

# Double helix director

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## 1 Selinger free energy

To investigate this system, we start with the Frank free energy as written by Selinger:

$$F = \frac{1}{2} (K_{11} - K_{24}) S^2 + \frac{1}{2} (K_{22} - K_{24}) T^2 + \frac{1}{2} K_{33} |\mathbf{B}|^2 + K_{24} \text{Tr} (\Delta^2) \quad (1)$$

with the following definitions for the distortion modes:

$$S = \nabla \cdot \hat{\mathbf{n}} \quad (2)$$

$$T = \hat{\mathbf{n}} \cdot (\nabla \times \hat{\mathbf{n}}) \quad (3)$$

$$B = \hat{\mathbf{n}} \times (\nabla \times \hat{\mathbf{n}}) \quad (4)$$

$$\begin{aligned} \Delta_{ij} = \frac{1}{2} [ & \partial_i n_j + \partial_j n_i \\ & - n_i n_k \partial_k n_j - n_j n_k \partial_k n_i \\ & - \delta_{ij} \partial_k n_k + n_i n_j \partial_k n_k ] \end{aligned} \quad (5)$$

## 2 Rotated system

We make two assumptions about the system: i) the  $z$ -dependence of the director corresponds to a rotation of a plane perpendicular to the cylindrical axis about the cylindrical axis by some angle  $\alpha z$ , and ii) the director stays in a plane perpendicular to the cylindrical axis. We note that in an infinitely long cylindrical system, i) is true by translational symmetry. In this case, we may write:

$$\hat{\mathbf{n}} = R(\alpha z) [\cos \theta \quad \sin \theta \quad 0]^T \quad (6)$$

for some director angle  $\theta$  as measured from the  $x$ -axis in the  $x$ - $y$ -plane, and  $R(z)$  a rotation about the  $z$ -axis and a function of  $z$ . We note that  $\theta$  must be a function of  $x$ ,  $y$ , and  $z$ , with the  $z$ -dependence corresponding to an *inverse* rotation of angle  $\alpha z$  about the  $z$ -axis.<sup>1</sup> This gives:

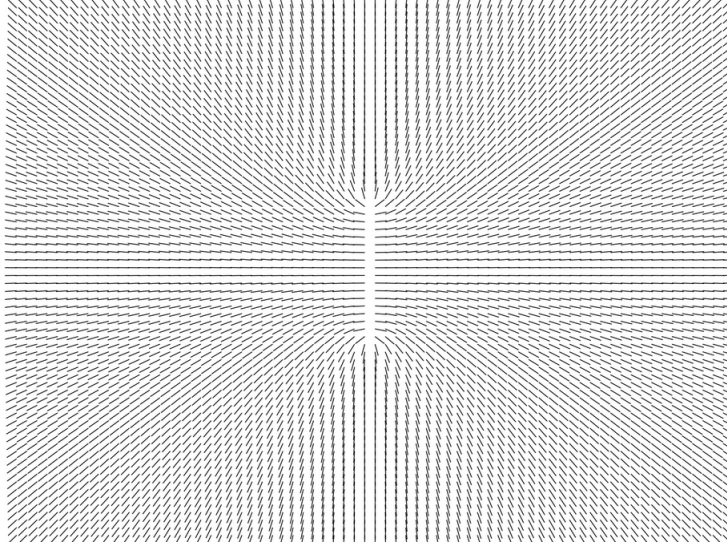
$$\begin{aligned} \begin{bmatrix} x' \\ y' \end{bmatrix} &= R^T(\alpha z) \begin{bmatrix} x \\ y \end{bmatrix} \\ &= \begin{bmatrix} \cos(\alpha z) x + \sin(\alpha z) y \\ -\sin(\alpha z) x + \cos(\alpha z) y \end{bmatrix} \end{aligned} \quad (7)$$

### 3 Rotated isotropic solution free energy

Taking  $\theta$  to be the standard isotropic solution for two  $+1/2$  disclinations gives:

$$\begin{aligned}\theta(x', y') &= \frac{1}{2} \tan^{-1} \left( \frac{y'}{x' - \frac{d}{2}} \right) + \frac{1}{2} \tan^{-1} \left( \frac{y'}{x' + \frac{d}{2}} \right) \\ &= \frac{1}{2} \tan^{-1} \left( \frac{-\sin(\alpha z) x + \cos(\alpha z) y}{\cos(\alpha z) x + \sin(\alpha z) y - \frac{d}{2}} \right) + \frac{1}{2} \tan^{-1} \left( \frac{-\sin(\alpha z) x + \cos(\alpha z) y}{\cos(\alpha z) x + \sin(\alpha z) y + \frac{d}{2}} \right)\end{aligned}\tag{8}$$

where here  $d$  is the disclination spacing. The result of plotting  $\theta + \alpha z$  for  $\alpha z = \pi/2$  gives the following rotated configuration:



One may explicitly calculate the free energy density for such a configuration. By symmetry, the free energy density at every  $z$ -value should be the same, so we evaluate at  $z = 0$  to simplify the expressions. What we find is that (expectedly) only the twist and saddle splay terms depend on  $\alpha$ . These give:

$$T^2(\alpha) = \alpha^2 f(x, y) \cos^4 \theta \tag{9}$$

$$|\Delta|^2(\alpha) = \alpha^2 f(x, y) + g(x, y) \tag{10}$$

with

$$f(x, y) = \frac{d^2 (d^2 - 4x^2 + 4y^2)^2}{(d^4 - 8d^2x^2 + 8d^2y^2 + 16x^4 + 32x^2y^2 + 16y^4)^2} \tag{11}$$

and  $g(x, y)$  some function independent of  $\alpha$ . Then the entire free energy goes as:

$$F = (K_{22} + (B - A)K_{24}) \alpha^2 + C \tag{12}$$

with

$$\begin{aligned}B &= \int_{\Omega} f(x, y) dV \\ A &= \int_{\Omega} f(x, y) \cos^4 \theta dV\end{aligned}\tag{13}$$

Clearly  $B > A$  always, and so a twisted configuration will never be the minimum, at least for the configuration that we've written down.

## 4 Selinger Euler-Lagrange equation

To find the equilibrium state, we must minimize the Selinger free energy subject to the constraint that  $\hat{\mathbf{n}}$  be a unit vector everywhere. The constraint can be written:

$$g(\mathbf{x}, \hat{\mathbf{n}}) = \hat{\mathbf{n}} \cdot \hat{\mathbf{n}} - 1 = 0 \quad (14)$$

Then the corresponding Lagrangian to be minimized is:

$$L = F - \lambda(\mathbf{x})g(\mathbf{x}, \hat{\mathbf{n}}) \quad (15)$$

The resulting functional derivative is is:

$$\delta L = \delta F - (2\lambda(\mathbf{x})\hat{\mathbf{n}}) \cdot \delta \hat{\mathbf{n}} \quad (16)$$

The resulting Euler-Lagrange equation then reads:

$$\frac{\delta F}{\delta \hat{\mathbf{n}}} = \lambda(\mathbf{x})\hat{\mathbf{n}} \quad (17)$$

where we have absorbed the factor of 2 into  $\lambda(\mathbf{x})$  since it is arbitrary anyways. If we operate on both sides with  $(I - \hat{\mathbf{n}} \otimes \hat{\mathbf{n}})$  we get the following:

$$(I - \hat{\mathbf{n}} \otimes \hat{\mathbf{n}}) \frac{\delta F}{\delta \hat{\mathbf{n}}} = \lambda(\mathbf{x}) [\hat{\mathbf{n}} - (\hat{\mathbf{n}} \cdot \hat{\mathbf{n}}) \hat{\mathbf{n}}] = 0 \quad (18)$$

where we have used the constraint on the left-hand side.

Below we calculate the functional derivative of  $F$ . This will simplify when we restrict the director to only polar-planar configurations. We do this one term at a time:

$$\begin{aligned} \delta(S^2) &= \int_{\Omega} 2S (\delta S) dV \\ &= \int_{\Omega} 2S (\nabla \cdot \delta \hat{\mathbf{n}}) dV \\ &= - \int_{\Omega} 2 (\nabla S) \cdot \delta \hat{\mathbf{n}} dV + \int_{\partial\Omega} 2 (S \boldsymbol{\nu}) \cdot \delta \hat{\mathbf{n}} dS \end{aligned} \quad (19)$$

$$\begin{aligned} \delta(T^2) &= \int_{\Omega} 2T (\delta T) dV \\ &= \int_{\Omega} 2T (\delta \hat{\mathbf{n}} \cdot (\nabla \times \hat{\mathbf{n}}) + \hat{\mathbf{n}} \cdot (\nabla \times \delta \hat{\mathbf{n}})) dV \\ &= \int_{\Omega} 4T (\nabla \times \hat{\mathbf{n}}) \cdot \delta \hat{\mathbf{n}} dV - \int_{\partial\Omega} 2T \boldsymbol{\nu} \cdot (\hat{\mathbf{n}} \times \delta \hat{\mathbf{n}}) dS \end{aligned} \quad (20)$$

where we have used the following identity<sup>2</sup>:

$$A \cdot (\nabla \times B) = -\nabla \cdot (A \times B) + B \cdot (\nabla \times A) \quad (21)$$

Also:

$$\begin{aligned} \delta |\mathbf{B}|^2 &= \int_{\Omega} 2\mathbf{B} \cdot (\delta \mathbf{B}) dV \\ &= \int_{\Omega} 2\mathbf{B} \cdot (\delta \hat{\mathbf{n}} \times (\nabla \times \hat{\mathbf{n}}) + \hat{\mathbf{n}} \times (\nabla \times \delta \hat{\mathbf{n}})) dV \\ &= \int_{\Omega} 2 [\delta \hat{\mathbf{n}} \cdot ((\nabla \times \hat{\mathbf{n}}) \times \mathbf{B}) + (\nabla \times \delta \hat{\mathbf{n}}) \cdot (\mathbf{B} \times \hat{\mathbf{n}})] dV \\ &= \int_{\Omega} 2 [\delta \hat{\mathbf{n}} \cdot ((\nabla \times \hat{\mathbf{n}}) \times \mathbf{B}) + \nabla \cdot (\delta \hat{\mathbf{n}} \times (\mathbf{B} \times \hat{\mathbf{n}})) + \delta \hat{\mathbf{n}} \cdot (\nabla \times (\mathbf{B} \times \hat{\mathbf{n}}))] dV \\ &= \int_{\Omega} 2 [\nabla \times (\mathbf{B} \times \hat{\mathbf{n}}) + (\nabla \times \hat{\mathbf{n}}) \times \mathbf{B}] \cdot \delta \hat{\mathbf{n}} dV + \int_{\partial\Omega} 2 [\boldsymbol{\nu} \cdot (\delta \hat{\mathbf{n}} \times (\mathbf{B} \times \hat{\mathbf{n}}))] dS \end{aligned} \quad (22)$$

where we have used the following identities:

$$A \cdot (B \times C) = C \cdot (A \times B) = B \cdot (C \times A) \quad (23)$$

and

$$\nabla \cdot (A \times B) = (\nabla \times A) \cdot B - (\nabla \times B) \cdot A \quad (24)$$

And finally, we look at the  $\Delta$  term:

$$\begin{aligned} \delta(\Delta_{ij}\Delta_{ji}) &= \int_{\Omega} 2\Delta_{ij}(\delta\Delta_{ij}) dV \\ &= \int_{\Omega} 2\Delta_{ij} [2\partial_i\delta n_j - 2\delta n_i n_k \partial_k n_j - 2n_i \delta n_k \partial_k n_j - 2n_i n_k \partial_k \delta n_j \\ &\quad + \delta n_i n_j \partial_k n_k + n_i \delta n_j \partial_k n_k + n_i n_j \partial_k \delta n_k] dV \\ &= \int_{\Omega} 2[-2\Delta_{ij}\delta n_i n_k \partial_k n_j - 2\Delta_{ij}n_i \delta n_k \partial_k n_j + \Delta_{ij}\delta n_i n_j \partial_k n_k + \Delta_{ij}n_i \delta n_j \partial_k n_k \\ &\quad + 2\Delta_{ij}\partial_i \delta n_j - 2\Delta_{ij}n_i n_k \partial_k \delta n_j + \Delta_{ij}n_i n_j \partial_k \delta n_k] dV \\ &= \int_{\Omega} 2[-2\Delta_{kj}n_i \partial_i n_j - 2\Delta_{ij}n_i \partial_k n_j + \Delta_{kj}n_j \partial_i n_i + \Delta_{ik}n_i \partial_j n_j] \delta n_k dV \\ &\quad + \int_{\Omega} 2[-2\partial_i \Delta_{ik} + 2\partial_j (\Delta_{ik}n_i n_j) - \partial_k (\Delta_{ij}n_i n_j)] \delta n_k dV \\ &\quad + \int_{\partial\Omega} 2[2\Delta_{ij}\nu_i \delta n_j - 2\Delta_{ij}n_i n_k \nu_k \delta n_j + \Delta_{ij}n_i n_j \nu_k \delta n_k] dV \end{aligned} \quad (25)$$

For now, we assume that the boundaries are fixed so that the surface terms vanish. Putting all of these terms together gives the following Euler-Lagrange equation:

$$\begin{aligned} 0 = (I - \hat{\mathbf{n}} \otimes \hat{\mathbf{n}}) \Bigg[ &-(K_{11} - K_{24}) \nabla S \\ &+ 2(K_{22} - K_{24}) T(\nabla \times \hat{\mathbf{n}}) \\ &+ K_{33} [\nabla \times (\mathbf{B} \times \hat{\mathbf{n}}) + (\nabla \times \hat{\mathbf{n}}) \times \mathbf{B}] \\ &+ 4K_{24} [\Delta \cdot \hat{\mathbf{n}} (\nabla \cdot \hat{\mathbf{n}}) - (\hat{\mathbf{n}} \cdot \nabla \hat{\mathbf{n}}) \cdot \Delta - (\nabla \hat{\mathbf{n}}) \cdot \Delta \cdot \hat{\mathbf{n}} \\ &\quad - \nabla \cdot \Delta + \nabla \cdot (\hat{\mathbf{n}} \otimes (\hat{\mathbf{n}} \cdot \Delta)) - \frac{1}{2} \nabla (\hat{\mathbf{n}} \cdot \Delta \cdot \hat{\mathbf{n}})] \Bigg] \end{aligned} \quad (26)$$

The idea here is to look at a general expression for a twisted planar configuration:

$$\hat{\mathbf{n}}' = R(\alpha z) \begin{bmatrix} \cos(\theta(x', y')) \\ \sin(\theta(x', y')) \\ 0 \end{bmatrix} \quad (27)$$

with

$$\begin{aligned} x' &= \cos(\alpha z)x + \sin(\alpha z)y \\ y' &= -\sin(\alpha z)x + \cos(\alpha z)y \end{aligned} \quad (28)$$

If we plug into eq. (26) and set  $z = 0$  we will get a PDE in  $x$  and  $y$ . Imposing homeotropic boundary conditions gives us a minimum-energy configuration for a fixed  $\alpha$ . Presumably we will have to solve this perturbatively with a regular and non-regular part. The non-regular part will have to be the two-defect configuration separated by a distance  $d$ . We may map out the free energy landscape for these two parameters, at the very least.

## 5 Bend-Splay Euler-Lagrange, as a check

To check our calculation, we just consider Bend-Splay terms. Taking  $\epsilon = (K_{33} - K_{11})/(K_{33} + K_{11})$  gives:

$$(I - \hat{\mathbf{n}} \otimes \hat{\mathbf{n}}) \left[ -(1 + \epsilon) \nabla S + (1 - \epsilon) [\nabla \times (\mathbf{B} \times \hat{\mathbf{n}}) + (\nabla \times \hat{\mathbf{n}}) \times \mathbf{B}] \right] = 0 \quad (29)$$

We calculate each term separately:

$$\nabla S - (\hat{\mathbf{n}} \cdot \nabla S) \hat{\mathbf{n}} \quad (30)$$

$$\hat{\mathbf{n}} \cdot \nabla \times (\mathbf{B} \times \hat{\mathbf{n}}) = \nabla \cdot (\hat{\mathbf{n}} \times (\mathbf{B} \times \hat{\mathbf{n}})) + (\nabla \times \hat{\mathbf{n}}) \cdot (\mathbf{B} \times \hat{\mathbf{n}}) \quad (31)$$

$$\begin{aligned} \hat{\mathbf{n}} \cdot [(\nabla \times \hat{\mathbf{n}}) \times \mathbf{B}] &= (\nabla \times \hat{\mathbf{n}}) \cdot (\mathbf{B} \times \hat{\mathbf{n}}) \\ &= (\nabla \times \hat{\mathbf{n}}) \cdot ((\hat{\mathbf{n}} \times (\nabla \times \hat{\mathbf{n}})) \times \hat{\mathbf{n}}) \\ &= (\nabla \times \hat{\mathbf{n}}) \cdot ((-\hat{\mathbf{n}} \cdot \nabla) \hat{\mathbf{n}} \times \hat{\mathbf{n}}) \end{aligned} \quad (32)$$

## 6 Simplified free energy

### 6.1 Free energy and Euler-Lagrange equation

For sake of ease, we assume  $K_{24} = 0$  (in an infinite system we assume it does not matter) and  $K_{11} = K_{33} = K$ . We take  $\zeta$  to be our twist elastic constant:

$$\zeta = \frac{K - K_{22}}{K + K_{22}} \quad (33)$$

This gives:

$$K_{22} = K \frac{1 - \zeta}{1 + \zeta} \quad (34)$$

Then the free energy is given by:

$$F = \int_{\Omega} (1 + \zeta) S^2 + (1 - \zeta) T^2 + (1 + \zeta) |\mathbf{B}|^2 dV \quad (35)$$

We may plug in for a planar  $\hat{\mathbf{n}}$  to get an expression in terms of  $\theta$ . Calculating explicitly gives:

$$F = \int_{\Omega} (1 + \zeta) |\nabla \theta|^2 - 2\zeta \theta_z^2 dV \quad (36)$$

The differential is:

$$\begin{aligned} \delta F &= \int_{\Omega} 2(1 + \zeta) (\nabla \theta) \cdot (\nabla \delta \theta) - 4\zeta \left( \frac{d\theta}{dz} \right) \left( \frac{d\delta \theta}{dz} \right) dV \\ &= \int_{\Omega} 2(1 + \zeta) [\nabla \cdot (\delta \theta \nabla \theta) - (\nabla^2 \theta) \delta \theta] - 4\zeta \left[ \frac{d}{dz} \left( \delta \theta \frac{d\theta}{dz} \right) - \left( \frac{d^2 \theta}{dz^2} \right) \delta \theta \right] dV \\ &= \int_{\Omega} -2 \left[ (1 + \zeta) \nabla^2 \theta - 2\zeta \frac{d^2 \theta}{dz^2} \right] \delta \theta dV \end{aligned} \quad (37)$$

where we have assumed that the variation goes to zero at all the boundaries. Then the Euler-Lagrange equation reads:

$$(1 + \zeta) \nabla^2 \theta - 2\zeta \frac{d^2 \theta}{dz^2} = 0 \quad (38)$$

## 6.2 Constant twist angular velocity configuration

We now consider a director given by:

$$\theta(x, y, z) = \theta(x', y') + \alpha z \quad (39)$$

where

$$\begin{aligned} x' &= \cos(\alpha z)x + \sin(\alpha z)y \\ y' &= -\sin(\alpha z)x + \cos(\alpha z)y \end{aligned} \quad (40)$$

We calculate this explicitly as follows:

$$\frac{\partial \theta}{\partial x} = \frac{\partial \theta}{\partial x'} \frac{\partial x'}{\partial x} + \frac{\partial \theta}{\partial y'} \frac{\partial y'}{\partial x} = \frac{\partial \theta}{\partial x'} \cos(\alpha z) - \frac{\partial \theta}{\partial y'} \sin(\alpha z) \quad (41)$$

so that

$$\frac{\partial^2 \theta}{\partial x^2} = \frac{\partial^2 \theta}{\partial x'^2} \cos^2(\alpha z) - 2 \frac{\partial^2 \theta}{\partial x' \partial y'} \cos(\alpha z) \sin(\alpha z) + \frac{\partial^2 \theta}{\partial y'^2} \sin^2(\alpha z) \quad (42)$$

similarly for  $y$ :

$$\frac{\partial^2 \theta}{\partial y^2} = \frac{\partial^2 \theta}{\partial x'^2} \sin^2(\alpha z) + 2 \frac{\partial^2 \theta}{\partial x' \partial y'} \cos(\alpha z) \sin(\alpha z) + \frac{\partial^2 \theta}{\partial y'^2} \cos^2(\alpha z) \quad (43)$$

and finally:

$$\frac{\partial \theta}{\partial z} = \frac{\partial \theta}{\partial x'} \frac{\partial x'}{\partial z} + \frac{\partial \theta}{\partial y'} \frac{\partial y'}{\partial z} = \frac{\partial \theta}{\partial x'} \alpha y' - \frac{\partial \theta}{\partial y'} \alpha x' \quad (44)$$

so that:

$$\begin{aligned} \frac{\partial^2 \theta}{\partial z^2} &= \frac{\partial^2 \theta}{\partial x' \partial z} \alpha y' + \frac{\partial \theta}{\partial x'} \alpha \frac{\partial y'}{\partial z} - \frac{\partial^2 \theta}{\partial y' \partial z} \alpha x' - \frac{\partial \theta}{\partial y'} \alpha \frac{\partial x'}{\partial z} \\ &= \frac{\partial^2 \theta}{\partial x'^2} \alpha^2 y'^2 - \frac{\partial^2 \theta}{\partial x' \partial y'} \alpha^2 y' x' - \frac{\partial \theta}{\partial x'} \alpha^2 x' + \frac{\partial^2 \theta}{\partial y'^2} \alpha^2 x'^2 - \frac{\partial^2 \theta}{\partial y' \partial x'} \alpha^2 x' y' - \frac{\partial \theta}{\partial y'} \alpha^2 y' \end{aligned} \quad (45)$$

For an infinite system with cylindrical symmetry, every  $z$ -axis is the same, so we consider the slice for  $z = 0$ . Altogether the Euler-Lagrange equation reads:

$$(1 + \zeta) \nabla^2 \theta + (1 - \zeta) \alpha^2 (\mathbf{x} \times \nabla)^2 \theta = 0 \quad (46)$$

where here  $\nabla = \frac{\partial}{\partial x} \hat{\mathbf{x}} + \frac{\partial}{\partial y} \hat{\mathbf{y}}$  and  $\mathbf{x} = x \hat{\mathbf{x}} + y \hat{\mathbf{y}}$ . We may decompose  $\theta$  into  $\theta_{\text{iso}} + \theta_c$  where  $\theta_{\text{iso}} = \frac{1}{2}(\varphi_1 + \varphi_2)$  with  $\varphi_1, \varphi_2$  the polar coordinates centered at  $(\pm \frac{d}{2}, 0)$  and  $\theta_c$  is a regular correction. Note that  $d$  is the spacing of the two  $+1/2$  disclinations. Since  $\nabla^2 \theta_{\text{iso}} = 0$  this gives the following linear equation for  $\theta_c$ :

$$\left[ (1 + \zeta) \nabla^2 + (1 - \zeta) \alpha^2 (\mathbf{x} \times \nabla)^2 \right] \theta_c = -(1 - \zeta) \alpha^2 (\mathbf{x} \times \nabla)^2 \theta_{\text{iso}} \quad (47)$$

## 6.3 Constant twist weak form

The  $(\mathbf{x} \times \nabla)$  operator also has a nice product rule<sup>4</sup>. Also note that, in two dimensions, it has a nice integration formula<sup>5</sup>. Taking the inner product with some test function  $\eta$  then yields the following weak form:

$$(1 + \zeta) \langle \eta, \nabla^2 \theta_c \rangle + (1 - \zeta) \alpha^2 \langle \eta, (\mathbf{x} \times \nabla)^2 \theta_c \rangle = -(1 - \zeta) \alpha^2 \langle \eta, (\mathbf{x} \times \nabla)^2 \theta_{\text{iso}} \rangle \quad (48)$$

which finally yields:

$$\begin{aligned} &-(1 + \zeta) \langle \nabla \eta, \nabla \theta_c \rangle \\ &-(1 - \zeta) \alpha^2 \langle (\mathbf{x} \times \nabla) \eta, (\mathbf{x} \times \nabla) \theta_c \rangle = (1 - \zeta) \alpha^2 \langle (\mathbf{x} \times \nabla) \eta, (\mathbf{x} \times \nabla) \theta_{\text{iso}} \rangle \\ &\quad - (1 + \zeta) \langle \eta, \boldsymbol{\nu} \cdot \nabla \theta_c \rangle_{\partial \Omega} \\ &\quad - (1 - \zeta) \alpha^2 \langle \eta, (\mathbf{x} \times \boldsymbol{\nu}) (\mathbf{x} \times \nabla) \theta_c \rangle_{\partial \Omega} \end{aligned} \quad (49)$$

## 6.4 Variable twist angular velocity

Here we assume a director configuration whose twist angular velocity  $\alpha$  is a function of  $z$ . In this case, the  $x$ - and  $y$ -derivatives are unchanged, but the  $z$  derivatives vary considerably:

$$\frac{\partial \theta}{\partial z} = \frac{\partial \theta}{\partial x'}(\alpha + z\alpha')y' - \frac{\partial \theta}{\partial y'}(\alpha + z\alpha')x' \quad (50)$$

and then

$$\begin{aligned} \frac{\partial^2 \theta}{\partial z^2} &= \frac{\partial^2 \theta}{\partial x'^2}(\alpha + z\alpha')^2 y'^2 - \frac{\partial^2 \theta}{\partial x' \partial y'}(\alpha + z\alpha')^2 y'x' + \frac{\partial \theta}{\partial x'}(2\alpha' + z\alpha'')y' - \frac{\partial \theta}{\partial x'}(\alpha + z\alpha')^2 x' \\ &\quad + \frac{\partial^2 \theta}{\partial y'^2}(\alpha + z\alpha')^2 x'^2 - \frac{\partial^2 \theta}{\partial y' \partial x'}(\alpha + z\alpha')^2 x'y' - \frac{\partial \theta}{\partial y'}(2\alpha' + z\alpha'')x' - \frac{\partial \theta}{\partial y'}(\alpha + z\alpha')^2 y' \end{aligned} \quad (51)$$

Finally we have:

$$\frac{\partial^2}{\partial z^2} \alpha z = \frac{\partial}{\partial z} [\alpha' z + \alpha] = \alpha'' z + 2\alpha' \quad (52)$$

## Notes

<sup>1</sup> Suppose  $\mathbf{v}(\mathbf{x})$  is a vector field. Take  $L$  to be a linear transformation. We would like to act on  $\mathbf{v}$  by  $L$  in an *active* way. This means that, if  $L$  rotates a plane by some angle  $\theta$ , then we are imagining taking  $\mathbf{v}$  (say on a piece of paper) and rotating the whole thing by the angle  $\theta$ . There's two pieces to this: i) is that we must act on each of the vectors outputted by  $\mathbf{v}$  by  $L$  (again, think of rotating a vector field printed on a piece of paper). ii) is that, if we want to get the correct vector field at  $\mathbf{x}$ , we must actually sample  $\mathbf{v}$  at a point  $L^{-1}\mathbf{x}$ . This is because  $L^{-1}\mathbf{x}$  is the point that will get mapped to  $\mathbf{x}$  by  $L$ .

<sup>2</sup>

$$\begin{aligned} A \cdot (\nabla \times B) &= A_i \epsilon_{ijk} \partial_j B_k \\ &= \epsilon_{ijk} (\partial_j (A_i B_k) - B_k \partial_j A_i) \\ &= -\partial_j (\epsilon_{jik} A_i B_k) + B_k \epsilon_{kji} \partial_j A_i \\ &= -\nabla \cdot (A \times B) + B \cdot (\nabla \times A) \end{aligned} \quad (53)$$

<sup>3</sup>

$$\begin{aligned} (\mathbf{x} \times \nabla)^2 &= \left( x \frac{\partial}{\partial y} - y \frac{\partial}{\partial x} \right) \left( x \frac{\partial}{\partial y} - y \frac{\partial}{\partial x} \right) \\ &= \left( x^2 \frac{\partial}{\partial y^2} - x \frac{\partial}{\partial x} - xy \frac{\partial}{\partial y} \frac{\partial}{\partial x} - y \frac{\partial}{\partial y} - yx \frac{\partial}{\partial x} \frac{\partial}{\partial y} + y^2 \frac{\partial}{\partial x^2} \right) \end{aligned} \quad (54)$$

<sup>4</sup>

$$\begin{aligned} (\mathbf{x} \times \nabla)(fg) &= \left( x \frac{\partial}{\partial y} - y \frac{\partial}{\partial x} \right) (fg) \\ &= x \left( g \frac{\partial f}{\partial y} + f \frac{\partial g}{\partial y} \right) - y \left( g \frac{\partial f}{\partial x} + f \frac{\partial g}{\partial x} \right) \\ &= g \left( x \frac{\partial f}{\partial y} - y \frac{\partial f}{\partial x} \right) + f \left( x \frac{\partial g}{\partial y} - y \frac{\partial g}{\partial x} \right) \\ &= g(\mathbf{x} \times \nabla)f + f(\mathbf{x} \times \nabla)g \end{aligned} \quad (55)$$

<sup>5</sup> We first rewrite the operator as a divergence:  $(\mathbf{x} \times \nabla)f = \nabla \cdot \mathbf{g}$  with  $\mathbf{g} = f[-y \ x]^T$ . Then we may explicitly calculate the integration formula using the divergence theorem:

$$\begin{aligned} \int_{\Omega} (\mathbf{x} \times \nabla) f dV &= \int_{\Omega} \nabla \cdot \mathbf{g} dV \\ &= \int_{\partial \Omega} (\hat{\nu} \cdot \mathbf{g}) dS \\ &= \int_{\partial \Omega} f(-\nu_x y + \nu_y x) dS \\ &= \int_{\partial \Omega} f(\mathbf{x} \times \hat{\nu}) dS \end{aligned} \quad (56)$$

Then the simplified Euler-Lagrange equation is:

$$0 = -(1 + \zeta)\nabla S + 2(1 - \zeta)T (\nabla \times \hat{\mathbf{n}}) + (1 + \zeta) [\nabla \times (\mathbf{B} \times \hat{\mathbf{n}}) + (\nabla \times \hat{\mathbf{n}}) \times \mathbf{B}] \quad (57)$$