

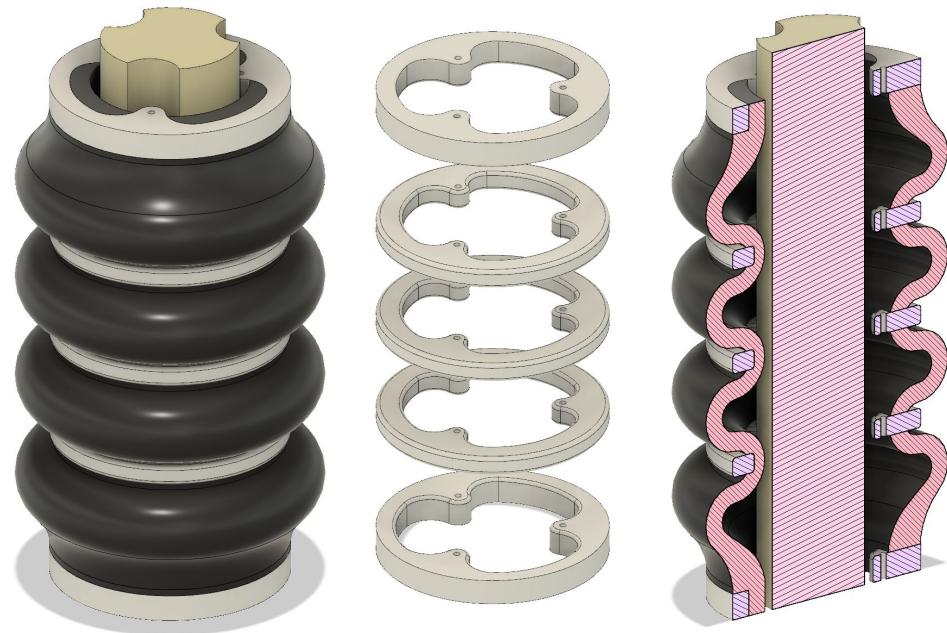
# Thesis Visuals for Personal Website

## Connex Design

- Soft Bellow Thickness: [ 1.5 2.0 2.5 ] mm

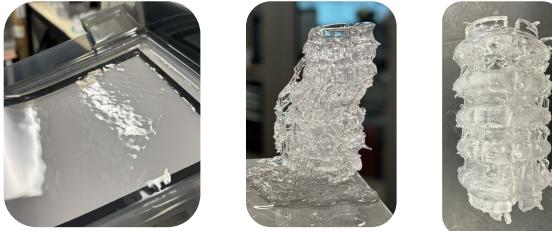
Next Steps:

- Characterize compression.
- Test functionality of tendon actuation.



## FormLabs

- Troubleshooting
  - New Material + Tank on the way!



# Model Design



Segments  
Lengths  
Diameter

All Possible  
Kappa, Phi, Ell

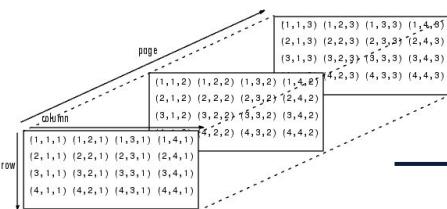
function

robotindependentmapping

ell, kappa, phi → [n x 16] matrix

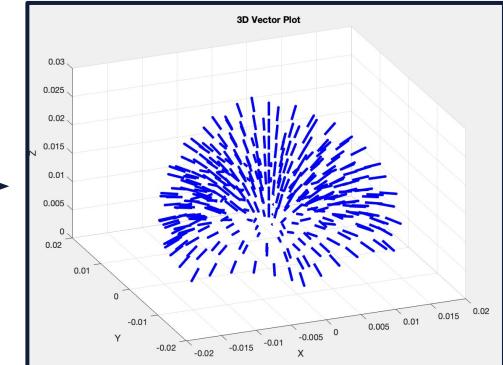
$$T_w = \begin{bmatrix} \cos^2 \phi (\cos \kappa s - 1) + 1 & \sin \phi \cos \phi (\cos \kappa s - 1) & \cos \phi \sin \kappa s & \frac{\cos \phi (1 - \cos \kappa s)}{\kappa} \\ \sin \phi \cos \phi (\cos \kappa s - 1) & \cos^2 \phi (1 - \cos \kappa s) + \cos \kappa s & \sin \phi \sin \kappa s & \frac{\sin \phi (1 - \cos \kappa s)}{\kappa} \\ -\cos \phi \sin \kappa s & -\sin \phi \sin \kappa s & \cos \kappa s & \frac{\sin \kappa s}{\kappa} \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

All possible curves

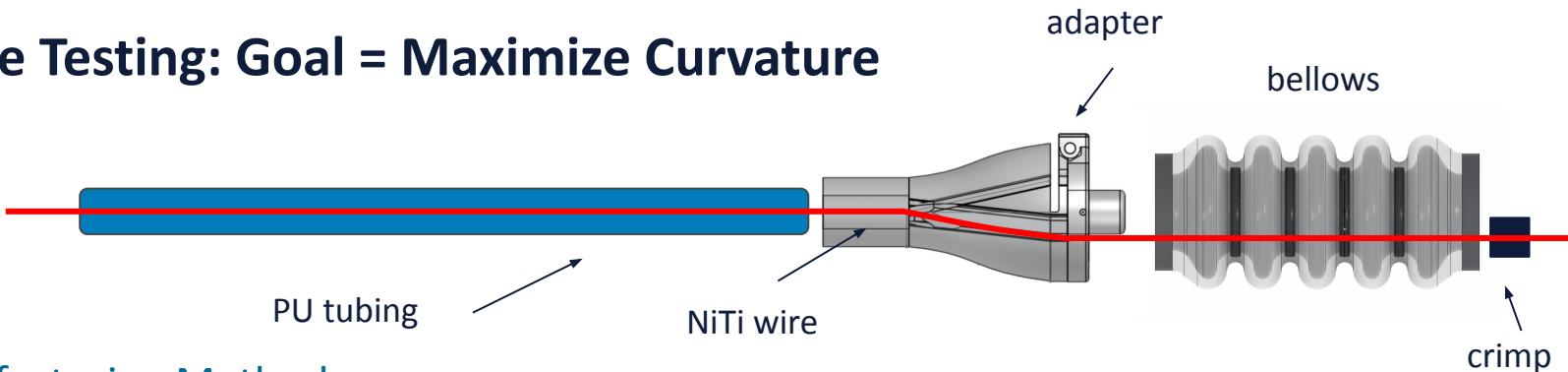


Extract vectors and origins

```
for idx = 1:size(mapping_results, 3)
    g = mapping_results(:, :, idx);
    vx = g(end, 9); % Extract the components of the vector
    vy = g(end, 10);
    vz = g(end, 11);
    x = g(end, 13); % Extract the origin of the vector
    y = g(end, 14);
    z = g(end, 15);
    all_points = [all_points; x, y, z, vx, vy, vz];
end
```



# Prototype Testing: Goal = Maximize Curvature

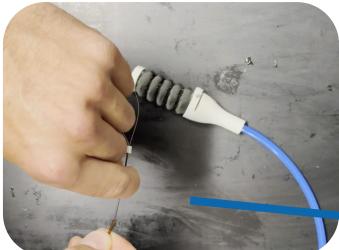


Progress:

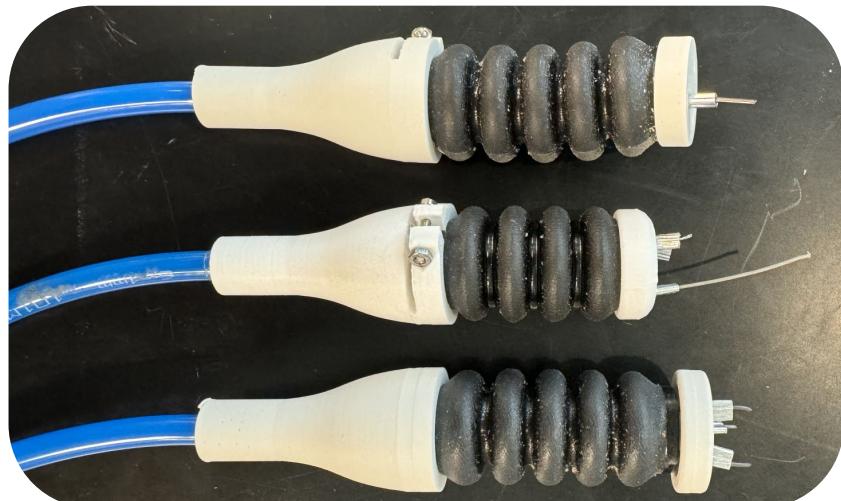
- Manufacturing Methods
- Bellow Geometry
- Tendon Guidance

Challenges

- Push/Pull Tendons



*CAD of latest Connex Print*



*Prints with Different Tendons Mounted*

# PROJECT AIMS

## Aim 1. Design and model a soft 3D printed manipulator.

A 3D printed prototype capable of greater than  $\pm 90^\circ$  of pitch, steerable by tendons. Also capable of extending and compressing over 30% of its nominal length respectively using pneumatics. The mechanism will have a 26mm outer diameter which is twice that of a standard colonoscope (2:1 scale). The overall length will be primarily influenced by the number of bellows, which are needed to ensure proper range of motion for steering.

## Aim 2. Characterize the extension/compression/steering of the mechanism.

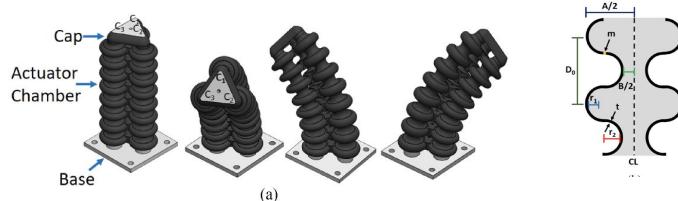
Characterize the scanning ability (in degrees of movement or using curvature) of mechanism using either Motion Tracking or IMUs. Provide comparisons of our characterization with the models that have been developed in Aim I. Characterize extension and compression ratios and map to tendon forces/air pressures that drive the respective movement.

## Aim 3. Demonstrate potential use of mechanism.

Mount the mechanism on a vine system designed for eversion and retraction. Develop a 2m long cylindrical demo environment that includes areas of interest that the mechanism can probe. This may be viewing with a camera or tracked using IMUs. Challenges will be completed to show the capabilities of the system.

# PROJECT AIMS - FIGURES

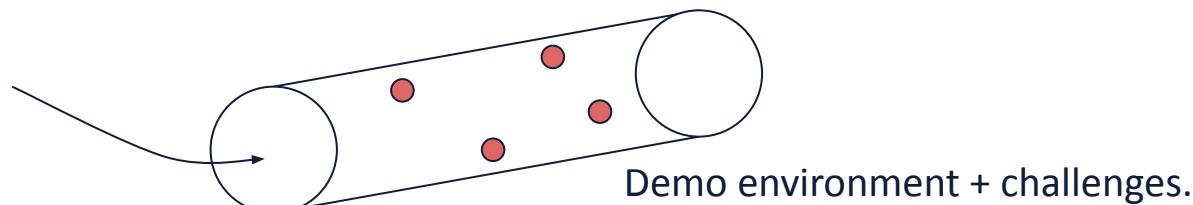
Aim 1. Design and model a soft 3D printed manipulator.



Aim 2. Characterize the extension/compression/steering of the mechanism.



Aim 3. Demonstrate potential use of mechanism.

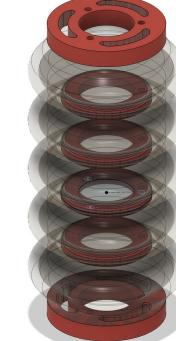


# Connex Print V2 Design Changes



- Internal Clamps
  - Compression
- 1.5mm Wall
  - Flexibility
- Top Clamp Thick
  - Termination
- Top Clamp Inner Material
  - Rigid
  - Easy to make air tight
- 1mm Guides

**V1 → V2**



# 3D Printed Bellow Mechanism for Vine Tip Scanning

## Connex Design Testing

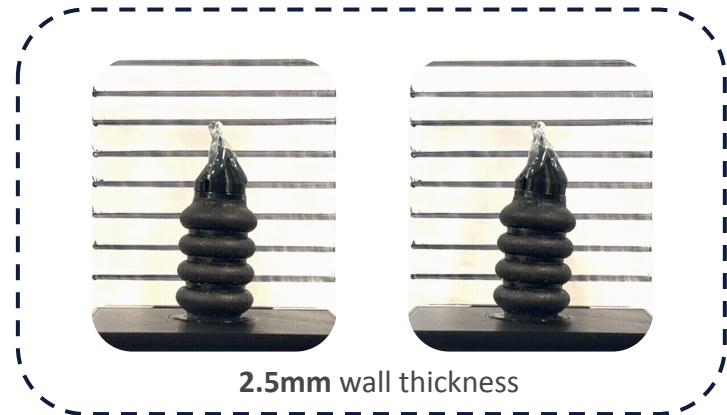
- 1.5, 2.0 ,2.5 mm
- Print Resolution, Bellow Thickness
- Elasticity



Wall Thickness	Nominal	Extended	Compressed	Force (Compression)
<b>1.5</b>	39.5	<b>50</b>	<b>27</b>	<b>8.8 N</b>
<b>2.0</b>	40	46	29	16.2 N
<b>2.5</b>	40	44	31	25.7 N



Rings and walls restrict compression and steering...

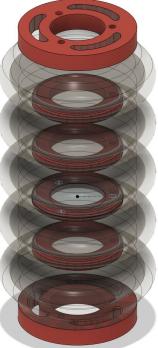


# Connex Print V2 Design Changes



V1 → V2

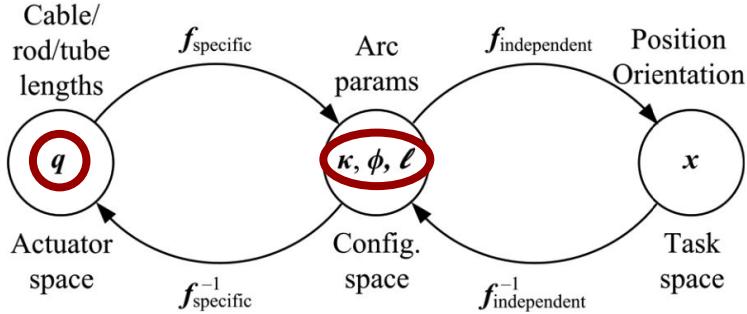
- Top Clamp Thickness + Inner Material
- Internal Clamps
- 1.5mm Wall
- Added +1 Bellow
- 1mm Guides



# Modeling Approach

## Design and Kinematic Modeling of Constant Curvature Continuum Robots: A Review

Robert J. Webster III<sup>1</sup> and Bryan A. Jones<sup>2</sup>



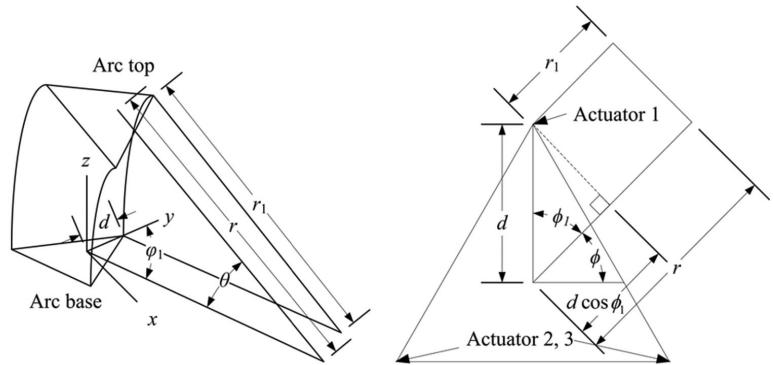
Mappings to define kinematics of constant-curvature robots... transforms actuator space variables  $q$  to configuration space variables  $k, l, \psi$ .

## How to Model Tendon-Driven Continuum Robots and Benchmark Modelling Performance

Priyanka Rao\*, Quentin Peyron, Sven Lilge and Jessica Burgner-Kahrs

## Kinematics for Multisection Continuum Robots

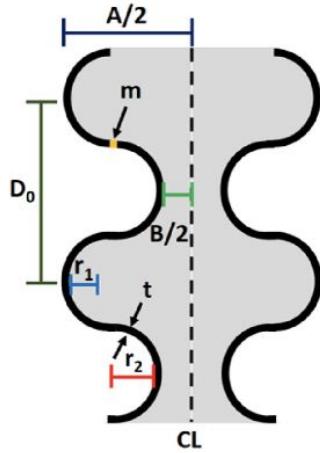
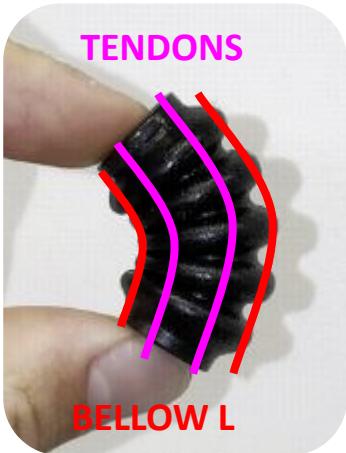
Bryan A. Jones, Member, IEEE, and Ian D. Walker, Fellow, IEEE



Arc section in which various arc parameters are defined and a diagram of the base section seen from above.

# Modeling Considerations

## How to consider max/min length of bellow



The deflection of the chamber is modeled using elemental load cases applied to a half- convolution of one of the bellows

The change in length of an individual bellows chamber  $\Delta l_i^e$  due to its internal pressure  $P_i$  is determined from

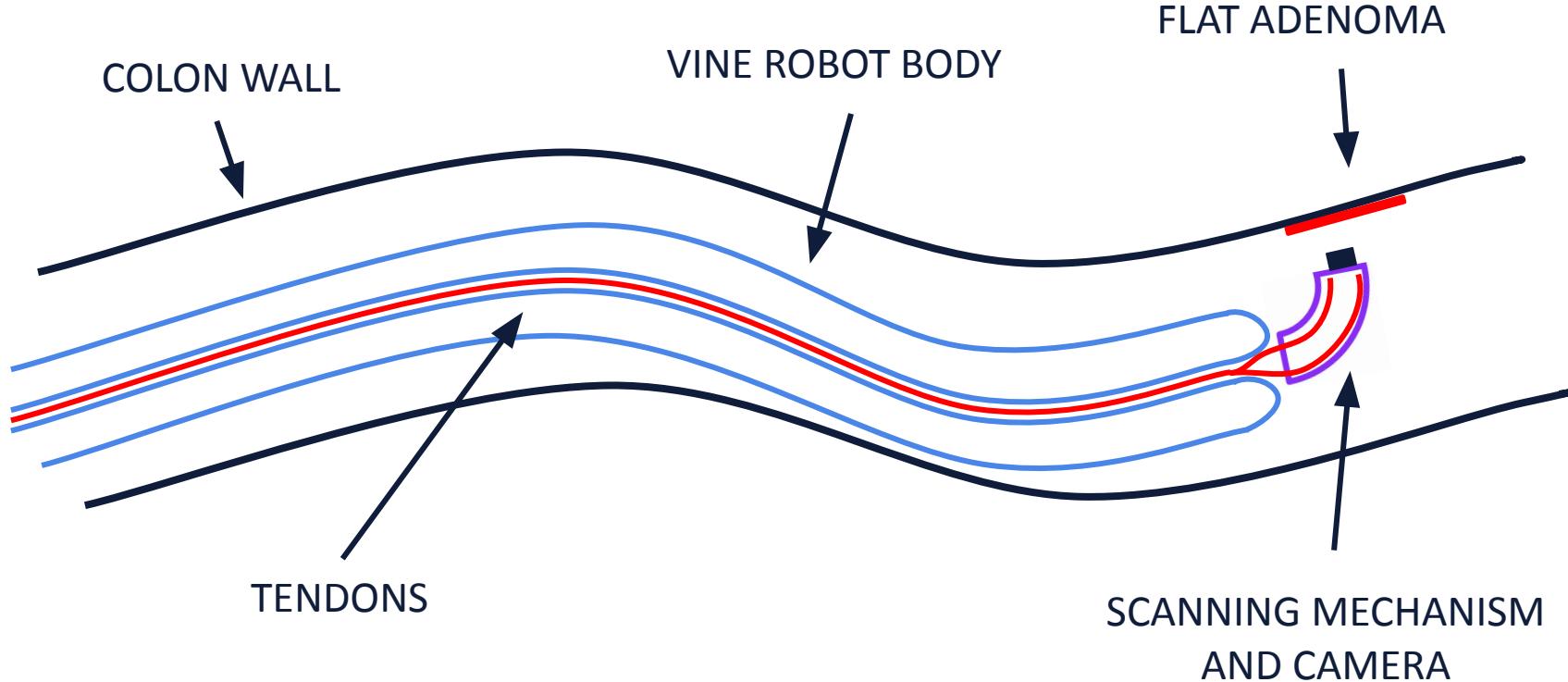
$$\Delta l_i^e = \frac{P_i A_p}{k_i} \quad (7)$$

$$l_i^e = \Delta l_i^e + l_0 \quad (8)$$

Assuming that the axial stiffness is similar in extension and compression, the stiffness  $k_i$  of chamber  $i$  is

$$k_i = \frac{1}{2n(\beta_1 + \beta_2)} \quad (5)$$

$$\beta_j = \frac{6\pi r_j^3 + 24mr_j^2 + m^3 + 3m^2r_j\pi \left(1 + \frac{t^2}{12r_j^2}\right)}{24EI} \quad (6)$$



Tango Black  
(flexible)



soft bellows

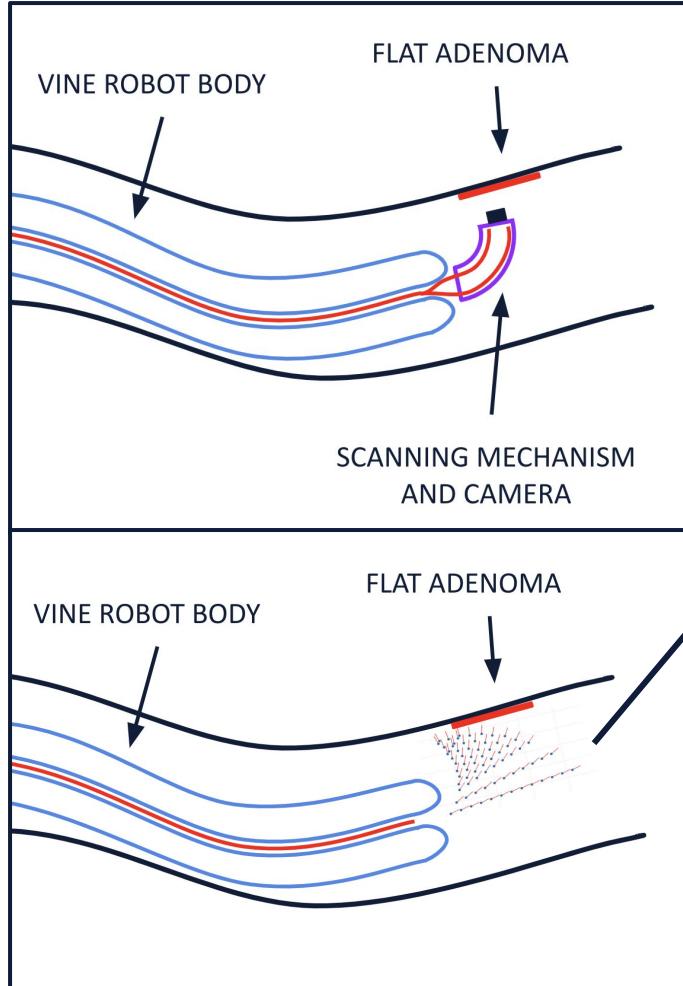
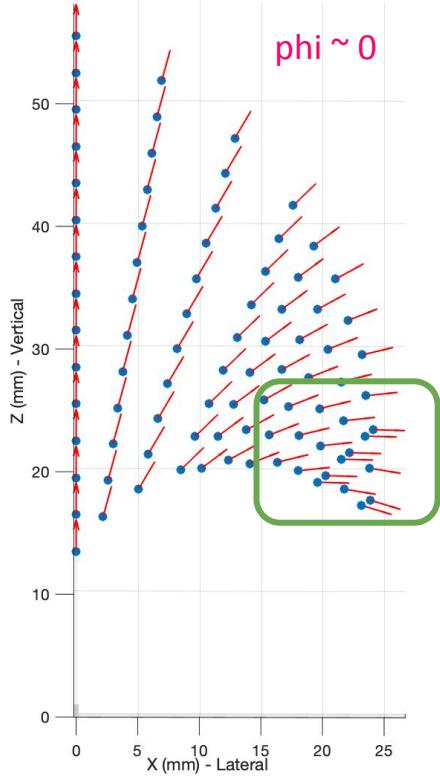
VeroClear  
(rigid)



tendon guides

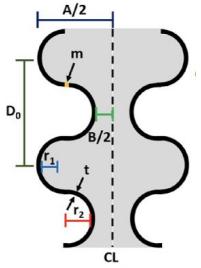
# Modeling Progress

Filtered Tip Positions and Directions of the Continuum Robot



# Modeling

- Estimated Bellows → Lengths
- Assume Constant Curvature

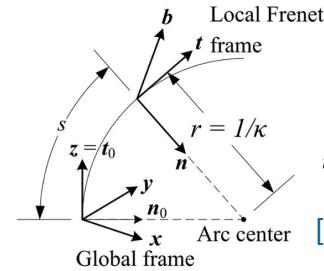


[1]

$$\phi(\mathbf{q}) = \tan^{-1} \left( \frac{\sqrt{3}(l_2 + l_3 - 2l_1)}{3(l_2 - l_3)} \right)$$

$$\ell(\mathbf{q}) = \frac{l_1 + l_2 + l_3}{3}$$

$$\kappa(\mathbf{q}) = \frac{2\sqrt{l_1^2 + l_2^2 + l_3^2 - l_1l_2 - l_1l_3 - l_2l_3}}{d(l_1 + l_2 + l_3)}$$



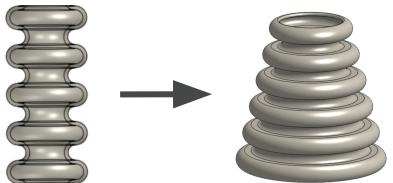
[2]

$$K(s) = \pi/2 - \phi$$

$$T(s) = \pi/2 - \kappa s$$

$$\mathbf{t}(s) = \begin{bmatrix} l(s) \sin K(s) \cos T(s) \\ l(s) \cos K(s) \cos T(s) \\ l(s) \sin T(s) ds \end{bmatrix}$$

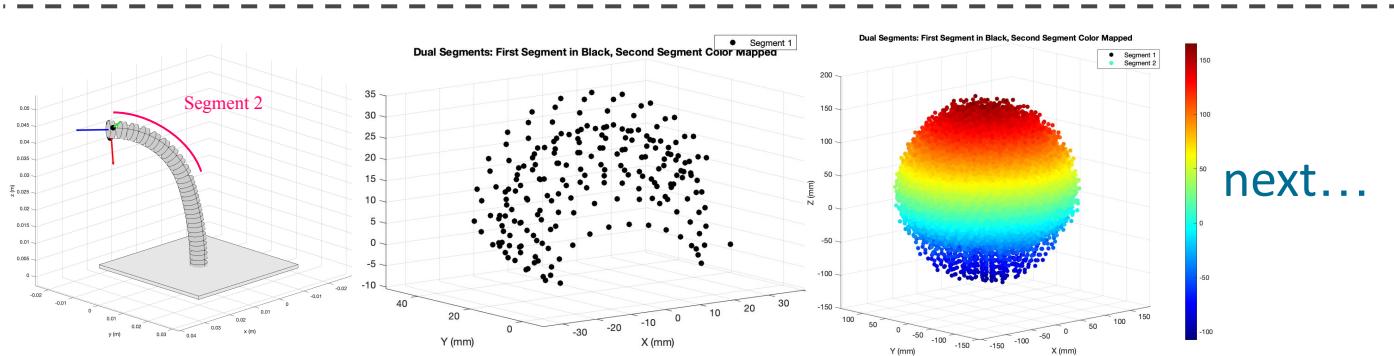
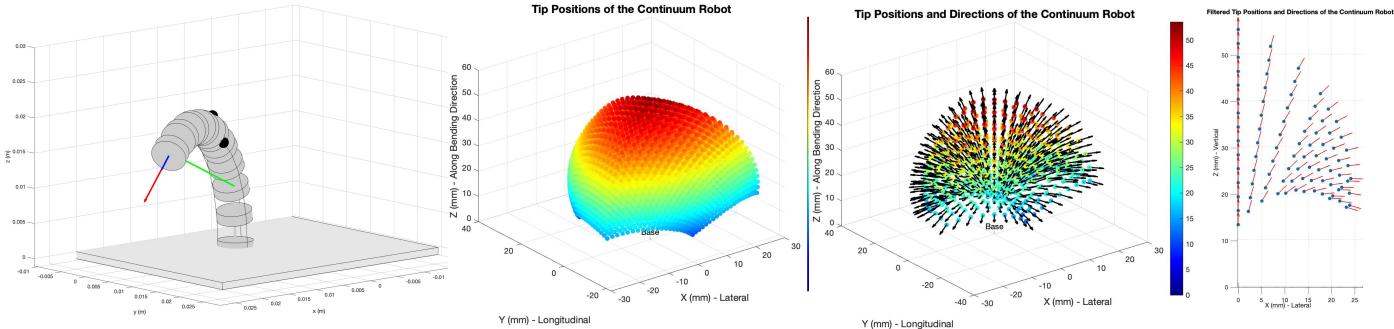
- Single Segment
- Frenet Frame  $\mathbf{t}$
- Maximize Lateral Reach



- Non-Constant Curvature
- Multi-Segment (Stepwise)

## Challenge

- Select for Bending Plane
- Second Segment length



next...