

LC Flow Velocity Eqs

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1 Elastic generalized force

From Svensek and Zumer, the free energy density is given by

$$f = \phi(Q) + \frac{1}{2}L\partial_i Q_{jk}\partial_i Q_{jk} \quad (1)$$

so that the homogeneous elastic part of the generalized force is given by:

$$h_{ij}^{he} = L\partial_k^2 Q_{ij} - \frac{\partial\phi}{\partial Q_{ij}} + \lambda\delta_{ij} + \lambda_k\epsilon_{kij} \quad (2)$$

where ϕ is the Landau de Gennes bulk free energy:

$$\phi(Q) = \frac{1}{2}AQ_{ij}Q_{ji} + \frac{1}{3}BQ_{ij}Q_{jk}Q_{ki} + \frac{1}{4}C(Q_{ij}Q_{ji})^2 \quad (3)$$

We begin by explicitly calculating the second term in terms of Q_{ij} , one term at a time in ϕ :

$$\begin{aligned} \frac{\partial}{\partial Q_{mn}} \left(\frac{1}{2}AQ_{ij}Q_{ji} \right) &= \frac{1}{2}A(\delta_{im}\delta_{jn}Q_{ji} + Q_{ij}\delta_{jm}\delta_{in}) \\ &= \frac{1}{2}A(Q_{nm} + Q_{nm}) \\ &= AQ_{mn} \end{aligned} \quad (4)$$

where in the last step we've used symmetry of Q_{ij} .

$$\begin{aligned} \frac{\partial}{\partial Q_{mn}} \left(\frac{1}{3}BQ_{ij}Q_{jk}Q_{ki} \right) &= \frac{1}{3}B(\delta_{im}\delta_{jn}Q_{jk}Q_{ki} + Q_{ij}\delta_{jm}\delta_{kn}Q_{ki} + Q_{ij}Q_{jk}\delta_{mk}\delta_{ni}) \\ &= \frac{1}{3}B(Q_{nk}Q_{km} + Q_{im}Q_{ni} + Q_{nj}Q_{jm}) \\ &= BQ_{ni}Q_{im} \end{aligned} \quad (5)$$

And the final term gives:

$$\begin{aligned} \frac{\partial}{\partial Q_{mn}} \left(\frac{1}{4}C(Q_{ij}Q_{ji})^2 \right) &= \frac{1}{4}C \cdot 2(Q_{ij}Q_{ji}) \frac{\partial(Q_{kl}Q_{lk})}{\partial Q_{mn}} \\ &= \frac{1}{4}C \cdot 2(Q_{ij}Q_{ji}) \cdot (\delta_{mk}\delta_{nl}Q_{lk} + Q_{kl}\delta_{lm}\delta_{kn}) \\ &= \frac{1}{4}C \cdot 2(Q_{ij}Q_{ji}) \cdot (Q_{nm} + Q_{nm}) \\ &= CQ_{mn}(Q_{ij}Q_{ji}) \end{aligned} \quad (6)$$

Thus, the total homogeneous and elastic force reads:

$$h_{ij}^{he} = L\partial^2 Q_{ij} - AQ_{ij} - BQ_{ik}Q_{kj} - CQ_{ij}(Q_{kl}Q_{lk}) + \lambda\delta_{ij} + \lambda_k\epsilon_{kij} \quad (7)$$

2 Viscous generalized force

Now we need the viscous force on the liquid crystals. From Svnsek and Zumer, the viscous force is given by:

$$-h_{ij}^v = \frac{1}{2}\mu_2 A_{ij} + \mu_1 N_{ij} \quad (8)$$

with

$$N_{ij} = \frac{dQ_{ij}}{dt} + W_{ik}Q_{kj} - Q_{ik}W_{kj} \quad (9)$$

and

$$\frac{dQ_{ij}}{dt} = \frac{\partial Q_{ij}}{\partial t} + (v \cdot \nabla)Q_{ij} \quad (10)$$

where

$$W_{ij} = \frac{1}{2}(\partial_i v_j - \partial_j v_i) \quad (11)$$

The second two terms in the expression for N_{ij} are quadratic in v_i and Q_{ij} so we may drop them, and $(v \cdot \nabla)Q_{ij}$ is clearly quadratic. Hence, we make the approximation

$$N_{ij} \approx \frac{\partial Q_{ij}}{\partial t} \quad (12)$$

We also have the definition

$$A_{ij} = (\partial_i v_j + \partial_j v_i) \quad (13)$$

Plugging this into the viscous force yields:

$$-h_{ij}^v = \frac{1}{2}\mu_2(\partial_i v_j + \partial_j v_i) + \mu_1 \frac{\partial Q_{ij}}{\partial t} \quad (14)$$

Balancing the forces gives the equation:

$$h_{ij}^e = -h_{ij}^v \quad (15)$$

Which yields:

$$\mu_1 \frac{\partial Q_{ij}}{\partial t} = L\partial^2 Q_{ij} - A_{ij}Q_{ij} - BQ_{ik}Q_{kj} - CQ_{ij}(Q_{kl}Q_{lk}) - \frac{1}{2}\mu_2(\partial_i v_j + \partial_j v_i) \quad (16)$$

(here we have dropped the Lagrange multipliers because we are going to explicitly ensure that Q_{ij} is traceless and symmetric).

3 Elastic stress tensor

The elastic stress tensor is obtained via

$$\sigma_{ij}^e = -\frac{\partial f}{\partial(\partial_i Q_{kl})}\partial_j Q_{kl} \quad (17)$$

Note that only the elastic part of the free energy make references to derivatives:

$$\begin{aligned} \frac{\partial f}{\partial(\partial_i Q_{kl})} &= \frac{\partial}{\partial(\partial_i Q_{kl})} \frac{1}{2}L\partial_j Q_{mn}\partial_j Q_{mn} \\ &= \frac{1}{2}L(\delta_{ij}\delta_{km}\delta_{ln}\partial_j Q_{mn} + \partial_j Q_{mn}\delta_{ij}\delta_{km}\delta_{ln}) \\ &= \frac{1}{2}L(\partial_i Q_{kl} + \partial_i Q_{kl}) \\ &= L\partial_i Q_{kl} \end{aligned} \quad (18)$$

Then the elastic stress tensor is given by

$$\sigma_{ij}^e = -L\partial_i Q_{kl}\partial_j Q_{kl} \quad (19)$$

4 Viscous stress tensor

The viscous stress tensor is given by

$$\sigma_{ij}^v = \beta_1 Q_{ij} Q_{kl} A_{kl} + \beta_4 A_{ij} + \beta_5 Q_{ik} A_{ki} + \frac{1}{2} \mu_2 N_{ij} - \mu_1 Q_{ik} N_{kj} + \mu_1 Q_{jk} N_{ki} \quad (20)$$

However, only the β_4 and μ_2 are linear in Q_{ij} and v_i . Hence, this simplifies to

$$\sigma_{ij}^v \approx \beta_4 A_{ij} + \frac{1}{2} \mu_2 N_{ij} \quad (21)$$

Again, plugging in for A_{ij} and N_{ij} as we did for the viscous force, we get

$$\sigma_{ij}^v \approx \beta_4 (\partial_i v_j + \partial_j v_i) + \frac{1}{2} \mu_2 \frac{\partial Q_{ij}}{\partial t} \quad (22)$$

Plugging in for the time evolution of Q_{ij} gives:

$$\sigma_{ij}^v \approx \beta_4 (\partial_i v_j + \partial_j v_i) + \frac{1}{2} \frac{\mu_2}{\mu_1} \left[L \partial^2 Q_{ij} - A Q_{ij} - B Q_{ik} Q_{kj} - C Q_{ij} (Q_{kl} Q_{lk}) - \frac{1}{2} \mu_2 (\partial_i v_j + \partial_j v_i) \right] \quad (23)$$

5 Fluid equation of motion

The equation of motion for the fluid is given by

$$\rho \frac{\partial v_i}{\partial t} = -\partial_i p + \partial_j (\sigma_{ji}^v + \sigma_{ji}^e) \quad (24)$$

We can make the assumption that $\partial v_i / \partial t \approx 0$. Using this and plugging in for σ_{ji}^v and σ_{ji}^e , we get:

$$\begin{aligned} \partial_i p = & \left(\beta_4 - \frac{1}{4} \frac{\mu_2^2}{\mu_1} \right) (\partial_i \partial_j v_j + \partial^2 v_i) \\ & + \frac{1}{2} \frac{\mu_2}{\mu_1} [L \partial^2 \partial_j Q_{ij} - A \partial_j Q_{ij} - B \partial_j (Q_{ik} Q_{kj}) - C \partial_j (Q_{ij} (Q_{kl} Q_{lk}))] \\ & - L \partial_j (\partial_i Q_{kl} \partial_j Q_{kl}) \end{aligned} \quad (25)$$

Note that, by incompressibility, $\partial_i v_i = 0$ so a term in parentheses goes away. Now define:

$$f_{\mu_2, i}(Q) = L \partial^2 \partial_j Q_{ij} - A \partial_j Q_{ij} - B \partial_j (Q_{ik} Q_{kj}) - C \partial_j (Q_{ij} (Q_{kl} Q_{lk})) \quad (26)$$

$$f_{L, i}(Q) = \partial_j (\partial_i Q_{kl} \partial_j Q_{kl}) \quad (27)$$

$$f_i(Q) = -\frac{1}{2} \frac{\mu_2}{\mu_1} f_{\mu_2, i}(Q) + L f_{L, i}(Q) \quad (28)$$

$$\alpha = \left(\beta_4 - \frac{1}{4} \frac{\mu_2^2}{\mu_1} \right)^{-1} \quad (29)$$

Then the fluid equation of motion becomes:

$$\partial^2 v_i = \alpha (\partial_i p + f_i) \quad (30)$$

6 Choosing a specific Q_{ij}

Now, we would like to choose f_i to be something which is just a sum of sines. These terminate at the endpoints, so it happens that we will fulfill our no slip condition ($v_i = 0$ at the boundary). Since we need to actually choose Q_{ij} to do that (so that we can use the same scenario for the stream function formulation), we will have to just guess and check. Note that many of the terms involved in f_i have third derivatives, so we will want to choose a cos to be the important term. Recall that, in the uniaxial case:

$$Q_{ij} = \frac{S}{2} (3n_i n_j - \delta_{ij}) \quad (31)$$

Choose S to be constant. Plugging Q_{ij} into the expression for $f_{\mu_2,i}$ yields:

$$\begin{aligned} f_{\mu_2,i}(Q) = & \frac{3S}{2} L \partial^2 \partial_j (n_i n_j) - \frac{3S}{2} A \partial_j (n_i n_j) - \frac{S^2}{4} B \partial_j (3n_i n_k - \delta_{ik}) (3n_k n_j - \delta_{kj}) \\ & - \frac{S^3}{8} C \partial_j [(3n_i n_j - \delta_{ij}) (3n_k n_l - \delta_{kl}) (3n_l n_k - \delta_{lk})] \end{aligned} \quad (32)$$

This simplifies to:

$$\begin{aligned} f_{\mu_2,i}(Q) = & \frac{3S}{2} L \partial^2 \partial_j (n_i n_j) - \frac{3S}{2} A \partial_j (n_i n_j) - \frac{3S^2}{2} B \partial_j (n_i n_j) - \frac{9S^3}{4} C \partial_j (n_i n_j) \\ = & \frac{3S}{2} \left(L \partial^2 - A - SB - \frac{3S^2}{2} C \right) \partial_j (n_i n_j) \end{aligned} \quad (33)$$

Do the same for $f_{L,i}$ to get:

$$f_{L,i}(Q) = \frac{9S^2}{4} \partial_j [\partial_i (n_k n_l) \partial_j (n_l n_k)] \quad (34)$$

Our first guess will be:

$$\hat{n} = (\cos k_x x, \sin k_x x, 0) \quad (35)$$

Note that this expression is independent of y so that any y -derivatives will be zero by default. We will do pieces at a time:

$$\begin{aligned} \partial_j (n_x n_j) &= \partial_x \cos^2 k_x x \\ &= 2 \cos k_x x (-k_x \sin k_x x) \\ &= -k_x \sin (2k_x x) \end{aligned} \quad (36)$$

Great, this still terminates at the endpoints. Now taking the Laplacian of this:

$$\begin{aligned} \partial^2 \partial_j (n_x n_j) &= \partial_x^2 (-k_x \sin (2k_x x)) \\ &= -4k_x^2 \partial_x \cos (2k_x x) \\ &= 8k_x^3 \sin (2k_x x) \end{aligned} \quad (37)$$

Cool, this also terminates at the endpoints. So far so good. Let's look at the y -component:

$$\begin{aligned} \partial_j (n_y n_j) &= \partial_x (\cos k_x x \sin k_x x) \\ &= \partial_x \frac{1}{2} \sin 2k_x x \\ &= -k_x \cos 2k_x x \end{aligned} \quad (38)$$

This certainly does not go to zero at the endpoints, so we have not met our no-slip condition. Dang. Now for the last term:

$$\begin{aligned}
\partial_j [\partial_x (n_k n_l) \partial_j (n_l n_k)] &= \partial_x \left[(\partial_x \cos^2 k_x x)^2 + (\partial_x \cos k_x x \sin k_x x)^2 + (\partial_x \cos k_x x \sin k_x x)^2 + (\partial_x \sin^2 k_x x)^2 \right] \\
&= \partial_x \left[k_x^2 \sin^2 (2k_x x) + 2 \left(\partial_x \frac{1}{2} \sin 2k_x x \right)^2 + k_x^2 \sin^2 (2k_x x) \right] \\
&= \partial_x [2k_x^2 \sin^2 (2k_x x) + 2k_x^2 \cos^2 (2k_x x)] \\
&= 0
\end{aligned} \tag{39}$$

Well this is not actually helpful to understanding why the elastic piece is so small – here it is actually zero. However, we can check the rest of the configuration with this scheme. In this case, we get:

$$f_i(x, y) = -\frac{\mu_2}{\mu_1} \frac{3S}{4} \left[8k_x^3 L + \left(A + SB + \frac{3S^2}{2} C \right) k_x \right] \sin(2k_x x) \tag{40}$$

Clearly we have that for all $k_y \neq 0$, we have $\hat{f}_{i, k_x k_y} = 0$ (since there is no y -dependence). Additionally, the only nonzero Fourier term is for $k_x = 4\pi/L_x$, and is completely imaginary since only sine is involved. This comes out to be:

$$f_{x, 4\pi/L_x, 0} = -i \frac{\mu_2}{\mu_1} \frac{3S}{4} \left[8k_x^3 L + \left(A + SB + \frac{3S^2}{2} C \right) k_x \right] \tag{41}$$

Now, we would like to choose f_i to be something which is just a sum of sines. These terminate at the endpoints, so we will fulfill our no slip condition ($v_i = 0$ at the boundaries) if we do that. Since we need to actually choose Q_{ij} to do that (so that we can use the same scenario for the stream function formulation), we will have to just guess and check. Note that many of the terms involved in f_i have third derivatives, so we will want to choose a cos to be the important term. Recall that:

$$Q_{ij} = \frac{S}{2} (3n_i n_j - \delta_{ij}) \tag{42}$$

Choose S to be constant. Plugging Q_{ij} into the expression for $f_{mu_2, i}$ yields:

$$\begin{aligned}
f_{\mu_2, i}(Q) &= \frac{3S}{2} L \partial^2 \partial_j (n_i n_j) - \frac{3S}{2} A \partial_j (n_i n_j) - \frac{S^2}{4} B \partial_j (3n_i n_k - \delta_{ik}) (3n_k n_j - \delta_{kj}) \\
&\quad - \frac{S^3}{8} C \partial_j [(3n_i n_j - \delta_{ij}) (3n_k n_l - \delta_{kl}) (3n_l n_k - \delta_{lk})]
\end{aligned} \tag{43}$$

This simplifies to:

$$\begin{aligned}
f_{\mu_2, i}(Q) &= \frac{3S}{2} L \partial^2 \partial_j (n_i n_j) - \frac{3S}{2} A \partial_j (n_i n_j) - \frac{3S^2}{2} B \partial_j (n_i n_j) - \frac{9S^3}{4} C \partial_j (n_i n_j) \\
&= \frac{3S}{2} \left(L \partial^2 - A - SB - \frac{3S^2}{2} C \right) \partial_j (n_i n_j)
\end{aligned} \tag{44}$$

Do the same for $f_{L, i}$ to get:

$$f_{L, i}(Q) = \frac{9S^2}{4} \partial_j [\partial_i (n_k n_l) \partial_j (n_l n_k)] \tag{45}$$

Our first guess will be:

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\end{aligned} \tag{48}$$

Cool, this also terminates at the endpoints. So far so good. Now for the last term:

$$\begin{aligned}
\partial_j [\partial_x (n_k n_l) \partial_j (n_l n_k)] &= \partial_x \left[(\partial_x \cos^2 k_x x)^2 + (\partial_x \cos k_x x \sin k_x x)^2 + (\partial_x \cos k_x x \sin k_x x)^2 + (\partial_x \sin^2 k_x x)^2 \right] \\
&= \partial_x \left[k_x^2 \sin^2(2k_x x) + 2 \left(\partial_x \frac{1}{2} \sin 2k_x x \right)^2 + k_x^2 \sin^2(2k_x x) \right] \\
&= \partial_x [2k_x^2 \sin^2(2k_x x) + 2k_x^2 \cos^2(2k_x x)] \\
&= 0
\end{aligned} \tag{49}$$

Well this is not actually helpful to understanding why the elastic piece is so small – here it is actually zero. However, we can check the rest of the configuration with this scheme. In this case, we get:

$$f_i(x, y) = -\frac{\mu_2}{\mu_1} \frac{3S}{4} \left[8k_x^3 L + \left(A + SB + \frac{3S^2}{2} C \right) k_x \right] \sin(2k_x x) \tag{50}$$

Clearly we have that for all $k_y \neq 0$, we have $\hat{f}_{i, k_x k_y} = 0$ (since there is no y -dependence). Additionally, the only nonzero Fourier term is for $k_x = 4\pi/L_x$, and is completely imaginary since only sine is involved. This comes out to be:

$$f_{x, 4\pi/L_x, 0} = -i \frac{\mu_2}{\mu_1} \frac{3S}{4} \left[8k_x^3 L + \left(A + SB + \frac{3S^2}{2} C \right) k_x \right] \tag{51}$$

Note that we only have nonzero \hat{f} for $i = x$ – we see this in previous calculations.