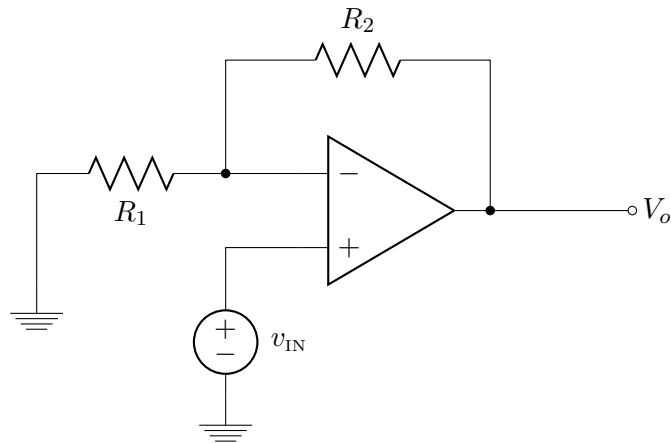


Problem 1. The non-inverting amplifier shown below uses a non-ideal op amp with a finite open-loop gain.

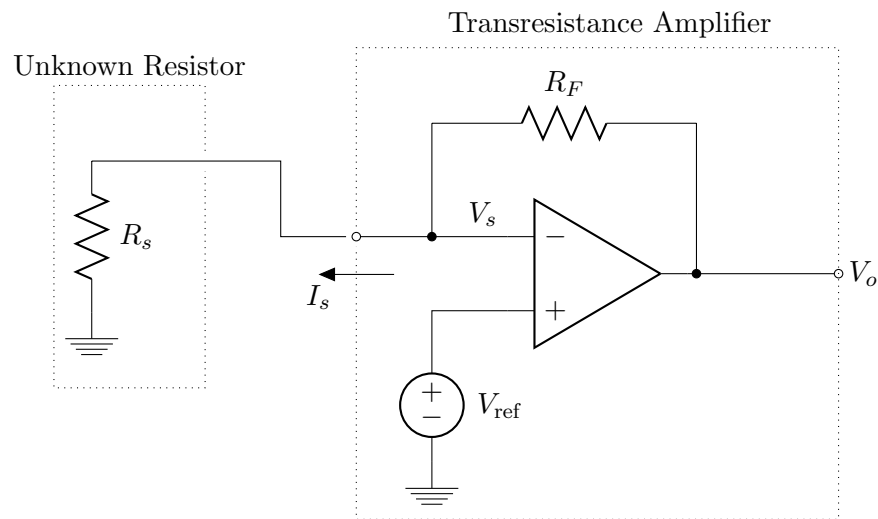


- (A) Calculate the *ideal gain* if the op amp has  $A \rightarrow \infty$ ,  $R_1 = 1\text{k}\Omega$  and  $R_2 = 9\text{k}\Omega$ .
- (B) Calculate the *actual gain* for the values in (A) if the gain is  $A = 100\text{ V/V}$ .
- (C) Suppose the op amp has a finite open-loop gain of  $A = 1000\text{ V/V}$ , and it is desired to have an actual circuit gain of  $G = 10\text{ V/V}$ . What is the ratio  $R_2/R_1$  that will achieve the desired gain?
- (D) Lastly, if the open loop gain varies from 100 to  $1000\text{ V/V}$ , and  $R_1$  is held constant at  $1\text{k}\Omega$ , what is the range of adjustments needed in  $R_2$  to maintain an actual gain of  $G = 10\text{ V/V}$ ?

Problem 2. The *transresistance amplifier* shown below is to be used in a sensor interface. The resistor  $R_s$  is an unknown resistance, which will be measured by the following method:

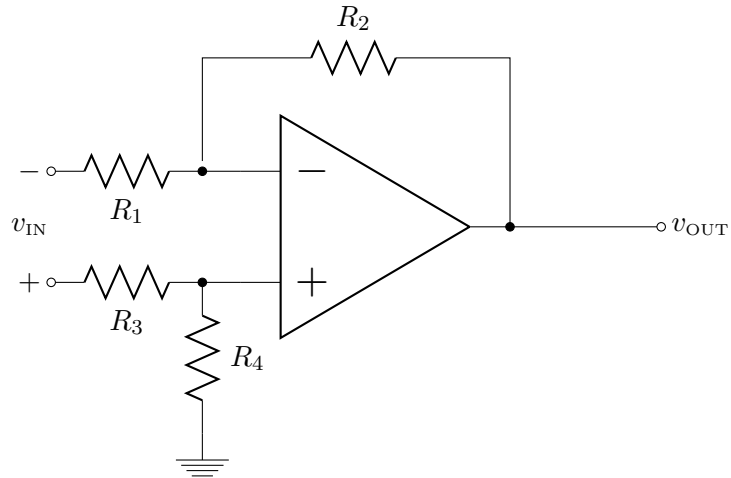
- (i) Apply a known potential  $V_{\text{ref}}$  to the op amp's non-inverting input terminal. Due to the virtual short effect, the same potential (or nearly the same) should then appear at the inverting input terminal.
- (ii) Measure the potential  $V_o$  appearing at the op amp's output terminal.
- (iii) Based on  $V_o$ , estimate the value of the current flowing through  $R_s$ . The resistance is then

$$R_s \approx V_s / I_s$$



- (A) If the op amp is ideal, obtain expressions for these items:  $V_s$ ,  $I_s$ , and  $V_o$ . For each item, the left-hand side of your expression should only include  $R_s$ ,  $V_{\text{ref}}$  and/or  $R_F$ . Finally, obtain an expression for  $R_s$ .
- (B) Repeat (A) for the case where the op amp has *finite gain* equal to  $A$  V/V. This time, the left-hand side of each expression should only include  $R_s$ ,  $V_{\text{ref}}$ ,  $R_F$  and/or  $A$ .
- (C) Suppose the op amp is ideal,  $R_s = 1\text{k}\Omega$ ,  $R_F = 2\text{k}\Omega$ , and  $V_{\text{ref}} = 1\text{V}$ . What are the values of  $V_s$ ,  $I_s$  and  $V_o$ ?
- (D) Repeat (C) for an op amp with finite gain  $A = 100$  V/V.
- (E) For the circuit described in (C) and (D), suppose  $R_s$  can vary between  $500\Omega$  and  $5\text{k}\Omega$ . What is the corresponding range of variation that may be seen in  $V_o$ ?
- (F) Estimate the value of  $R_s$  if  $V_o = 1.5\text{V}$ ,  $R_F = 10\text{k}\Omega$ ,  $V_{\text{ref}} = 1\text{V}$  and  $A \rightarrow \infty$ .

Problem 3. The difference amplifier shown below uses an op amp, but suffers from mismatch in its resistor values. By design,  $R_2 = R_4 = 10\text{k}\Omega$ , and  $R_1 = R_3 = 1\text{k}\Omega$ . In reality, all resistors vary within a  $\pm 5\%$  tolerance.



For this circuit, recall that there are two signal paths, called the *inverting* path and the *non-inverting* path. The goal is to balance the gains along these signal paths:

$$\begin{aligned} \text{inverting path : } -G_i &= -\frac{R_2}{R_1} \\ \text{non-inverting path : } G_{ni} &= \left(1 + \frac{R_2}{R_1}\right) \left(\frac{R_4}{R_3 + R_4}\right) \end{aligned}$$

Notice here that  $G_i$  is defined as a positive number. Based on these definitions, you can show that the differential gain and the common-mode gain are:

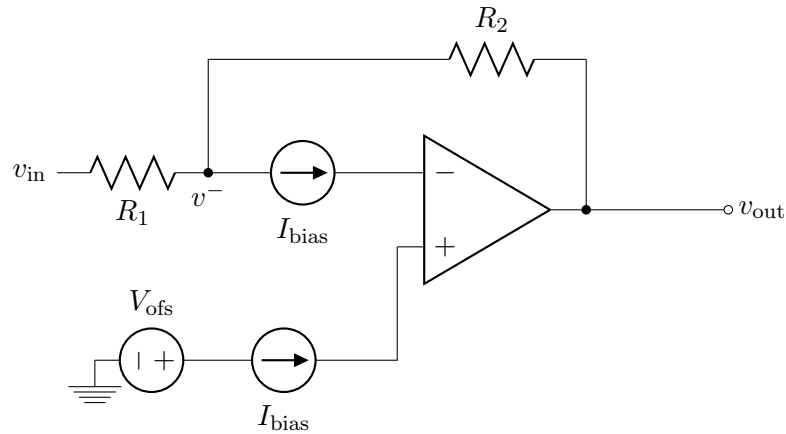
$$\begin{aligned} A_d &= \frac{1}{2} (G_i + G_{ni}) \\ A_{CM} &= |G_i - G_{ni}| \end{aligned}$$

- (A) If all the resistors were *perfectly matched* to their specified values, what should be the circuit's differential gain, common-mode gain and CMRR?
- (B) Suppose all resistors are mismatched from their specified values as follows:

$$\begin{aligned} R_1: & 5\% \text{ too large} & R_2: & 5\% \text{ too small} \\ R_3: & 5\% \text{ too small} & R_4: & 5\% \text{ too large} \end{aligned}$$

In this case, calculate the resistor values, the differential gain, the common-mode gain and the CMRR in dB.

Problem 4. A non-inverting op amp configuration is shown below. Also shown are current and voltage sources inserted to model the op amp's non-ideal bias current and offset voltage.



- (A) For this problem, suppose that  $V_{ofs} = 0$ ,  $I_{bias} = 20\mu\text{A}$ , and  $R_1 = 10\text{k}\Omega$ . The op amp's supply rails are at  $\pm 5\text{V}$ , and the op amp has infinite open-loop gain. If the input signal is a sinusoid with peak-to-peak amplitude  $10\text{mV}$ , what is the **maximum gain** (i.e. the maximum value for  $R_2$ ) that can be allowed without saturating the op amp?
- (B) For this problem, suppose that  $I_{bias} \approx 0$ ,  $R_2 = 5\text{k}\Omega$ ,  $R_1 = 1\text{k}\Omega$  and the op amp is otherwise ideal. If  $V_{ofs}$  varies in the range of  $\pm 10\text{mV}$ , what is the range of DC offset voltages that may appear at  $V_{OUT}$ ?