# Double helix director

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March 14, 2024

### 1 Selinger free energy

To investigate this system, we start with the Frank free energy as written by Selinger:

$$F = \frac{1}{2} (K_{11} - K_{24}) S^2 + \frac{1}{2} (K_{22} - K_{24}) T^2 + \frac{1}{2} K_{33} |\mathbf{B}|^2 + K_{24} \text{Tr} (\Delta^2)$$
 (1)

with the following definitions for the distortion modes:

$$S = \nabla \cdot \hat{\mathbf{n}} \tag{2}$$

$$T = \hat{\mathbf{n}} \cdot (\nabla \times \hat{\mathbf{n}}) \tag{3}$$

$$B = \hat{\mathbf{n}} \times (\nabla \times \hat{\mathbf{n}}) \tag{4}$$

$$\Delta_{ij} = \frac{1}{2} \left[ \partial_i n_j + \partial_j n_i - n_i n_k \partial_k n_j - n_j n_k \partial_k n_i - \delta_{ij} \partial_k n_k + n_i n_j \partial_k n_k \right]$$
(5)

# 2 Rotated system

We make two assumptions about the system: i) the z-dependence of the director corresponds to a rotation of a plane perpendicular to the cylindrical axis about the cylindrical axis by some angle  $\alpha z$ , and ii) the director stays in a plane perpendicular to the cylindrical axis. We note that in an infinitely long cylindrical system, i) is true by translational symmetry. In this case, we may write:

$$\hat{\mathbf{n}} = R(\alpha z) \begin{bmatrix} \cos \theta & \sin \theta & 0 \end{bmatrix}^T \tag{6}$$

for some director angle  $\theta$  as measured from the x-axis in the x-y-plane, and R(z) a rotation about the z-axis and a function of z. We note that  $\theta$  must be a function of x, y, and z, with the z-dependence corresponding to an *inverse* rotation of angle  $\alpha z$  about the z-axis. <sup>1</sup> This gives:

$$\begin{bmatrix} x' \\ y' \end{bmatrix} = R^{T}(\alpha z) \begin{bmatrix} x \\ y \end{bmatrix} 
= \begin{bmatrix} \cos(\alpha z) x + \sin(\alpha z) y \\ -\sin(\alpha z) x + \cos(\alpha z) y \end{bmatrix}$$
(7)

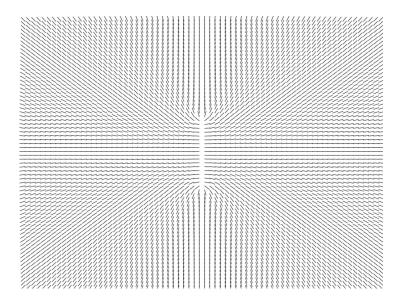
## 3 Rotated isotropic solution free energy

Taking  $\theta$  to be the standard isotropic solution for two +1/2 disclinations gives:

$$\theta(x',y') = \frac{1}{2} \tan^{-1} \left( \frac{y'}{x' - \frac{d}{2}} \right) + \frac{1}{2} \tan^{-1} \left( \frac{y'}{x' + \frac{d}{2}} \right)$$

$$= \frac{1}{2} \tan^{-1} \left( \frac{-\sin(\alpha z) x + \cos(\alpha z) y}{\cos(\alpha z) x + \sin(\alpha z) y - \frac{d}{2}} \right) + \frac{1}{2} \tan^{-1} \left( \frac{-\sin(\alpha z) x + \cos(\alpha z) y}{\cos(\alpha z) x + \sin(\alpha z) y + \frac{d}{2}} \right)$$
(8)

where here d is the disclination spacing. The result of plotting  $\theta + \alpha z$  for  $\alpha z = \pi/2$  gives the following rotated configuration:



One may explicitly calculate the free energy density for such a configuration. By symmetry, the free energy density at every z-value should be the same, so we evaluate at z=0 to simplify the expressions. What we find is that (expectedly) only the twist and saddle splay terms depend on  $\alpha$ . These give:

$$T^{2}(\alpha) = \alpha^{2} f(x, y) \cos^{4} \theta \tag{9}$$

$$|\Delta|^2(\alpha) = \alpha^2 f(x, y) + g(x, y) \tag{10}$$

with

$$f(x,y) = \frac{d^2 (d^2 - 4x^2 + 4y^2)^2}{(d^4 - 8d^2x^2 + 8d^2y^2 + 16x^4 + 32x^2y^2 + 16y^4)^2}$$
(11)

and q(x,y) some function independent of  $\alpha$ . Then the entire free energy goes as:

$$F = (K_{22} + (B - A)K_{24})\alpha^2 + C \tag{12}$$

with

$$B = \int_{\Omega} f(x, y) dV$$

$$A = \int_{\Omega} f(x, y) \cos^4 \theta dV$$
(13)

Clearly B > A always, and so a twisted configuration will never be the minimum, at least for the configuration that we've written down.

## 4 Selinger Euler-Lagrange equation

To find the equilibrium state, we must minimize the Selinger free energy subject to the constraint that  $\hat{\bf n}$  be a unit vector everywhere. The constraint can be written:

$$g(\mathbf{x}, \hat{\mathbf{n}}) = \hat{\mathbf{n}} \cdot \hat{\mathbf{n}} - 1 = 0 \tag{14}$$

Then the corresponding Lagrangian to be minimized is:

$$L = F - \lambda(\mathbf{x})g(\mathbf{x}, \hat{\mathbf{n}}) \tag{15}$$

The resulting functional derivative is is:

$$\delta L = \delta F - (2\lambda(\mathbf{x})\hat{\mathbf{n}}) \cdot \delta \hat{\mathbf{n}} \tag{16}$$

The resulting Euler-Lagrange equation then reads:

$$\frac{\delta F}{\delta \hat{\mathbf{n}}} = \lambda(\mathbf{x})\hat{\mathbf{n}} \tag{17}$$

where we have absorbed the factor of 2 into  $\lambda(\mathbf{x})$  since it is arbitrary anyways. If we operate on both sides with  $(I - \hat{\mathbf{n}} \otimes \hat{\mathbf{n}})$  we get the following:

$$(I - \hat{\mathbf{n}} \otimes \hat{\mathbf{n}}) \frac{\delta F}{\delta \hat{\mathbf{n}}} = \lambda(\mathbf{x}) \left[ \hat{\mathbf{n}} - (\hat{\mathbf{n}} \cdot \hat{\mathbf{n}}) \, \hat{\mathbf{n}} \right] = 0$$
(18)

where we have used the constraint on the left-hand side.

Below we calculate the functional derivative of F. This will simplify when we restrict the director to only polar-planar configurations. We do this one term at a time:

$$\delta(S^{2}) = \int_{\Omega} 2S (\delta S) dV$$

$$= \int_{\Omega} 2S (\nabla \cdot \delta \hat{\mathbf{n}}) dV$$

$$= -\int_{\Omega} 2 (\nabla S) \cdot \delta \hat{\mathbf{n}} dV + \int_{\partial \Omega} 2 (S \boldsymbol{\nu}) \cdot \delta \hat{\mathbf{n}} dS$$
(19)

$$\delta(T^{2}) = \int_{\Omega} 2T (\delta T) dV$$

$$= \int_{\Omega} 2T (\delta \hat{\mathbf{n}} \cdot (\nabla \times \hat{\mathbf{n}}) + \hat{\mathbf{n}} \cdot (\nabla \times \delta \hat{\mathbf{n}})) dV$$

$$= \int_{\Omega} 4T (\nabla \times \hat{\mathbf{n}}) \cdot \delta \hat{\mathbf{n}} dV - \int_{\partial \Omega} 2T \boldsymbol{\nu} \cdot (\hat{\mathbf{n}} \times \delta \hat{\mathbf{n}}) dS$$
(20)

where we have used the following identity<sup>2</sup>:

$$A \cdot (\nabla \times B) = -\nabla \cdot (A \times B) + B \cdot (\nabla \times A) \tag{21}$$

Also:

$$\delta |\mathbf{B}|^{2} = \int_{\Omega} 2\mathbf{B} \cdot (\delta \mathbf{B}) \ dV$$

$$= \int_{\Omega} 2\mathbf{B} \cdot (\delta \hat{\mathbf{n}} \times (\nabla \times \hat{\mathbf{n}}) + \hat{\mathbf{n}} \times (\nabla \times \delta \hat{\mathbf{n}})) \ dV$$

$$= \int_{\Omega} 2 \left[ \delta \hat{\mathbf{n}} \cdot ((\nabla \times \hat{\mathbf{n}}) \times \mathbf{B}) + (\nabla \times \delta \hat{\mathbf{n}}) \cdot (\mathbf{B} \times \hat{\mathbf{n}}) \right] \ dV$$

$$= \int_{\Omega} 2 \left[ \delta \hat{\mathbf{n}} \cdot ((\nabla \times \hat{\mathbf{n}}) \times \mathbf{B}) + \nabla \cdot (\delta \hat{\mathbf{n}} \times (\mathbf{B} \times \hat{\mathbf{n}})) + \delta \hat{\mathbf{n}} \cdot (\nabla \times (\mathbf{B} \times \hat{\mathbf{n}})) \right] \ dV$$

$$= \int_{\Omega} 2 \left[ \nabla \times (\mathbf{B} \times \hat{\mathbf{n}}) + (\nabla \times \hat{\mathbf{n}}) \times \mathbf{B} \right] \cdot \delta \hat{\mathbf{n}} \ dV + \int_{\partial \Omega} 2 \left[ \boldsymbol{\nu} \cdot (\delta \hat{\mathbf{n}} \times (\mathbf{B} \times \hat{\mathbf{n}})) \right] \ dS$$

$$(22)$$

where we have used the following identities:

$$A \cdot (B \times C) = C \cdot (A \times B) = B \cdot (C \times A) \tag{23}$$

and

$$\nabla \cdot (A \times B) = (\nabla \times A) \cdot B - (\nabla \times B) \cdot A \tag{24}$$

And finally, we look at the  $\Delta$  term:

$$\delta\left(\Delta_{ij}\Delta_{ji}\right) = \int_{\Omega} 2\Delta_{ij} \left[2\partial_{i}\delta n_{j} - 2\delta n_{i} n_{k}\partial_{k} n_{j} - 2n_{i}\delta n_{k}\partial_{k} n_{j} - 2n_{i}n_{k}\partial_{k}\delta n_{j} \right.$$

$$\left. + \delta n_{i}n_{j}\partial_{k}n_{k} + n_{i}\delta n_{j}\partial_{k}n_{k} + n_{i}n_{j}\partial_{k}\delta n_{k}\right] dV$$

$$= \int_{\Omega} 2\left[-2\Delta_{ij}\delta n_{i} n_{k}\partial_{k}n_{j} - 2\Delta_{ij}n_{i}\delta n_{k}\partial_{k}n_{j} + \Delta_{ij}\delta n_{i}n_{j}\partial_{k}n_{k} + \Delta_{ij}n_{i}\delta n_{j}\partial_{k}n_{k} \right.$$

$$\left. 2\Delta_{ij}\partial_{i}\delta n_{j} - 2\Delta_{ij}n_{i}n_{k}\partial_{k}\delta n_{j} + \Delta_{ij}n_{i}n_{j}\partial_{k}\delta n_{k}\right] dV$$

$$= \int_{\Omega} 2\left[-2\Delta_{kj}n_{i}\partial_{i}n_{j} - 2\Delta_{ij}n_{i}\partial_{k}n_{j} + \Delta_{kj}n_{j}\partial_{i}n_{i} + \Delta_{ik}n_{i}\partial_{j}n_{j}\right]\delta n_{k} dV$$

$$+ \int_{\Omega} 2\left[-2\partial_{i}\Delta_{ik} + 2\partial_{j}\left(\Delta_{ik}n_{i}n_{j}\right) - \partial_{k}\left(\Delta_{ij}n_{i}n_{j}\right)\right]\delta n_{k} dV$$

$$+ \int_{\partial\Omega} 2\left[2\Delta_{ij}\nu_{i}\delta n_{j} - 2\Delta_{ij}n_{i}n_{k}\nu_{k}\delta n_{j} + \Delta_{ij}n_{i}n_{j}\nu_{k}\delta n_{k}\right] dV$$

For now, we assume that the boundaries are fixed so that the surface terms vanish. Putting all of these terms together gives the following Euler-Lagrange equation:

$$0 = (I - \hat{\mathbf{n}} \otimes \hat{\mathbf{n}}) \left[ -(K_{11} - K_{24}) \nabla S + 2(K_{22} - K_{24}) T (\nabla \times \hat{\mathbf{n}}) + K_{33} [\nabla \times (\mathbf{B} \times \hat{\mathbf{n}}) + (\nabla \times \hat{\mathbf{n}}) \times \mathbf{B}] + 4K_{24} [\Delta \cdot \hat{\mathbf{n}} (\nabla \cdot \hat{\mathbf{n}}) - (\hat{\mathbf{n}} \cdot \nabla \hat{\mathbf{n}}) \cdot \Delta - (\nabla \hat{\mathbf{n}}) \cdot \Delta \cdot \hat{\mathbf{n}} - \nabla \cdot \Delta + \nabla \cdot (\hat{\mathbf{n}} \otimes (\hat{\mathbf{n}} \cdot \Delta)) - \frac{1}{2} \nabla (\hat{\mathbf{n}} \cdot \Delta \cdot \hat{\mathbf{n}})] \right]$$

$$(26)$$

The idea here is to look at a general expression for a twisted planar configuration:

$$\hat{\mathbf{n}}' = R(\alpha z) \begin{bmatrix} \cos(\theta(x', y')) \\ \sin(\theta(x', y')) \\ 0 \end{bmatrix}$$
(27)

with

$$x' = \cos(\alpha z)x + \sin(\alpha z)y$$
  

$$y' = -\sin(\alpha z)x + \cos(\alpha z)y$$
(28)

If we plug into eq. (26) and set z=0 we will get a PDE in x and y. Imposing homeotropic boundary conditions gives us a minimum-energy configuration for a fixed  $\alpha$ . Presumably we will have to solve this perturbatively with a regular and non-regular part. The non-regular part will have to be the two-defect configuration separated by a distance d. We may map out the free energy landscape for these two parameters, at the very least.

## 5 Bend-Splay Euler-Lagrange, as a check

To check our calculation, we just consider Bend-Splay terms. Taking  $\epsilon = (K_{33} - K_{11})/(K_{33} + K_{11})$  gives:

$$(I - \hat{\mathbf{n}} \otimes \hat{\mathbf{n}}) \left[ -(1 + \epsilon)\nabla S + (1 - \epsilon) \left[ \nabla \times (\mathbf{B} \times \hat{\mathbf{n}}) + (\nabla \times \hat{\mathbf{n}}) \times \mathbf{B} \right] \right] = 0$$
 (29)

We calculate each term separately:

$$\nabla S - (\hat{\mathbf{n}} \cdot \nabla S) \,\hat{\mathbf{n}} \tag{30}$$

$$\hat{\mathbf{n}} \cdot \nabla \times (\mathbf{B} \times \hat{\mathbf{n}}) = \nabla \cdot (\hat{\mathbf{n}} \times (\mathbf{B} \times \hat{\mathbf{n}})) + (\nabla \times \hat{\mathbf{n}}) \cdot (\mathbf{B} \times \hat{\mathbf{n}})$$
(31)

$$\hat{\mathbf{n}} \cdot [(\nabla \times \hat{\mathbf{n}}) \times \mathbf{B}] = (\nabla \times \hat{\mathbf{n}}) \cdot (\mathbf{B} \times \hat{\mathbf{n}}) 
= (\nabla \times \hat{\mathbf{n}}) \cdot ((\hat{\mathbf{n}} \times (\nabla \times \hat{\mathbf{n}})) \times \hat{\mathbf{n}}) 
= (\nabla \times \hat{\mathbf{n}}) \cdot ((-(\hat{\mathbf{n}} \cdot \nabla) \hat{\mathbf{n}}) \times \hat{\mathbf{n}})$$
(32)

## 6 Simplified free energy

### 6.1 Free energy and Euler-Lagrange equation

For sake of calculation, we rewrite the Frank free energy as:

$$F = \frac{1}{2}K_{11}S^2 + \frac{1}{2}K_{22}T^2 + \frac{1}{2}K_{33}\left|\mathbf{B}\right|^2 + \frac{1}{2}K_{24}P \tag{33}$$

with

$$P = \nabla \cdot [(\hat{\mathbf{n}} \cdot \nabla) \,\hat{\mathbf{n}} - \hat{\mathbf{n}} \,(\nabla \cdot \hat{\mathbf{n}})] \tag{34}$$

the saddle splay term.

We take  $\zeta$  to be our twist elastic constant:

$$\zeta = \frac{K - K_{22}}{K + K_{22}} \tag{35}$$

This gives:

$$K_{22} = K \frac{1 - \zeta}{1 + \zeta} \tag{36}$$

Then the free energy is given by:

$$F = \int_{\Omega} (1+\zeta)S^2 + (1-\zeta)T^2 + (1+\zeta)|\mathbf{B}|^2 + \frac{K_{24}}{K}PdV$$
 (37)

We may calculate each term explicitly for the planar director  $\hat{\mathbf{n}} = [\cos \theta, \sin \theta, 0]$  with  $\theta$  a function of (x, y, z):

$$S = -\theta_x \sin \theta + \theta_y \cos \theta \tag{38}$$

$$T = -\theta_z \tag{39}$$

$$\mathbf{B} = \sin\theta \left(\theta_x \cos\theta + \theta_y \sin\theta\right) \hat{\mathbf{x}} - \cos\theta \left(\theta_x \cos\theta + \theta_y \sin\theta\right) \hat{\mathbf{y}}$$
(40)

So that:

$$S^{2} = \theta_{x}^{2} \sin^{2} \theta + \theta_{y}^{2} \cos^{2} \theta - 2\theta_{x} \theta_{y} \sin \theta \cos \theta \tag{41}$$

$$T^2 = \theta_z^2 \tag{42}$$

$$|\mathbf{B}|^2 = \theta_x^2 \cos^2 \theta + \theta_y^2 \sin^2 \theta + 2\theta_x \theta_y \sin \theta \cos \theta \tag{43}$$

$$P = -\theta_{xy} + \theta_{yx} = 0 \tag{44}$$

Calculating the free energy explicitly then gives:

$$F = \int_{\Omega} (1+\zeta) \left| \nabla \theta \right|^2 + (1-\zeta) \theta_z^2 dV \tag{45}$$

with  $\nabla = \partial_x \hat{\mathbf{x}} + \partial_y \hat{\mathbf{y}}$  the two-dimensional gradient operator. The differential is:

$$\delta F = 2 \int_{\Omega} (1+\zeta) \left(\nabla \theta\right) \cdot \left(\nabla \delta \theta\right) + \left(1-\zeta\right) \left(\frac{d\theta}{dz}\right) \left(\frac{d\delta \theta}{dz}\right) dV 
= 2 \int_{\Omega} (1+\zeta) \left[\nabla \cdot \left(\delta \theta \nabla \theta\right) - \left(\nabla^2 \theta\right) \delta \theta\right] + \left(1-\zeta\right) \left[\frac{d}{dz} \left(\delta \theta \frac{d\theta}{dz}\right) - \left(\frac{d^2 \theta}{dz^2}\right) \delta \theta\right] dV 
= \int_{\Omega} -2 \left[ (1+\zeta) \nabla^2 \theta + (1-\zeta) \frac{d^2 \theta}{dz^2} \right] \delta \theta dV$$
(46)

where we have assumed that the variation goes to zero at all the boundaries. Then the Euler-Lagrange equation reads:

$$(1+\zeta)\nabla^{2}\theta + (1-\zeta)\frac{d^{2}\theta}{dz^{2}} = 0$$
(47)

### 6.2 Constant twist angular velocity configuration

We now consider a director given by:

$$\theta(x, y, z) = \theta(x', y') + \alpha z \tag{48}$$

where

$$x' = \cos(\alpha z)x + \sin(\alpha z)y$$
  

$$y' = -\sin(\alpha z)x + \cos(\alpha z)y$$
(49)

We calculate this explicitly as follows:

$$\frac{\partial \theta}{\partial x} = \frac{\partial \theta}{\partial x'} \frac{\partial x'}{\partial x} + \frac{\partial \theta}{\partial y'} \frac{\partial y'}{\partial x} = \frac{\partial \theta}{\partial x'} \cos(\alpha z) - \frac{\partial \theta}{\partial y'} \sin(\alpha z)$$
 (50)

so that

$$\frac{\partial^2 \theta}{\partial x^2} = \frac{\partial^2 \theta}{\partial x'^2} \cos^2(\alpha z) - 2 \frac{\partial^2 \theta}{\partial x' \partial y'} \cos(\alpha z) \sin(\alpha z) + \frac{\partial^2 \theta}{\partial y'^2} \sin^2(\alpha z)$$
 (51)

similarly for y:

$$\frac{\partial^2 \theta}{\partial y^2} = \frac{\partial^2 \theta}{\partial x'^2} \sin^2(\alpha z) + 2 \frac{\partial^2 \theta}{\partial x' \partial y'} \cos(\alpha z) \sin(\alpha z) + \frac{\partial^2 \theta}{\partial y'^2} \cos^2(\alpha z)$$
 (52)

Together this gives:

$$\nabla^2 \theta = \frac{\partial^2 \theta}{\partial x} + \frac{\partial^2 \theta}{\partial y} = \frac{\partial^2 \theta}{\partial x'} + \frac{\partial^2 \theta}{\partial y'}$$
 (53)

so that it does not matter which plane we look at.

For the z-derivative we get:

$$\frac{\partial \theta}{\partial z} = \frac{\partial \theta}{\partial x'} \frac{\partial x'}{\partial z} + \frac{\partial \theta}{\partial y'} \frac{\partial y'}{\partial z} = \frac{\partial \theta}{\partial x'} \alpha y' - \frac{\partial \theta}{\partial y'} \alpha x' = -\alpha \left( \mathbf{x} \times \nabla \right) \theta \tag{54}$$

where  $\mathbf{x} = x\hat{\mathbf{x}} + y\hat{\mathbf{y}}$ . The second derivative gives:

$$\frac{\partial^{2} \theta}{\partial z^{2}} = \frac{\partial^{2} \theta}{\partial x' \partial z} \alpha y' + \frac{\partial \theta}{\partial x'} \alpha \frac{\partial y'}{\partial z} - \frac{\partial^{2} \theta}{\partial y' \partial z} \alpha x' - \frac{\partial \theta}{\partial y'} \alpha \frac{\partial x'}{\partial z} 
= \frac{\partial^{2} \theta}{\partial x'^{2}} \alpha^{2} y'^{2} - \frac{\partial^{2} \theta}{\partial x' \partial y'} \alpha^{2} y' x' - \frac{\partial \theta}{\partial x'} \alpha^{2} x' + \frac{\partial^{2} \theta}{\partial y'^{2}} \alpha^{2} x'^{2} - \frac{\partial^{2} \theta}{\partial y' \partial x'} \alpha^{2} x' y' - \frac{\partial \theta}{\partial y'} \alpha^{2} y' 
= \alpha^{2} (\mathbf{x} \times \nabla)^{2} \theta$$
(55)

<sup>3</sup>. The expression for energy then becomes:

$$F = \int_{\Omega} (1 + \zeta) |\nabla \theta|^2 + (1 - \zeta) \alpha^2 \left[ (\mathbf{x} \times \nabla) \theta \right]^2 dV$$
 (56)

and the Euler-Lagrange equation reads:

$$(1+\zeta)\nabla^2\theta + (1-\zeta)\alpha^2(\mathbf{x}\times\nabla)^2\theta = 0$$
(57)

We may decompose  $\theta$  into  $\theta_{\rm iso} + \theta_c$  where  $\theta_{\rm iso} = \frac{1}{2} (\varphi_1 + \varphi_2)$  with  $\varphi_1, \varphi_2$  the polar coordinates centered at  $(\pm \frac{d}{2}, 0)$  and  $\theta_c$  is a regular correction. Note that d is the spacing of the two +1/2 disclinations. Since  $\nabla^2 \theta_{\rm iso} = 0$  this gives the following linear equation for  $\theta_c$ :

$$\left[ (1+\zeta)\nabla^2 + (1-\zeta)\alpha^2 \left( \mathbf{x} \times \nabla \right)^2 \right] \theta_c = -(1-\zeta)\alpha^2 \left( \mathbf{x} \times \nabla \right)^2 \theta_{\text{iso}}$$
 (58)

#### 6.3 Constant twist weak form

The  $(\mathbf{x} \times \nabla)$  operator also has a nice product rule<sup>4</sup>. Also note that, in two dimensions, it has a nice integration formula<sup>5</sup> Taking the inner product with some test function  $\eta$  then yields the following weak form:

$$(1+\zeta)\left\langle \eta, \nabla^{2}\theta_{c}\right\rangle + (1-\zeta)\alpha^{2}\left\langle \eta, (\mathbf{x}\times\nabla)^{2}\theta_{c}\right\rangle = -(1-\zeta)\alpha^{2}\left\langle \eta, (\mathbf{x}\times\nabla)^{2}\theta_{\mathrm{iso}}\right\rangle$$
(59)

which finally yields:

$$-(1+\zeta)\langle\nabla\eta,\nabla\theta_{c}\rangle$$

$$-(1-\zeta)\alpha^{2}\langle(\mathbf{x}\times\nabla)\eta,(\mathbf{x}\times\nabla)\theta_{c}\rangle = (1-\zeta)\alpha^{2}\langle(\mathbf{x}\times\nabla)\eta,(\mathbf{x}\times\nabla)\theta_{\mathrm{iso}}\rangle$$

$$-(1+\zeta)\langle\eta,\boldsymbol{\nu}\cdot\nabla\theta_{c}\rangle_{\partial\Omega}$$

$$-(1-\zeta)\alpha^{2}\langle\eta,(\mathbf{x}\times\boldsymbol{\nu})(\mathbf{x}\times\nabla)\theta_{c}\rangle_{\partial\Omega}$$

If we maintain Dirichlet boundary conditions, this becomes:

$$(1+\zeta)\langle\nabla\eta,\nabla\theta_c\rangle + \alpha^2(1-\zeta)\langle(\mathbf{x}\times\nabla)\eta,(\mathbf{x}\times\nabla)\theta_c\rangle = -\alpha^2(1-\zeta)\langle(\mathbf{x}\times\nabla)\eta,(\mathbf{x}\times\nabla)\theta_{\mathrm{iso}}\rangle \quad (61)$$

Additionally, we note that, in polar coordinates we have:

$$\frac{\partial \varphi}{\partial x} = -\frac{1}{r}\sin\varphi \tag{62}$$

$$\frac{\partial \varphi}{\partial y} = \frac{1}{r} \cos \varphi \tag{63}$$

This is true for polar coordinates centered at any origin. Then we also have that:

$$x = r_i \cos \varphi_i \pm \frac{d}{2} \tag{64}$$

$$y = r_i \sin \varphi_i \tag{65}$$

with - for i = 1 and + for i = 2. This implies:

$$r_i^2 = \left(x \mp \frac{d}{2}\right)^2 + y^2 \tag{66}$$

In that case:

$$\frac{\partial \varphi}{\partial x} = -\frac{y}{(x \mp \frac{d}{2})^2 + y^2} \tag{67}$$

$$\frac{\partial \varphi}{\partial y} = \frac{x \mp \frac{d}{2}}{(x \mp \frac{d}{2})^2 + y^2} \tag{68}$$

Putting this altogether we get:

$$(\mathbf{x} \times \nabla)\theta_{\text{iso}} = \frac{1}{2} \left[ \frac{x^2 + y^2 + \frac{d}{2}x}{\left(x + \frac{d}{2}\right)^2 + y^2} + \frac{x^2 + y^2 - \frac{d}{2}x}{\left(x - \frac{d}{2}\right)^2 + y^2} \right]$$
(69)

For the boundary conditions, homeotropic anchoring demands that:

$$\theta|_{\partial\Omega} = \varphi \tag{70}$$

However, we have that:

$$\frac{1}{2} \left[ \operatorname{atan2} \left( y, x + \frac{d}{2} \right) + \operatorname{atan2} \left( y, x - \frac{d}{2} \right) \right] \tag{71}$$

Hence, we must have:

$$\theta_c = \operatorname{atan2}(y, x) - \frac{1}{2} \left[ \operatorname{atan2}\left(y, x + \frac{d}{2}\right) + \operatorname{atan2}\left(y, x - \frac{d}{2}\right) \right]$$
 (72)

#### 6.4 Discussion of constant twist energy

In this section we more closely consider Eq. (56). We note that  $|\nabla \theta|^2$  is minimized by  $\theta_{\rm iso}$  because it solves Laplace's equation. Further,  $[(\mathbf{x} \times \nabla)\theta]^2 > 0$  always. Hence, for any  $0 < \zeta < 1$  we have that:

$$(1+\zeta)\left|\nabla\theta_{\rm iso}\right|^2 \le (1+\zeta)\left|\nabla\theta\right|^2 \le (1+\zeta)\left|\nabla\theta\right|^2 + \alpha^2(1-\zeta)\left[(\mathbf{x}\times\theta)\theta\right]^2 \tag{73}$$

with the first comparison an equality only when  $\theta = \theta_{\rm iso}$  by uniqueness of the solutions of Laplace's equation, and the second comparison an equality only when  $\alpha = 0$  (or  $(\mathbf{x} \times \nabla)\theta = 0$  which seems impossible for a configuration with two disclinations). This means that the minimizer is always  $\theta = \theta_{\rm iso}$  with  $\alpha = 0$ . Since  $\zeta < 1$  always (lest we let  $K_33 < 0$ ) this is always the case, and the director formalism will never produce a planar minimum energy configuration which has constant twist angular velocity.

#### 6.5 Variable twist angular velocity

Here we assume a director configuration whose twist angular velocity  $\alpha$  is a function of z. In this case, the x- and y-derivatives are unchanged, but the z derivatives vary considerably:

$$\frac{\partial \theta}{\partial z} = \frac{\partial \theta}{\partial x'} (\alpha + z\alpha') y' - \frac{\partial \theta}{\partial y'} (\alpha + z\alpha') x' \tag{74}$$

and then

$$\frac{\partial^{2} \theta}{\partial z^{2}} = \frac{\partial^{2} \theta}{\partial x'^{2}} (\alpha + z\alpha')^{2} y'^{2} - \frac{\partial^{2} \theta}{\partial x' \partial y'} (\alpha + z\alpha')^{2} y' x' + \frac{\partial \theta}{\partial x'} (2\alpha' + z\alpha'') y' - \frac{\partial \theta}{\partial x'} (\alpha + z\alpha')^{2} x' + \frac{\partial^{2} \theta}{\partial y'^{2}} (\alpha + z\alpha')^{2} x'^{2} - \frac{\partial^{2} \theta}{\partial y' \partial x'} (\alpha + z\alpha')^{2} x' y' - \frac{\partial \theta}{\partial y'} (2\alpha' + z\alpha'') x' - \frac{\partial \theta}{\partial y'} (\alpha + z\alpha')^{2} y' \tag{75}$$

Finally we have:

$$\frac{\partial^2}{\partial z^2} \alpha z = \frac{\partial}{\partial z} \left[ \alpha' z + \alpha \right] = \alpha'' z + 2\alpha' \tag{76}$$

#### Notes

<sup>1</sup> Suppose  $\mathbf{v}(\mathbf{x})$  is a vector field. Take L to be a linear transformation. We would like to act on  $\mathbf{v}$  by L in an active way. This means that, if L rotates a plane by some angle  $\theta$ , then we are imagining taking  $\mathbf{v}$  (say on a piece of paper) and rotating the whole thing by the angle  $\theta$ . There's two pieces to this: i) is that we must act on each of the vectors outputted by  $\mathbf{v}$  by L (again, think of rotating a vector field printed on a piece of paper). ii) is that, if we want to get the correct vector field at  $\mathbf{x}$ , we must actually sample  $\mathbf{v}$  at a point  $L^{-1}\mathbf{x}$ . This is because  $L^{-1}\mathbf{x}$  is the point that will get mapped to  $\mathbf{x}$  by L.

2

$$A \cdot (\nabla \times B) = A_{i} \epsilon_{ijk} \partial_{j} B_{k}$$

$$= \epsilon_{ijk} (\partial_{j} (A_{i} B_{k}) - B_{k} \partial_{j} A_{i})$$

$$= -\partial_{j} (\epsilon_{jik} A_{i} B_{k}) + B_{k} \epsilon_{kji} \partial_{j} A_{i}$$

$$= -\nabla \cdot (A \times B) + B \cdot (\nabla \times A)$$

$$(77)$$

3

$$(\mathbf{x} \times \nabla)^2 = \left( x \frac{\partial}{\partial y} - y \frac{\partial}{\partial x} \right) \left( x \frac{\partial}{\partial y} - y \frac{\partial}{\partial x} \right)$$

$$= \left( x^2 \frac{\partial}{\partial y^2} - x \frac{\partial}{\partial x} - xy \frac{\partial}{\partial y} \frac{\partial}{\partial x} - y \frac{\partial}{\partial y} - yx \frac{\partial}{\partial x} \frac{\partial}{\partial y} + y^2 \frac{\partial}{\partial x^2} \right)$$
(78)

4

$$(\mathbf{x} \times \nabla) (fg) = \left( x \frac{\partial}{\partial y} - y \frac{\partial}{\partial x} \right) (fg)$$

$$= x \left( g \frac{\partial f}{\partial y} + f \frac{\partial g}{\partial y} \right) - y \left( g \frac{\partial f}{\partial x} + f \frac{\partial g}{\partial x} \right)$$

$$= g \left( x \frac{\partial f}{\partial y} - y \frac{\partial f}{\partial x} \right) + f \left( x \frac{\partial g}{\partial y} - y \frac{\partial g}{\partial x} \right)$$

$$= g (\mathbf{x} \times \nabla) f + f (\mathbf{x} \times \nabla) g$$

$$(79)$$

<sup>5</sup> We first rewrite the operator as a divergence:  $(\mathbf{x} \times \nabla)f = \nabla \cdot \mathbf{g}$  with  $\mathbf{g} = f[-y \ x]^T$ . Then we may explicitly calculate the integration formula using the divergence theorem:

$$\int_{\Omega} (\mathbf{x} \times \nabla) f \, dV = \int_{\Omega} \nabla \cdot \mathbf{g} \, dV$$

$$= \int_{\partial \Omega} (\hat{\boldsymbol{\nu}} \cdot \mathbf{g}) \, dS$$

$$= \int_{\partial \Omega} f \left( -\nu_x y + \nu_y x \right) dS$$

$$= \int_{\partial \Omega} f \left( \mathbf{x} \times \hat{\boldsymbol{\nu}} \right) dS$$
(80)

Then the simplified Euler-Lagrange equation is:

$$0 = -(1+\zeta)\nabla S + 2(1-\zeta)T \left(\nabla \times \hat{\mathbf{n}}\right) + (1+\zeta)\left[\nabla \times (\mathbf{B} \times \hat{\mathbf{n}}) + (\nabla \times \hat{\mathbf{n}}) \times \mathbf{B}\right]$$
(81)