

Structured illumination microscopy

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Illumination plays an important role in optical microscopy. Köhler illumination, introduced more than a century ago, has been the backbone of optical microscopes. The last few decades have seen the evolution of new illumination techniques meant to improve certain imaging capabilities of the microscope. Most of them are, however, not amenable for wide-field observation and hence have restricted use in microscopy applications such as cell biology and micro-scale profile measurements. The method of structured illumination microscopy has been developed as a wide-field technique for achieving higher performance. Additionally, it is also compatible with existing microscopes. This method consists of modifying the illumination by superposing a well-defined pattern on either the sample itself or its image. Computational techniques are applied on the resultant images to remove the effect of the structure and to obtain the desired performance enhancement. This method has evolved over the last two decades and has emerged as a key illumination technique for optical sectioning, super-resolution imaging, surface profiling, and quantitative phase imaging of microscale objects in cell biology and engineering. In this review, we describe various structured illumination methods in optical microscopy and explain the principles and technologies involved therein. © 2015 Optical Society of America

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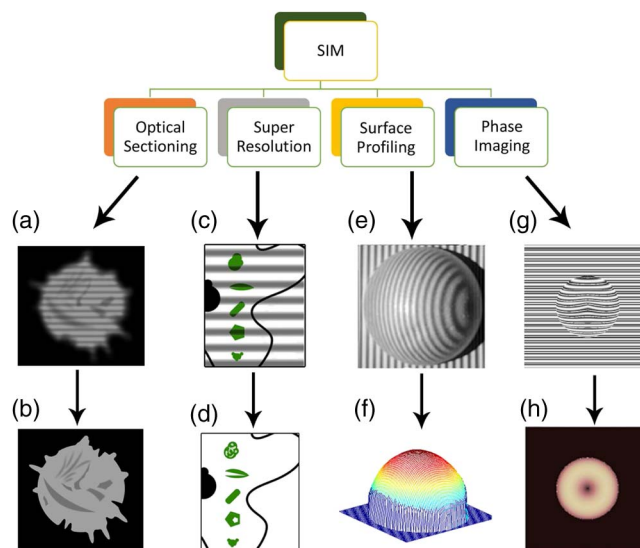
1. Introduction

Sample illumination is an important aspect of optical microscopy. Since the 19th century, considerable attention has been paid to illumination methods. Earlier microscopes used lamp light and critical (or Nelsonian) illumination, in which the light source was focused in the plane of the specimen. This method proved inadequate, more so with the invention of electric light sources wherein the structure of the filament dominated the sample features. A robust and flexible method of illumination was proposed by Köhler in 1893 [1]. This configuration involves a combination of two lenses and two apertures to generate uniform illumination at the sample plane. This method came to be known as Köhler illumination and has remained a mainstay of bright-field and fluorescence microscopy ever since.

The need to reduce out-of-focus light in semitransparent biological specimens and improve spatial resolution to observe subcellular features gave rise to a number of modifications in the Köhler illumination scheme. The introduction of an opaque stop in the illumination arm reduced the background light in dark-field microscopy [2]. Illuminating the sample at an angle enhanced the details of the patterns in the transparent specimens in oblique illumination microscopy [3]. Introducing a pinhole in a plane conjugate to the plane of observation in the sample, or focusing collimated laser light onto the sample, considerably reduced out-of-focus light. This technique is known as confocal microscopy [4]. Arranging the illumination and detection optical axes at an azimuthal angle of 90° led to improved axial resolution. This method is known as confocal theta microscopy [5]. Illuminating the sample side-on with a thin sheet of light helped in reducing the out-of-focus light. This is known as light sheet microscopy [6]. Illumination and detection through two objective lenses helped in improving the axial resolution in 4Pi microscopy [7] and I^5 M [8].

Of the above, confocal microscopy, also known as confocal laser scanning microscopy (CLSM), has been established as the standard method for high-resolution optical bio-imaging. While it is based on point scanning, the utilization of high-speed point detectors makes it attractive for time-resolved measurements. Apart from CLSM, most of the other methods have found limited use in applications in live cell imaging where temporal resolution is important. This is due to the fact that they are not amenable for high-speed wide-field observation. The method of structured illumination microscopy (SIM), which evolved out of synthetic aperture imaging introduced by Lukosz [9,10], has developed over the years into a wide-field technique that can achieve multiple objectives in different setups. Applications of structured illumination in microscopy include but are not restricted to the removal of out-of-focus light from transparent samples (optical sectioning), the improvement of lateral and axial resolution (super-resolution imaging), the determination of surface topography

Fig. 1.



Schematic illustrating the broad classification of microscopy techniques that employ structured illumination. (a), (c), (e), and (g) represent raw images taken in the respective imaging techniques, and (b), (d), (f), and (h) represent the respective reconstructed images.

information (surface profiling), and the gathering of integrated optical path length information (quantitative phase imaging). SIM consists of modifying the Köhler illumination by superposing a well-defined pattern on the sample. In certain cases, structure is imposed on an intermediate image plane to take advantage of magnification of the microscope. Computational techniques are then applied on the resultant images to remove the effect of the structure and to obtain the desired image. An added advantage of SIM is that it is compatible with conventional microscopes with usually a simple add-on.

In the current literature, there are articles reviewing optical sectioning, super-resolution, or both [11–23]. Most of them treated structured illumination as one of the many techniques. However, a review that encompasses all applications of SIM has not been published yet, to our knowledge.

In this review, we intend to provide an overview of microscopy techniques, which leverage structured illumination to achieve optical sectioning, super-resolution, surface profiling, and phase imaging. The illustration (shown in Fig. 1) depicts the major classification of techniques that are covered in this review article. The central theme of the current review is to provide a wider perspective of structured-illumination-based microscopy techniques. This will not only highlight the impact made by structured illumination in bringing advancements in various related fields but also provide the impetus for further developments.

2. Optical Sectioning

Biological specimens are usually thicker than the microscope objective's depth of field. Consequently, the image has contributions from both the in-focus plane as well as blurred out-of-focus planes. This reduces the contrast and resolution of the specimen. Optical sectioning is the method of acquiring images of thin slices

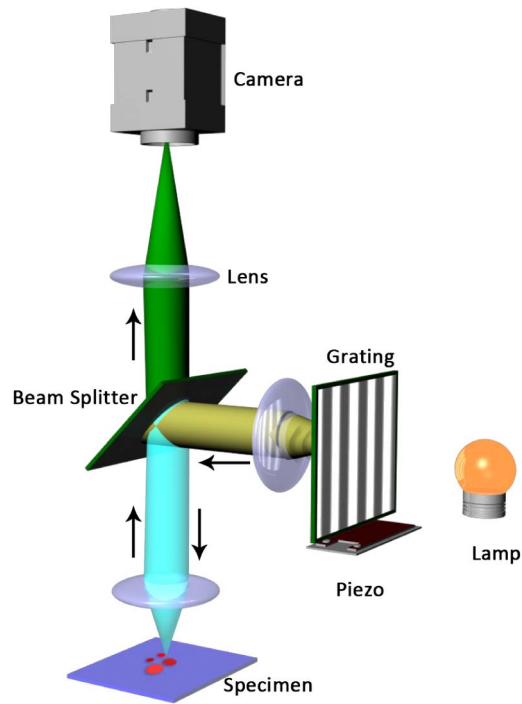
of a thick specimen by removing the contribution of out-of-focus light in each image plane. This removal of unwanted light provides greater contrast. It also permits three-dimensional (3D) reconstruction by computationally combining data from images having different slices in focus (called the image stack).

Out-of-focus light is removed optically, computationally, or using a combination of optical and computational methods. Optical approaches include multi-photon fluorescence, confocal microscopy, and planar illumination. Multi-photon fluorescence has been used to produce a fluorescence signal from only a small volume confined at the focus owing to nonlinear interaction between light and matter [24]. Confocal microscopy uses a pinhole mask to reject light from planes above and below the focus. Planar-illumination-based methods illuminate the sample side-on over a thin cross section either with a light sheet or with a line-like thin beam of light and image the emitted fluorescence perpendicular to the illumination plane/line, respectively. All of the above methods avoid the out-of-focus light prior to the detector. Most of these are either point-based or line-based, thus necessitating a long time for the entire scanning of the object, though there have been a few temporal focusing methods (such as multifocal temporal focusing) that perform scanning at an ultrafast rate by eliminating the need for imparting mechanical movement to the parts of the system [25]. Alternatively, deconvolution is a computational approach wherein the blur due to the out-of-focus contribution is numerically eliminated from the recorded images by either rejecting the out-of-focus contribution or reassigning the blurred light to an in-focus location. The former category of deconvolution algorithms, known as deblurring algorithms, essentially operate on the two-dimensional (2D) images of the image stack while subtracting the blur due to out-of-focus planes from the in-focus plane [26,27]. The latter category of deconvolution algorithms, known as image restoration algorithms, operate on the entire 3D stack either by blind 3D deconvolution [28] or by utilizing knowledge of the point spread function (PSF) of the imaging system [29]. Although the deconvolution can improve the wide-field images, they all fail at plane-like fluorescent structures (e.g., lamin labeled nuclei) whose Fourier transformation falls into the missing cone region. However, confocal and SIM fill the missing cone and thus can reliably image such structures as well.

Optical sectioning techniques were employed to image the biological samples such as the 3D chromatin distribution in neuroblastoma nuclei [30], the 3D chromosome topography in an intact nucleus [31], and the whole brain functional imaging at cellular resolution [32]. Out of several applications that optical sectioning found in the biological imaging, one of the major advancements is *in vivo* high-resolution deep imaging of thick tissues using two-photon excitation microscopy [33]. SIM employs a combination of optical and computational techniques to realize optical sectioning with advantages such as wide-field imaging and less photo toxicity.

In the structured illumination method, the Köhler illumination is modulated by predefined spatially varying illumination. The usual method to do so is to introduce a grating at the conjugate plane of the sample (Fig. 2). Alternative methods for generating fringe patterns onto the sample are discussed in Section 6. A set of images are recorded, each corresponding to different phases of the projected structured pattern. The recorded images are then subjected to post-processing so as to eliminate the manifestation of the illumination pattern, and to obtain an optically sectioned image. The sectioning effect here has

Fig. 2.



Setup for achieving optical sectioning using structured illumination.

essentially two origins: (1) the blurring of the illumination grating with out-of-focus and (2) the subsequent demodulation of emitted light. Typically spatially incoherent illumination is used for sectioning as it causes better blurring of the illumination grating with defocus, and reduces the speckle problems. However, the use of coherent light finds its importance in high-resolution SIM (for super-resolution), where the use of high-frequency structured illumination is necessary.

It can be said that the concept of structured illumination in optical sectioning originated from the need to obtain better light efficiency compared to confocal microscopy, while still retaining the optical sectioning capability. In the earliest efforts, an aperture mask was placed in the path of illumination and correlation techniques were applied to achieve 25%–50% light efficiency [34]. There were also efforts by a few other groups in the direction of achieving optical sectioning with the introduction of a structure in the sample and/or image planes mechanically and/or digitally [35,36].

In the demonstration of structured illumination for optical sectioning by Neil *et al.*, a grating pattern was introduced in the illumination system of the microscope causing its image to project onto the sample [37]. The resulting incoherent illumination intensity on the sample is given by

$$I_{in} = I_o[1 + m \cos(2\pi k_o x + \phi_o)], \quad (1)$$

where m is the modulation depth, k_o is the spatial frequency, and ϕ_o is the initial phase. The image generated is given by

$$I(u, v) = I_{in} S \otimes |h|^2, \quad (2)$$

where u, v are the coordinates in the image plane, S is the sample structure, and h is the PSF of the imaging lens. Modulation in the illumination light causes the resulting image intensity to have a base-band wide-field image and additional modulated images superposed on each other. This can be seen by substituting Eq. (1) in Eq. (2) to obtain

$$I(u, v) = I_w(u, v) + I_c(u, v) \cos(\phi_0) + I_s(u, v) \sin(\phi_0), \quad (3)$$

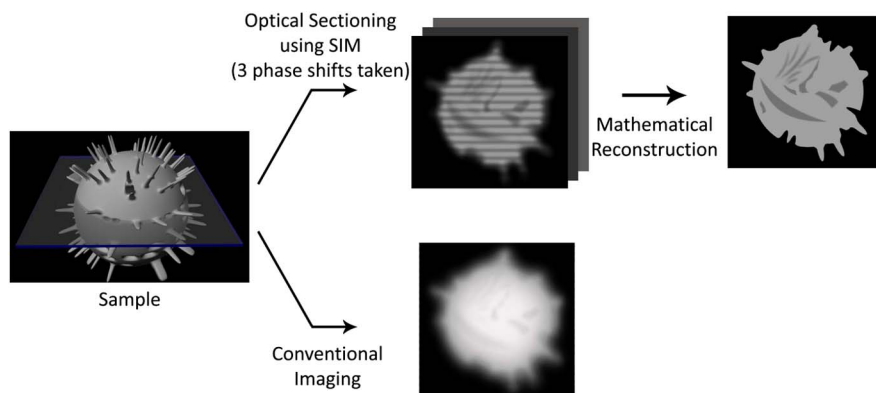
where I_w is the wide-field image and I_c and I_s are the modulated images arising due to the cosine term in Eq. (1). The modulated images contain the grid pattern in the plane that is in best focus. At all other planes, the grid pattern is defocused. This introduces a constant additive background. The background contribution and grid structure need to be removed to obtain an optical section. This is done computationally by acquiring three images I_1, I_2 , and I_3 with a relative phase shift of the projected grating pattern by $\frac{2\pi}{3}$. These phase shifts can be introduced, for example (as shown in Fig. 2), by translating the grating laterally by a piezo stage, in steps of a fraction of the grating's pitch. The sectioned image is then obtained by

$$I_{\text{section}} = \frac{\sqrt{2}}{3} \sqrt{(I_1 - I_2)^2 + (I_2 - I_3)^2 + (I_3 - I_1)^2}. \quad (4)$$

Figure 3 shows the steps involved in obtaining an optically sectioned image using structured illumination and a comparison with the conventional imaging.

This method, which was initially demonstrated for bright-field microscopy [37], was later extended to fluorescence microscopy using interference fringes [38] and grid/grating projection [39]. The use of interference fringes for optical sectioning is different from that of using a grating, as the interference fringes do not defocus, while the grating does. However, in the case of fluorescence imaging, even with the use of interference fringes, only the fluoresced signal from the in-focus plane of the imaging camera will be sharp and from other planes it will be blurred, thereby meeting the essentials for achieving optical sectioning. Using this technique, optical sectioning capability of the order of 400 nm or less was demonstrated [38].

Fig. 3.



Schematic illustrating the steps involved in obtaining optically sectioned images using structured illumination.

The advantage of structured illumination is that it is a wide-field technique. Other competitive methods for optical sectioning are either point-based (confocal, multi-photon fluorescence) or line-based (line scanning planar illumination). Additionally, structured illumination works for both fluorescence imaging and nonfluorescence imaging. The setup is relatively simple compared to other methods. Acquisition of more than three images with different phase shifts has also shown to help in achieving better contrast [40].

One disadvantage of SIM is that the detectors should have large dynamic range as the background light is also captured along with an in-focus signal. This has been addressed in [41,42] using digital micro-mirror device (DMD) based imaging. Another practical issue is that inaccuracy in the value of phase shift of the projected structured pattern can leave residual grating lines, when the images are computationally post-processed using Eq. (4). To overcome this, arbitrary phase shifts are considered and least squares demodulation has been proposed [40,43]. Another way of circumventing this problem is through a variant of SIM, namely HiLo microscopy, which captures two images (instead of three phase shifted images), one with uniform illumination and the other with structured illumination [44].

The time resolution of structured-illumination-based techniques is limited by the requirement of sequential capturing of images with multiple phase shifts. There have been attempts to improve the speed using smart detectors [45], using a color grating and a color camera [46], via innovative demodulation using two grid illuminated images [47], and utilizing polarization coding [48].

Structured illumination is employed as an add-on to other existing microscopy regimes such as plane illumination [44,49–52] and two-photon [53–55] to improve the sectioning capability of thick specimens. The use of structured illumination has also enabled snapshot hyperspectral imaging of volumetric samples by resolving the issue of spatial spectral crosstalk due to out-of-focus light, which any conventional hyperspectral imaging system suffers from [56].

The method for image reconstruction described here provides sectioning capability when the pattern is coarse or when the object is smooth in the lateral plane. But for fine gratings (high-frequency patterns), this method gives artifacts. These artifacts indeed carry the super-resolution information that is in fact recovered by the method described in the following section.

3. Super-Resolution

Spatial resolution has always been the most important parameter of cellular microscopy. Fluorescence microscopy is one of the most widely used techniques for observing subcellular features with high spatial resolution. The spatial resolution of a fluorescence microscope is governed by the Abbe diffraction limit ($\lambda/2$). This Abbe diffraction limit is valid for oblique uniform illumination, far-field optical illumination and detection, and linear absorption and emission regimes. Super-resolution is the method of achieving resolution in an optical microscope that is beyond the predicted diffraction limit, upon working outside these constraints. There have been many efforts by researchers around the globe in the direction of enhancing the resolution of optical microscopy, thereby leading to the development of various super-resolution techniques. The super-resolution techniques can be classified according to the distance of the excitation

source or detection probe from the sample (as near-field or far-field) and the response (linear or nonlinear) of the sample to its locally illuminating irradiance.

In the case of near-field techniques the excitation source or detection probe is kept near the sample, thereby facilitating the capture of an evanescent signal from the sample. As the Abbe diffraction limit is valid for light that has propagated a substantially larger distance than its wavelength, near-field techniques lead to an enhancement in resolution that is far beyond the diffraction limit. Some techniques, such as total internal reflection fluorescence microscopy (TIRFM), sophisticated near-field microscopy (SNOM), and near-field scanning optical microscopy (NSOM), have demonstrated the capability of near-field techniques in achieving subdiffraction resolution less than 100 nm [57–62]. However, near-field techniques have limited scope in terms of their applicability as only surface features can be imaged.

To overcome the limitations produced by near-field techniques and achieve super-resolution in the far-field, several techniques were developed. They can be further classified into ensemble imaging approaches and single-molecule-based imaging techniques. In the case of techniques belonging to the former class, resolution enhancement is achieved by spatially modulating the fluorescence behavior of molecules in the diffraction-limited region, such that not all of them emit simultaneously. The most popular ones among the ensemble based imaging techniques are stimulated emission depletion (STED) microscopy, reversible saturable optical fluorescence transitions (RESOLFTs), and SIM [63–67]. The latter class of techniques takes advantage of single-molecule imaging, using targeted signal switching, stochastic single-molecule switching, or other mechanisms to activate individual molecules within the diffraction-limited region at different times. Images with enhanced resolution are then reconstructed from the measured positions of individual fluorophores. These techniques are known as stochastic optical reconstruction microscopy (STORM), photo-activated localization microscopy (PALM), and fluorescence photo-activation localization microscopy (FPALM) [68–71].

Even though the developmental history of super-resolution techniques is short, they have found a large number of applications in various fields of biology such as cell biology, microbiology, and neurobiology. Some applications worth mentioning, which not only demonstrate the potential of super-resolution techniques in their resolving powers but also are instrumental in the visualization of molecular structures and interactions in cells, are the quantification of syntaxin molecules per cluster and cluster size in plasma membranes [72], studies on the dynamics of influenza hemagglutinin proteins in live cell membranes [73], imaging of MreB in *Calobacter crescentus* [74], the shape and dynamics of dendritic spines in live neuron cells [75], etc. In this section we discuss the various principles involved and the developments that have taken place in structured-illumination-based super-resolution microscopy in providing resolution enhancement for both incoherent and coherent imaging modalities.

In the case of incoherent imaging modalities (that image the incoherent light from the sample) such as fluorescence, the image intensity (D) detected by the detector is given as the convolution of the light intensity (I_s) from the sample and the incoherent detection PSF (h) of the imaging system:

$$D(\mathbf{r}) = (I_s \otimes h)(\mathbf{r}), \quad (5)$$

where \otimes denotes the convolution operation, and \mathbf{r} denotes the position vector on the detector. In general the light intensity from fluorescent samples (I_s) is dependent on the incident light intensity (I_{in}) and the sample structure (fluorophore density, S) as

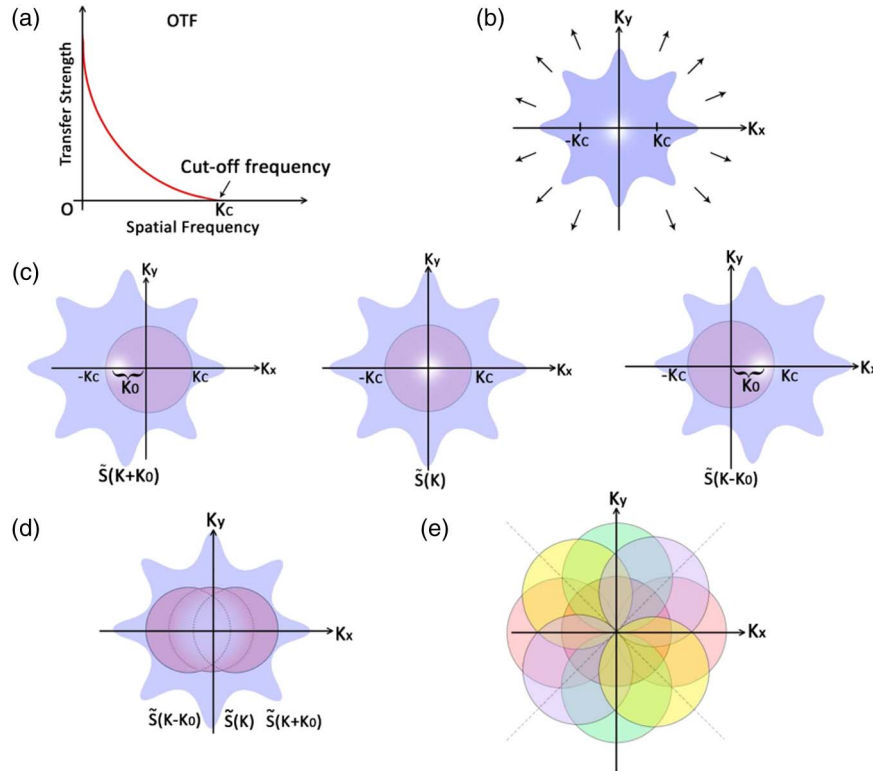
$$I_s = I_{in}S. \quad (6)$$

The frequency spectrum detected by the detector is given by

$$\tilde{D}(\mathbf{k}) = (\tilde{I}_{in} \otimes \tilde{S})\tilde{h}(\mathbf{k}), \quad (7)$$

where \tilde{I}_{in} , \tilde{S} , and \tilde{h} are the frequency spectra of incident light, the sample, and the incoherent PSF, respectively. The frequency spectrum of the PSF is known as the optical transfer function (OTF), and the typical OTF is shown in Fig. 4(a). The figure indicates that there is a cut-off frequency (k_c) beyond which the OTF is zero (known as the pass band of the imaging system). From Fig. 4(a) and Eq. (7) we can infer that the frequency spectrum of the sample detected by

Fig. 4.



(a) Frequency spectrum of the PSF, (b) frequency spectrum of the object (arrows indicate the infinite extent of the spectrum), and (c) shifted frequency spectrum components of the object collected by the imaging system for a fringe pattern projected in one orientation. (d) The region mapped by the circles indicates the reconstructed frequency spectrum of the object after appropriately assembling the parts in (c). (e) Extended frequency spectrum of the object after assembling the similar parts in (d) for four different orientations of the projected fringe pattern.

the imaging system is limited by k_c . This limitation on the detected frequency spectrum is a cause for limitation on the resolution of the imaging system. One way of circumventing this limitation is to somehow bring the frequency spectrum of the object [see Fig. 4(b)] that is beyond k_c into the pass band of the detection system. This is what the structured illumination accomplishes in producing super-resolution.

Consider plane wave illumination onto the sample; its frequency spectrum is given by

$$\tilde{I}_{in} = I_o \delta(k). \quad (8)$$

The detected frequency spectrum is

$$\tilde{D}(k) = [I_o \delta(k') \otimes \tilde{S}(k')](k) \tilde{h}(k) = I_o \tilde{S}(k) \tilde{h}(k), \quad (9)$$

thus being frequency-limited to the pass band of $\tilde{h}(k)$. For the sinusoidal pattern

$$I_{in} = I_o [1 + m \cos(2\pi k_o x + \phi)] \quad (10)$$

incident on the sample, with frequency spectrum

$$\tilde{I}_{in} = I_o [\delta(k) + (m/2)e^{i\phi} \delta(k - k_o) + (m/2)e^{-i\phi} \delta(k + k_o)], \quad (11)$$

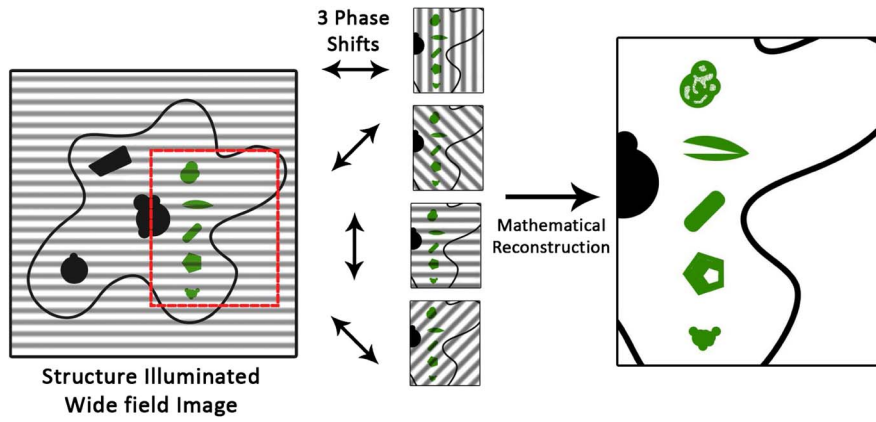
the detection frequency spectrum is given by

$$\tilde{D}(k) = I_o \tilde{h}(k) [\tilde{S}(k) + (m/2)e^{i\phi} \tilde{S}(k - k_o) + (m/2)e^{-i\phi} \tilde{S}(k + k_o)]. \quad (12)$$

The first term in the above expression corresponds to the frequency spectrum detected for a uniform illumination, and the second and third terms represent the shifted versions of the frequency spectrum for the uniform illumination by k_o and $-k_o$, respectively. These second and third terms bring additional information that corresponds to higher frequencies into the pass band of the imaging system as shown in Fig. 4(c). The raw image captured will have an overlap with all of these frequency spectra. To separate these frequency spectra the object is illuminated with three different phase shifted sinusoidal intensity patterns, which thereby results in three different frequency spectrum images $\tilde{D}(k)$. Having knowledge of these phase shifts and the respective $\tilde{D}(k)$, the three terms in Eq. (12) can be computationally extracted/separated out. The extracted high-frequency spectra are appropriately shifted to yield an extended detection frequency spectrum of the object as illustrated in Fig. 4(d). Taking the inverse Fourier transform of this spectrum yields a reconstructed super-resolved image. The direction in which super-resolution is achieved depends on the orientation of the illuminated sinusoidal pattern; for example, it is along the x axis for Figs. 4(c) and 4(d). To uniformly cover the entire lateral plane of the object we need to repeat the above procedure for at least three orientations of the pattern [Fig. 4(e)]. Figure 5 shows the schematic for achieving lateral super-resolution using structured illumination. Lateral super-resolution with SIM was successfully demonstrated by various groups around the world onto various biological samples such as the actin cytoskeleton of HeLa cells [66,76,77].

Let us further analyze the above scenario to see how many folds of enhancement in resolution this technique has brought forth and evaluate the limit of the achievable super-resolution. If there is no such limit for achievable

Fig. 5.



Schematic illustrating the steps involved in super-resolving an object using structured illumination. Arrows indicate the direction along which resolution enhancement is achieved.

super-resolution, then let us analyze under what conditions unlimited super-resolution is possible. The reconstructed frequency spectrum of the object has a cut-off at $k_o + k_c$, which can be increased upon increasing k_o . For the case in which the sinusoidal pattern projected onto the object is through the interference of two plane waves, the maximum spatial frequency that can be generated is $k_{o \max} = 2/\lambda_i$, where λ_i is the wavelength of the incident light onto the object inside the medium. For the fluorescence emission, the maximum cut-off frequency is $k_{c \max} = 2/\lambda_e$, where λ_e is the wavelength of the emitted light. As λ_i and λ_e are close enough the maximum detectable frequency of the object is

$$k_{o \max} + k_{c \max} = 4/\lambda \approx 2(2/\lambda_e), \quad (13)$$

where λ is the harmonic mean of λ_i , λ_e . Hence this technique can exceed the fundamental lateral resolution limit of the wide-field fluorescence microscope by a factor of 2.

The resolution enhancement can be furthered by utilizing the nonlinear response of the fluorescent molecules to the incident light intensity as in two-photon absorption, stimulated emission, and ground state depletion [67,78,79]. Figure 6(a) shows a schematic of the one-dimensional (1D) plot of intensities of emitted fluorescent light for both the linear and nonlinear response of fluorescent molecules to incident light. Such a nonlinear response can typically be expanded as a power series expansion in I_{in} ,

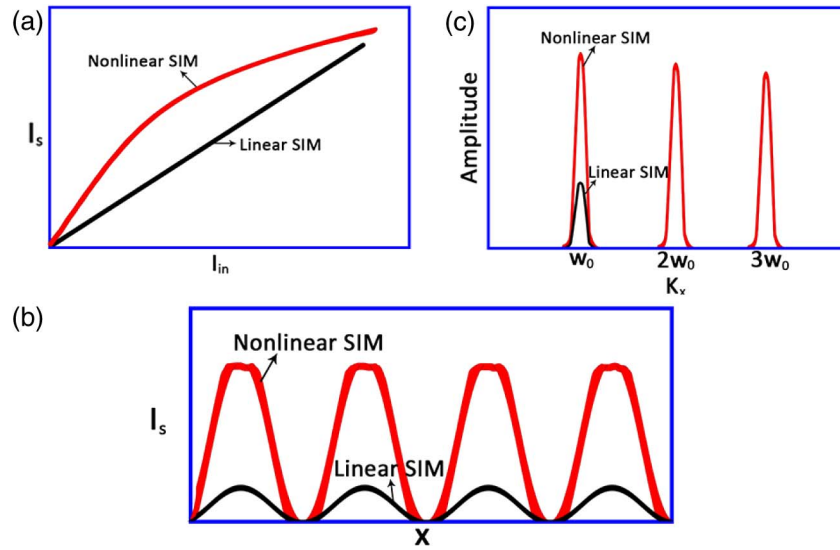
$$I_s = a_o + a_1 I_{in} + a_2 I_{in}^2 + \dots \quad (14)$$

For the fluorescent molecules that respond nonlinearly to the illumination intensity, the use of sinusoidal illumination as in Eq. (10) leads to an emission intensity I_s as shown in Fig. 6(b) and can be expressed as

$$I_s = \sum_{n=0}^{\infty} b_n \cos[n(2\pi k_o x + \phi)]. \quad (15)$$

From the above equation we can see that the emitted light has contributions from harmonics of the illuminated light frequency, which is uniquely distinct from that of linear SIM, which has contributions only from the first-harmonic of the incident

Fig. 6.



Schematic illustrating the emergence of higher harmonics in nonlinear SIM. (a) Plot of intensity of emitted fluorescent light. (b) 1D spatial variation of emitted intensity along x due to sinusoidal excitation. (c) Their respective frequency spectra for both linear and nonlinear response of fluorescent molecules.

light. A schematic representing the frequency spectrum of the emitted light (I_s), for a nonlinearity that has contributions from three-harmonics of the illuminated frequency, is shown in Fig. 6(c). For a general nonlinear response of the fluorophores as in Eq. (15), the detected frequency spectrum takes the form of

$$\tilde{D}(k) = \tilde{h}(k) \sum_{n=-\infty}^{\infty} b_n \tilde{S}(k - nk_o) e^{-in\phi}. \quad (16)$$

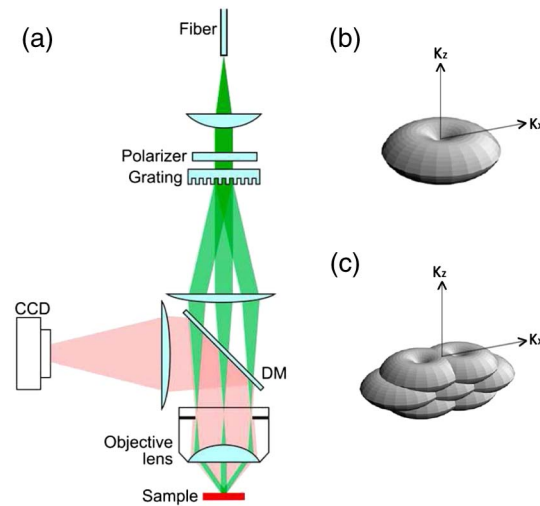
The above equation tells us that for a nonlinear response that cannot be expressed as a polynomial expansion with a finite number of terms, the pass band of the imaging system will have contributions from all the higher frequencies of the object frequency spectrum. Hence such a nonlinear response will yield unlimited super-resolution, in the absence of noise and fluorophore saturation.

Figure 7(b) shows the OTF of a typical imaging system with uniform planar illumination in 3D. The missing cone of frequencies along the axial (k_z) direction is the cause for poor resolution in depth. To achieve 3D super-resolution a three-beam interference method was proposed by Gustafsson *et al.* [80] [Fig. 7(a)]. The three-beam interference pattern was generated using the coherent superposition of the zeroth and first order diffraction orders (0, +1, and -1) emanating from a grating. The 3D excitation intensity pattern generated through such a coherent superposition of the three plane waves (diffraction orders) with wave vectors \mathbf{k}_j ($j = -1, 0, 1$) is given by

$$I_{in3D} = \left| \sum_{j=-1,0,1} E_j e^{i\mathbf{k}_j \cdot \mathbf{r}} \right|^2 = \sum_{j,q=-1,0,1} E_j E_q^* e^{i(\mathbf{k}_j - \mathbf{k}_q) \cdot \mathbf{r}}. \quad (17)$$

The above equation when expanded leads to seven distinct wave vectors ($\mathbf{k}_j - \mathbf{k}_q$), thereby producing an excitation pattern that is a combination of three

Fig. 7.



(a) Setup for achieving 3D super-resolution. (b) 3D OTF of a standard imaging system with k_z being the axial direction and k_x as one of the lateral directions. (c) Extended frequency spectrum of the object in both axial and lateral directions. DM, dichroic mirror. Figures are adapted with permission from [80].

sinusoidal patterns along the lateral and axial directions, and a uniform illumination pattern. Lateral sinusoidal patterns contribute to the lateral resolution enhancement upon bringing the high-frequency components into the lateral pass band of the imaging system. Meanwhile, the axial sinusoidal patterns convolve with the OTF and extend it in the axial direction, thereby increasing the axial resolution [Fig. 7(c)]. It should be noted that for high-resolution SIM, laser illumination interference is essential. A detailed discussion on 3D super-resolution using structured illumination for both static and dynamic objects can be found in [80–82]. Combining 3D structured illumination with I³M resulted in a technique known as I³S, which yielded a spatial resolution of the order of 100 nm in all three directions [83].

The possibility of achieving super-resolution in the case of coherent imaging modalities that utilize nonlinear interaction between the sample and incident light such as in coherent anti-Stokes Raman scattering (CARS) [84,85] has been explored. However, structured illumination cannot offer super-resolution in the case of coherent imaging modalities that utilize simple scattering phenomena such as bright-field microscopy [86]. For coherent light illumination, any illumination structure on the sample can be represented as an interference of light waves incident at oblique angles. The Abbe diffraction limit was derived precisely for such coherent imaging modalities that involve illumination at all possible oblique angles.

Even though structured illumination cannot achieve super-resolution in coherent imaging modalities that utilize simple scattering, it has been utilized for synthesizing a higher numerical aperture system using a low numerical aperture objective. This has been reported to achieve better spatial resolution [87–93] or greater depth of field [94,95].

The structured illumination technique has also been utilized in different microscopy modalities such as total internal reflection fluorescence [96], solid

immersion [97], line scanning [98], digital holography [99], differential interference contrast (DIC) [100], single-molecule localization [101], and light sheet [102] to achieve improved resolution. Plasmon-assisted excitation in conjunction with structured illumination has also been shown to provide improved lateral resolution [103,104].

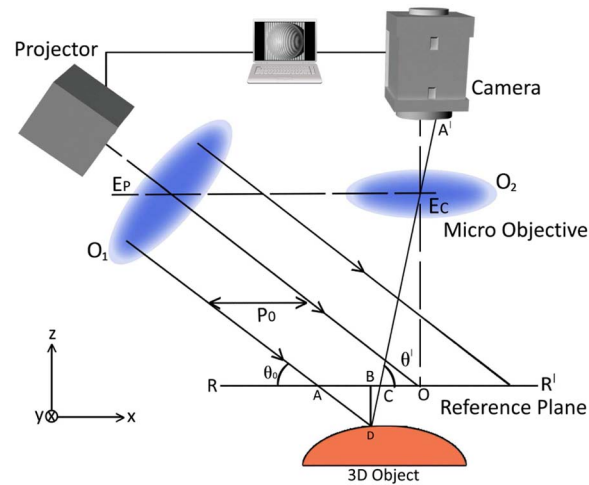
Fluorescence structured illumination super-resolution techniques are widely used in cell biology. Some of the applications include imaging nuclear periphery [105], chromosome structure [106], living cells [107], plant plasmodesmata [108], DNA replication [109], human centrosomes [110], retinal drusen [111], and fluorescent nanodiamonds [112].

4. Surface Profiling

Surface topography is one of the most important parameters in areas such as automotive and other metal working industries, where surface roughness of the order of fractions of a micrometer is important to the functioning of sliding components. Surfaces of hulls, propellers of ships, wind-tunnel models, etc., require surface topography measurements to minimize the hydrodynamic drag. To satisfy the demands of the emerging technologies and industry, researchers have developed wide variety of optical and nonoptical techniques for surface profile determination. Optical techniques can be further classified depending upon whether the surface profile determination is based on point scanning (laser triangulation), line scanning (light sheet, raster), or whole-field. Some of the most prominent whole-field optical surface profiling techniques to mention are based on structured illumination, interferometry, and focus detection. Interferometric techniques either measure the surface height profile directly or measure the slope of the surface based on the shifts in the interference fringes. Focus detection techniques determine the surface profile by either maintaining the focus of the optical system or making use of the principle of the optical focus. Both interferometric and focus detection techniques are capable of providing subnanometer axial resolution and submicrometer lateral resolution [113–115]. Nonoptical techniques such as scanning tunneling microscopy (STM), atomic force microscopy (AFM), scanning electron microscopy (SEM), and the stylus profilometer are point-by-point techniques and are slow to operate but do provide high axial and lateral resolution [116–118]. For an extensive discussion on various surface profiling techniques the reader can refer to [119].

Decades of research on surface profiling techniques have led to significant advancement in the profiling techniques and a commensurate expansion of applications. Depending upon the quality of the surface and the desired sensitivity of measurement the choice of the profiling technique will be made. Applications range from the surface profile determination of the gear tooth and engine bore surface [119], where the intrinsic hardness of the materials makes them suitable to be profiled with stylus profilers, to the polished brass surface [119], where the use of high spatial and axial resolution techniques such as STM and AFM is a necessity, to magnetic tapes [120], thick film superconductors [119], and soft metallic biomaterials [121], which demand the use of optical techniques. Structured illumination comes with the advantages of noncontact and whole-field imaging, thereby possessing the ability for rapid surface profiling. This technique found applications in diverse fields for 3D shape measurement of various micro- and macro-scopic objects that are both static and dynamic.

Fig. 8.



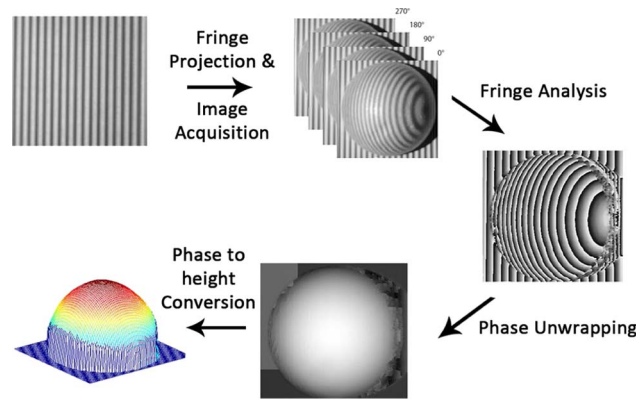
General schematic representing the experimental setup and the optical geometry for the analysis of a deformed fringe pattern in microscopic surface profiling.

For a thorough discussion on various surface profiling techniques using structured illumination for macroscopic objects the reader is referred to the cited tutorial by Geng [122]. In this paper we limit our discussion to the use of SIM for surface profiling of microscopic objects.

Figure 8 shows the general schematic for determining the surface profile of rough surface objects with microscopic features using structured illumination. The experimental setup mainly comprises the projector, the sample, and the detector. The projector illuminates the sample with a structured pattern and the reflected/scattered light is captured by the detector. The height profile of the sample is extracted from the captured images of the deformed pattern. The above process can be broadly divided into four important steps: 1) projection and acquisition, 2) fringe analysis, 3) phase unwrapping, and 4) calibration. The schematic illustrating the above steps is shown in Fig. 9. Several measurement techniques for obtaining the surface profile using structured illumination were reported in the literature, depending upon the variations that were brought in one or many of the steps involved. In general these techniques are classified based on the fringe analysis methods employed. In this review we discuss one of the most common techniques employed for the 3D shape measurement of objects with microscopic features such as MEMS and optical surfaces, namely the phase stepping (or shifting) technique [123]. The sinusoidal fringe pattern is the most commonly used structured light in all of the phase stepping techniques.

A sinusoidal fringe pattern with a pitch P is projected onto the sample surface through a long working distance micro-objective (O_1). The diffusively reflected pattern is captured onto the camera using another micro-objective (O_2). E_p and E_c represent the exit and entrance pupils of micro-objectives O_1 and O_2 , respectively (Fig. 8). RR' represents a plane perpendicular to the plane containing the optical axes of the projector (E_pO) and the detector (E_cO) and passing through their intersection point O . This plane RR' acts as a reference with respect to which the height of the sample surface is measured. If the sample surface is above the reference plane the height is considered positive; otherwise it is negative. The diffusively reflected fringes from the sample undergo deformation

Fig. 9.



Schematic illustrating the steps involved in surface profiling using structured illumination.

due to the angle between projection and image acquisition. In an ideal scenario when the projected fringe pattern is having a single frequency and the sample surface is perfectly smooth the fringe pattern is expected to be modulation free. In this section we refer to the image plane coordinates as u, v and the reference plane (the sample plane) coordinates as x, y . The modulation of the fringe pattern at location $A'(u, v)$ in the image plane is related to the phase change $\Delta\phi(x, y)$ that the fringe pattern undergoes, due to the height $h(x, y)$ variations of the sample surface at $D(x, y)$ with respect to the reference plane.

Assuming that the working distance of the micro-objectives is quite large enough compared to the specimen size, the fringe pattern can be assumed to be telecentrically (no divergence or convergence of the beam) projected onto the specimen. Hence the below analysis assumes the constancy of the pitch in the entire field of view of the specimen. The intensity of the projected sinusoidal fringe pattern at a point C on the reference plane is given by

$$I_c = a(x, y) + b(x, y) \cos(2\pi OC/p_o + \phi_o), \quad (18)$$

where $a(x, y)$ is the background light intensity, $b(x, y)$ is the fringe contrast, p_o is the pitch of the pattern as seen in the reference plane, OC is the geometric distance between points O and C, and ϕ_o is the phase of the fringe pattern at O. It is assumed that the fringe intensity variation is only along x but no variation along y .

From Fig. 8 we can observe that the intensity at point D on the surface would have been the same as that at point A on the reference plane, except for a multiplicative factor of surface reflectivity, $r(x, y)$. This implies that the phase at point A is the same as that at point D. The phase difference between points D and C (ϕ_{CD}) detected by the same pixel in the camera is the same as that of the phase difference between points A and C and hence can be related to the geometric path difference AC as

$$\phi_{CD} = 2\pi AC/p_o. \quad (19)$$

Using the relation between the surface height BD and AC, BD is expressed in terms of ϕ_{CD} as [123]

$$BD = h(x, y) = (p_o/2\pi)\varphi_{CD} \tan(\theta_o)/[1 + \tan(\theta_o)/\tan(\theta')], \quad (20)$$

where θ_o and θ' are shown in Fig. 8.

To determine the phase change $\Delta\varphi(u, v)$ of the fringe pattern recorded by the camera in the image plane, we employ a fringe analysis method known as the phase stepping technique, as mentioned earlier. A typical phase stepping technique operates on prior knowledge of the number of phase shifted images that need to be captured for the fringe analysis. In an N (≥ 3) step phase stepping technique, N images of fringe patterns, each having an increment in phase by $2\pi/N$ from the previous one, are projected onto the sample, and the reflected images I_1, I_2, \dots, I_N are captured onto the camera. The captured intensity images I_n are represented as

$$I_n = r(x, y)[a(x, y) + b(x, y) \cos(2\pi OC/p_o + \varphi_o + 2\pi n/N)], \quad (21)$$

where $n = 1, 2, \dots, N$. The phase change $\Delta\varphi(u, v)$ is extracted from these N intensity images using the following formula:

$$\Delta\varphi(u, v) = \tan^{-1} \left[\frac{\sum_{n=1}^N I_n \sin(2\pi n/N)}{\sum_{n=1}^N I_n \cos(2\pi n/N)} \right]. \quad (22)$$

This phase change may be simply referred to as phase or phase map in the following paragraphs.

The phase change estimated using the above expression gives a value at each pixel that lies between $-\pi$ and π , even though the surface height may lead to a phase change that exceeds 2π . This results in artificial discontinuities for the recovered phase change. Such a reconstructed phase with artificial discontinuities is known as a wrapped phase. The process of removing such artificial discontinuities upon adding an appropriate integral multiple of 2π is known as phase unwrapping. One of the simplest methods for removing such fake discontinuities is using the Itoh algorithm [124]. This algorithm is implemented on the rows and then on the columns of an image or vice versa. Consider a row of an image; the process of phase unwrapping involves finding the difference between a pixel and the preceding pixel (immediately to its left). When this difference is either larger than $+\pi$ or smaller than $-\pi$, a phase wrap is detected. Once a phase wrap is detected, the next step involves either adding or subtracting 2π to/from the pixel and from all the pixels on the right-hand side of it. Once the above procedure is implemented on the rows, the same process is repeated on the columns of this semi-unwrapped image.

The above discussed unwrapping algorithm may not give an unwrapped phase map for real-world phase images as they suffer from various sources of error. The main sources of error that complicate the unwrapping process are 1) noise, 2) undersampling, 3) sudden and abrupt phase changes in the image, and 4) errors produced by the phase extraction algorithm. To overcome the above challenges several phase unwrapping algorithms were developed, and some of the popular ones among them are Goldstein's algorithm [125], the fringe frequency analysis based algorithm [126], region growing phase unwrapping [127], and the multilevel quality guided phase unwrapping algorithm [128]. For applications involving dynamic deformation/3D shape measurement, there comes a need for unwrapping the stack of 2D wrapped phase images captured at different instants

of time, known as 3D phase unwrapping [129]. For an exhaustive set of references on phase unwrapping applied in the field of surface profiling, the reader is referred to the cited articles [130,131].

The unwrapped phase change $\Delta\varphi(u, v)$ has to be mapped from the image plane to the sample plane. This can be achieved using the standard camera calibration techniques [132,133]. The surface height map is estimated from the phase map on the sample plane and the expression in Eq. (20). This process of obtaining the height map from the unwrapped phase map in the image plane is known as calibration. In most of the practical scenarios the sample sizes can be large or comparable to the working distance of the micro-objectives used. Hence the approximation of telecentricity fails. In such cases the pitch of the fringe pattern no longer remains constant within the field of view on the specimen. Even then the above phase stepping technique helps in estimating the phase map accurately. Estimating the height map is not a straightforward task as it generally requires the measurements of θ_o and θ' accurately. In addition to that for nontelecentric cases Eq. (20) is not valid for estimating the height map. Over the years many techniques have been developed to overcome the above-mentioned problems [130,134,135], and also special efforts have been made in the direction of developing flexible/generalized calibration techniques [130,136,137] that are capable of automatically determining relevant geometrical parameters of the setup for an arbitrary position of the camera, the projector, and the object.

Another noteworthy limitation that the above configuration possesses is its inability to provide high lateral spatial resolution. 3D surface measurement techniques based on structured illumination must have an angle between the illumination (projection) and the detection beam paths. This angle will restrict the applications of the surface profiling technique to only very long working distance objectives. Objectives with high numerical aperture cannot be used in this geometry, thereby limiting the lateral spatial resolution of the approach.

The most sensitive surface profiling method for reflective surfaces using structured illumination is actually not imaging the structure that is projected on the surface, but the one in focus at a very large distance from it, via the optical surface of interest. This way very small deviations from the design angle of the surface normal can be detected reliably. This mode of SIM for shape reconstructions is found to offer accuracy in the nanometer range [138].

Structured-illumination-based surface profiling has found applications in the measurement of crater wear [139], 3D fingerprint information for recognition [140], 3D reconstruction of wafer solder bumps [141,142], intra-oral surface measurement [143] etc. Structured illumination has also been applied in cases that do not fall under the category of diffusively reflecting surfaces, for example, the deformation measurement of a micro-mirror as a function of applied voltage in DMDs [144] and the determination of micro-drop deformation [145]. Combining SI with common path interferometry helped in achieving nanoscale topography of the samples, which was successfully applied for the real-time characterization of spatial light modulators [146].

5. Phase Imaging

Wide-field imaging in the context of microscopy involves various important aspects such as magnification, contrast, and resolution. Before the introduction

of phase contrast microscopy in the 1930s [147] the imaging of phase objects such as unstained biological samples was poor in contrast due to their weakly scattering and/or absorbing nature, even after having the better magnification and resolving capability of a microscope. The understanding and utilization of the role played by phase in imaging started an era of new imaging techniques that are both qualitative and quantitative. Techniques such as phase contrast and DIC [148] are generally qualitative in the sense that they do not give quantitative phase information but convert that information into suitable intensity modulation to enhance the contrast of the phase objects. Contrary to that, quantitative phase imaging techniques image the phase map of the phase object as a function of its spatial position. Quantitative phase imaging techniques can be broadly classified into interferometric and noninterferometric techniques. Interferometric techniques involve those quantitative imaging techniques that utilize the interference pattern between the reference beam and the object beam to encode the phase information. Some of the interferometric techniques are digital holographic microscopy [149], diffractive phase microscopy (DPM) [150], Fourier phase microscopy [151], spatial light interference microscopy [152], optical quadrature microscopy [153], and quantitative DIC [154]. Meanwhile, noninterferometric techniques do not involve interference in the phase estimation, for example, transport of intensity equation (TIE) [155] based phase imaging and quantitative structured illumination phase microscopy [156]. A comprehensive review on various quantitative phase imaging techniques can be found in [157].

The impact made by phase imaging techniques in the context of biological imaging such as cells was a revolutionary one. Some of the applications of phase imaging include the investigation of chemical-induced apoptosis and the dynamic phagocytosis process of macrophages [158], wide-field imaging of invasive carcinoma cells within human breast sections [159], morphological imaging of unstained spermatozoa in their natural physical surroundings [160], membrane nanoscale fluctuations of live erythrocytes [161], counting the number of cells in embryos [162], and cell growth monitoring [163]. In this section we refer to those phase imaging techniques in which structured illumination was utilized either directly or indirectly in producing a phase image.

Pavani *et al.* devised a technique for quantitative phase imaging of homogeneous objects [156]. This technique involves illuminating a structured light onto the phase object or placing the phase object immediately next to the patterned mask in the line of illumination of a bright-field microscope, followed by imaging the illuminated structure. Capturing images of the structure with and without the presence of the phase object gives information about the deformation (lateral shift) that the structure has undergone in the presence of the phase object. This information will be unique to the phase objects with different optical path length profiles. Under the assumption that the optical path length gradients are very small ($\ll 1$), a closed-form analytical solution for optical path length was derived using the ray optics model. The derived optical path length showed the dependence on the square root of the integrated deformation. Measuring this deformation helps in estimating the optical path length of the phase object and hence the phase image.

A group led by Popescu *et al.* devised a phase imaging method [150], known as DPM, that uses a structure (blazed diffraction grating) on the image of the sample. The light from the image plane is allowed to pass through a 4-f system that

has a filter in the 2-f plane, and a camera in the 4-f plane, as shown in Fig. 10. The diffraction grating produces a diffraction pattern in the 2-f plane. Each order of the diffraction is nothing but a copy of the frequency spectrum of the image of the sample with different magnitudes. This is expected because the light distribution in the image plane can be written as a product of the sample-image light distribution and the transparency pattern of the grating. In the 2-f plane we observe the Fourier transform of this light distribution, which is the same as the convolution of the frequency spectrum of the sample image and the diffraction pattern of the grating. The intensities of these orders can be controlled upon choosing a suitable blazed grating.

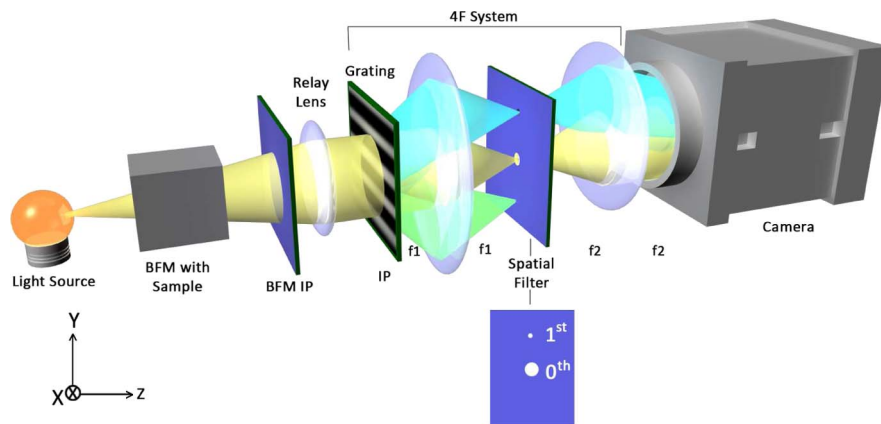
In DPM only the zeroth and first orders of the frequency spectrum are of interest. Choosing an appropriate filter in the 2-f plane, as shown in Fig. 10, the orders that are of interest can be passed onto the second half of the 4-f system. The filter used contains a sufficiently large hole, to allow the zeroth order to fully pass through, and a pinhole, to allow only the DC component of the first order to pass through. As this light distribution passes through the second half of the 4-f system, it undergoes another Fourier transform. This converts the light from the pinhole into a plane wave and the light from the zeroth order into a sample wave field at the 4-f plane. These two wave fields interfere and produce an interference pattern on the camera. The expression for the resulting interference pattern is given as [164]

$$I(x, y) = I_o(x, y) + a(x, y) \cos[\phi(x, y) + \beta y], \quad (23)$$

where $I(x, y)$ is the intensity of the interference pattern, $I_o(x, y)$ is the background intensity, $a(x, y)$ is the modulation factor, $\phi(x, y)$ is the phase delay due to the object, β is the carrier frequency of the fringes specific to the grating pitch and the 4-f system, and the y axis is along the direction of the grating periodicity.

If analyzed carefully the main use of the grating and the 4-f system was to implement a common path interferometry configuration, apart from a few other advantages the combination serves. This common path interferometry helps in encoding the optical phase of the sample wave field in the recorded interference

Fig. 10.



Setup for diffraction phase microscopy. BFM, bright-field microscope; IP, image plane.

pattern. One of the main advantages of common path geometry when compared to off-axis interferometric techniques is the reduction of phase noise due to mechanical vibrations and air fluctuations. Consequently DPM is able to provide highly precise quantitative phase maps compared to general off-axis interferometric techniques.

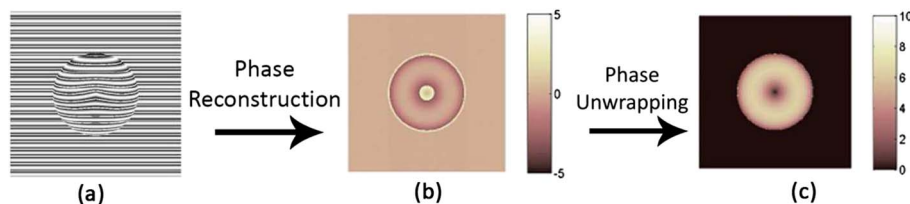
The phase reconstruction can be performed from Eq. (23) using any of the standard integral operator methods, such as Fourier and Hilbert transforms, using the wavelet-based space-scale analysis method [165], or using a derivative method [166], which is computationally less intensive compared to the above integral-operator-based techniques. The derivative method performs the phase reconstruction under the assumption that the background intensity and the modulation factor do not change over the interferogram and the phase is a slowly varying function along the direction of the periodicity of the grating. It uses the following expression for extracting $\phi(x, y)$ from the interferogram (I) and its derivatives (I' , I'' , first and second derivatives, respectively):

$$\phi(x, y) = \tan^{-1}(\beta I' / I'') - (\beta y). \quad (24)$$

The extracted phase will have artificial discontinuities of 2π [Fig. 11(b)] and can be removed using the standard phase unwrapping algorithms. Figure 11 shows the steps involved in the phase map reconstruction using the DPM technique.

This method by Popescu *et al.* (conventional DPM) can in principle be implemented similarly to the other techniques of structured illumination, in which the image of the structure or grating is directly formed on the sample and then immediately followed by a 4-f system with a filter (as used in conventional DPM), to form an interference pattern between the image wave field and the reference wave field. Conventional DPM possesses two distinct advantages when compared with direct illumination on the sample. The first advantage is that the 4-f system along with the grating can be added as a simple add-on to the existing bright-field microscope. For a given 4-f system we need a high-frequency grating to avoid aliasing between various orders in the 2-f plane, for the case of direct structured illumination on the sample. The presence of an objective with a magnification in the bright-field setup helps in demagnifying the frequency spectrum of the sample. This serves as a second advantage for conventional DPM as it requires a grating with low spatial frequency while simultaneously avoiding aliasing in the 2-f plane.

Fig. 11.



Illustrating the steps involved in reconstructing the phase image with DPM. (a) Raw image captured, (b) wrapped phase map, and (c) reconstructed unwrapped phase map. The color bars show the phase in radians.

A comprehensive treatment on the different types of DPM, their advantages and disadvantages, and the variety of applications that are possible with DPM is found in the review article by Bhaduri *et al.* [164]. Some of the noteworthy applications of structured-illumination-based phase imaging are the dynamic phase imaging of red blood cell membrane fluctuations [167], the fluorescence phase imaging of mitotic kidney cells [168], and the quantitative study of cell growth [169]. Structured illumination is also found to be helpful in improving the performance of TIE-based phase imaging. TIE-based phase images generally suffer with low-frequency noise as it requires solving a second-order differential equation for phase. Illuminating the phase object with structured light and capturing the defocused images has two distinct advantages: 1) it helps in converting the second-order differential equation of phase into first order, thereby reducing the noise, and 2) it produces a multiplicative factor that depends upon the gradient of illumination intensity [170]. Hence with a suitable choice of illumination pattern, the signal-to-noise ratio (SNR) of the estimated phase can considerably be enhanced.

6. Illumination Methods

The structured illumination required in the above imaging techniques is typically generated using one of the following procedures: casting the image of a mask onto the sample, placing the mask on the image of the sample, through the interference of coherent light waves, and using a spatial light modulator (SLM) like DMDs, liquid crystal SLM, liquid crystal on silicon (LCOS), etc. In Köhler-illumination-based microscopes, casting the image of the mask onto the sample is achieved by placing the mask at the plane of the field stop in the illumination path. The phase shift of the sinusoidal pattern illuminated onto the sample is controlled upon moving the mask appropriately.

Two coherent light beams, with the plane of polarization perpendicular to the plane containing them, can be made to interfere to form a sinusoidal pattern. These light beams can be generated either using beam splitters or using a grating. If the grating is used for generating the beams, selected diffraction orders (generally $+1$, -1) are allowed to interfere. The latter gives a mechanically more stable fringe pattern compared to the former, because the diffraction orders typically go through the same optical elements before they are brought to interfere (forming a common path interferometer). The phase of the fringe pattern can be controlled either upon changing the optical path length of one of the beams with respect to the other, or moving the grating in the grating vector direction.

The above techniques generally require mechanical intervention for phase shifting and changing the orientation of the fringe pattern. The use of piezo-actuators, electro-optic modulators in single beam lines, etc., can produce sufficiently fast phase shifting. However, orientation change and flexibility in changing the pattern stood as difficult/impossible issues with the above-mentioned techniques. State-of-the-art programmable SLMs have emerged as a boon, as these possess excellent capability to produce orientation change, and flexible structured illumination patterns, thereby replacing the use of etched gratings, masks, and interference beams for structured illumination. For some of the SIM techniques based on mask/grating [37,39,66,76,83,150], interference [38,77], the use of diffractive optical elements [171], subwavelength hole arrays [172], and SLMs [79,173,174], the reader is referred to the respective cited articles.

7. Summary and Perspectives

The role played by structured illumination in achieving enhanced performance in various optical microscopy techniques is presented. Specifically, the paper described the underlying principles in the implementation of microscopy techniques with structured illumination, such as optical sectioning, super-resolution, surface profiling, and phase imaging. Wide-field and noncontact imaging are the main advantages offered by SIM. In optical sectioning, structured illumination enables the rejection of out-of-focus light while simultaneously increasing the light efficiency when compared with confocal microscopy. SIM offers 3D super-resolution in the case of incoherent imaging modalities such as fluorescence, upon expanding the detected frequency spectrum of the object. Projecting a fringe pattern onto the sample and collecting the resulting phase modulated fringe patterns yielded the surface topography of diffusively reflecting samples. A set of phase imaging techniques were developed by introducing a grating structure onto the image of the sample in combination with a spatial filter, and thereby having an interference between the image light field and the reference light field in a common path geometry. All the SIM techniques found a large number of applications in the field of bio-medical imaging. Some of the applications to mention are the imaging of biological samples such as cytoplasmic GFP-labeled neurons in a fixed mouse brain slice in optical sectioning, cellular nuclear periphery, chromosome structure in super-resolution, intra-oral surface measurement in surface profiling, and capturing dynamic phenomena such as red blood cell membrane fluctuations in phase imaging. SIM is an interesting combination of optical and computational methods for obtaining enhanced performance, thereby constantly provoking researchers across different disciplines to develop various optical techniques and reconstruction/image analysis algorithms, or for its deployment in challenging applications. Through this article we attempted to show glimpses of various aspects of SIM, starting from basic theory to the computational algorithms involved, while drawing attention to the advancements contributing to the continuous evolution of SIM capabilities.

With the rapid development of modern technologies, it is expected that SIM would attract a lot of attention in practical applications. Future developments made in the following aspects of SIM would further enhance and extend the applicability of the technique to various other domains: 1) deep optical sectioning and super-resolution imaging for thick biological samples such as tissues has always been a challenging task due to scattering. Recently there have been efforts in the direction of enhancing the resolution for deep tissue imaging using a combination of techniques such as SIM and photon reassignment [175], SIM and line scanning [98], and nonlinear SIM and temporal focusing multi-photon excitation microscopy [55]. Utilizing a combination of techniques seems to be a good idea in which the advantages of the respective techniques are preserved, for achieving deep optical sectioning and super-resolution imaging of thick samples. 2) As the steps involved in optical sectioning and super-resolution are very similar, the development of systems capable of simultaneously providing optical sectioning and super-resolution while offering the optimal SNR reconstructions is yet another interesting advancement needed for biological applications. 3) The number of images to be acquired in SIM for achieving optical sectioning and super-resolution seems to be a limitation for capturing dynamic phenomena. To reduce the number of images needed for reconstruction, techniques such as color

SIM [46], picoSIM [48], and HiLo microscopy [44] have been developed. Even then the number of images needed for reconstruction of full objects seems to be large, for capturing faster dynamic phenomena. The development of multiplexed excitation patterns and the simultaneous detection/acquisition of the patterns would potentially help in reducing the number of sequential images needed and hence the time for recording. This would enable faster volume imaging of dynamic/live extended objects with cellular/molecular resolution. In a different perspective, this indicates the need for the development of 3D structured patterns and the related developments in imaging and computational methods. While the above approach is to reduce the number of images needed and/or design better structured patterns for illumination, a different approach would be to increase the speed of acquisition. High-speed SIM may help unravel new phenomena that are hitherto difficult to capture, similar to what recent high-speed 2D imaging techniques have been found to be capable of [176–179]. 4) The development of ultra-large field-of-view surface profiling systems for 3D imaging of macro-objects such as micro-patterned wafers of several inches diameter with micro/nano meter resolution is likely to have a stronger impact on the field of surface profilometry. (5) Ultra-large field-of-view phase imaging of transparent objects such as microfluidic and optofluidic devices, optical components, and tissue biopsy slides/smears on slides would have potential applications in the fields of characterization of micro-/nano-fabricated devices, surface finish measurement of optical components, and clinical diagnostics. These advancements could possibly be realized by further encashing the wider field-of-view imaging capability of SIM and the development of required large area illumination and imaging devices.

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[†] These authors contributed equally to this work.

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