

# ICSEA paper outline

Danielle Stewart  
University of Minnesota  
Department of Computer Science and Engineering  
Email: dkstewar@umn.edu

Michael W. Whalen  
University of Minnesota  
Department of Computer Science and Engineering  
Email: whalen@umn.edu

Jing (Janet) Liu  
Rockwell Collins  
Advanced Technology Center  
Email: Jing.Liu@rockwellcollins.com

Darren Cofer  
Rockwell Collins  
Advanced Technology Center  
Email: Darren.Cofer@rockwellcollins.com

**Abstract**—This paper describes a new methodology with tool support for model-based safety analysis. It is implemented as a *Safety Annex* for the Architecture Analysis and Design Language (AADL). The Safety Annex provides the ability to describe faults and faulty component behaviors in AADL models. In contrast to previous AADL-based approaches, the Safety Annex leverages a formal description of the nominal system behavior to propagate faults in the system. This approach ensures consistency with the rest of the system development process and simplifies the work of safety engineers. The language for describing faults is extensible and allows safety engineers to weave various types of faults into the nominal system model. The Safety Annex supports the injection of faults into component level outputs, and the resulting behavior of the system can be analyzed using model checking through the Assume-Guarantee Reasoning Environment (AGREE).

## I. INTRODUCTION

System safety analysis techniques are well-established and are a required activity in the development of safety-critical systems. Model-based systems engineering (MBSE) methods and tools based on formal methods now permit system-level requirements to be specified and analyzed early in the development process [5], [14]. While model-based development methods are widely used in the aerospace industry, they are only recently being applied to system safety analysis.

In this paper, we describe a *Safety Annex* for the Architecture Analysis and Design Language (AADL) [15] that provides the ability to reason about faults and faulty component behaviors in AADL models. In the Safety Annex approach, we use formal assume-guarantee contracts to define the nominal behavior of system components. The nominal model is then verified using the Assume Guarantee Reasoning Environment (AGREE) [14]. The Safety Annex provides a way to weave faults into the nominal system model and analyze the behavior of the system in the presence of faults. The Safety Annex also provides a library of common fault node definitions that is customizable to the needs of system and safety engineers. Our approach adapts the work of Joshi et. al in [21] to the AADL modeling language, and provides a domain specific language for the kinds of analysis performed manually in previous work [30].

The Safety Annex supports model checking and quantitative reasoning by attaching behavioral faults to components and then using the normal behavioral propagation and proof mechanisms built into the AGREE AADL annex. This allows users to reason about the evolution of faults over time, and produce counterexamples demonstrating how component faults lead to system failures. It can serve as the shared model to capture system design and safety-relevant information, and produce both qualitative and quantitative description of the causal relationship between faults/failures and system safety requirements. Thus, the contributions of the Safety Annex and this paper are:

- Close integration of behavioral fault analysis into the *architectural design language* AADL, which allows close connection between system and safety analysis and system generation from the model,
- support for *behavioral specification of faults* and their *implicit propagation* through behavioral relationships in the model, in contrast to existing AADL-based annexes (HiP-HOPS, EMV2) and other related toolsets (COMPASS, Cecilia, etc.),
- additional support to capture binding relationships between hardware and software and logical and physical communications, and
- guidance on integration into a traditional safety analysis process.

## II. BACKGROUND

Background information on fault trees, IVCs, and Soteria.

## III. METHODOLOGY

The details of implementation and formalisms.

### A. Danielles Notes

1) *Constraint systems*: Consider a constraint system  $C$  as an ordered set of  $n$  constraints  $\{C_1, C_2, \dots, C_n\}$  over a set of variables. Each constraint restricts the allowed assignments to the variables in some way. We need a way to determine for any subset  $S \subseteq C$ , whether  $S$  is *satisfiable* (SAT) meaning there exists an allowable assignment for all  $C_i \in S$  or *unsatisfiable* (UNSAT) meaning no such assignment exists.

Some useful subsets of unsatisfiable constraint systems with particular properties:

- *Minimal Unsatisfiable Subset* (MUS)  $M$  of a constraint system  $C$  is a subset  $M \subseteq C \ni M$  is UNSAT and  $\forall c \in M : M/\{c\}$  is SAT. An MUS is the minimal explanation of the systems unsatisfiability.
- *Maximal Satisfiable Subset* (MSS)  $M$  of a constraint system  $C$  is a subset  $M \subseteq C \ni M$  is SAT and  $\forall c \in M : M \cup \{c\}$  is UNSAT.
- *Minimal Correction Set* (MCS)  $M$  of a constraint system  $C$  is a subset  $M \subseteq C \ni C/M$  is SAT and  $\forall S \subset M : C/S$  is UNSAT. The removal from  $C$  corrects the infeasibility.

Notes: MSS and MCS are complementary: any MSS of  $C$  is the complement (relative to  $C$ ) of some MCS and vice versa. This provides two ways of encoding the same information. MCSs used more often in practice because MCS is smaller than its complement. The goal of MUS/MSS enumeration algorithms given some constraint system  $C$  is the exploration of the power set of the constraints  $P(C)$ .

- Every subset of  $C$  is either SAT or UNSAT.
- If a subset is SAT, then every subset is SAT.
- If a subset is UNSAT, then every superset is UNSAT.

2) *IVC approach*: Formulate the model into a boolean problem called transition relation.

Assert negation of the safety property.

Ask solver if both of these are satisfiable together.

If the solver returns UNSAT, then it is impossible to satisfy the negation of the safety property so a request is made for the MUSs : the minimal explanation for infeasability. These are traced back to the model elements and hence these are the model elements necessary for the proof of the safety property.

3) *Minimal cut sets and fault trees*: Top level event occurs if one of the MCSs occur. Hence the MCSs are connected to the TLE through an OR gate. This corresponds to the probabilistic operation:

$$P(A \cup B) = P(A) + P(B) - P(A \cap B)$$

Since failure probabilities on fault trees tend to be small,  $P(A \cap B)$  becomes an error term and the output of the OR gate can be conservatively approximated using the assumption that the inputs are mutually exclusive events. They are not in reality since a basic event can be shared between MCSs, but it is a safe approximation to make. This type of dependency

is called *positive dependency* and gives a more conservative estimate for the probability of occurrence of the TLE.

An MCS contains the combination of basic events which together lead to the occurrence of the TLE. Thus the basic events are connected through an AND gate. This corresponds to the operation:

$$P(A \cap B) = P(A)P(B)$$

So in a more formal way: The probability of the TLE is given by:

$$P_{tle}(t) \leq \sum_{j=1}^k [\hat{P}_j(t)]$$

where  $\hat{P}_j(t)$  is the failure probability of the MCS  $M_j$  :

$$\hat{P}_j(t) = \prod_{i \in M_j} b_i(t) \text{ for basic events } b_i \in M_j.$$

#### IV. CASE STUDIES

Case studies or tool comparisons.

#### V. RELATED WORK

A model-based approach for safety analysis was proposed by Joshi et. al in [19]–[21]. In this approach, a safety analysis system model (SASM) is the central artifact in the safety analysis process, and traditional safety analysis artifacts, such as fault trees, are automatically generated by tools that analyze the SASM.

The contents and structure of the SASM differ significantly across different conceptions of MBSA. We can draw distinctions between approaches along several different axes. The first is whether they propagate faults explicitly through user-defined propagations, which we call *failure logic modeling* (FLM) or through existing behavioral modeling, which we call *failure effect modeling* (FEM). The next is whether models and notations are *purpose-built* for safety analysis vs. those that extend *existing system models* (ESM).

For FEM approaches, there are several additional dimensions. One dimension involves whether *causal* or *non-causal* models are allowed. Non-causal models allow simultaneous (in time) bi-directional failure propagations, which allow more natural expression of some failure types (e.g. reverse flow within segments of a pipe), but are more difficult to analyze. A final dimension involves whether analysis is *compositional* across layers of hierarchically-composed systems or *monolithic*. Our approach is an extension of AADL (ESM), causal, compositional, mixed FLM/FEM approach.

Tools such as the AADL Error Model Annex, Version 2 (EMV2) [16] and HiP-HOPS for EAST-ADL [12] are *FLM*-based *ESM* approaches. As previously discussed, given many possible faults, these propagation relationships require substantial user effort and become more complex. In addition, it becomes the analyst’s responsibility to determine whether faults can propagate; missing propagations lead to unsound analyses. In our Safety Annex, propagations occur through system behaviors (defined by the nominal contracts) with no additional user effort.

Closely related to our work is the model-based safety assessment toolset called COMPASS (Correctness, Modeling project and Performance of Aerospace Systems) [6]. COMPASS is a mixed *FLM/FEM*-based, *causal compositional* tool suite that uses the SLIM language, which is based on a subset of AADL, for its input models [7], [10]. In SLIM, a nominal system model and the error model are developed separately and then transformed into an extended system model. This extended model is automatically translated into input models for the NuSMV model checker [13], [25], MRMC (Markov Reward Model Checker) [22], [24], and RAT (Requirements Analysis Tool) [27]. The safety analysis tool xSAP [3] can be invoked in order to generate safety analysis artifacts such as fault trees and FMEA tables [4]. COMPASS is an impressive tool suite, but some of the features that make AADL suitable for SW/HW architecture specification: event and event-data ports, threads, and processes, appear to be missing, which means that the

SLIM language may not be suitable as a general system design notation (ESM).

SmartIFlow [18] is a *FEM*-based, *purpose-built*, *monolithic non-causal* safety analysis tool that describes components and their interactions using finite state machines and events. Verification is done through an explicit state model checker which returns sets of counterexamples for safety requirements in the presence of failures. SmartIFlow allows *non-causal* models containing simultaneous (in time) bi-directional failure propagations. On the other hand, the tools do not yet appear to scale to industrial-sized problems, as mentioned by the authors [18]: “As current experience is based on models with limited size, there is still a long way to go to make this approach ready for application in an industrial context”.

The Safety Analysis and Modeling Language (SAML) [17] is a *FEM*-based, *purpose-built*, *monolithic causal* safety analysis language. System models constructed in SAML can be used for both qualitative and quantitative analyses. It allows for the combination of discrete probability distributions and non-determinism. The SAML model can be automatically imported into several analysis tools like NuSMV [13], PRISM (Probabilistic Symbolic Model Checker) [23], or the MRMC probabilistic model checker [22].

AltaRica [2], [26] is a *FEM*-based, *purpose-built*, *monolithic* safety analysis language with several dialects. There is one dialect of AltaRica which use dataflow (*causal*) semantics, while the most recent language update (AltaRica 3.0) uses non-causal semantics. The dataflow dialect has substantial tool support, including the commercial Cecilia OCAS tool from Dassault. For this dialect the Safety assessment, fault tree generation, and functional verification can be performed with the aid of NuSMV model checking [8]. Failure states are defined throughout the system and flow variables are updated through the use of assertions [1]. AltaRica 3.0 has support for simulation and Markov model generation through the OpenAltaRica ([www.openaltarica.fr](http://www.openaltarica.fr)) tool suite.

Formal verification tools based on model checking have been used to automate the generation of safety artifacts [3], [8], [11]. This approach has limitations in terms of scalability and readability of the fault trees generated. Work has been done towards mitigating these limitations by the scalable generation of readable fault trees [9].

#### VI. CONCLUSION

We have developed an extension to the AADL language with tool support for formal analysis of system safety properties in the presence of faults. Faulty behavior is specified as an extension of the nominal model, allowing safety analysis and system implementation to be driven from a single common model. This new Safety Annex leverages the AADL structural model and nominal behavioral specification (using the AGREE annex) to propagate faulty component behaviors without the need to add separate propagation specifications to the model. Next steps will include extensions to automate injection of Byzantine faults as well as automatic generation of fault trees. For more details on the tool, models, and approach, see the

technical report [29]. To access the tool plugin, users manual, or models, see the repository [28].

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