Course Outline - 1st Half



- Review Classical Feedback Control
- Review Vector/Matrix Theory
- State-Space Representations
- LTI Response, Matrix Exponential
- Transfer Functions & Eigenvalues
- Frequency-Domain Analysis
- Harmonic & Impulse Responses
- Pole Placement
- Controllability

Intro to Controllability - I



The concepts of *controllability* and *observability* are important to state-space design techniques.

Controllability is related to whether or not we can arbitrarily place the closedloop poles using full-state feedback.

Observability is related to our ability to design state observers or estimators for output feedback (more later)

Intro to Controllability - II



Consider the following state-space system:

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \\ \dot{x}_3 \end{bmatrix} = \begin{bmatrix} -1 & 0 & 0 \\ 0 & -2 & 1 \\ 0 & 2 & -2 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} + \begin{bmatrix} 0 & 1 \\ 1 & 0 \\ 1 & 0 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix}$$

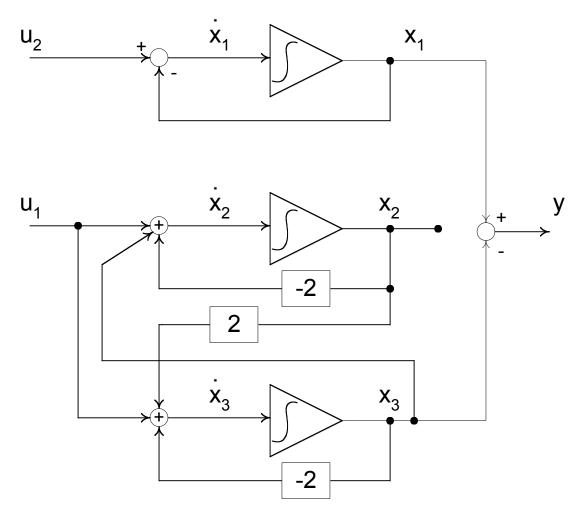
$$y(t) = \begin{bmatrix} 1 & 0 & -1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix}$$

Which states are controllable? Which states are observable?

Intro to Controllability - III

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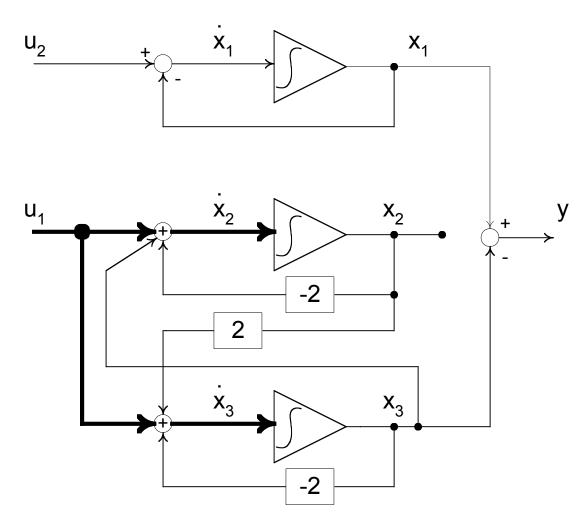
First, let's draw a block diagram



Intro to Controllability - IV



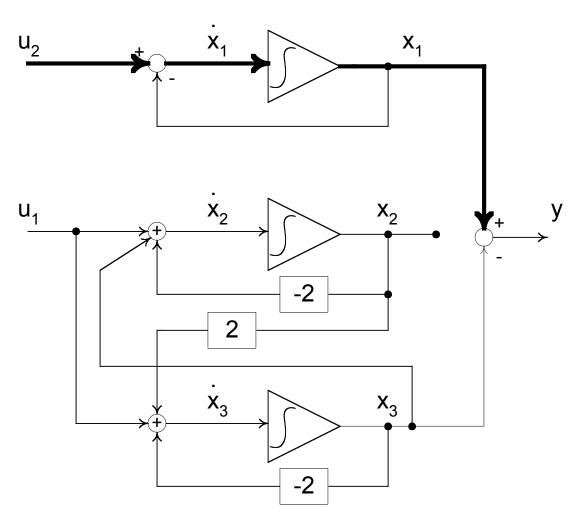
Can x_2 and x_3 be affected by u_1 ?



Intro to Controllability - V

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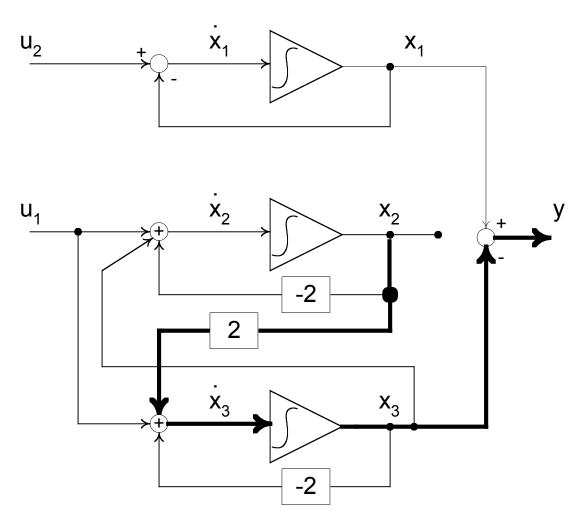
Can x_2 and x_3 be affected by u_2 ?



Intro to Controllability - VI

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Can x_2 be "seen" in y?



Intro to Controllability - VII



Some results (there are others...):

1. x_2 and x_3 are controllable from u_1 .

2. x_2 and x_3 are not controllable from u_2 .

3. x_2 is observable from y.

Intro to Controllability - VIII



Consider the response to the input

$$\begin{bmatrix} u_1 \\ u_2 \end{bmatrix} = \begin{bmatrix} \sin t \\ 0 \end{bmatrix}$$

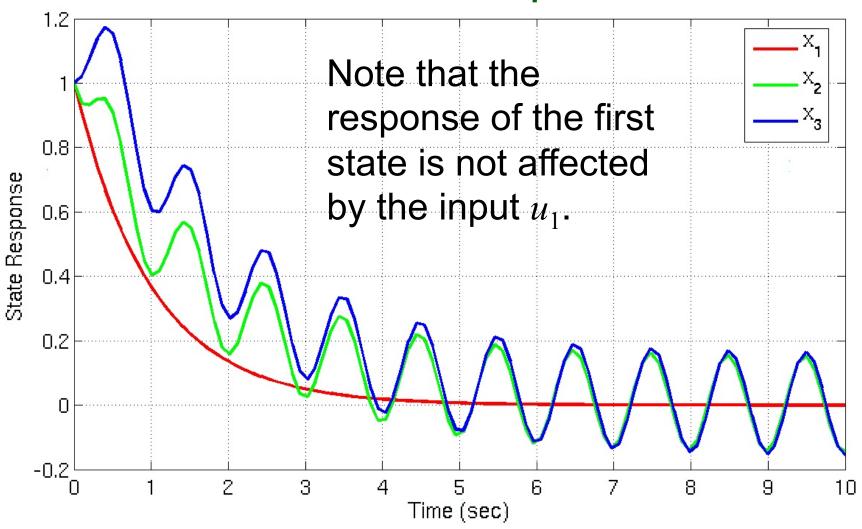
with the non-zero initial conditions

$$\mathbf{x}(0) = \begin{bmatrix} 1 \\ 1 \\ 1 \end{bmatrix}$$

Intro to Controllability - IX



The state vector time-response is:



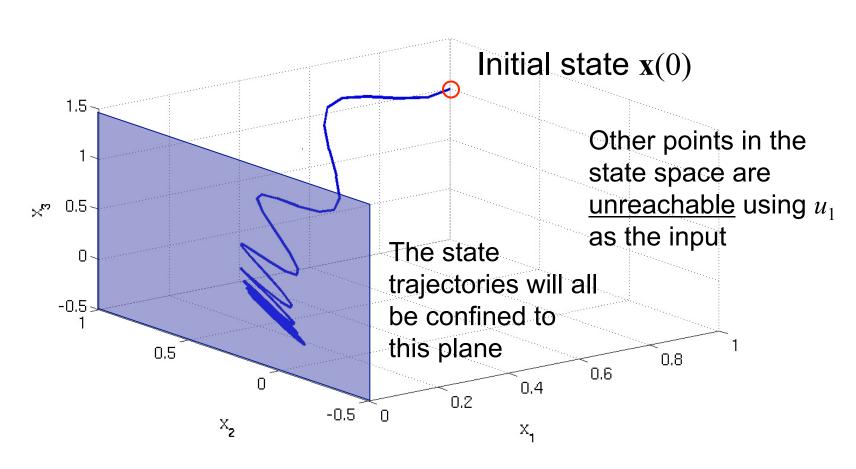
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L10a/S10

Intro to Controllability - X



We can plot the same data as a state trajectory in three dimensions:



Controllability Conditions - I



Formal definition of controllability for LTI systems:

The linear differential system

$$\dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t) + \mathbf{B}\mathbf{u}(t)$$

is said to be <u>completely controllable</u> if and only if it can be transferred from any initial state \mathbf{x}_0 at any initial time t_0 to any terminal state $\mathbf{x}(t_1) = \mathbf{x}_1$ within a finite time $t_1 - t_0$

Controllability Conditions - II



Equivalent definition: A system is controllable if and only if the column vectors of the controllability matrix

$$\mathbf{Q}_{[N \times NM]} = \begin{bmatrix} \mathbf{B} & \mathbf{AB} & \mathbf{A}^2 \mathbf{B} & \cdots & \mathbf{A}^{N-1} \mathbf{B} \\ [N \times M] & [N \times M] & [N \times M] & \cdots & [N \times M] \end{bmatrix}$$

span the *N*-dimensional space. This is equivalent to **Q** having rank *N*.

The <u>rank</u> of a matrix is the number of linearly independent columns or rows.

In-Class Assignment - I



Consider the following example

$$\mathbf{A} = \begin{bmatrix} 0 & 1 \\ 0 & -1 \end{bmatrix} \qquad \mathbf{B} = \begin{bmatrix} 1 \\ 0 \end{bmatrix}$$

Is the system controllable?

First, form the controllability matrix:

$$Q = [B \quad AB] =$$

In-Class Assignment - II



Now try the following modified example

$$\mathbf{A} = \begin{bmatrix} 0 & 1 \\ 0 & -1 \end{bmatrix} \qquad \qquad \mathbf{B} = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$$

$$\mathbf{B} = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$$

First compute the controllability matrix:

$$Q = [B \quad AB] =$$

In-Class Assignment - III



What is the rank of the matrix **Q**?

$$\mathbf{Q} = \begin{bmatrix} 1 & 0 & 1 \\ 1 & 2 & 3 \\ 3 & -2 & 1 \end{bmatrix}$$

Controllability Conditions - III



How do we check the rank for larger matrices or for matrices where the rank is not so obvious?

A <u>square matrix</u> whose rank is less than the number of columns (or rows) will have a zero determinant.

In Matlab, use det (Q) to get the determinant. A zero determinant indicates that the rank is less than N.

Controllability Conditions - IV



The number of linearly independent columns or rows can be computed for any matrix (i.e. square or nonsquare) using the rank (Q) function in Matlab

```
» Q = [1 0 1;1 2 3;3 -2 1];
» rank(Q)
ans =
```

Example 2



Given the system

$$\mathbf{A} = \begin{bmatrix} -2 & 1 \\ 0 & -1 \end{bmatrix} \qquad \mathbf{B} = \begin{bmatrix} 1 \\ a \end{bmatrix}$$

Use the rank of the controllability matrix to determine the values of *a* that result in an uncontrollable system.

Example 2



First construct the controllability matrix

$$\mathbf{Q} = \begin{bmatrix} \mathbf{B} & \mathbf{A}\mathbf{B} \end{bmatrix} = \begin{bmatrix} \begin{bmatrix} 1 \\ a \end{bmatrix} & \begin{bmatrix} -2 & 1 \\ 0 & -1 \end{bmatrix} \begin{bmatrix} 1 \\ a \end{bmatrix} = \begin{bmatrix} 1 & a-2 \\ a & -a \end{bmatrix}$$

Since **Q** is a square matrix, we can check the determinant to evaluate the rank (not true for multiple inputs!)

$$|\mathbf{Q}| = (1)(-a) - (a)(a-2) = -a^2 + a = -a(a-1)$$

Result: rank(\mathbf{Q}) < 2 when $a = \{0,1\}$

Integral Conditions - II



A corollary of the controllability statement on L10/S12 is the following:

If an LTI system is completely controllable, then we should be able to find a control $\mathbf{u}(t)$ that transfers the state from any initial state $\mathbf{x}_0(t_0)$ to any terminal state $\mathbf{x}(t_1)$

Let's try to find such a control.

Integral Conditions - III



From our study of the state transition matrix we know the response at t_1 is

$$\mathbf{x}(t_1) = e^{\mathbf{A}(t_1 - t_0)} \mathbf{x}(t_0) + \int_{t_0}^{t_1} e^{\mathbf{A}(t_1 - \tau)} \mathbf{B}\mathbf{u}(\tau) d\tau$$

Now define a matrix called the Controllability Grammian

$$\mathbf{P}(t_1,t_0) = \int_{t_0}^{t_1} e_{[N\times N]}^{\mathbf{A}(t_1-\tau)} \mathbf{B}_{[N\times M][M\times N]} \mathbf{B}^T e_{[N\times N]}^{\mathbf{A}^T(t_1-\tau)} d\tau$$

Integral Conditions - IV



It is not obvious, but the input

$$\mathbf{u}(t) = \mathbf{B}^T e^{\mathbf{A}^T (t_1 - t)} \mathbf{P}^{-1} (t_1, t_0) \left[\mathbf{x}(t_1) - e^{\mathbf{A}(t_1 - t_0)} \mathbf{x}(t_0) \right]$$

will transfer the system from the initial state $\mathbf{x}(t_0)$ to the final state $\mathbf{x}(t_1)$.

How do we show this is the answer?

Integral Conditions - V



Substitute this result into the expression for the final state response

$$\mathbf{x}(t_1) = e^{\mathbf{A}(t_1 - t_0)} \mathbf{x}(t_0) + \int_{t_0}^{t_1} e^{\mathbf{A}(t_1 - \tau)} \mathbf{B} \mathbf{B}^T e^{\mathbf{A}^T(t_1 - \tau)} \mathbf{P}^{-1}(t_1, t_0) \left[\mathbf{x}(t_1) - e^{\mathbf{A}(t_1 - t_0)} \mathbf{x}(t_0) \right] d\tau$$

$$\mathbf{x}(t_1) = e^{\mathbf{A}(t_1 - t_0)} \mathbf{x}(t_0) + \underbrace{\int_{t_0}^{t_1} e^{\mathbf{A}(t_1 - \tau)} \mathbf{B} \mathbf{B}^T e^{\mathbf{A}^T (t_1 - \tau)} d\tau}_{\mathbf{P}(t_1, t_0)} \times \mathbf{P}^{-1}(t_1, t_0) \Big[\mathbf{x}(t_1) - e^{\mathbf{A}(t_1 - t_0)} \mathbf{x}(t_0) \Big]$$

$$\mathbf{x}(t_1) = e^{\mathbf{A}(t_1 - t_0)} \mathbf{x}(t_0) + \underbrace{\mathbf{P}(t_1, t_0) \mathbf{P}^{-1}(t_1, t_0)}_{\mathbf{I}} \left[\mathbf{x}(t_1) - e^{\mathbf{A}(t_1 - t_0)} \mathbf{x}(t_0) \right]$$

$$\mathbf{x}(t_1) = e^{\mathbf{A}(t_1 - t_0)} \mathbf{x}(t_0) + \mathbf{x}(t_1) - e^{\mathbf{A}(t_1 - t_0)} \mathbf{x}(t_0) = \mathbf{x}(t_1)$$

Integral Conditions - VI



The input that transforms the states from the initial state to the final state depends on the existence of the inverse of the controllability grammian

$$\mathbf{u}(t) = \mathbf{B}^T e^{\mathbf{A}^T (t_1 - t)} \mathbf{P}^{-1} (t_1, t_0) \mathbf{x}(t_1) - e^{\mathbf{A}(t_1 - t_0)} \mathbf{x}(t_0)$$

An equivalent requirement is that an LTI system is completely controllable if and only if the controllability grammian is nonsingular.

Integral Conditions - VII



Let's return to the example on L10/S14:

$$\mathbf{A} = \begin{bmatrix} 0 & 1 \\ 0 & -1 \end{bmatrix} \qquad \mathbf{B} = \begin{bmatrix} 1 \\ 0 \end{bmatrix}$$

For this system, the state transition matrix is:

$$e^{\mathbf{A}t} = \begin{bmatrix} 1 & 1 - e^{-t} \\ 0 & e^{-t} \end{bmatrix}$$

Integral Conditions - VIII



The controllability grammian is

$$\mathbf{P}(t_1, t_0) = \int_{t_0}^{t_1} \begin{bmatrix} 1 & 1 - e^{-(t_1 - \tau)} \\ 0 & e^{-(t_1 - \tau)} \end{bmatrix} \begin{bmatrix} 1 \\ 0 \end{bmatrix} \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 1 - e^{-(t_1 - \tau)} & e^{-(t_1 - \tau)} \end{bmatrix} d\tau$$

After simplification

$$\mathbf{P}(t_1, t_0) = \int_{t_0}^{t_1} \begin{bmatrix} 1 & 0 \\ 0 & 0 \end{bmatrix} d\tau = \begin{bmatrix} (t_1 - t_0) & 0 \\ 0 & 0 \end{bmatrix}$$

The controllability grammian is singular therefore this system is uncontrollable.

Integral Conditions - IX



Now recall the example on L10/S15 where only the **B** vector was changed.

$$\mathbf{A} = \begin{bmatrix} 0 & 1 \\ 0 & -1 \end{bmatrix} \qquad \mathbf{B} = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$$

$$\mathbf{B} = \begin{bmatrix} 0 \\ 1 \end{bmatrix}$$

The state transition matrix does not depend on B so it is still

$$e^{\mathbf{A}t} = \begin{bmatrix} 1 & 1 - e^{-t} \\ 0 & e^{-t} \end{bmatrix}$$

Integral Conditions - X



Now the controllability grammian is

$$\mathbf{P}(t_1, t_0) = \int_{t_0}^{t_1} \begin{bmatrix} 1 & 1 - e^{-(t_1 - \tau)} \\ 0 & e^{-(t_1 - \tau)} \end{bmatrix} \begin{bmatrix} 0 \\ 1 \end{bmatrix} \begin{bmatrix} 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 1 - e^{-(t_1 - \tau)} & e^{-(t_1 - \tau)} \end{bmatrix} d\tau$$

Setting $t_0 = 0$ (for convenience) we have

$$\mathbf{P}(t_1,0) = \int_0^{t_1} \begin{bmatrix} \left(1 - e^{-(t_1 - \tau)}\right)^2 & \left(1 - e^{-(t_1 - \tau)}\right) e^{-(t_1 - \tau)} \\ \left(1 - e^{-(t_1 - \tau)}\right) e^{-(t_1 - \tau)} & \left(e^{-(t_1 - \tau)}\right)^2 \end{bmatrix} d\tau$$

$$= \begin{bmatrix} -\frac{3}{2} + e^{-2t_1} \left(t_1 e^{2t_1} + 2e^{t_1} - \frac{1}{2}\right) & \frac{1}{2} + e^{-2t_1} \left(\frac{1}{2} - e^{t_1}\right) \\ \frac{1}{2} + e^{-2t_1} \left(\frac{1}{2} - e^{t_1}\right) & \frac{1}{2} - \frac{1}{2}e^{-2t_1} \end{bmatrix}$$

Integral Conditions - XI



The determinant of the controllability grammian is

$$|\mathbf{P}(t_1,0)| = -1 + 2e^{-t_1} + \frac{1}{2}t_1 - \frac{1}{2}t_1e^{-2t_1} - e^{-2t_1}$$

Is this determinant equal to zero for all final times $t_1 > 0$?

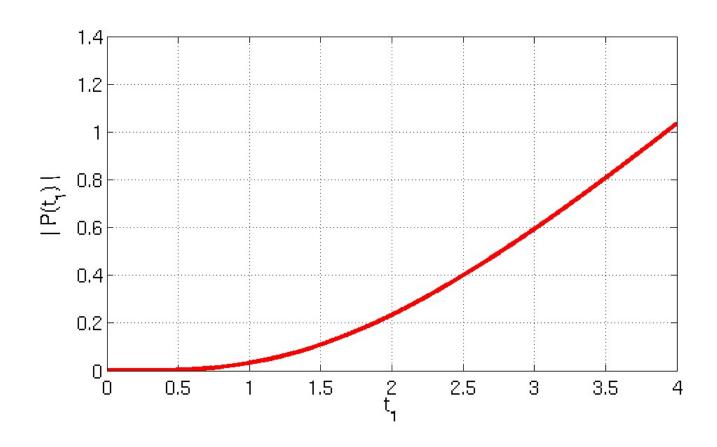
$$\left| \mathbf{P}(t_1, 0) \right| = -1 + \underbrace{\frac{1}{2}t_1}_{\to \infty} + \underbrace{2e^{-t_1} - \frac{1}{2}t_1e^{-2t_1} - e^{-2t_1}}_{\to 0}$$
as
$$t_1 \to \infty$$

$$t_1 \to \infty$$

Integral Conditions - XII



 $|\mathbf{P}(t_1,0)|$ is never zero for $t_1 > 0$, therefore the system is always controllable.



Summary - I



We have looked at several physical interpretations of controllability:

- No path through a block diagram
 Good visual aid, but can be difficult for large systems
- Unreachable locations in the state space

The state vector can pass through unreachable locations, but we cannot control our system to go there

Summary - II



We have also looked at several mathematical tests for controllability:

Controllability matrix must be full rank.

$$\mathbf{Q} = \begin{bmatrix} \mathbf{B} & \mathbf{A}\mathbf{B} & \mathbf{A}^2\mathbf{B} & \cdots & \mathbf{A}^{N-1}\mathbf{B} \end{bmatrix}$$

 Controllability grammian must be nonsingular.

$$\mathbf{P}(t_1,t_0) = \int_{t_0}^{t_1} e^{\mathbf{A}(t_1-\tau)} \mathbf{B} \mathbf{B}^T e^{\mathbf{A}^T(t_1-\tau)} d\tau$$

Note that both tests require **A** and **B**! Are these tests related?