

Double helix director

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1 Selinger free energy

To investigate this system, we start with the Frank free energy as written by Selinger:

$$F = \frac{1}{2} (K_{11} - K_{24}) S^2 + \frac{1}{2} (K_{22} - K_{24}) T^2 + \frac{1}{2} K_{33} |\mathbf{B}|^2 + K_{24} \text{Tr} (\Delta^2) \quad (1)$$

with the following definitions for the distortion modes:

$$S = \nabla \cdot \hat{\mathbf{n}} \quad (2)$$

$$T = \hat{\mathbf{n}} \cdot (\nabla \times \hat{\mathbf{n}}) \quad (3)$$

$$B = \hat{\mathbf{n}} \times (\nabla \times \hat{\mathbf{n}}) \quad (4)$$

$$\begin{aligned} \Delta_{ij} = \frac{1}{2} [& \partial_i n_j + \partial_j n_i \\ & - n_i n_k \partial_k n_j - n_j n_k \partial_k n_i \\ & - \delta_{ij} \partial_k n_k + n_i n_j \partial_k n_k] \end{aligned} \quad (5)$$

2 Rotated system

We make two assumptions about the system: i) the z -dependence of the director corresponds to a rotation of a plane perpendicular to the cylindrical axis about the cylindrical axis by some angle αz , and ii) the director stays in a plane perpendicular to the cylindrical axis. We note that in an infinitely long cylindrical system, i) is true by translational symmetry. In this case, we may write:

$$\hat{\mathbf{n}} = R(\alpha z) [\cos \theta \quad \sin \theta \quad 0]^T \quad (6)$$

for some director angle θ as measured from the x -axis in the x - y -plane, and $R(z)$ a rotation about the z -axis and a function of z . We note that θ must be a function of x , y , and z , with the z -dependence corresponding to an *inverse* rotation of angle αz about the z -axis.¹ This gives:

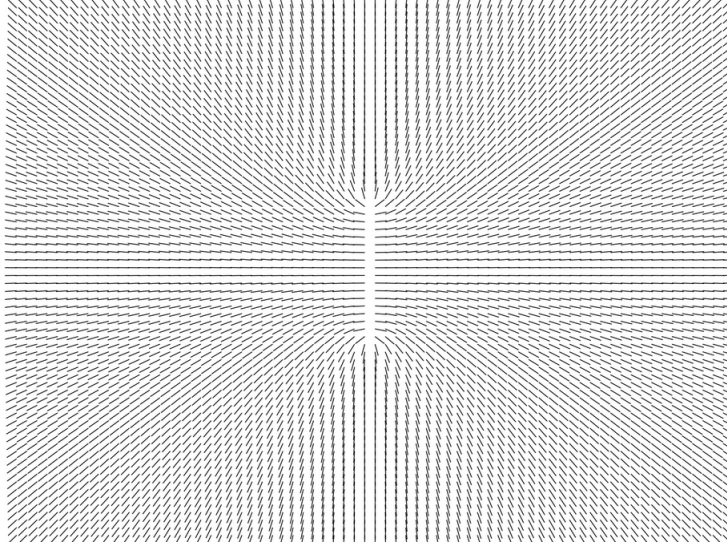
$$\begin{aligned} \begin{bmatrix} x' \\ y' \end{bmatrix} &= R^T(\alpha z) \begin{bmatrix} x \\ y \end{bmatrix} \\ &= \begin{bmatrix} \cos(\alpha z) x + \sin(\alpha z) y \\ -\sin(\alpha z) x + \cos(\alpha z) y \end{bmatrix} \end{aligned} \quad (7)$$

3 Rotated isotropic solution free energy

Taking θ to be the standard isotropic solution for two $+1/2$ disclinations gives:

$$\begin{aligned}\theta(x', y') &= \frac{1}{2} \tan^{-1} \left(\frac{y'}{x' - \frac{d}{2}} \right) + \frac{1}{2} \tan^{-1} \left(\frac{y'}{x' + \frac{d}{2}} \right) \\ &= \frac{1}{2} \tan^{-1} \left(\frac{-\sin(\alpha z) x + \cos(\alpha z) y}{\cos(\alpha z) x + \sin(\alpha z) y - \frac{d}{2}} \right) + \frac{1}{2} \tan^{-1} \left(\frac{-\sin(\alpha z) x + \cos(\alpha z) y}{\cos(\alpha z) x + \sin(\alpha z) y + \frac{d}{2}} \right)\end{aligned}\tag{8}$$

where here d is the disclination spacing. The result of plotting $\theta + \alpha z$ for $\alpha z = \pi/2$ gives the following rotated configuration:



One may explicitly calculate the free energy density for such a configuration. By symmetry, the free energy density at every z -value should be the same, so we evaluate at $z = 0$ to simplify the expressions. What we find is that (expectedly) only the twist and saddle splay terms depend on α . These give:

$$T^2(\alpha) = \alpha^2 f(x, y) \cos^4 \theta \tag{9}$$

$$|\Delta|^2(\alpha) = \alpha^2 f(x, y) + g(x, y) \tag{10}$$

with

$$f(x, y) = \frac{d^2 (d^2 - 4x^2 + 4y^2)^2}{(d^4 - 8d^2x^2 + 8d^2y^2 + 16x^4 + 32x^2y^2 + 16y^4)^2} \tag{11}$$

and $g(x, y)$ some function independent of α . Then the entire free energy goes as:

$$F = (K_{22} + (B - A)K_{24}) \alpha^2 + C \tag{12}$$

with

$$\begin{aligned}B &= \int_{\Omega} f(x, y) dV \\ A &= \int_{\Omega} f(x, y) \cos^4 \theta dV\end{aligned}\tag{13}$$

Clearly $B > A$ always, and so a twisted configuration will never be the minimum, at least for the configuration that we've written down.

4 Selinger Euler-Lagrange equation

We begin by calculating the general Euler-Lagrange equation for the Frank free energy with all terms. This will simplify when we restrict the director to only polar-planar configurations. We do this one term at a time:

$$\begin{aligned}
\delta(S^2) &= \int_{\Omega} 2S (\delta S) dV \\
&= \int_{\Omega} 2S (\nabla \cdot \delta \hat{\mathbf{n}}) dV \\
&= - \int_{\Omega} 2 (\nabla S) \cdot \delta \hat{\mathbf{n}} dV + \int_{\partial\Omega} 2 (S \boldsymbol{\nu}) \cdot \delta \hat{\mathbf{n}} dS
\end{aligned} \tag{14}$$

$$\begin{aligned}
\delta(T^2) &= \int_{\Omega} 2T (\delta T) dV \\
&= \int_{\Omega} 2T (\delta \hat{\mathbf{n}} \cdot (\nabla \times \hat{\mathbf{n}}) + \hat{\mathbf{n}} \cdot (\nabla \times \delta \hat{\mathbf{n}})) dV \\
&= \int_{\Omega} 4T (\nabla \times \hat{\mathbf{n}}) \cdot \delta \hat{\mathbf{n}} dV - \int_{\partial\Omega} 2T \boldsymbol{\nu} \cdot (\hat{\mathbf{n}} \times \delta \hat{\mathbf{n}}) dS
\end{aligned} \tag{15}$$

where we have used the following identity²:

$$A \cdot (\nabla \times B) = -\nabla \cdot (A \times B) + B \cdot (\nabla \times A) \tag{16}$$

Also:

$$\begin{aligned}
\delta |\mathbf{B}|^2 &= \int_{\Omega} 2\mathbf{B} \cdot (\delta \mathbf{B}) dV \\
&= \int_{\Omega} 2\mathbf{B} \cdot (\delta \hat{\mathbf{n}} \times (\nabla \times \hat{\mathbf{n}}) + \hat{\mathbf{n}} \times (\nabla \times \delta \hat{\mathbf{n}})) dV \\
&= \int_{\Omega} 2 [\delta \hat{\mathbf{n}} \cdot ((\nabla \times \hat{\mathbf{n}}) \times \mathbf{B}) + (\nabla \times \delta \hat{\mathbf{n}}) \cdot (\mathbf{B} \times \hat{\mathbf{n}})] dV \\
&= \int_{\Omega} 2 [\delta \hat{\mathbf{n}} \cdot ((\nabla \times \hat{\mathbf{n}}) \times \mathbf{B}) + \nabla \cdot (\delta \hat{\mathbf{n}} \times (\mathbf{B} \times \hat{\mathbf{n}})) + \delta \hat{\mathbf{n}} \cdot (\nabla \times (\mathbf{B} \times \hat{\mathbf{n}}))] dV \\
&= \int_{\Omega} 2 [\nabla \times (\mathbf{B} \times \hat{\mathbf{n}}) + (\nabla \times \hat{\mathbf{n}}) \times \mathbf{B}] \cdot \delta \hat{\mathbf{n}} dV + \int_{\partial\Omega} 2 [\boldsymbol{\nu} \cdot (\delta \hat{\mathbf{n}} \times (\mathbf{B} \times \hat{\mathbf{n}}))] dS
\end{aligned} \tag{17}$$

where we have used the following identities:

$$A \cdot (B \times C) = C \cdot (A \times B) = B \cdot (C \times A) \tag{18}$$

and

$$\nabla \cdot (A \times B) = (\nabla \times A) \cdot B - (\nabla \times B) \cdot A \tag{19}$$

And finally, we look at the Δ term:

$$\begin{aligned}
\delta(\Delta_{ij}\Delta_{ji}) &= \int_{\Omega} 2\Delta_{ij}(\delta\Delta_{ij}) dV \\
&= \int_{\Omega} 2\Delta_{ij} [2\partial_i\delta n_j - 2\delta n_i n_k \partial_k n_j - 2n_i \delta n_k \partial_k n_j - 2n_i n_k \partial_k \delta n_j \\
&\quad + \delta n_i n_j \partial_k n_k + n_i \delta n_j \partial_k n_k + n_i n_j \partial_k \delta n_k] dV \\
&= \int_{\Omega} 2[-2\Delta_{ij}\delta n_i n_k \partial_k n_j - 2\Delta_{ij}n_i \delta n_k \partial_k n_j + \Delta_{ij}\delta n_i n_j \partial_k n_k + \Delta_{ij}n_i \delta n_j \partial_k n_k \\
&\quad 2\Delta_{ij}\partial_i \delta n_j - 2\Delta_{ij}n_i n_k \partial_k \delta n_j + \Delta_{ij}n_i n_j \partial_k \delta n_k] dV \quad (20) \\
&= \int_{\Omega} 2[-2\Delta_{kj}n_i \partial_i n_j - 2\Delta_{ij}n_i \partial_k n_j + \Delta_{kj}n_j \partial_i n_i + \Delta_{ik}n_i \partial_j n_j] \delta n_k dV \\
&\quad + \int_{\Omega} 2[-2\partial_i \Delta_{ik} + 2\partial_j (\Delta_{ik}n_i n_j) - \partial_k (\Delta_{ij}n_i n_j)] \delta n_k dV \\
&\quad + \int_{\partial\Omega} 2[2\Delta_{ij}\nu_i \delta n_j - 2\Delta_{ij}n_i n_k \nu_k \delta n_j + \Delta_{ij}n_i n_j \nu_k \delta n_k] dV
\end{aligned}$$

For now, we assume that the boundaries are fixed so that the surface terms vanish. Putting all of these terms together gives the following Euler-Lagrange equation:

$$\begin{aligned}
0 = & -(K_{11} - K_{24}) \nabla S \\
& + 2(K_{22} - K_{24}) T (\nabla \times \hat{\mathbf{n}}) \\
& + K_{33} [\nabla \times (\mathbf{B} \times \hat{\mathbf{n}}) + (\nabla \times \hat{\mathbf{n}}) \times \mathbf{B}] \\
& + 4K_{24} [\Delta \cdot \hat{\mathbf{n}} (\nabla \cdot \hat{\mathbf{n}}) - (\hat{\mathbf{n}} \cdot \nabla \hat{\mathbf{n}}) \cdot \Delta - (\nabla \hat{\mathbf{n}}) \cdot \Delta \cdot \hat{\mathbf{n}} \\
& - \nabla \cdot \Delta + \nabla \cdot (\hat{\mathbf{n}} \otimes (\hat{\mathbf{n}} \cdot \Delta)) - \frac{1}{2} \nabla (\hat{\mathbf{n}} \cdot \Delta \cdot \hat{\mathbf{n}})] \quad (21)
\end{aligned}$$

The idea here is to look at a general expression for a twisted planar configuration:

$$\hat{\mathbf{n}}' = R(\alpha z) \begin{bmatrix} \cos(\theta(x', y')) \\ \sin(\theta(x', y')) \\ 0 \end{bmatrix} \quad (22)$$

with

$$\begin{aligned}
x' &= \cos(\alpha z)x + \sin(\alpha z)y \\
y' &= -\sin(\alpha z)x + \cos(\alpha z)y \quad (23)
\end{aligned}$$

If we plug into eq. (21) and set $z = 0$ we will get a PDE in x and y . Imposing homeotropic boundary conditions gives us a minimum-energy configuration for a fixed α . Presumably we will have to solve this perturbatively with a regular and non-regular part. The non-regular part will have to be the two-defect configuration separated by a distance d . We may map out the free energy landscape for these two parameters, at the very least.

5 Simplified free energy

For sake of ease, we assume $K_{24} = 0$ (in an infinite system we assume it does not matter) and $K_{11} = K_{33} = K$. We take ζ to be our twist elastic constant:

$$\zeta = \frac{K - K_{22}}{K + K_{22}} \quad (24)$$

This gives:

$$K_{22} = K \frac{1 - \zeta}{1 + \zeta} \quad (25)$$

Then the simplified Euler-Lagrange equation is:

$$0 = -(1 + \zeta) \nabla S + 2(1 - \zeta) T (\nabla \times \hat{\mathbf{n}}) + (1 + \zeta) [\nabla \times (\mathbf{B} \times \hat{\mathbf{n}}) + (\nabla \times \hat{\mathbf{n}}) \times \mathbf{B}] \quad (26)$$

Notes

¹ Suppose $\mathbf{v}(\mathbf{x})$ is a vector field. Take L to be a linear transformation. We would like to act on \mathbf{v} by L in an *active* way. This means that, if L rotates a plane by some angle θ , then we are imagining taking \mathbf{v} (say on a piece of paper) and rotating the whole thing by the angle θ . There's two pieces to this: i) is that we must act on each of the vectors outputted by \mathbf{v} by L (again, think of rotating a vector field printed on a piece of paper). ii) is that, if we want to get the correct vector field at \mathbf{x} , we must actually sample \mathbf{v} at a point $L^{-1}\mathbf{x}$. This is because $L^{-1}\mathbf{x}$ is the point that will get mapped to \mathbf{x} by L .

2

$$\begin{aligned}
 A \cdot (\nabla \times B) &= A_i \epsilon_{ijk} \partial_j B_k \\
 &= \epsilon_{ijk} (\partial_j (A_i B_k) - B_k \partial_j A_i) \\
 &= -\partial_j (\epsilon_{jik} A_i B_k) + B_k \epsilon_{kji} \partial_j A_i \\
 &= -\nabla \cdot (A \times B) + B \cdot (\nabla \times A)
 \end{aligned} \tag{27}$$