

(1)

(3)

(2)

1

$$T_d = 38^\circ\text{C}$$

$$RH = 50\%$$

$$\omega_1 = 0.02105$$

$$T_d = 10.5^\circ\text{C}$$

$$RH = 100\%$$

$$\omega_3 = 7.882 \times 10^{-3} \text{ kg}$$

$$T_d = 25^\circ\text{C}$$

$$RH = 40\%$$

cooling

heating

$$\dot{m}_a = \frac{\dot{V}}{v}$$

$$R_v = \frac{\bar{R}}{MW_{H_2O}} = \frac{8.314}{18}$$

$$v = \frac{T(1+\omega)}{\frac{P_a}{R_a} + \frac{P_v}{R_v}} = \frac{(311)(1+0.02105)}{\left[\frac{1.01325 - 0.03316}{0.287} + \frac{0.03316}{0.462} \right] \frac{100}{\text{bar} \rightarrow \text{kPa}}}$$

$$= 0.9107 \text{ m}^3/\text{kg d.a.}$$

$$\dot{m}_a = \frac{75 \text{ m}^3/\text{min}}{0.9107 \text{ m}^3/\text{kg d.a.}}$$

$$= 82.35 \frac{\text{kg d.a.}}{\text{min}} = 1.373 \frac{\text{kg}}{\text{s}}$$

$$h_1 = C_p T_1 + \omega_1 h_g(T_1) = (1.005)(38) + (0.02105)(2570.7) = 92.3 \text{ kJ/kg d.a.}$$

$$h_3 = C_p T_3 + \omega_3 h_g(T_3) = (1.005)(10.5) + (0.00788)(2476.5) = 30.1 \text{ kJ/kg d.a.}$$

$$h_f(10.5^\circ\text{C}) = 4.182 \times 10.5 = 43.91 \text{ kJ/kg d.a.}$$

$$(1.373)(92.3) + \dot{Q} = (1.373)(0.02015 - 0.00788) \times 43.91 + (1.373)(30.1)$$

$$\dot{Q} = -84.7 \text{ kW}$$

$$\dot{Q} = \dot{m}_f h_f(10.5^\circ\text{C}) + \dot{m}_a (C_p T_3 + \omega_3 h_g(T_3)) + \dot{m}_a (C_p T_1 + \omega_1 h_g(T_1))$$

Power required for AC unit = $COP = \frac{\dot{Q}}{\dot{W}}$ 2

$$\Rightarrow \dot{W} = \frac{\dot{Q}}{COP} = \frac{+84.7}{3} = 28.2 \text{ kW.}$$

e From (3) \rightarrow (2), heating.

$$h_2 = C_p T_2 + \omega_2 h_g(T_2) = (1.005)25 + (0.00788)(2547.2)$$

$$= 45.2 \text{ kJ/kg d.a.}$$

$$\begin{aligned} \dot{H}_3 + \dot{Q} &= \dot{H}_2 \\ \dot{m}_a h_3 + \dot{Q} &= \dot{m}_a h_2 \end{aligned} \Rightarrow \dot{Q} = \dot{m}_a (h_2 - h_3)$$

$$= (1.373)(45.2 - 30.1)$$

$$\dot{Q} = 20.73 \text{ kW}$$

\approx adiabatic sat. temp $= T_2$

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Moist air with dry bulb temperature of 22°C and wet bulb temperature of 9°C enters a steam-spray humidifier. It is desired to bring the humidity to 50% with the same dry bulb temperature. Saturated steam at 100°C and 1 atm is available. How much steam needs to be sprayed per kg of d.a. in the moist air stream?

$$\omega_1 = \frac{c_p a (T_w - T_d) + \omega_w h_{fg}(T_w)}{h_g(T_d) - h_f(T_w)}$$

$$\omega_1 = \frac{c_p a (T_2 - T_1) + \omega_2 h_{fg}(T_2)}{h_g(T_1) - h_f(T_2)}$$

$$T_d = 22^\circ\text{C}$$

$$T_w = 9^\circ\text{C}$$

$$p_{\text{sat}}(9^\circ\text{C}) = 0.0115 \text{ bar}$$

$$h_{fg}(9^\circ\text{C}) = 2480.1$$

$$h_f(9^\circ\text{C}) = 37.805$$

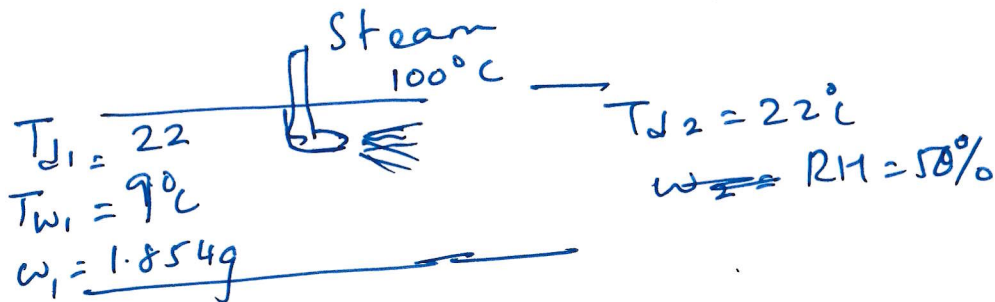
$$\omega_1 = \frac{(0.622) \cdot 0.0115}{1.01325 - 0.0115} = 7.14 \times 10^{-3}$$

$$\omega_1 = \frac{(1.005)(9 - 22) + (0.00714)(2480.1)}{2541.7 - 37.805} = 1.854 \times 10^{-3} \text{ kg/kg d.a.}$$

$$\text{For } 22^\circ\text{C} - p_{\text{sat}} = 0.02645$$

$$p_{v2} = (0.5)(0.02645) = 0.01323 \text{ bar}$$

$$\omega_2 = \frac{(0.622) \cdot 0.01323}{0.622 \cdot 1.01325 - 0.01323} = 0.00823 \text{ kg/kg d.a.}$$



$$\text{Mass of steam sprayed per kg d.a.} = \omega_2 - \omega_1 = 0.00823 - 0.001854 = 6.375 \text{ g/kg d.a.}$$

$$\dot{H}_1 + \dot{H}_{\text{steam}} = \dot{H}_2 \rightarrow \dot{m}_a h_1 + \dot{m}_{\text{steam}} h_g = \dot{m}_a h_2 \quad [4]$$

$$\dot{m}_a h_1 + (\omega_2 - \omega_1) h_g = \dot{m}_a h_2$$

$$h_1 = c_p T_1 + \omega_1 h_g(T_1) = (1.005)(22) + (0.001854)(2541.7) = 26.82 \text{ kJ/kg d.a.}$$

$$h_g(100^\circ\text{C}) = 2676.1 \text{ kJ/kg}$$

$$26.82 + (0.00823 - 0.001854)2676.1 = h_2 = 43.88 \text{ kJ/kg d.a.}$$

Find T_2 corresponding to $h_2 = 43.88$ and $\omega_2 = 0.00823$

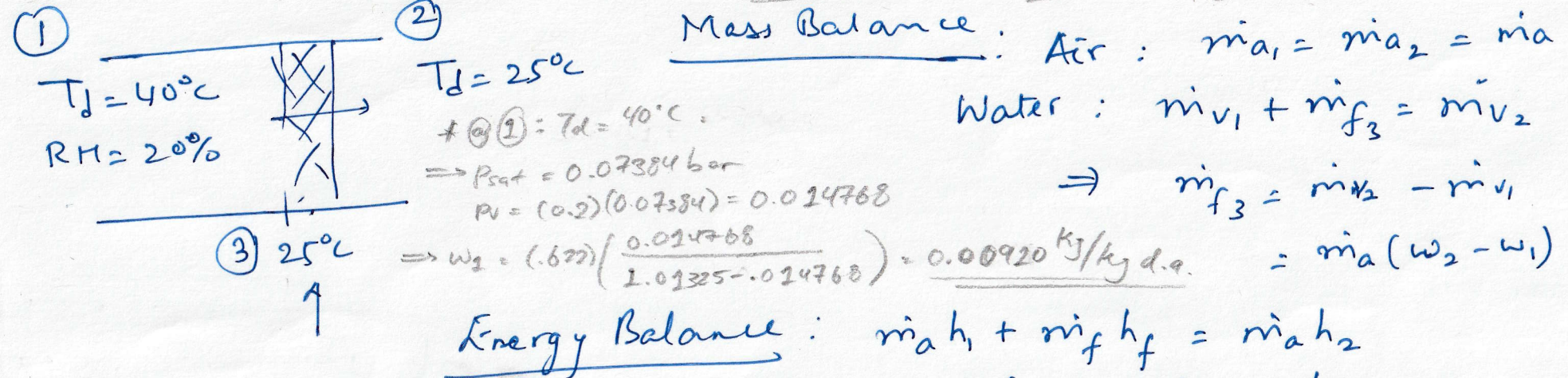
$$h_2 = c_p T_2 + (2500 + 1.9 T_2) \omega_2$$

$$43.88 = (1.005) T_2 + (2500 + (1.9) T_2) (0.00823)$$

$$\Rightarrow 43.88 - (2500)(0.00823) = ((1.9)(0.00823) + 1.005) T_2$$

$$\Rightarrow \boxed{T_2 = 22.84^\circ\text{C}}$$

Air at 40°C and 20% RH enters an evaporative cooler with a flow rate of 120 kg/min. It is to be cooled down to 25°C. How much water is needed per minute? What is the relative humidity at the exit? $\rightarrow \phi_2$



1) First find h_1 using T_d & RH.

2) $h_2 = h_1$
 $= C_{p_a} T_2 + w(2500 + 1.9 T_2)$
 $= C_{p_a} T_2 + w_2 h_g(T_2)$

Solve for w_2

$h_g(25^\circ\text{C}) = 2547.2$
 $h_g(40^\circ\text{C}) = 2574.3$

$\Rightarrow C_{p_a} T_2 + w_2 h_g(T_2) = C_{p_a} T_1 + w_1 h_g(T_1)$

$\Rightarrow w_2 = \frac{C_{p_a} T_1 + w_1 h_g(T_1) - C_{p_a} T_2}{h_g(T_2)} = \frac{(1.005)(40) + (0.0092)(2574.3) - (1.005)(25)}{2547.2}$

$\Rightarrow w_2 = 0.0152 \Rightarrow P_v = \frac{w_2 P}{0.622 + w_2} = \frac{(0.0152)(1.01325)}{0.622 + 0.0152} = 0.0242 \text{ bar} \Rightarrow$

$$\phi_2 = \frac{P_i}{P_{i,sat}} = \frac{0.0242}{0.03169} = \underline{\underline{76\%}}$$

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$$P_{sat} @ 25^\circ C = 0.03169 \text{ bar}$$

$$\Rightarrow \text{Water required?} \Rightarrow w_2 - w_1 = 0.0152 - 0.0092 = 0.006 \text{ kg/kg d.a.}$$

$$\begin{aligned} * \dot{m}_a &= 120 \text{ kg/min} \quad , \quad \dot{m}_{f_3} = \dot{m}_a (w_2 - w_1) \\ &= 120 (0.006) = \boxed{0.72 \text{ kg/min}} \end{aligned}$$