

KINEMATIC MODELLING AND ANALYSIS OF 5 DOF ROBOTIC ARM

VIVEK DESHPANDE¹ & P M GEORGE²

¹Associate Professor, Mechanical Engineering, G H Patel College of Engineering & Technology,
Vallabh Vidyanagar, Anand, Gujarat, India

²Professor & Head, Mechanical Engineering, Birla Vishwakarma Mahavidyalaya College of Engineering,
Vallabh Vidyanagar, Anand, Gujarat, India

ABSTRACT

The control of a robotic arm has been a challenge since earlier days of robots. The kinematics problem is defined as the transformation from the Cartesian space to the joint space and vice versa. This paper aims to model the forward and inverse kinematics of a 5 DOF Robotic Arm for simple pick and place application. A general D-H representation of forward and inverse matrix is obtained. An analytical solution for the forward and inverse kinematics of 5 DOF robotic arm presented, to analyze the movement of arm from one point in space to another point. The 5 DOF robotic arm is a vertical articulated robot, with five revolute joints. It is a dependable and safe robotic system designed for educational purpose. This versatile system allows students to gain theoretical and practical experience in robotics, automation and control systems.

KEYWORDS: Forward Kinematics, Inverse Kinematics, Robotic Arm

INTRODUCTION

The mathematical modeling of robot kinematics is motivated by the complexity of robotic systems, which possess highly nonlinear characteristics. Inverse kinematics modeling has been one of the main problems in robotics research. The most popular method for controlling robotic arms is still based on look-up tables that are usually designed in a manual manner [1-4].

The kinematics solution of any robot manipulator consists of two sub problems forward and inverse kinematics. Forward kinematics will determine where the robot's manipulator hand will be if all joints are known whereas inverse kinematics will calculate what each joint variable must be if the desired position and orientation of end-effector is determined. Hence Forward kinematics is defined as transformation from joint space to Cartesian space whereas Inverse kinematics is defined as transformation from Cartesian space to joint space. General methods do exist for solving forward kinematics [5-8]. The objective in this paper is to present an analytical solution for the forward and inverse kinematics of 5 DOF robotic arm, to analyze the movement of arm from one point in space to another point.

KINEMATIC MODEL OF 5 DOF ROBOTIC ARM

For the research work, 5 DOF Robotic Arm was selected. It is a vertical articulated robot, with five revolute joints. It has a stationary base, shoulder, elbow, tool pitch and tool roll. This simple block diagram indicates the relationship between direct and inverse kinematics problem as shown in Figure 1a. Figure 1b indicates robot arm links. The coordinate frame assignment is shown in Figure 2.

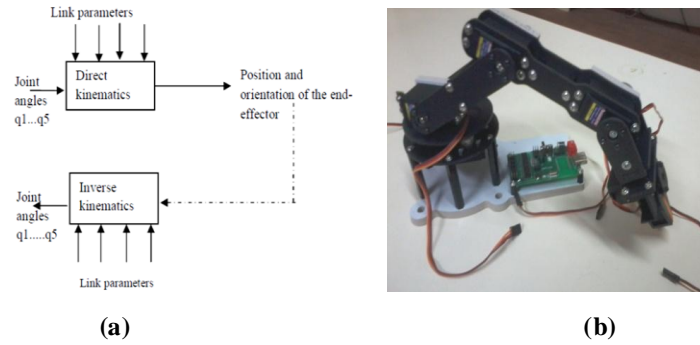


Figure 1(a): Forward and Inverse Kinematics Model; (b) Robot Arm Links

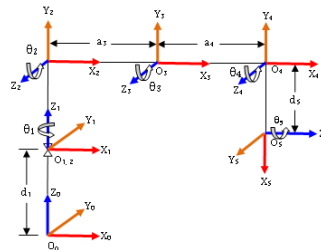


Figure 2: Coordinate Frame Assignment

FORWARD AND INVERSE KINEMATIC ANALYSIS OF 5 DOF ROBOTIC ARM

Forward Kinematic Analysis

In this study, the standard Denavit-Hartenberg (DH) [9] convention and methodology are used to derive its kinematics. Denavit-Hartenberg algorithm helps to find the position and orientation of end-effector with respect to base. Totally 20 Parameters are involved in 5- DOF robotic arm design as shown in Table 1.

Table 1: D-H Parameter for 5 DOF Robotic Arm

Joint i	Type	α_i (deg)	a_i (mm)	d_i (mm)	θ_i (deg)
1	Base	0	0	86	θ_1
2	Shoulder	90	0	0	θ_2
3	Elbow	0	96	0	θ_3
4	Wrist	0	96	0	θ_4
5	Gripper	90	0	59.5	θ_5

Based on the DH convention, the transformation matrix from joint i to joint i+1 is given by:

$${}^{i-1}T_i = \begin{bmatrix} C\theta_i & -S\theta_i C\alpha_i & S\theta_i S\alpha_i & a_i C\theta_i \\ S\theta_i & C\theta_i C\alpha_i & -C\theta_i S\alpha_i & a_i S\theta_i \\ 0 & S\alpha_i & C\alpha_i & d_i \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad (1)$$

where, $S\theta_i = \sin \theta_i$, $C\theta_i = \cos \theta_i$, $S\alpha_i = \sin \alpha_i$, $C\alpha_i = \cos \alpha_i$, $S_{ijk} = \sin(\theta_i + \theta_j + \theta_k)$, $C_{ijk} = \cos(\theta_i + \theta_j + \theta_k)$

$${}^0T_1 = \begin{bmatrix} c_1 & -s_1 & 0 & 0 \\ s_1 & c_1 & 0 & 0 \\ 0 & 0 & 1 & d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad (2)$$

$${}^0T_2 = \begin{bmatrix} c_2 & 0 & s_2 & 0 \\ s_2 & 0 & -c_2 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad (3)$$

$${}^2T_3 = \begin{bmatrix} c_3 & -s_3 & 0 & a_3 * c_3 \\ s_3 & c_3 & 0 & a_3 * s_3 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad (4)$$

$${}^3T_4 = \begin{bmatrix} c_4 & -s_4 & 0 & a_4 * c_4 \\ s_4 & c_4 & 0 & a_4 * s_4 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad (5)$$

$${}^4T_5 = \begin{bmatrix} c_5 & 0 & s_5 & 0 \\ s_5 & 0 & -c_5 & 0 \\ 0 & 1 & 0 & d_5 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad (6)$$

$${}^0T_5 = \begin{bmatrix} c_{12}c_{345} & s_{12} & c_{12}s_{345} & s_{12}d_5 + c_{12}a_4c_{34} + c_{12}a_3c_3 \\ s_{12}c_{345} & -c_{12} & s_{12}s_{345} & -c_{12}d_5 + s_{12}a_4c_{34} + s_{12}a_3c_3 \\ s_{345} & 0 & -c_{345} & a_4s_{34} + a_3s_3 + d_1 \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad (7)$$

$$T_e = \begin{bmatrix} n_x & o_x & a_x & p_x \\ n_y & o_y & a_y & p_y \\ n_z & o_z & a_z & p_z \\ 0 & 0 & 0 & 1 \end{bmatrix} \quad (8)$$

where T_e is end-effector transformation matrix.

$${}^0T_5 = T_e \quad (9)$$

Where,

$$\left. \begin{aligned} n_x &= c_{12} * c_{345}; n_y = s_{12} * c_{345}; n_z = s_{345}; \\ o_x &= s_{12}; o_y = -c_{12}; o_z = 0; \\ a_x &= c_{12} * s_{345}; a_y = s_{12} * s_{345}; a_z = -c_{345}; \\ p_x &= s_{12} * d_5 + c_{12} * a_4 * c_{34} + c_{12} * a_3 * c_3 \\ p_y &= -c_{12} * d_5 + s_{12} * a_4 * c_{34} + s_{12} * a_3 * c_3 \\ p_z &= a_4 * s_{34} + a_3 * s_3 + d_1 \end{aligned} \right\} \quad (10)$$

INVERSE KINEMATIC ANALYSIS

Now solving ${}^0T_5 = T_e$ by equating individual terms of both matrices, we get the inverse solution. The following equations will be used to obtain the solution for the inverse kinematics problem [4, 10].

$$T_e = {}^0T_1 * {}^1T_2 * {}^2T_3 * {}^3T_4 * {}^4T_5 = {}^0T_5 \quad (11)$$

$$X_1 = ({}^0T_1)^{-1} T_e = {}^1T_2 * {}^2T_3 * {}^3T_4 * {}^4T_5 = {}^1T_5 \quad (12)$$

$$X_1 =$$

$$\begin{aligned}
& [c_1 * n_x + s_1 * n_y, c_1 * o_x + s_1 * o_y, c_1 * a_x + s_1 * a_y, c_1 * p_x + s_1 * p_y] \\
& [-s^1 * n^x + c^1 * n^y, -s^1 * o^x + c^1 * o^y, -s^1 * a^x + c^1 * a^y, -s^1 * p^x + c^1 * p^y] \\
& [n_z, o_z, a_z, p_z] \\
& [d_1 * n_z, d_1 * o_z, d_1 * a_z, 1 + d_1 * p_z] \\
& {}^1T_5 = \\
& [c_2 * c_{345}, s_2, c_2 * s_{345}, s_2 * d_5 + c_2 * a_4 * c_{34} + c_2 * a_3 * c_3] \\
& [s_2 * c_{345}, -c_2, s_2 * s_{345}, -c_2 * d_5 + s_2 * a_4 * c_{34} + s_2 * a_3 * c_3] \\
& [s_{345}, 0, -c_{345}, a_4 * s_{34} + a_3 * s_3] \\
& [0, 0, 0, 1] \quad (13)
\end{aligned}$$

From Equation (13), we do not get any “ θ ” values.

Equation (12), will further be multiplied by $({}^2T_3)^{-1} * ({}^3T_4)^{-1} * ({}^4T_5)^{-1}$, to get

$$X_2 = T_e * ({}^0T_1)^{-1} * ({}^2T_3)^{-1} * ({}^3T_4)^{-1} * ({}^4T_5)^{-1} = {}^0T_1 \quad (14)$$

From the element (1, 3) of the Equation (14), we get,

$$\begin{aligned}
& c_{345} * c_2 * a_x + c_{345} * s_2 * a_y + s_{345} * a_z = 0; \\
& \theta_{345} = \tan^{-1} \{ (-a_z) / (c_2 * a_x + s_2 * a_y) \} \quad (15)
\end{aligned}$$

From the element (2, 4) of the Equation (14), we get,

$$\begin{aligned}
& s_2 * p_x - c_2 * p_y = 0; \\
& \theta_2 = \tan^{-1} (p_y / p_x) \quad (16)
\end{aligned}$$

$$\theta_1 = \theta_{12} - \theta_2 \quad (17)$$

Equation (11), will further be multiplied by $({}^1T_2)^{-1}$, to get

$$X_3 = ({}^0T_1)^{-1} * ({}^1T_2)^{-1} * T_e = {}^2T_3 * {}^3T_4 * {}^4T_5 = {}^2T_5 \quad (18)$$

$$X_3 =$$

$$\begin{aligned}
& [c_{12} * n_x + s_{12} * n_y, c_{12} * o_x + s_{12} * o_y, c_{12} * a_x + s_{12} * a_y, c_{12} * p_x + s_{12} * p_y] \\
& [n_z, o_z, a_z, p] \\
& [s_{12} * n_x - c_{12} * n_y, s_{12} * o_x - c_{12} * o_y, s_{12} * a_x - c_{12} * a_y, s_{12} * p_x - c_{12} * p_y] \\
& [d_1 * n_z, d_1 * o_z, d_1 * a_z, 1 + d_1 * p_z] \\
& {}^1T_5 = \\
& [c_{345}, 0, s_{345}, a_4 * c_{34} + a_3 * c_3] \\
& [s_{345}, 0, -c_{345}, a_4 * s_{34} + a_3 * s_3]
\end{aligned}$$

$$[0, 1, 0, d]$$

$$[0, 0, 0, 1] \quad (19)$$

From the element (1, 4) & (2, 4) of the Equation (19), we get

$$\left. \begin{aligned} c_{12} * p_x + s_{12} * p_y &= a_4 * c_{34} + a_3 * c_3 \\ p_z &= a_4 * s_{34} + a_3 * s_3 \end{aligned} \right\} \quad (20)$$

Squaring both side and then adding the squares gives, we get

$$\begin{aligned} (c_{12} * p_x + s_{12} * p_y)^2 + (p_z)^2 &= (a_4 * c_{34} + a_3 * c_3)^2 + (a_4 * s_{34} + a_3 * s_3)^2 \\ &= (a_3)^2 + (a_4)^2 + 2 * a_3 * a_4 * c_4 \end{aligned}$$

$$\text{Since, } s_3 * s_{34} + c_3 * c_{34} = \cos [(\theta_3 + \theta_4) - \theta_3] = \cos \theta_4$$

$$c_4 = \{(c_{12} * p_x + s_{12} * p_y)^2 + (p_z)^2 - (a_3)^2 + (a_4)^2\} / (2 * a_3 * a_4) \quad (21)$$

Knowing that, $s_4 =$, we can say that,

$$\theta_4 = \tan^{-1} (s_4 / c_4) \pm \sqrt{1 + c_4^2} \quad (22)$$

Now again referring to the Equation (20), we can calculate θ_3 as follows.

$$c_3 = (c_{12} * p_x + s_{12} * p_y - a_4 * c_{34}) / a_3;$$

$$s_3 = (p_z - a_4 * s_{34}) / a_3;$$

$$\theta_3 = \tan^{-1} (s_3 / c_3) \quad (23)$$

$$X_4 = ({}^0T_1)^{-1} * ({}^1T_2)^{-1} * ({}^2T_3)^{-1} * ({}^3T_4)^{-1} * T_e = {}^4T_5 \quad (24)$$

From the element (1, 4) of the Equation (23), we get

$$c_{34} * c_{12} * p_x + c_{34} * s_{12} * p_y + s_{34} * p_z = 0;$$

$$\theta_{34} = -\tan^{-1} \{(c_{12} * p_x + s_{12} * p_y) / p_z\} \quad (25)$$

$$\theta_5 = \theta_{345} - \theta_{34} \quad (26)$$

FORWARD KINEMATIC CASE-STUDY & RESULT

For the given set of parameter, a program in MATLAB 8.0 is made. Developed model is used to determine position and orientation of end effector. For the values of $\theta_1 = 30^\circ$, $\theta_2 = 50^\circ$, $\theta_3 = 45^\circ$, $\theta_4 = 25^\circ$ and $\theta_5 = 0^\circ$, results obtained is shown below.

The DH parameters of 5 DOF Robotic Arm is as follows:

a alpha d theta

0.0000 0.0000 86.0000 50.0000

0.0000 90.0000 0.0000 30.0000

96.0000 0.0000 0.0000 45.0000

96.0000 0.0000 0.0000 25.0000
 0.0000 90.0000 59.5000 0.0000

The Final Matrix (0T_5) by Matlab Program is as follows:

0.0594 0.9848 0.1632 76.0852
 0.3368 -0.1736 0.9254 88.8540
 0.9397 0.0000 -0.3420 244.0927
 0.0000 0.0000 0.0000 1.0000

The final end-effector position is $P_x = 76.0852$, $P_y = 88.8540$, $P_z = 244.0927$.

For the given set of parameter, a program in MATLAB 8.0 is made. Developed model is used to determine position and orientation of end effector. For the values of $\theta_1 = 30^\circ$, $\theta_2 = 50^\circ$, $\theta_3 = 45^\circ$, $\theta_4 = 25^\circ$ and $\theta_5 = 0^\circ$, results obtained is shown below.

The DH parameters of 5 DOF Robotic Arm is as follows:

a	alpha	d	theta
0.0000	0.0000	86.0000	50.0000
0.0000	90.0000	0.0000	30.0000
96.0000	0.0000	0.0000	45.0000
96.0000	0.0000	0.0000	25.0000
0.0000	90.0000	59.5000	0.0000

The Final Matrix (0T_5) by Matlab Program is as follows:

0.0594 0.9848 0.1632 76.0852
 0.3368 -0.1736 0.9254 88.8540
 0.9397 0.0000 -0.3420 244.0927
 0.0000 0.0000 0.0000 1.0000

The final end-effector position is $P_x = 76.0852$, $P_y = 88.8540$, $P_z = 244.0927$.

CONCLUSIONS

A complete analytical solution to the forward and inverse kinematics of 5 DOF Robotic arm is derived in this paper. The forward kinematic analysis of 5 DOF robotic arm is investigated. The mathematical model is prepared and solved for positioning and orienting the end effectors by preparing a programme in MATLAB 8.0. The result of the forward kinematics can be crossed checked by the analytical method of inverse kinematic model. Hence this proves the utility of the 5 DOF robotic arm as an educational tool for undergraduate robotics courses.

ACKNOWLEDGEMENTS

The authors wish to thank "Sophisticated Instrumentation Centre for Applied Research and Testing" (SICART) for permitting to use the facilities to carry out research work.

REFERENCES

1. R. D. Klafter, T. A. Chmielewski and M. Negin. (1989). *Robotic Engineering: An Integrated Approach*. Prentice Hall.
2. R K Mittal, J Nagrath. (2005). "Robotics and Control", Tata McGraw-Hill.
3. P. J. McKerrow. (1991). *Introduction to Robotics*. Addison-Wesley.
4. S. B. Niku. (2001). *Introduction to Robotics: Analysis, Systems, Applications*. Prentice Hall.
5. Baki Koyuncu, and Mehmet Güzel, —Software Development for the Kinematic Analysis of a Lynx 6 Robot Arm, *World Academy of Science, Engineering and Technology* 30 2007.
6. Paul, R. P.(1981). *Robot Manipulators: Mathematics, Programming and Control*. Cambridge, MIT Press.
7. Featherstone, R. (1983). Position and velocity transformations between robot end-effector coordinates and joint angles. *Int. J. Robotics Res.* 2, 35-45.
8. Lee, C. S. G. (1982). Robot arm kinematics, dynamics, and control. *Computer*, 15, 62-80.
9. Denavit J. & R.S. Hartenberg (1955). A kinematic Notation for Lower- Pair Mechanism Based on Matrices. *ASME Journal of Applied Mechanics*, 215-221.
10. Dr. Anurag Verma & Vivek Deshpande (2011). End-effector Position Analysis of SCORBOT-ER Vplus Robot. *International Journal of Advanced Science and Technology*, Vol. 29. pp 61 -66.

