

# **ME 5554 - AOE 5754 - ECE 5754**

## **Applied Linear Systems**

**Instructor: Dr. Steve Southward**

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# Syllabus Review

## Class Schedule

- 11:00-12:15 Tu & Th

## Office Hours & Consultation

- By appointment
- Skype
- Scholar Chat
- Email: [scsouth@vt.edu](mailto:scsouth@vt.edu)
- Telephone: **540-231-7385**

# Syllabus Review

## Electronic Information

- Lecture notes will be posted on Scholar prior to each class
- Grades, homework assignments, and solutions will be posted on Scholar
- Course announcements will be posted on Scholar and/or sent via email
- Do **NOT** send any hardcopy documents to my department mailbox or office
- Lectures will be recorded and the links posted on Scholar (can take up to 24 hours for posting!)
- Some lectures may be pre-recorded

# Assignment Policy

- Virginia Tech Graduate Honor Code will be strictly enforced
- All graded assignments **MUST** be submitted electronically through Scholar
- No graded assignments will be accepted past the due date/time
- All assignments are due by midnight of the stated due date
- Electronic submissions must be in PDF format
- No hardcopy submissions to my department mailbox or office will be accepted
- You are encouraged to work with others on all assignments except take-home exams, but your submission must be the result of your own efforts

# Grading

Homework:	10%
Quiz:	15%
Midterm Exam (10/4):	25%
Midterm Project (10/28):	25%
Final Project (12/9):	25%
Optional Final Exam (12/9):	25%

- Lowest grade of ME, MP, FP, FE will be dropped
- Must qualify for optional final: >50% on all other grades

# Grading Policy

- Homework solutions available on Scholar after due date
- Each student is responsible for assigning their own homework grade (subject to the VT Graduate Honor Code)
  - 2 points for attempting ALL problems and getting >80% correct
  - 1 point for attempting ALL problems and getting >40% correct
  - 0 points otherwise
- Each student is responsible for electronically submitting homework grade to instructor within 48 hours of the original due date
- Grading disputes for exams and/or projects must be electronically submitted with a written explanation.
- **NO extra credit assignments**

# Controls Curriculum Options @ VT

FALL	SPRING
<b>Linear Systems Theory</b>  cross-listed as  ECE 5744 AOE 5744 ME 5544  Fall 2009, listed as ECE 5704, taught by Dan Stilwell  <a href="#">Proposed official syllabus</a>	<b>Linear Control Theory</b>  cross-listed as  ECE 6744 AOE 6744 ME 6544  Tentatively scheduled to be taught each spring semester.  <a href="#">Proposed official syllabus</a>
<b>Applied Linear Systems</b>  cross-listed as  ECE 5754 AOE 5754 ME 5554  Fall 2009, listed as ME5505, taught by Steve Southward  <a href="#">Proposed official syllabus</a>	<b>Applied Linear Control</b>  cross-listed as  AOE 5764 ME 5564  Tentatively scheduled to be taught each spring semester.  <a href="#">Proposed official syllabus</a>
<b>Nonlinear Systems Theory</b>  cross-listed as  ECE 5774 AOE 5774 ME 5574  Fall 2009, listed as AOE 5344, taught by Craig Woolsey.  <a href="#">Proposed official syllabus</a>	<b>Adaptive Controls Systems</b>  cross-listed as  ECE 6774 AOE 6774 ME 6574  Tentatively scheduled to be taught each spring semester.  <a href="#">Proposed official syllabus</a>

# Course Goals

## In this course you will learn how to:

- Represent multi-input-multi-output (MIMO) dynamic systems using state-space models
- Solve for the dynamic response of a linear dynamic system and relate the response to the state-space system description
- Design linear control systems using frequency domain, state estimation, and pole placement techniques

**In-Class Participation is EXPECTED!!!**



# Course Prerequisites

## Classical feedback control background:

- Block diagram manipulation & analysis
- Laplace transforms
- Root locus analysis
- Frequency response & transfer functions
- Frequency domain feedback control design

## Mandatory Software:

- Matlab 8.0 R2012b (or later)
- Simulink, Control system toolbox
- Powerpoint, Word, Equation Editor
- PDF conversion software

# Reference Material

## Textbook:

- *Linear State-Space Control Systems*, Robert Williams & Douglas Lawrence, John Wiley & Sons, 2007

## Additional References:

- Franklin, G.F., Powell, J.D., and Emami-Naeini, A., *Feedback Control of Dynamic Systems*, Addison-Wesley, Reading, MA, 1991.
- Kuo, B.C., *Automatic Control Systems*, Prentice-Hall, Englewood Cliffs, NY, 1987.
- Dorf, R.C., Bishop, R.H., *Modern Control Systems*, Addison-Wesley, Reading, MA, 1995.
- Bolton, W., *Control Engineering*, Longman, Harlow, Essex, England, 1996.
- Levine, W., *The Control Handbook*, CRC Press, 1996.
- Friedland, B., *Control System Design – An Introduction to State-Space Methods*, McGraw-Hill, 1986.

# Course Outline - 1st Half

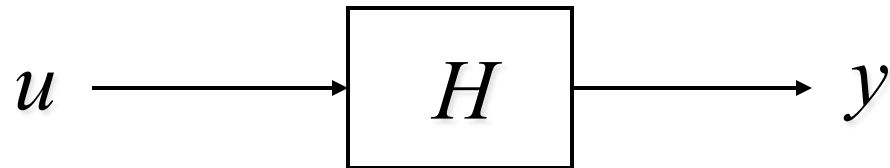
- Review Classical Feedback Control
- Review Vector/Matrix Theory
- State-Space Representations
- LTI Response & Matrix Exponential
- Transfer Functions & Eigenvalues
- Frequency-Domain Analysis
- Harmonic & Impulse Responses
- Pole Placement
- Controllability

## Course Outline - 2nd Half

- Full State Feedback for MIMO
- Stabilizability
- State Estimation & Output Feedback
- Observability & Duality
- Exogenous Inputs, Integral Control
- Optimal Control (LQR/LQG)
- Robustness & Sensitivity
- Kalman Filtering
- Introduction to Discrete Time

# Control System Basics

## Single-Input Single-Output (SISO) System



Input  $u$  is the command (control) signal

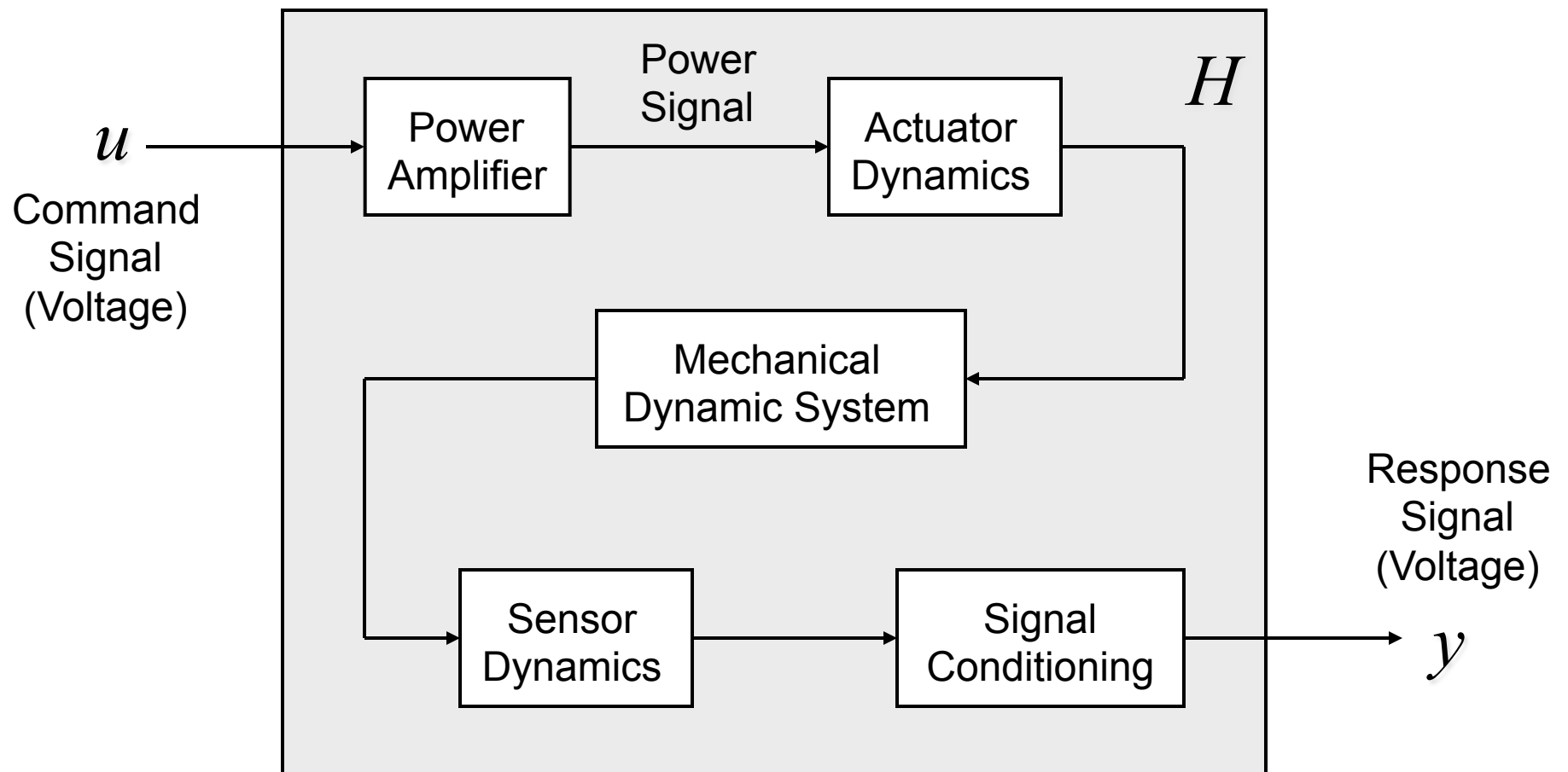
Output  $y$  is the response (measurement) signal

Process (a.k.a. “Plant”)  $H$  is a dynamic system that transforms the input into the output

Control objective: Find  $u$  to generate a desired  $y$

# Control System Basics

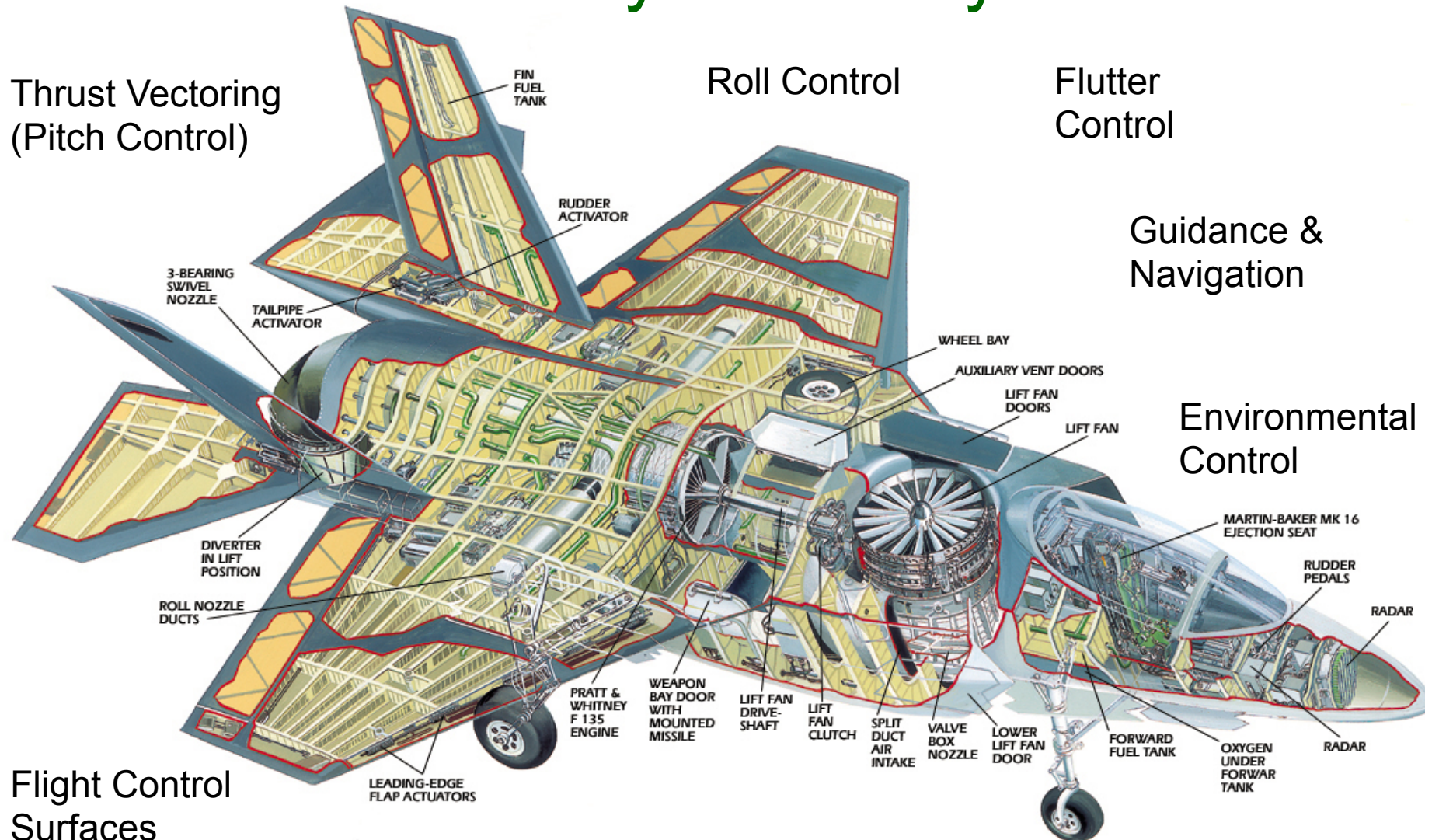
Typical electro-mechanical plants are made up of connected dynamic subsystems:





# Example Control Systems

Aircraft utilize many control systems:



[http://media.popularmechanics.com/images/lg\\_cutaway-lg.jpg](http://media.popularmechanics.com/images/lg_cutaway-lg.jpg)

The left diagram is a schematic cross-section of a CD-ROM drive. It shows the optical path starting from a **Laser** at the top, passing through **Lens 1 (collimating lens)**, then through a **Beam splitter 1** and **Beam splitter 2**. The beam then passes through a **Circularizer** and an **Astigmatic lens** before reaching the **Disk**. The reflected beam travels back through the **Astigmatic lens**, **Beam splitter 2**, and **Beam splitter 1** to a **Detector (power servo)**. A **Servo detector** is also shown at the bottom. **Data detectors** are located at the very bottom of the assembly.

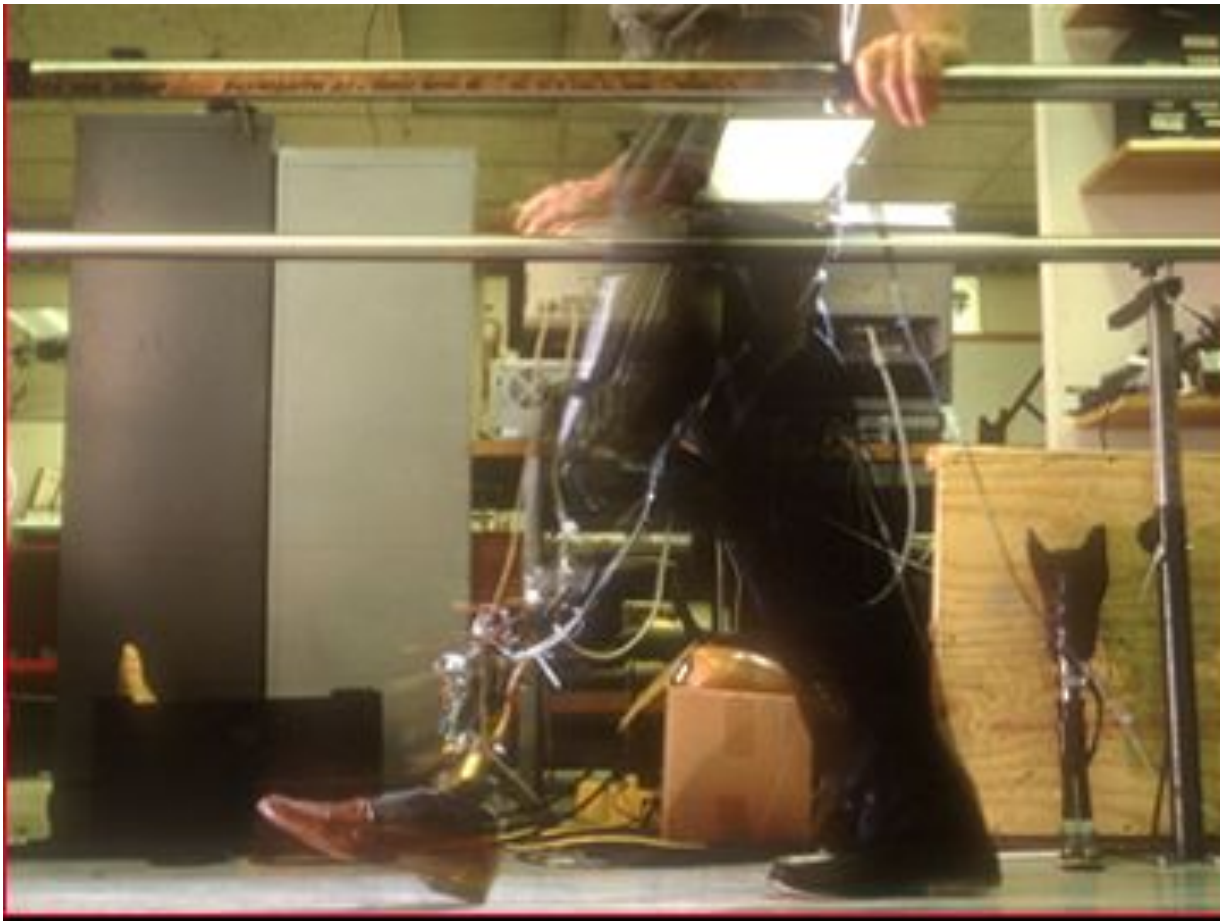
The right diagram is a 3D exploded view of the drive's mechanical components. It shows the **Spindle motor** at the bottom left, which rotates the disk. Above it is the **Coarse actuator**, which moves the lens assembly. The **Objective lens** is mounted on the coarse actuator. The **Fine focus and tracking actuator** is shown moving the objective lens vertically. The **Disk** is shown at the top, positioned between the objective lens and the spindle motor.

L1/S16



## Example Control Systems

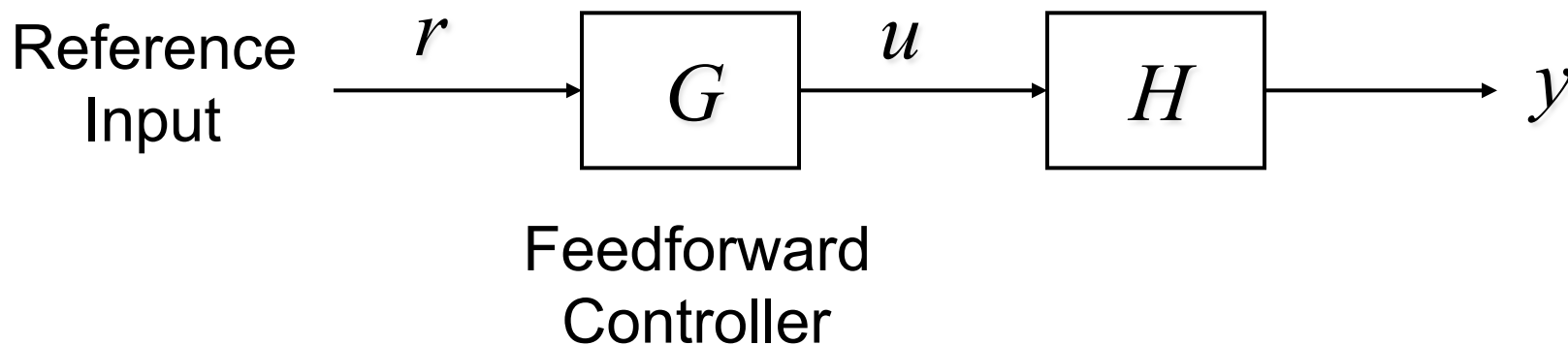
Control is also used in advanced biomedical devices:



Control must be used to position the artificial knee properly and change the ‘feel’ of the knee to match that of an actual knee.

# Feedforward Control System

**Feedforward** control is a form of **Open-Loop** control (i.e. no explicit feedback loops)



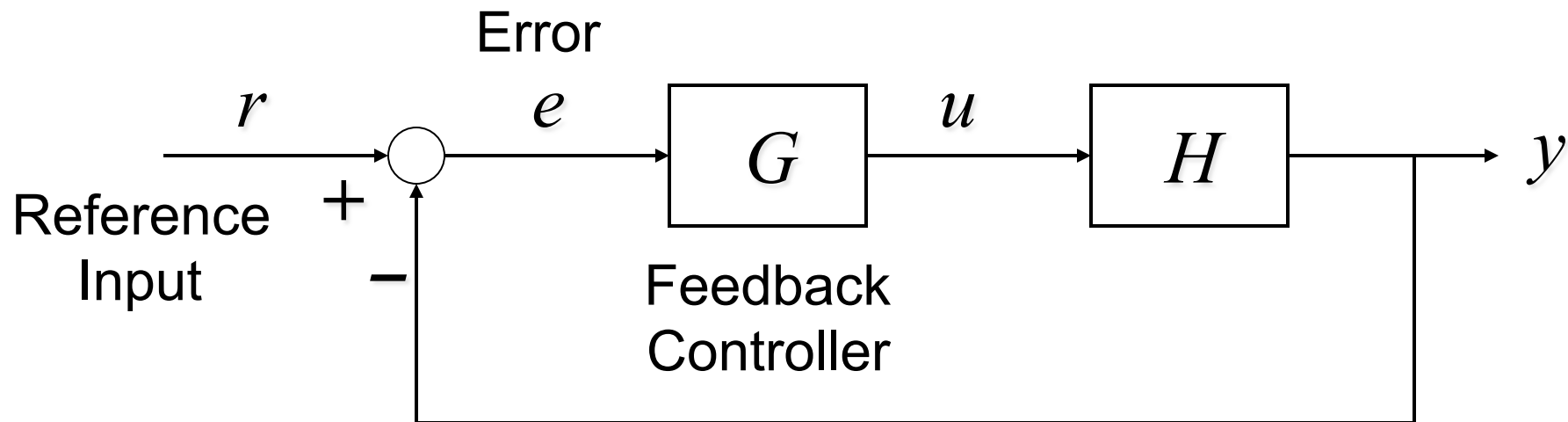
**Feedforward control...**

is typically used for **command shaping** and/or **disturbance rejection**,

does not alter the dynamics of the process

# Feedback Control System

**Feedback** control is **Closed-Loop** control,  
where the control signal  $u$  is a function of the  
process output  $y$



**Feedback control...**

is typically used for **regulation** or **tracking**,  
changes the process dynamics

# Question for Open Discussion

What are some relative strengths and weaknesses of feedback and feedforward control?

# Course Focus

This course will focus on the analysis and design of continuous-time (analog) feedback control systems using state-space methods

- How do we model the process?
- How do we design a feedback controller?
- How do we analyze the performance?

# Review of Continuous Control

Your previous study of control system design probably centered around ***classical control*** techniques for SISO systems.

Classical synthesis & analysis techniques are still valuable and widely used today

For the remainder of this session we will briefly review two main topics in classical control system design:

- Process modeling
- Compensator design techniques

# Process Modeling - I

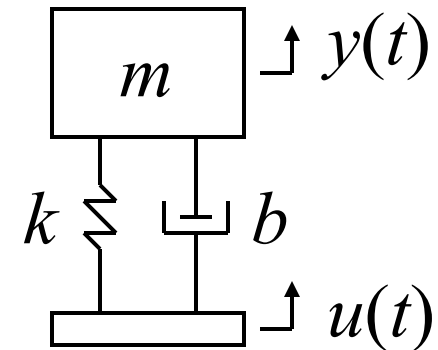
Example: base-excited mechanical oscillator

Free-body diagram force balance:

$$m\ddot{y} = \underbrace{b(\dot{u} - \dot{y})}_{\text{damper force}} + \underbrace{k(u - y)}_{\text{spring force}}$$

Collect terms:

$$m\ddot{y} + b\dot{y} + ky = b\dot{u} + ku$$



In the Laplace domain:

$$(ms^2 + bs + k)Y(s) = (bs + k)U(s)$$

The resulting process Transfer Function is:

$$H(s) = \frac{Y(s)}{U(s)} = \left( \frac{bs + k}{ms^2 + bs + k} \right)$$

## Process Modeling - II

Most continuous-time linear systems are represented in the Laplace domain as a ratio of polynomials:

$$H(s) = \left( \frac{b_m s^m + b_{m-1} s^{m-1} + \cdots + b_1 s + b_0}{a_n s^n + a_{n-1} s^{n-1} + \cdots + a_1 s + a_0} \right) \quad n \geq m$$

The variable  $s$  ( $= \sigma + j\omega$ ) is the Laplace variable from the Laplace Transform:

$$H(s) = \int_0^{\infty} e^{-st} h(t) dt$$

$h(t)$  is the process impulse response



## Process Modeling - III

Any linear, causal input-output (I/O) relationship can be modeled using Laplace transforms

The controller (or compensator) is usually also represented by a transfer function  $G(s)$  which is a ratio of polynomials

$$G(s) = \frac{U(s)}{E(s)}$$

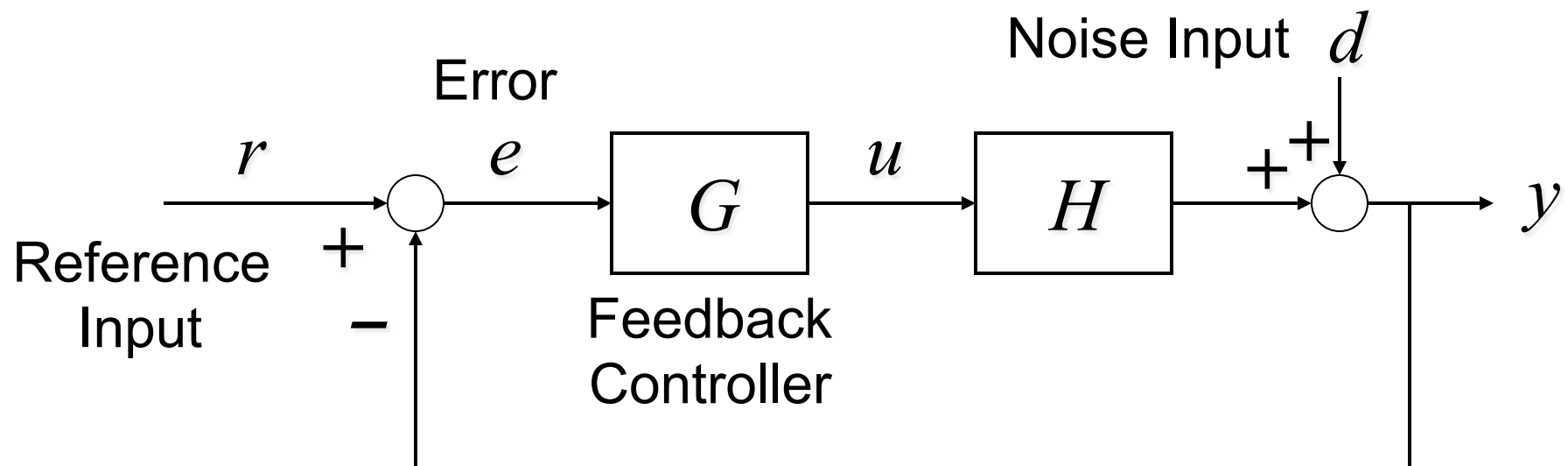
# Classical Control Design - I

Typical design problem:

Design a controller  $G(s)$  such that:

output  $y(t)$  tracks the reference input  $r(t)$

output  $y(t)$  is insensitive to measurement noise  $d(t)$



# Classical Control Design - II

The output is given by:

$$Y(s) = H(s)U(s) + D(s) = H(s)[G(s)E(s)] + D(s)$$

And the error (for negative feedback) is:

$$E(s) = R(s) - Y(s)$$

Combining yields the following:

$$Y(s) = G(s)H(s)[R(s) - Y(s)] + D(s)$$

$$[1 + G(s)H(s)]Y(s) = [G(s)H(s)]R(s) + D(s)$$

## Classical Control Design - III

The Closed-Loop I/O relationships are obtained by solving for  $Y(s)$  in terms of the inputs  $R(s)$  and  $D(s)$

$$Y(s) = \underbrace{\left( \frac{G(s)H(s)}{1 + G(s)H(s)} \right)}_{\text{Complementary Sensitivity } T(s)} R(s) + \underbrace{\left( \frac{1}{1 + G(s)H(s)} \right)}_{\text{Sensitivity Function } S(s)} D(s)$$

# Classical Control Design - IV

For Tracking, we want  $Y(s)$  approximately equal to  $R(s)$ :

$$Y(s) \approx R(s) \quad \text{IF} \quad T(s) \approx 1 \quad \Rightarrow \quad G(s)H(s) \gg 1$$

For Disturbance Rejection, we want:

$$S(s) \approx 0 \quad \Rightarrow \quad G(s)H(s) \gg 1$$

Both goals appear to be satisfied with the same criterion.

# Classical Control Design - V

## Good news:

All we need to do is “turn up” the compensator gain to achieve both objectives.

## Bad news:

Turning up the gain too much can cause instability. An unstable system is going to have worse performance than the uncontrolled process.

# Classical Control Design - VI

## Fundamental Design Tradeoff:

Designing a high-gain compensator  $GH \gg 1$  improves tracking performance and reduces the sensitivity to disturbances (good news) ....but....decreases the stability margin and increases the chance of closed-loop instability (bad news).

# Classical Design Methods - I

## Root Locus

The Characteristic Equation (CE) is given by:

$$1 + G(s)H(s) = 0$$

Objective: Insure that the roots of the CE remain in the left-half plane (LHP) as a selected control parameter is varied

For example, plot the roots as a function of the compensator gain  $k$ :

$$G(s) = k \left( \frac{B(s)}{A(s)} \right) \Rightarrow A(s) + kB(s)H(s) = 0$$



# Classical Design Methods - II

## Loop Shaping in the Frequency-Domain

The Open Loop transfer function is:  $G(s)H(s)$

Objective: Manipulate the magnitude and phase of the loop to achieve the performance objectives while maintaining stability

Designs are analyzed in the frequency domain for Gain Margin and Phase Margin:

Bode Diagram: Mag. & Phase vs. frequency

Nyquist Diagram: Real vs. Imaginary

Nichols Chart: Magnitude vs. Phase

# Classical Design Methods - III

There are two common choices for classical compensator designs that you should be familiar with:

## PID Compensation

$$G_{PID}(s) = \underbrace{k_P}_{\text{Proportional Control}} + \underbrace{k_I \left( \frac{1}{s} \right)}_{\text{Integral Control}} + \underbrace{k_D s}_{\text{Derivative Control}}$$

## Lag/Lead Compensation

$$G(s) = k \left( \frac{s+b}{s+a} \right) \quad \begin{cases} a < b & \text{Lag Compensation} \\ b < a & \text{Lead Compensation} \end{cases}$$

# Important Review Topics

Please review the following Classical Control topics:

- Block diagram manipulation
- Laplace transforms ( $t \rightarrow s$  and  $s \rightarrow t$ )
- Frequency-domain design (Bode)
- Lead/Lag & PID compensation
- Root locus