Energy savings for UAV flight in unsteady gusting conditions through trajectory optimization

Lou Grimaud

Illinois Institute of Technology

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- 1. Introduction
- 2. The trajectory optimization problem
 - Dynamic soaring
 - Neutral energy loop
 - Implementation validation
 - Quasi-steady aerodynamic model results
- 3. The unsteady aerodynamic model
 - Experimental setup
 - The Goman and Khrabrov model
 - Determination and validation of the model
- 4. Unsteady trajectory optimization
 - Time constant equivalence
 - Gust duration dependency
 - Phase results
- 5. Conclusion



Introduction

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Introduction

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Different types of soaring

Figure: something about soaring

Spatial wind gradients

- Thermal updrafts
- Horizontal wind gradients

Temporal wind gradients

- ► Natural turbulences
- Building and natural feature wake



Defining the energy extraction problem

What is an "optimal trajectory"?

- Maximum energy at the end of the cycle
- Maximizing the energy gain at each instant of the cycle
- Minimize the energy input needed for sustainable flight

The neutral energy loop

Finding the minimal wind gust that allows to maintain altitude and speed over a gust.



$$\ddot{x} = -L' \cdot \sin(\gamma) + D' \cdot \cos(\gamma)$$
$$\ddot{z} = L' \cdot \cos(\gamma) - D' \cdot \sin(\gamma) - m \cdot g$$

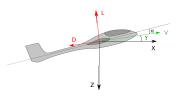


Figure : Coordinate system used for the optimization

Lissaman's non-dimensional variables

- $lackbox{ Velocities with } V^* \mbox{ the optimal glide speed}$
- ▶ Time with $T = \frac{V^*}{g}$
- Lift and drag coefficients $L = \frac{C_l}{C_l^*}$ and $D = \frac{C_{d}}{C^*}$
- \blacktriangleright Dynamic pressure $Q=\frac{L'}{MgL}=\frac{\frac{1}{2}\rho V^2C_lC_l^*}{Mg}$

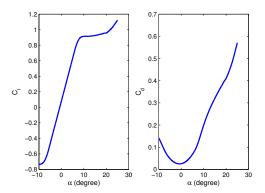
$$\begin{array}{l} \frac{dU}{dT} = -LQ \cdot \sin(\gamma) + DQ \cdot \cos(\gamma) \\ \frac{dW}{dT} = LQ \cdot \cos(\gamma) - DQ \cdot \sin(\gamma) - 1 \end{array}$$



Quasi-steady lift and drag model

► NACA0009 characteristic

Lissaman's quadratic drag



 $D = \frac{1+L^2}{2G^*}$

Figure: Simplified lift and drag for the NACA0009 airfoil



Wind profiles

We define three different wind profiles:

► Vertical wind gust:

$$W_g = W_a \cdot \sin(2\pi T)$$
$$U_g = 0$$

Horizontal wind gust:

$$W_g = 0$$
$$U_g = W_a \cdot \cos(2\pi T)$$

Combined wind gust:

$$W_g = W_a \cdot \sin(2\pi T)$$

$$U_g = W_a \cdot \cos(2\pi T + \varphi)$$



The cycle is discretized

$$x = \begin{bmatrix} \dots \\ X_i \\ Z_i \\ U_i \\ W_i \\ L_i/\alpha_i \\ \dots \\ W_a \end{bmatrix} \quad i \in [1, N]$$

Constraints formulation

Comparison with Lissaman's results

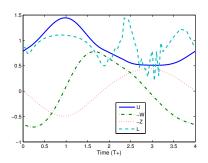


Figure : Optimization results for a 4T long vertical gust

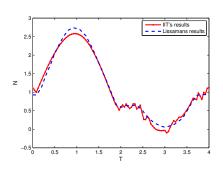


Figure : Comparison with Lissaman's non-dimensional normal force N for a 4T long vertical gust



Quasi-steady lift to drag model

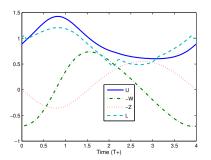


Figure : 4T long vertical gust for the NACA0009 airfoil, $W_a=0.205$

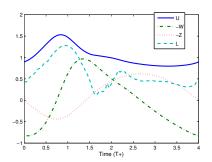


Figure : 4T long combined gust for the NACA0009 airfoil, $W_a = 0.387$



Tg dependency

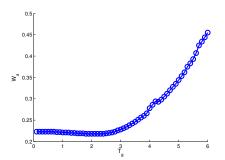


Figure: Influence of gust duration on the minimum gust amplitude for vertical gusts

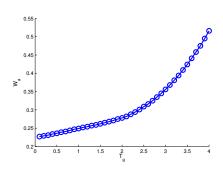


Figure: Influence of gust duration on the minimum gust amplitude for combined gusts



Difference between short and long gusts

We can see that there is tipping point around $T_q=2.5$

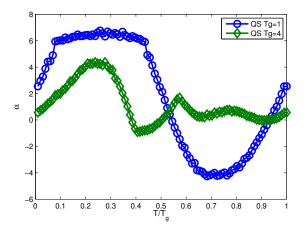


Figure : Difference between short and long gust angle of attack profile for combined gusts

Angle of attack limitation

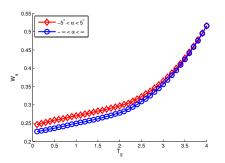


Figure: Difference in performance for combined wind gusts if no high angle of attack are allowed

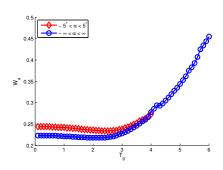


Figure: Difference in performance for vertical wind gusts if no high angle of attack are allowed



Phase influence

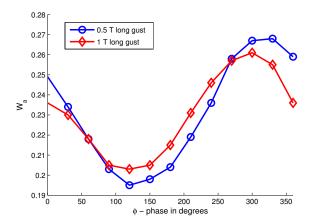


Figure : Influence of the phase between the components of the combined gust



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Pitching mechanism and experimental conditions

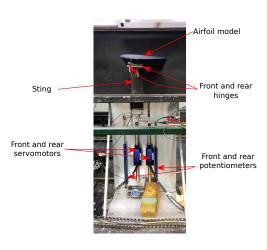


Figure: Airfoil model inside the wind tunnel

Experimental conditions

- ► Free stream velocity: 3 m/s
- Airfoil: NACA0009
- ► Reynolds number 50000

Controller and data acquisition

- Angle of attack controlled by simulink[®] and two servomotors
- Servos position measured by two linear potentiometers
- Piezoelectric force balance (NANO17) to measure the forces on the airfoil



The GK model concept

The Goman and Khrabrov model¹ - a non-linear state space model

$$C_l = f(\alpha, x(\alpha))$$

$$C_d = g(\alpha, x(\alpha))$$

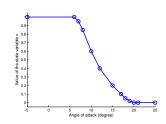
$$\tau_1 \frac{dx}{dt} + x = x_0(\alpha - \tau_2 \dot{\alpha})$$

Lift and drag model

Non-linear state map

Time constants τ_1 and τ_2

$$C_l = 2\pi\alpha(0.6x + 0.4) + C_{l0}$$
$$C_d = \frac{((2-x)C_l)^2}{G_{\text{max}}} + C_{d0}$$



¹Goman M and Khrabrov A. Journal of Aircraft, 31(5):11091115,1994.

Quasi-steady map and state variable

$$C_l(\alpha, x) = 2\pi \cdot \alpha(0.6x + 0.4) + C_{l0}$$

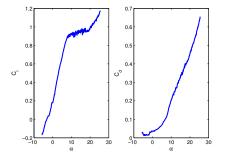


Figure: Lift and drag coefficient in the quasi-steady case

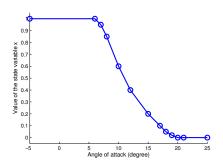


Figure : Quasi-steady profile for the state variable x



Time constant determination





Pseudo-random case

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Unsteady optimization

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put Wa vs Tg curve and alpha tg to explain on the same slide?



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