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DUT de-embedding
using a 2x Thru

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For sake of simplicity, we limit this discussion to 2-port analysis.

Assume DUT is embedded between identical (but mirrored) feed-in structures.

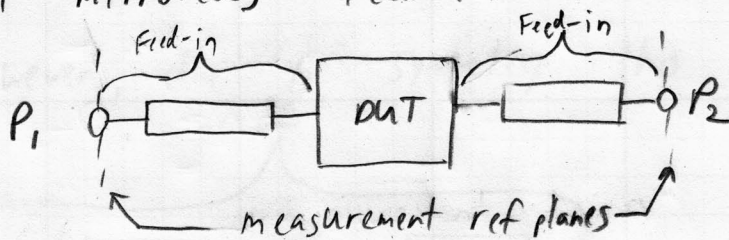


Fig 1

Our goal is to move the reference planes around the DUT. To this end, we design copies of feed-in structure and cascade them.

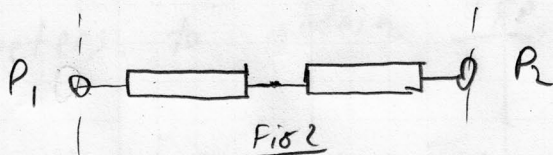


Fig 2

Thus, we have two measurements.

Let $\underline{S_E}$: end-to-end, measured S-param matrix for Fig 1

$\underline{S_F}$: feed-in structures measured S-param matrix for Fig 2

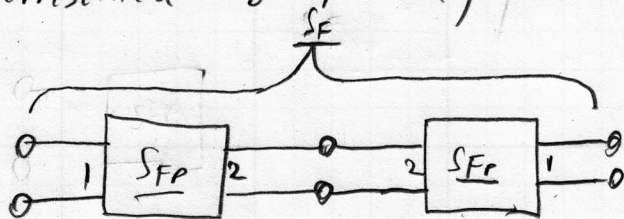
We now show the method to split $\underline{S_F}$ to obtain S-parameters for the individual feed-in structures.

Since we made feed-in structures identical, $\underline{S_E}$ is a cascade of two identical S-parameters.

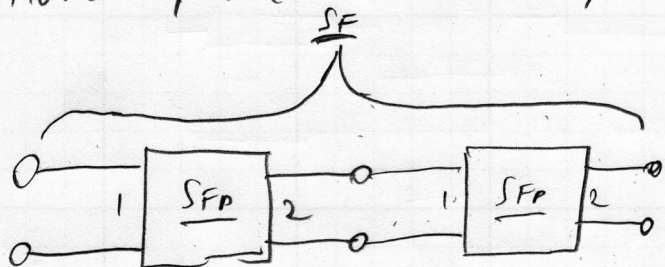
Using the well-known fact that passive linear systems yield symmetrical matrices, we define a matrix $\underline{S_{FP}}$ that represents the individual feed-in structure with the property:

$$\underline{S_{FP}} = \underline{S_{FP}}^T$$

Represented graphically (and observing the mirroring)!



However, due to symmetry this is same as



Since this is a cascade, it is easier to use T-parameters. to obtain $\underline{S_{FP}}$.

Thus,
$$\underline{T_F} = \underline{T_{FP}} \underline{T_{FP}} = \underline{T_{FP}}^2 \Rightarrow \underline{T_{FP}} = \sqrt{\underline{T_F}}$$

The square root of $\underline{T_F}$ can be found through the diagonalization procedure (See Appendix II).

Once obtained, $\underline{T_{FP}}$ can be inverted and cascaded against $\underline{S_E}$.

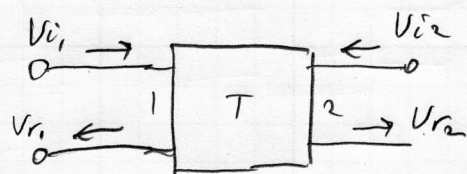
and $\underline{S_E} \Rightarrow \underline{I_E} = \underline{T_{FP}}^{-1} \underline{T_F} \underline{T_{FP}}$

$$\underline{T_{out}} = \underline{T_{FP}}^{-1} (\underline{T_F}) \underline{T_{FP}} = \underline{T_{FP}}^{-1} (\underline{T_{FP}} \underline{T_{out}} \underline{T_{FP}}) \underline{T_{FP}}^{-1}$$

Appendix I

$S \rightarrow T, T \rightarrow S$ conversions

The following is described in terms of voltages rather than power as it is assumed the reference impedance is same for all ports. Thus, we describe the parameters in terms of incident & reflected voltages at each port.



Where V_{ix} is incident voltage at port x
 V_{rx} is reflected voltage at port x

We then define (for 2-ports)

$$\begin{bmatrix} V_{i1} \\ V_{r1} \end{bmatrix} = \begin{bmatrix} T_{11} & T_{12} \\ T_{21} & T_{22} \end{bmatrix} \begin{bmatrix} V_{r2} \\ V_{i2} \end{bmatrix} \quad (1)$$

To see this via example, let

$$\begin{bmatrix} V_{1i1} \\ V_{1r1} \end{bmatrix} = \begin{bmatrix} T_{11} & T_{12} \\ T_{21} & T_{22} \end{bmatrix} \begin{bmatrix} V_{1i2} \\ V_{1r2} \end{bmatrix} \quad \text{for } (2a)$$

&

$$\begin{bmatrix} V_{2i1} \\ V_{2r1} \end{bmatrix} = \begin{bmatrix} T_{21} & T_{22} \\ T_{21} & T_{22} \end{bmatrix} \begin{bmatrix} V_{2i2} \\ V_{2r2} \end{bmatrix} \quad \text{for } (2b)$$

If cascaded, then

$$\begin{bmatrix} V_{1i2} \\ V_{1r2} \end{bmatrix} = \begin{bmatrix} V_{2r1} \\ V_{2i1} \end{bmatrix} \quad (3)$$

So that, using (2a), (2b), (3)

$$\begin{bmatrix} V_{1i1} \\ V_{1r1} \end{bmatrix} = \begin{bmatrix} T_1 \end{bmatrix} \begin{bmatrix} T_2 \end{bmatrix} \begin{bmatrix} V_{2i2} \\ V_{2r2} \end{bmatrix} \quad (4)$$

S → T

Expressing (1) a)

For S-params

$$V_{i1} = T_{11} V_{r2} + T_{12} V_{i2} \quad (5a)$$

$$V_{r1} = T_{21} V_{r2} + T_{22} V_{i2}$$

$$\begin{aligned} V_{r1} &= S_{11} V_{i1} + S_{12} V_{i2} \\ V_{r2} &= S_{21} V_{i1} + S_{22} V_{i2} \end{aligned} \quad (5b)$$

$$V_{i1} = \frac{1}{S_{21}} V_{r2} - \frac{S_{22}}{S_{21}} V_{i2}$$

$$\begin{aligned} V_{r1} &= S_{11} \left[\frac{1}{S_{21}} V_{r2} - \frac{S_{22}}{S_{21}} V_{i2} \right] + S_{12} V_{i2} \\ &= \frac{S_{11}}{S_{21}} V_{r2} + \left(S_{12} - \frac{S_{22}}{S_{21}} \right) V_{i2} \end{aligned}$$

$$\underline{T} = \begin{bmatrix} \frac{1}{S_{21}} & -\frac{S_{22}}{S_{21}} \\ \frac{S_{11}}{S_{21}} & \frac{S_{21} S_{12} - S_{11} S_{22}}{S_{21}} \end{bmatrix}$$

T → S

Similarly comparing (5a) & (5b)

$$V_{r2} = \frac{V_{i1} - T_{12} V_{i2}}{T_{11}}$$

$$V_{r1} = T_{21} \left[\frac{V_{i1} - T_{12} V_{i2}}{T_{11}} \right] + T_{22} V_{i2} = \frac{T_{21}}{T_{11}} V_{i1} + \left[\frac{T_{11} T_{22} - T_{21} T_{12}}{T_{11}} \right] V_{i2}$$

$$\underline{S} = \begin{bmatrix} \frac{T_{21}}{T_{11}} & \frac{T_{11} T_{22} - T_{21} T_{12}}{T_{11}} \\ \frac{1}{T_{11}} & -\frac{T_{12}}{T_{11}} \end{bmatrix}$$

Appendix II

matrix square root through diagonalization

Recall eigenvector decomposition:

$$\underline{A} \vec{C}_i = \lambda_i \vec{C}_i \quad (1)$$

where

\underline{A} is $n \times n$ matrix

λ_i is i^{th} eigenvalue of \underline{A}

\vec{C}_i is i^{th} eigenvector of \underline{A} of length n .

We can apply a diagonalization procedure as follows:

$$\text{Let } \underline{C} = [\vec{C}_1 \vec{C}_2 \dots \vec{C}_i \dots \vec{C}_n] \quad (2)$$

$$\& \underline{A} = \text{diag}[\lambda_1, \lambda_2 \dots \lambda_i \dots \lambda_n] = \begin{bmatrix} \lambda_1 & & \phi \\ & \lambda_2 & \\ \phi & & \ddots & \\ & & \lambda_i & \\ & & & \ddots & \\ & & & & \lambda_n \end{bmatrix} \quad (3)$$

Then we can rewrite the decomposition in (1) as

$$\underline{A} \vec{C}_i = \lambda_i \vec{C}_i \Rightarrow \underline{A} \underline{C} = \underline{\Lambda} \underline{C} \quad (4)$$

If $\text{rank}(\underline{C}) = n$ (i.e. eigenvectors are linearly independent)

then \underline{C} is invertible:

$$\underline{C} \underline{C}^{-1} = \underline{I} \quad (5)$$

where \underline{I} is identity matrix

$$\text{Then, } \underline{A} = \underline{C} \underline{\Lambda} \underline{C}^{-1} \quad (6)$$

Next, recognize that power of $\underline{\Lambda}$ can be computed

simply by taking the power of diagonal elements λ_i .

In the particular case of square root,

$$\text{Let } \underline{A} = \underline{A}' \underline{A}' \quad (7)$$

Then, using (4) & (5)

$$\underline{A} = \underline{C} \underline{A}' \underline{A}' \underline{C}^{-1} \quad (8)$$

$$= \underline{C} \underline{A}' \underline{C}^{-1} \underline{C} \underline{A}' \underline{C}^{-1}$$

$$= \underline{A}' \underline{A}'$$

Therefore, $\underline{A}' = \sqrt{\underline{A}} \quad (9)$