_{f,i} + 273.15} \tag{83}$$

$$u_{f,i} = \frac{\dot{M}_f}{\rho_{f,i} \cdot A_f} \tag{84}$$

$$cp_{f,i} = 1300 \text{ [J/kg·K]}$$
 (85)

$$T_{f,i+1} = T_{f,i} - \dot{Q}_{cal,i} \cdot \frac{nbr_{rangee\#}}{\dot{M}_f \cdot cp_{f,i}}$$

$$(86)$$

end (87)

# Valeurs globales

$$T_{out,f} = T_{f,nbr,cal\#/nbr,rangee\#+1}$$
(88)

$$T_{we,moy} = \frac{\text{Sum}(T_{we,out,i} \cdot nbr_{rangee\#}, i = 1, nbr_{cal\#}/nbr_{rangee\#})}{nbr_{cal\#}}$$
(89)

$$\dot{Q}_{total} = \text{Sum} \Big( \dot{Q}_{cal,i} \cdot nbr_{rangee\#}, \ i = 1, \ nbr_{cal\#}/nbr_{rangee\#} \Big)$$

$$(90)$$

$$\dot{Q}_{total,limit,ent} = \text{Sum} \left( \dot{Q}_{limit,ent,i} \cdot nbr_{rangee\#}, \ i = 1, \ nbr_{cal\#}/nbr_{rangee\#} \right)$$
(91)

$$\dot{Q}_{moy} = \dot{Q}_{total}/nbr_{cal\#} \tag{92}$$

$$\dot{Q}_{max} = \dot{Q}_{cal,1} \tag{93}$$

$$\dot{Q}_{min} = \dot{Q}_{cal,nbr,cal\#/nbr,rangee\#} \tag{94}$$

$$\dot{Q}_{limit,ent,max} = \dot{Q}_{limit,ent,1} \tag{95}$$

$$\dot{Q}_{limit,ent,min} = \dot{Q}_{limit,ent,nbr,cal\#/nbr,rangee\#}$$
(96)

$$\dot{Q}_{limit,ent,moy} = \dot{Q}_{total,limit,ent}/nbr_{cal\#}$$
(97)

## 3 Performance ORC

$$\dot{Q}_{ev} = \dot{Q}_{total} \tag{98}$$

$$P_{ev} = P_{sat} \left( ORCFluid\$, \mathbf{T} = T_{ev,wf} \right)$$
(99)

$$P_{cd} = P_{sat} \left( ORCFluid\$, \mathbf{T} = T_{cd} \right) \tag{100}$$

$$h_{in,tur} = h\left(ORCFluid\$, \mathbf{P} = P_{ev}, \mathbf{X} = 1\right)$$
 (101)

$$s_{in,tur} = s(ORCFluid\$, \mathbf{P} = P_{ev}, \mathbf{X} = 1)$$
 (102)

$$h_{out,s,tur} = h\left(ORCFluid\$, \mathbf{s} = s_{in,tur}, \mathbf{P} = P_{cd}\right)$$
 (103)

$$w_{s,tur} = h_{in,tur} - h_{out,s,tur} \tag{104}$$

$$w_{tur} = w_{s,tur} \cdot \epsilon_{s,tur} \tag{105}$$

$$h_{out,tur} = h_{in,tur} - w_{tur} ag{106}$$

$$T_{out,tur} = T(ORCFluid\$, \mathbf{P} = P_{cd}, \mathbf{h} = h_{out,tur})$$
 (107)

$$h_{out,cd} = h\left(ORCFluid\$, \mathbf{P} = P_{cd}, \mathbf{X} = 0\right) \tag{108}$$

$$s_{out,cd} = s\left(ORCFluid\$, \mathbf{P} = P_{cd}, \mathbf{X} = 0\right)$$
 (109)

$$h_{out,s,pp} = h\left(ORCFluid\$, \mathbf{P} = P_{ev}, \mathbf{s} = s_{out,cd}\right)$$
 (110)

$$w_{s,pp} = h_{out,s,pp} - h_{out,cd} \tag{111}$$

$$w_{pp} = w_{s,pp}/\epsilon_{s,pp} \tag{112}$$

$$h_{out,pp} = h_{out,cd} + w_{pp} \tag{113}$$

$$T_{out,pp} = T\left(ORCFluid\$, \mathbf{P} = P_{ev}, \mathbf{h} = h_{out,pp}\right)$$
(114)

$$cp_{out,tur} = c_p \left( ORCFluid\$, \mathbf{P} = P_{cd}, \mathbf{h} = h_{out,tur} \right)$$
 (115)

$$cp_{out,pp} = c_p \left( ORCFluid\$, \mathbf{P} = P_{ev}, \mathbf{h} = h_{out,pp} \right)$$
 (116)

$$\dot{C}_{min} = Min \left( \dot{M}_r \cdot cp_{out,tur}, \ \dot{M}_r \cdot cp_{out,pp} \right) \tag{117}$$

$$\dot{Q}_{rec} = \dot{C}_{min} \cdot \epsilon_{rec} \cdot (T_{out,tur} - T_{out,pp}) \tag{118}$$

$$T_{out,rec,fr} = T_{out,pp} + \frac{\dot{Q}_{rec}}{\dot{M}_r \cdot cp_{out,pp}}$$
(119)

$$T_{out,rec,ch} = T_{out,tur} - \frac{\dot{Q}_{rec}}{\dot{M}_r \cdot cp_{out,tur}}$$
(120)

$$\dot{Q}_{total} + \dot{Q}_{rec} = \dot{M}_r \cdot (h_{in,tur} - h_{out,pp}) \tag{121}$$

$$\dot{W}_{pp} = \dot{M}_r \cdot (h_{out,pp} - h_{out,cd}) \tag{122}$$

$$\dot{W}_{tur} = \dot{M}_r \cdot (h_{in,tur} - h_{out,tur}) \tag{123}$$

$$\dot{W}_{net} = \dot{W}_{tur} - \dot{W}_{pp} \tag{124}$$

$$\eta_{gross,ORC} = \dot{W}_{tur} / \dot{Q}_{total} \tag{125}$$

$$\eta_{net,ORC} = \dot{W}_{net}/\dot{Q}_{total} \tag{126}$$

# 7 Pertes de charges conduit fumées

$$L_{ech} = (S_L + d_o) \cdot nbr_{cal\#} / nbr_{rangee\#}$$
 Encombrement dans le sens de l'écoulement (127)

$$S_T = \frac{D_{ech}}{nbr_{rangee\#} + 1} \tag{128}$$

$$\Delta P = 100000 \cdot \Delta P_f \tag{129}$$

# Stack effect



