

## 6.6 Vibration of membranes and plates

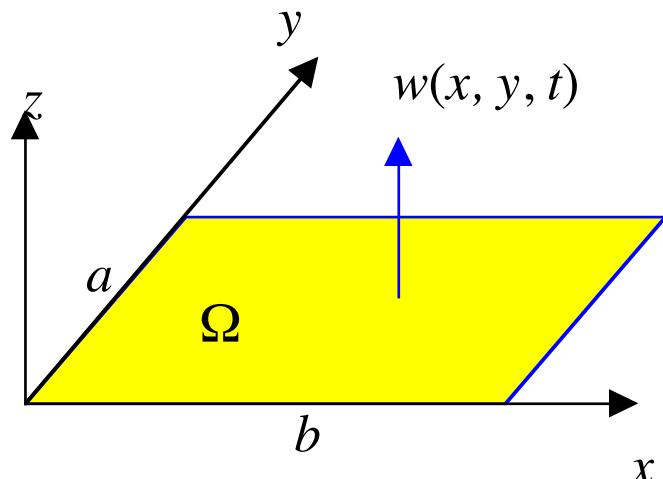


Figure 6.13

- The domain ( $\Omega$ ) is now a plane rather than a line: Two dimensional
- Membrane is a two dimensional string
- Plate is a two dimensional beam

# The membrane equation:

$$\tau \nabla^2 w(x, y, t) = \rho w_{tt}(x, y, t), \quad x, y \in \Omega$$

Tension per unit length

density(mass/area)

$$\nabla^2 = \frac{\partial^2}{\partial x^2} + \frac{\partial^2}{\partial y^2}$$

The *Laplace operator*

$$\frac{\partial^2 w(x, y, t)}{\partial x^2} + \frac{\partial^2 w(x, y, t)}{\partial y^2} = \frac{1}{c^2} \frac{\partial^2 w(x, y, t)}{\partial t^2}$$

$$c = \sqrt{\frac{\tau}{\rho}}$$

# Boundary and initial conditions

$w(x, y, t) = 0$  for some part of the boundary  $\partial\Omega$

$\frac{\partial w(x, y, t)}{\partial n} = 0$  for some other part of the boundary  $\partial\Omega$

where this derivative denotes the derivative  
normal to the plane of the membrane

plus the usual initial conditions

Example 6.6.1 Compute the natural frequencies of a square membrane of 1 m side.

$$c^2 \left[ \frac{\partial^2 w}{\partial^2 x} + \frac{\partial^2 w}{\partial^2 y} \right] = \frac{\partial^2 w}{\partial^2 t}, \quad x, y \in \Omega$$

$$w(x, y, t) = X(x)Y(y)T(t) \Rightarrow$$

$$X''YT + XY''T = \frac{1}{c^2} XY\ddot{T} \Rightarrow \underbrace{\frac{X''Y + XY''}{XY}}_{\text{Temporal equation}} = \frac{1}{c^2} \frac{\ddot{T}(t)}{T(t)} = -\omega^2$$

$$\frac{X''Y + XY''}{XY} = \frac{X''}{X} + \frac{Y''}{Y} = -\omega^2 \Rightarrow \frac{X''}{X} = -\frac{Y''}{Y} - \omega^2 = -\alpha^2$$

$$\Rightarrow \begin{cases} \frac{X''}{X} = -\alpha^2 \\ \frac{Y''}{Y} = -\gamma^2 \end{cases}$$

Two spatial equations

$$\text{where } \omega^2 = \alpha^2 + \gamma^2$$

$$X''(x) + \alpha^2 X(x) = 0 \Rightarrow A \sin \alpha x + B \cos \alpha x$$

$$Y''(y) + \gamma^2 Y(y) = 0 \Rightarrow C \sin \gamma y + D \cos \gamma y$$

$$X(x)Y(y) = A_1 \sin \alpha x \sin \gamma y + A_2 \sin \alpha x \cos \gamma y$$

$$+ A_3 \cos \alpha x \sin \gamma y + A_4 \cos \alpha x \cos \gamma y$$

Now apply the boundary conditions:

along  $x = 0$  :

$$T(t)X(0)Y(y) = T(t)(A_3 \sin \gamma y + A_4 \cos \gamma y) = 0 \Rightarrow$$

$$A_3 \sin \gamma y + A_4 \cos \gamma y = 0 \text{ which must hold for any } y$$

$$\Rightarrow \underline{\underline{A_3 = A_4 = 0}}$$

Now we have :

$$X(x)Y(y) = A_1 \sin \alpha x \sin \gamma y + A_2 \sin \alpha x \cos \gamma y$$

Along  $x = 1$ ,  $w(1, y, t) = 0$  :

$$A_1 \sin \alpha \sin \gamma y + A_2 \sin \alpha \cos \gamma y = 0 \Rightarrow$$

$$\sin \alpha (A_1 \sin \gamma y + A_2 \cos \gamma y) = 0 \Rightarrow$$

either  $\sin \alpha = 0$     or  $A_1 = A_2 = 0$

$$\Rightarrow \sin \alpha = 0 \Rightarrow \underline{\alpha_n = n\pi, n = 1, 2, 3, 4\dots}$$

At this point:

$$X(x)Y(y) = A_1 \sin \alpha x \sin \gamma y + A_2 \sin \alpha x \cos \gamma y$$

At  $y=0$ ,  $w(x,0,t) = 0 \Rightarrow$

$$A_1 \sin \alpha x \sin 0 + A_2 \sin \alpha x \cos 0 = 0 \Rightarrow A_2 = 0$$

So  $X(x)Y(y) = A_1 \sin \alpha x \sin \gamma y$

At  $y=1$ ,  $w(x,1,t) = 0 \Rightarrow$

$$A_1 \sin \alpha x \sin \gamma 1 = 0 \Rightarrow \sin \gamma = 0$$

which gives  $\gamma_m = m\pi$ ,  $m = 1, 2, 3, 4\dots$

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# Frequencies and Mode Shapes

$$\sigma_n = n\pi, \gamma_m = m\pi \Rightarrow \omega_{nm} = \sqrt{\gamma_m^2 + \sigma_n^2} \Rightarrow$$

frequencies are

$$\omega_{nm} = \pi \sqrt{n^2 + m^2}$$

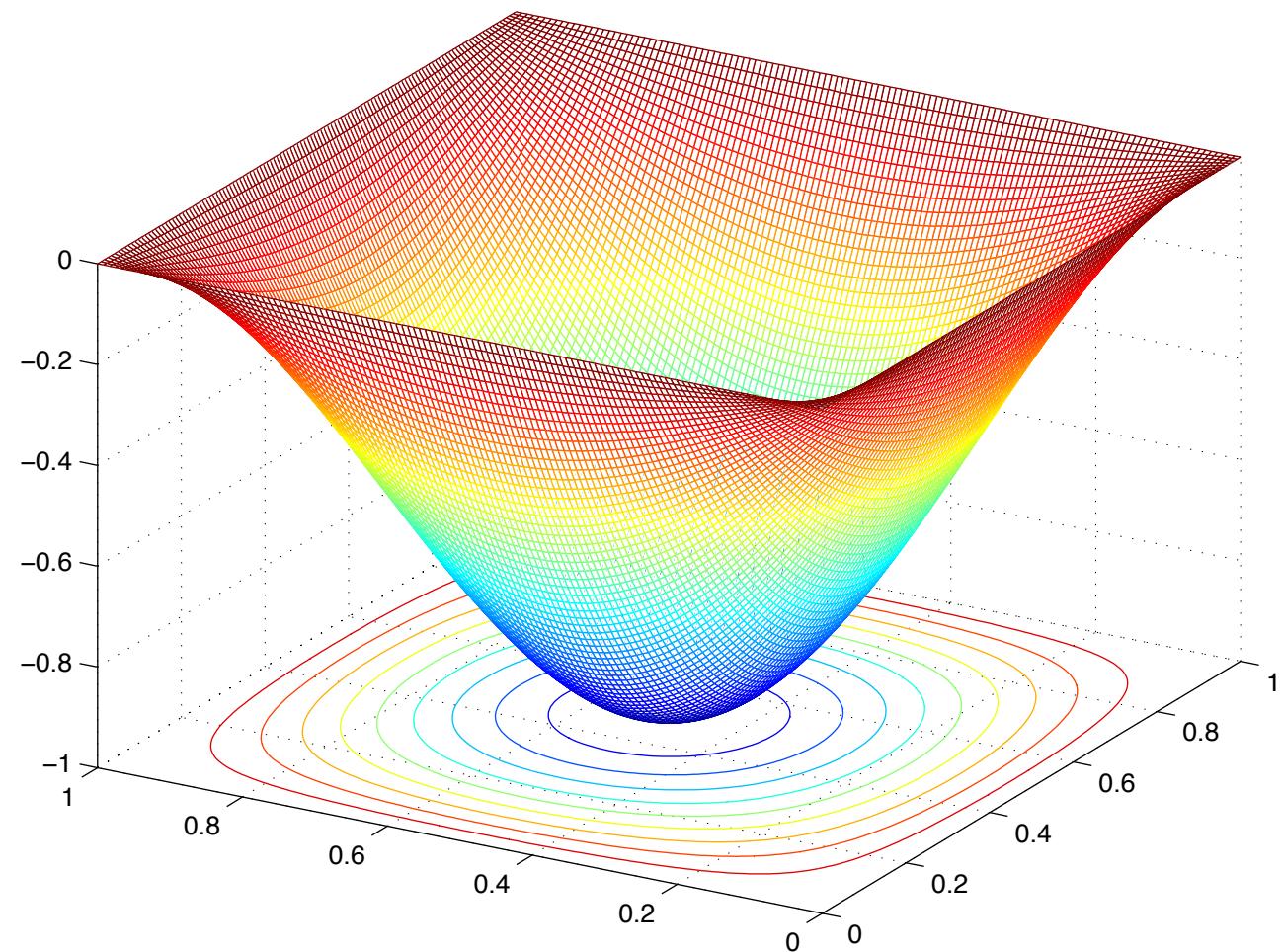
mode shapes

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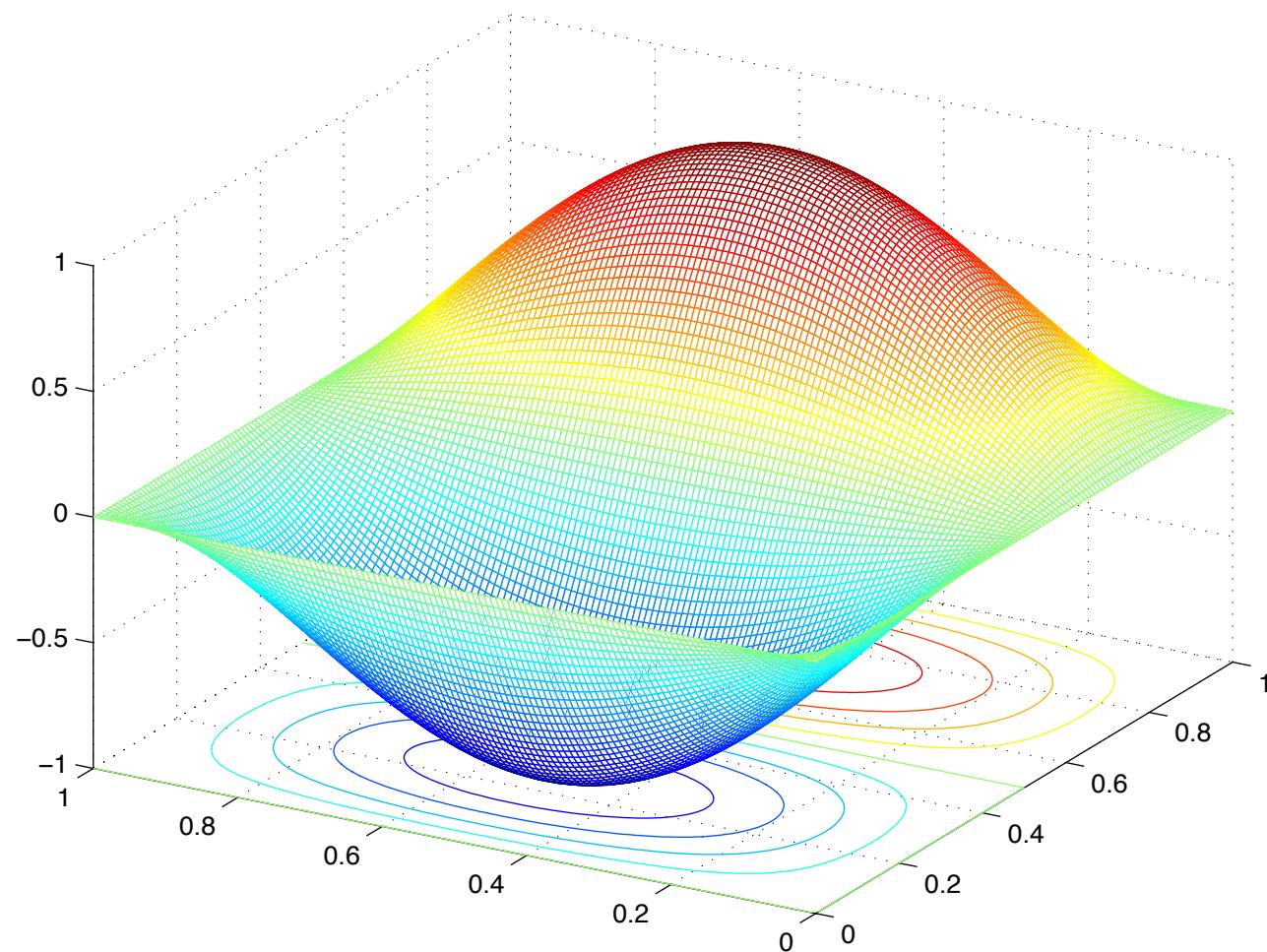
$$\left\{ \sin n\pi x \sin m\pi y \right\}_{n,m=1}^{\infty}$$

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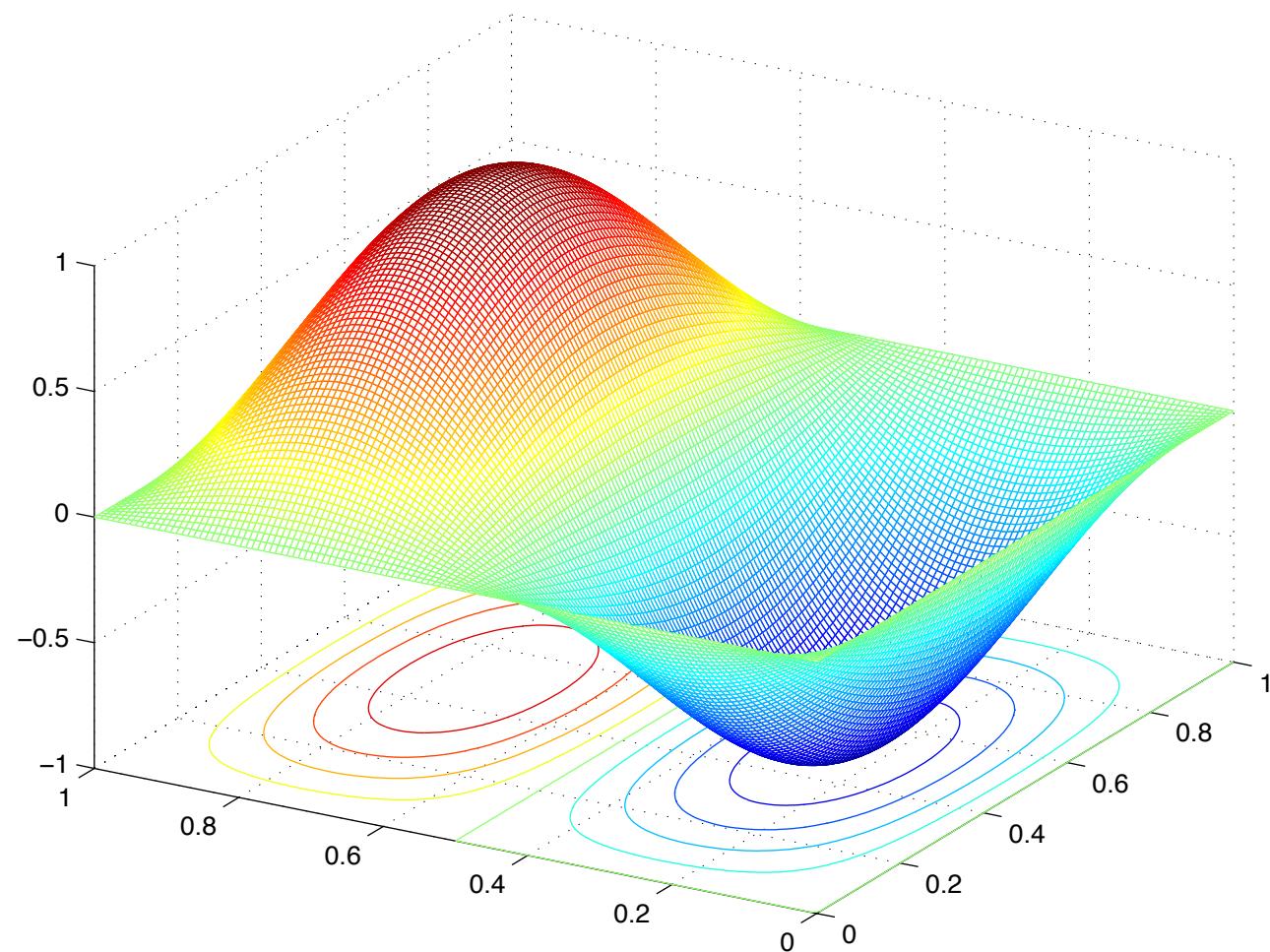
- Mode 11



- Mode 12

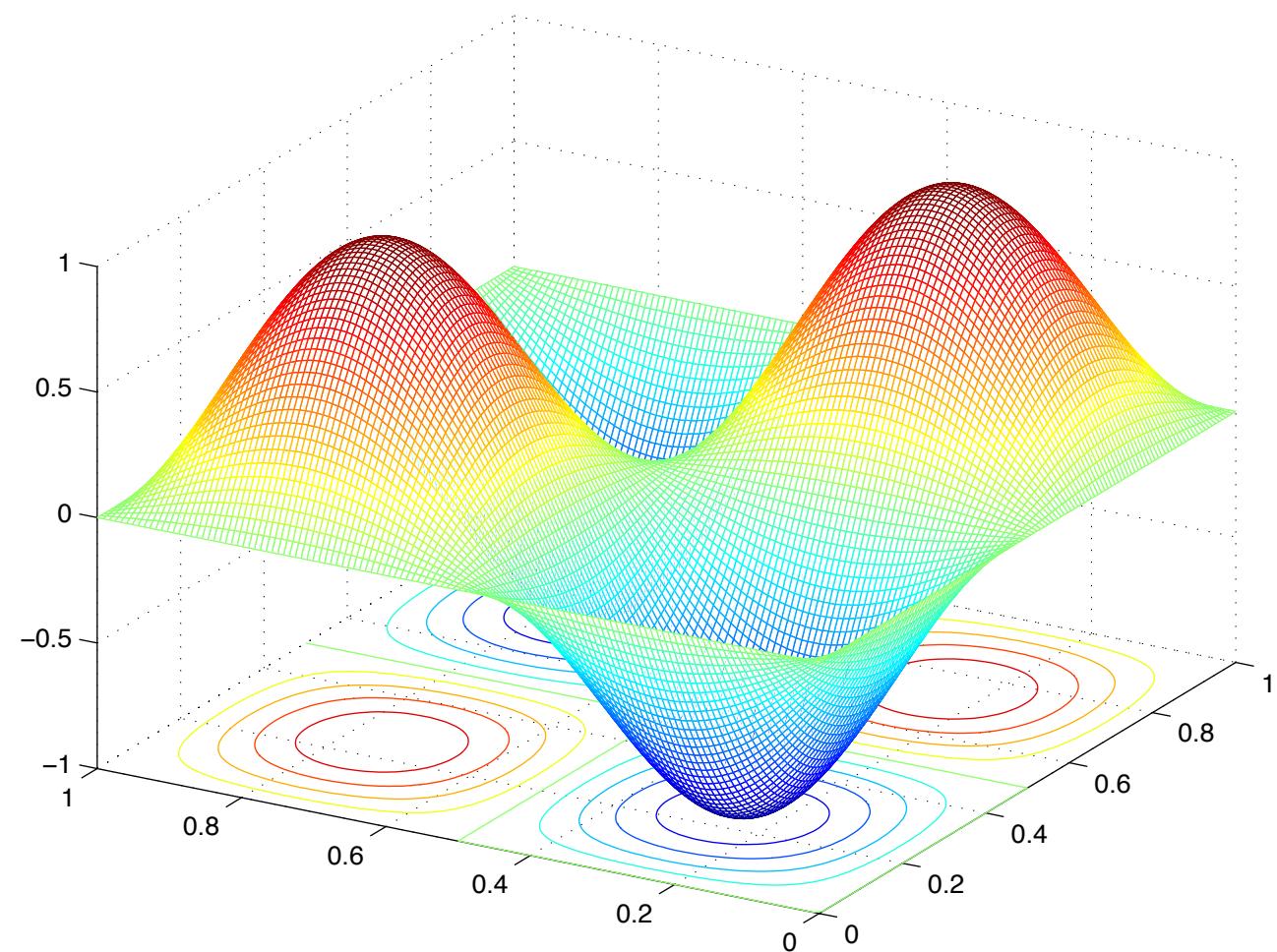


- Mode 21



$$\omega_{12} = \omega_{21}$$

- Mode 22



## Plate vibration:

$$D_E \nabla^4 w(x, y, t) = \rho w_{tt}(x, y, t), \quad x, y \in \Omega$$

$$D_E = \frac{Eh^3}{12(1 - \nu^2)}$$

$$\nabla^4 = \frac{\partial^4}{\partial x^4} + 2 \frac{\partial^4}{\partial x^2 \partial y^2} + \frac{\partial^4}{\partial y^4}$$

- Think of it as adding bending stiffness to the membrane
- Assume small deflections with respect to the thickness  $h$
- Plane through middle is called neutral plane and does not deform in bending
- No thickness stretch

# Boundary Conditions:

- This is a 2D analog of the EB beam theory and is called *thin plate* theory
- Must be enough boundary conditions for the 4th order derivatives:

$$w(x, y, t) = 0 \quad \text{and} \quad \frac{\partial w(x, y, t)}{\partial n} = 0 \quad \text{for } x, y \in \partial\Omega$$

For a simply supported (pinned) rectangular plate

$$w(x, y, t) = 0, \quad \text{along } x = 0, y = 0, x = \ell_1, y = \ell_2$$

$$\frac{\partial^2 w(x, y, t)}{\partial x^2} = 0, \quad \text{along } x = 0, x = \ell_1$$

$$\frac{\partial^2 w(x, y, t)}{\partial y^2} = 0, \quad \text{along } y = 0, y = \ell_2$$