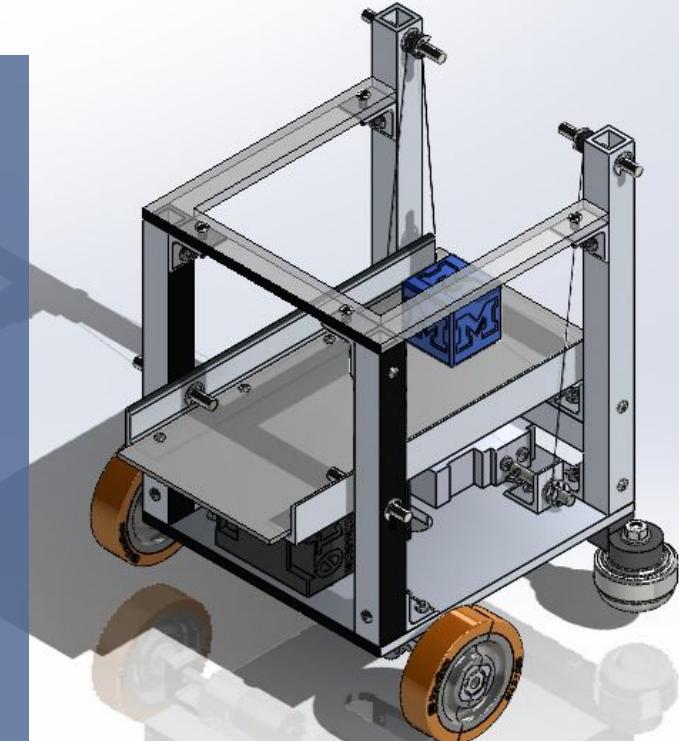


# ME 250 Design Review: Team 33

Luis Barcenas, Ethan Feng, Ashley Ortenburg, Genna Urbain



# RMP Strategy Selection

Our Strategy:

1. Traverse the space-time continuum
2. Turn on all of the stars in Q2
3. Prop the rocket open
4. Transport cubes between Mars and the rocket

Why:

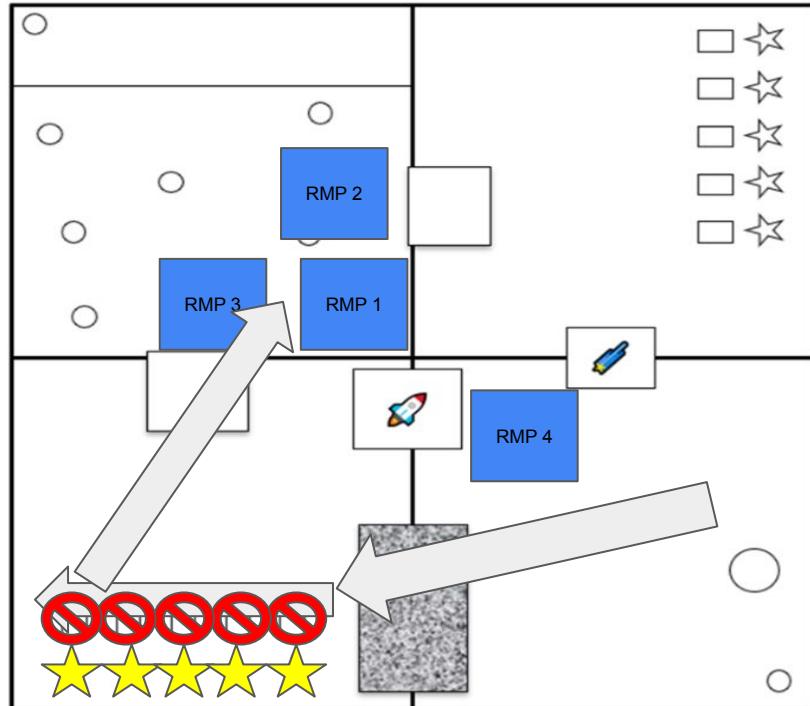
- Prop open rocket/deposit cubes was main task
- Space-time continuum is 1 of 2 ways to get to rocket opening
- We pass Q2 stars on the way to get to rocket opening

SQUAD STRATEGY	
- Mars - cube depositer, holds rocket open - Q2 stars → minerals → mars - over space time continuum	(33)
- flag? - Q4 stars - cubes-if time	(31)
- open rocket → open whole game, detachable? - push asteroid to earth	(32)
- Mars → push cubes → rocket - aliens knock down - Q4 minerals, Q4 ramp	(34)

# RMP Strategy Selection

Interactions:

- Traversing the space-time continuum
- Rely on RMP 4 to open rocket
- RMPs 2 & 3 rely on us to deposit cubes
- Collaborate with RMP 2 to turn on all 10 stars

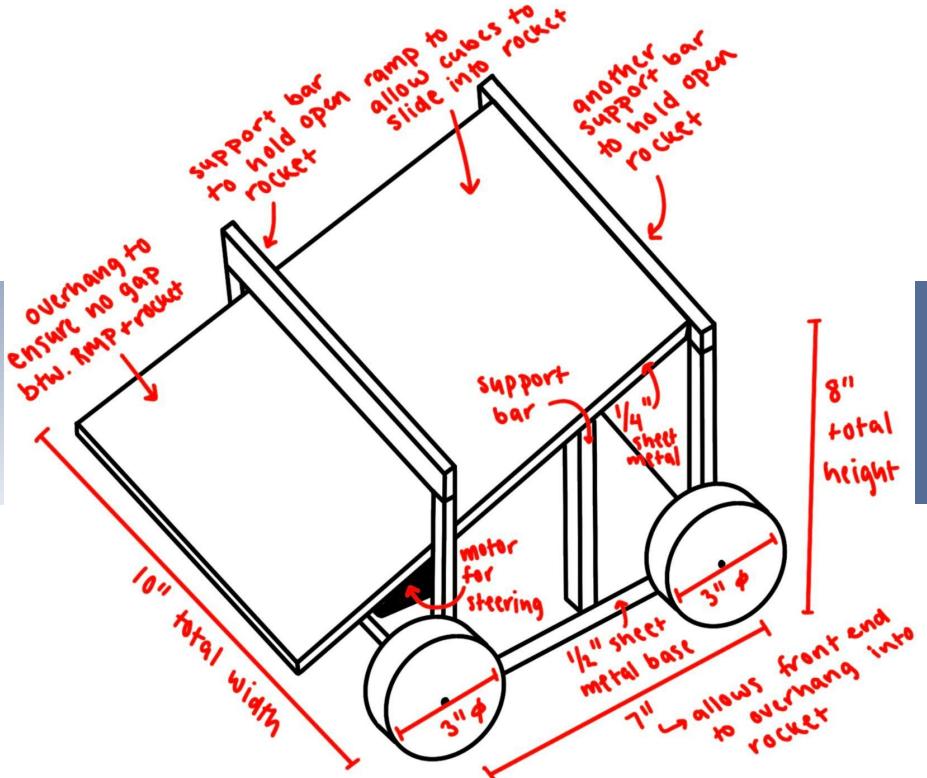


# Top 3 Functional Requirements

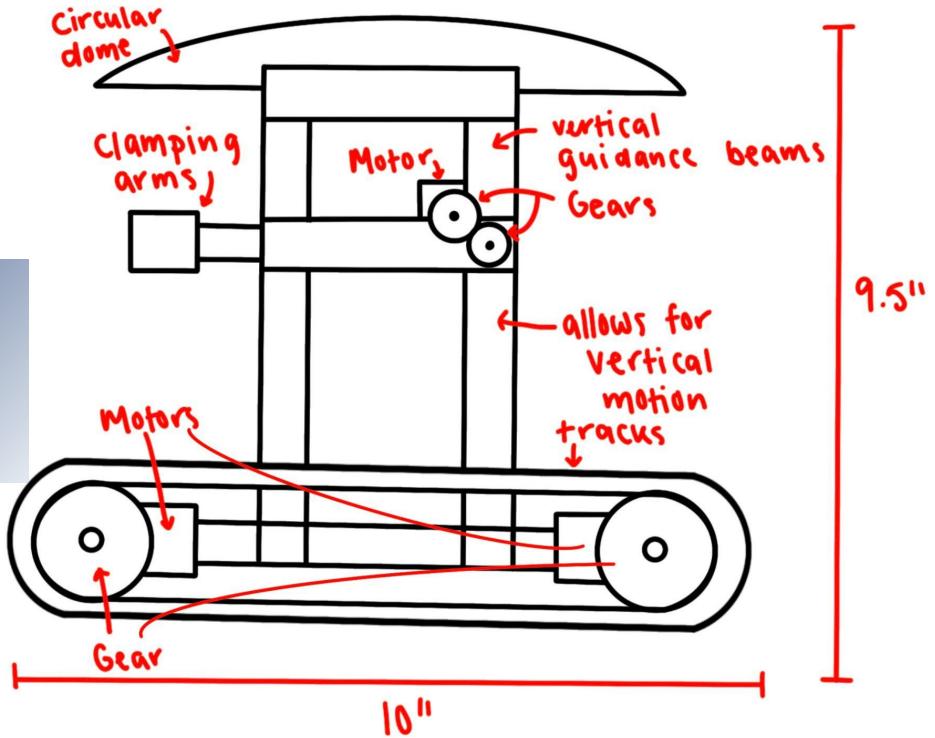
- RMP 1 must hold the rocket open at a height of 10 in ( $\pm 1$  in)
- RMP 1 must be able to deposit 2 cubes ( $\pm 1$  cube) at a time
- RMP 1 must be capable of driving up at least a 35° ramp

Why:

- If we cannot deposit cubes:
  - other RMPs must deposit them themselves (if they are even able to)
- If we cannot prop open the rocket:
  - other RMPs must move to Area 51 to deposit cubes (if they are even able to)
  - lose out on the point multiplier of the rocket
- If we cannot drive up ramp:
  - Same implications as above

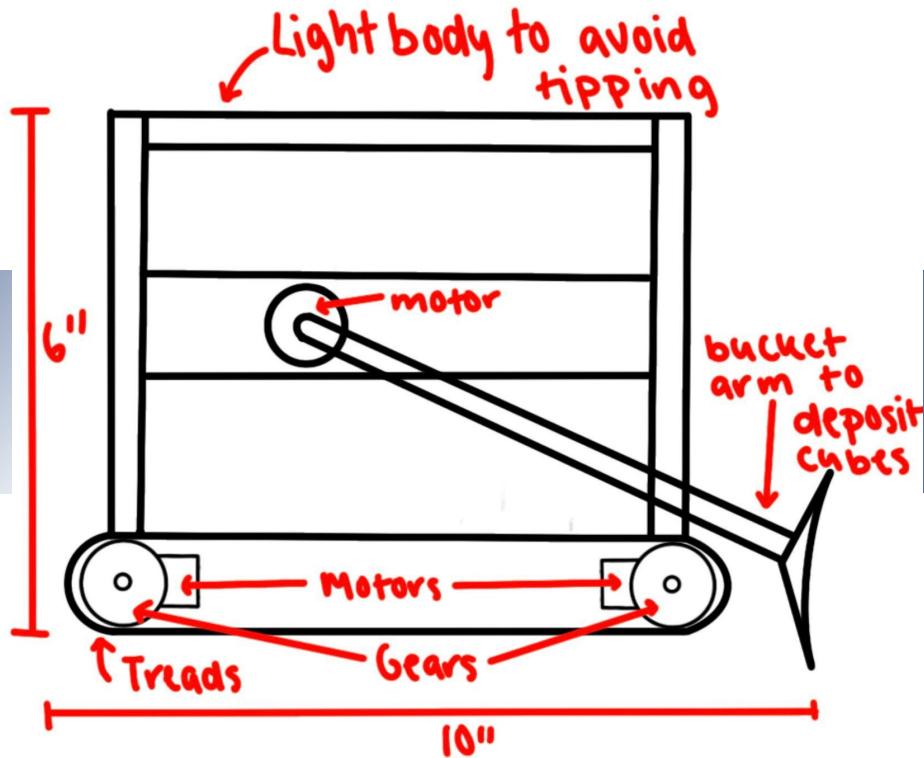


# Design Concept #1

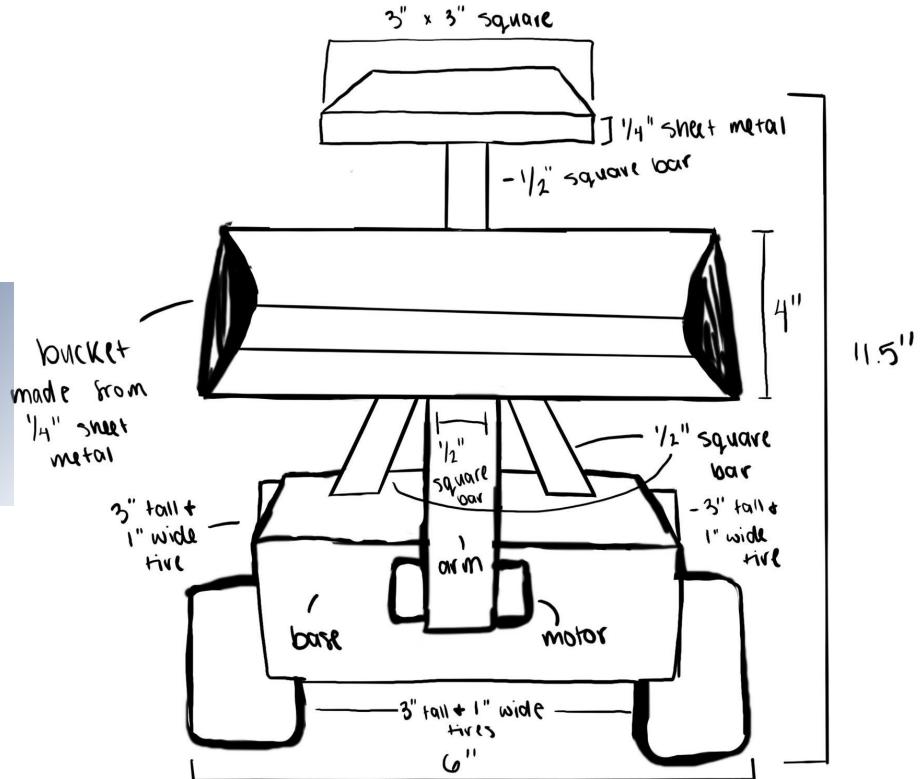


## Design Concept #2

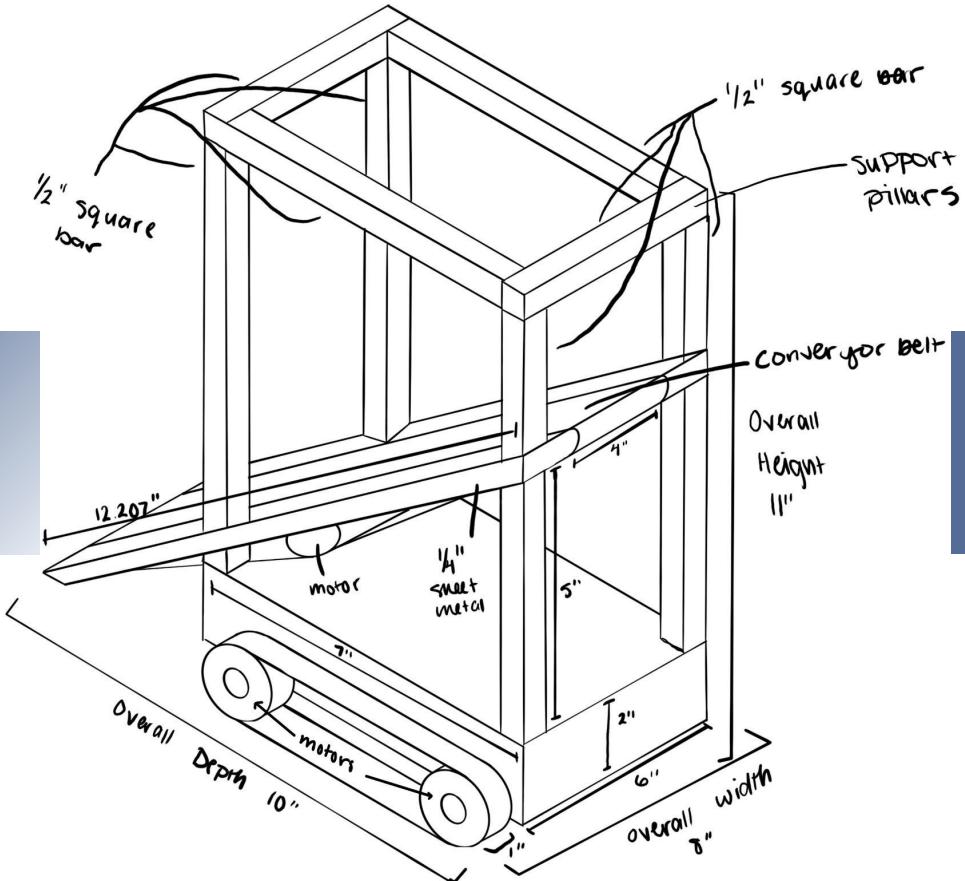
## Design Concept #3



Light body to avoid tipping



# Design Concept #4



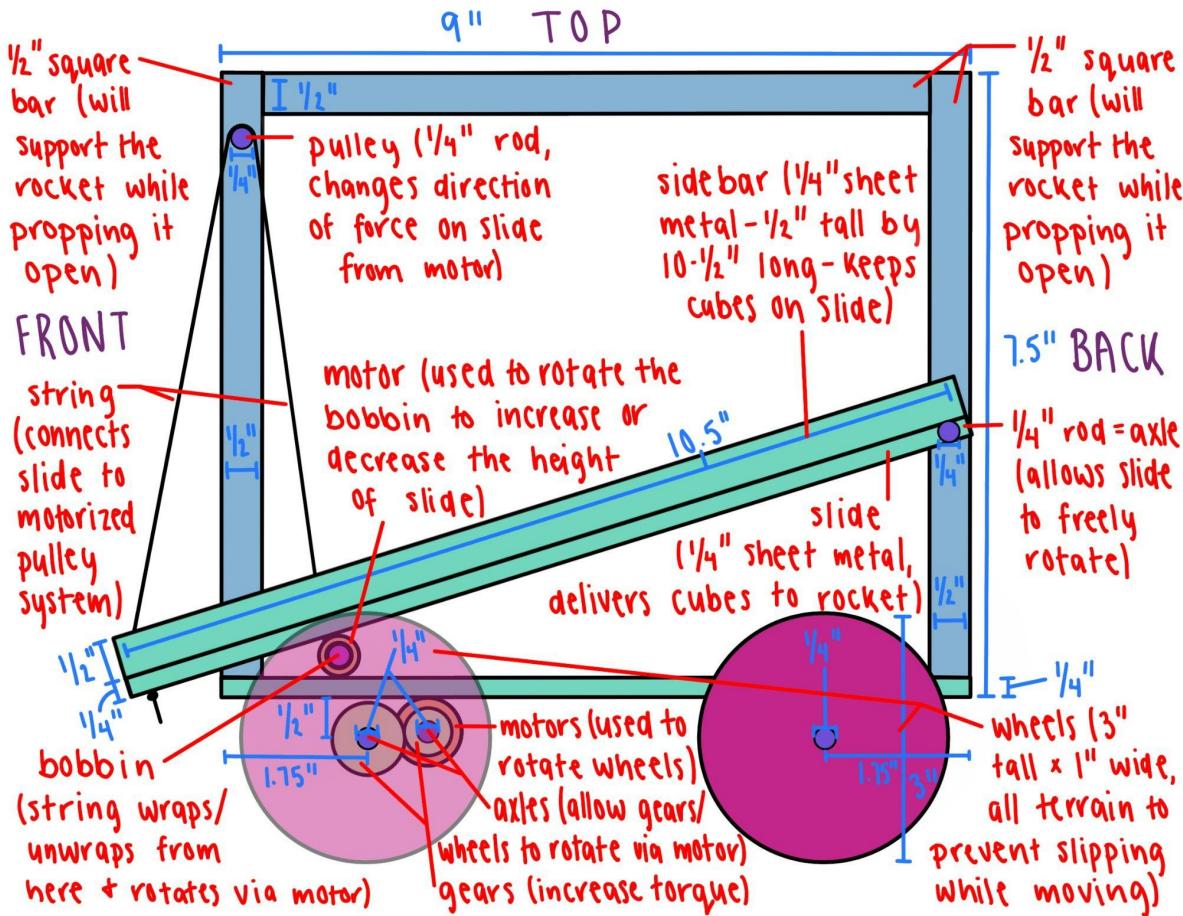
# Design Concept #5

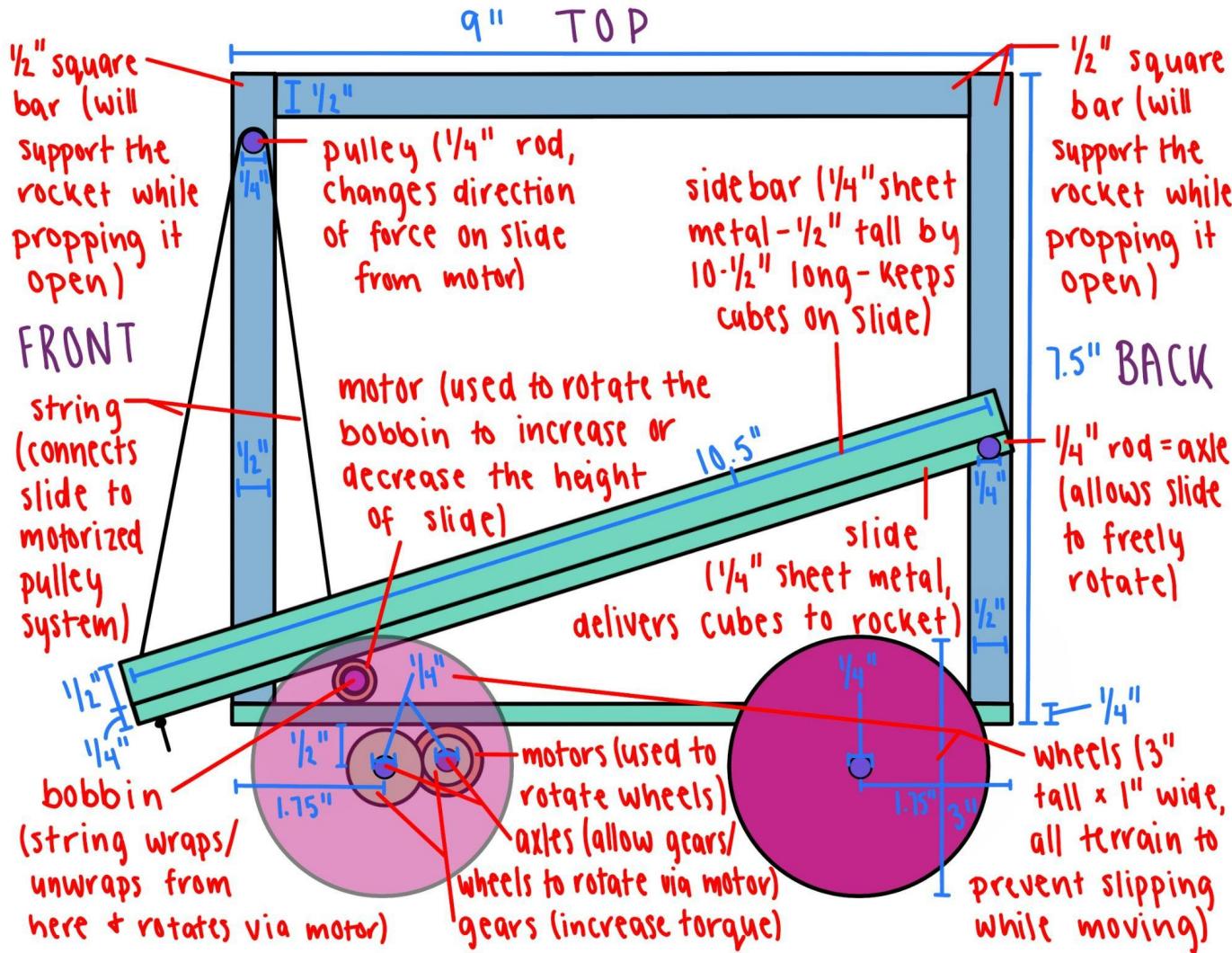
# Pugh Chart Analysis

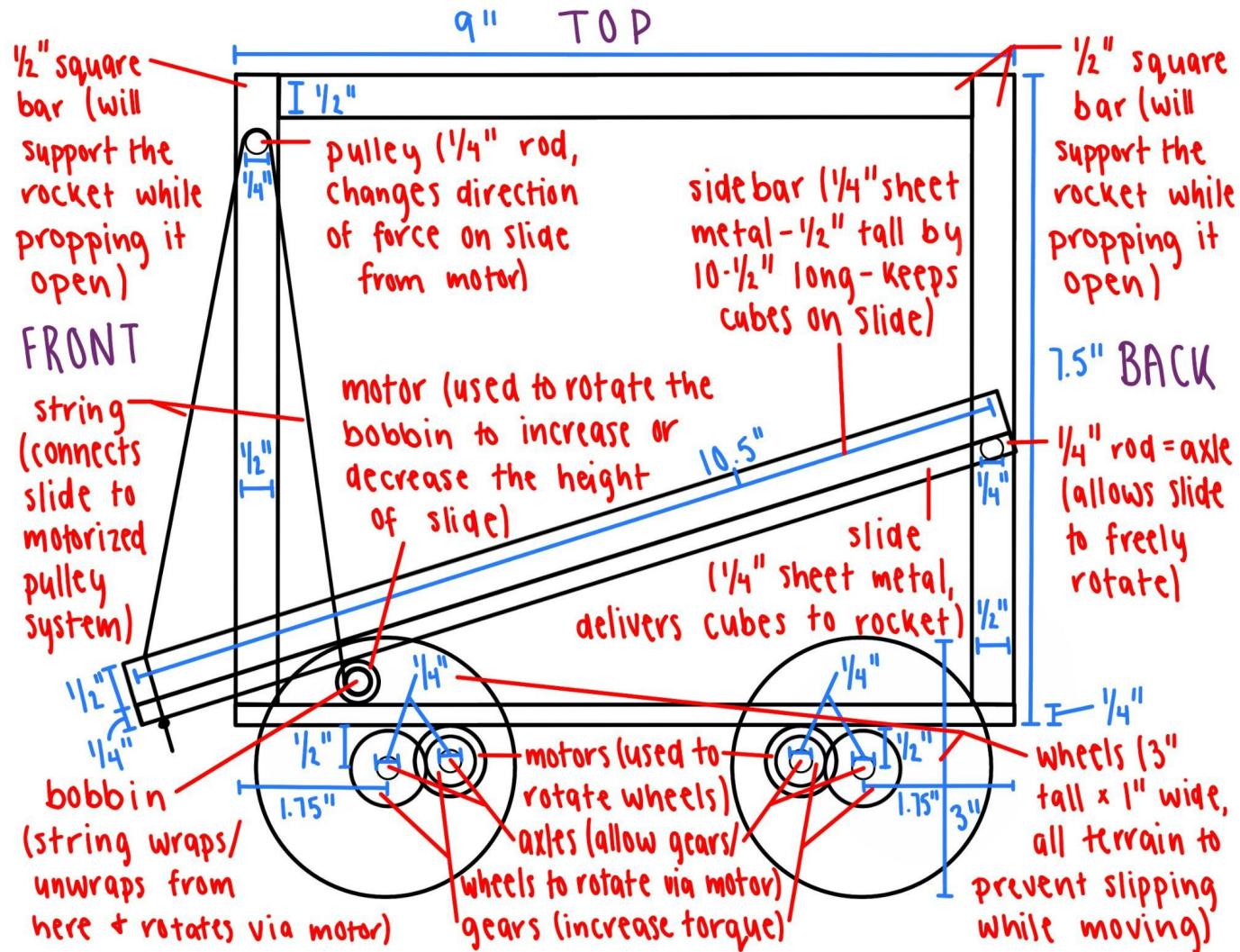
Requirement	Weight	Design Concept 1 (GU-1) <b>Baseline</b>	Design Concept 2 (EF-2)	Design Concept 3 (LB-1)	Design Concept 4 (AO-1)	Design Concept 5 (AO-2)
Can hold Rocket Open	3	0	+1	-1	0	+1
Can drive up the Ramp	3	0	0	+1	0	0
Can deposit Cubes	2	0	0	+1	-1	+1
Can traverse the Space-Time Continuum	2	0	-1	0	0	0
Can turn on stars	1	0	-1	-1	0	-1
Manufacturability	3	0	-1	0	0	0
Creativity	3	0	+1	0	+1	0
Total		0	0	+1	+1	+4

# Concept Sketches

Right View

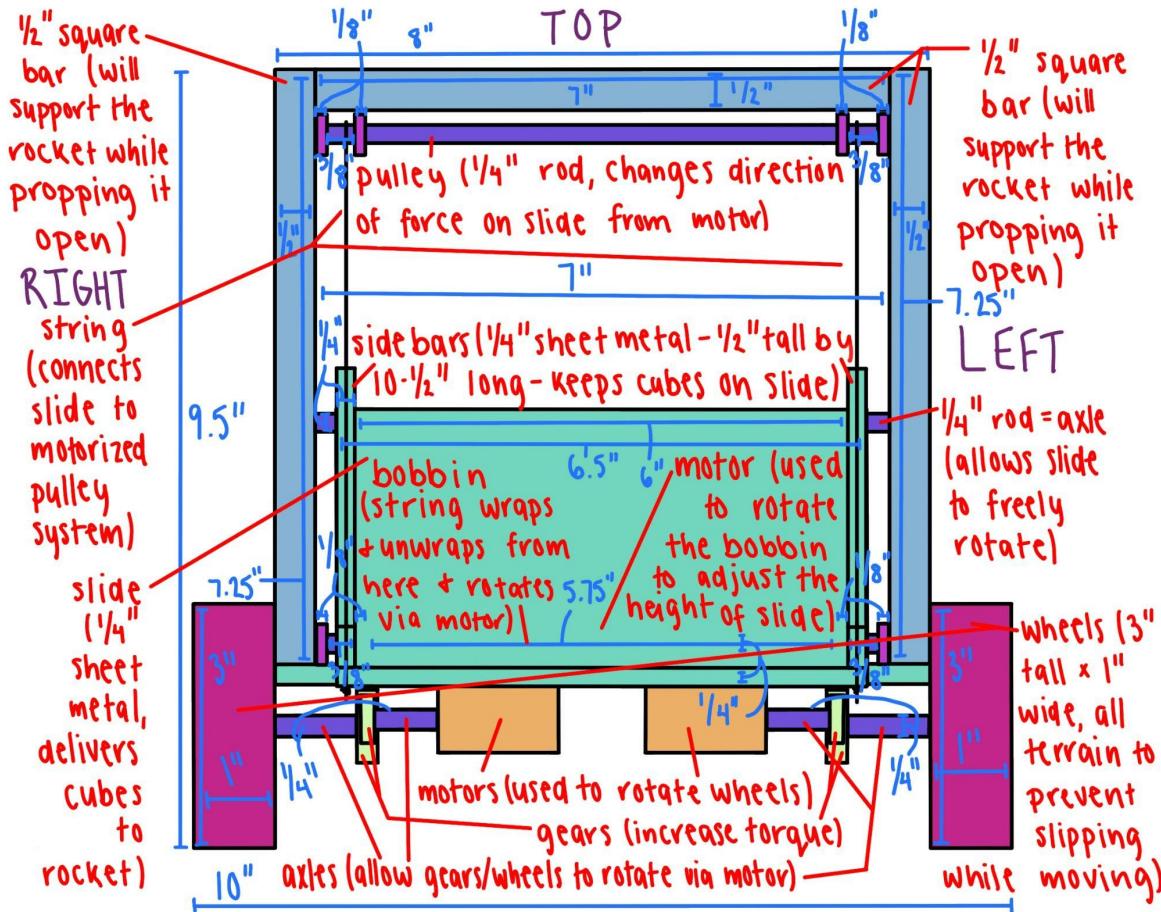


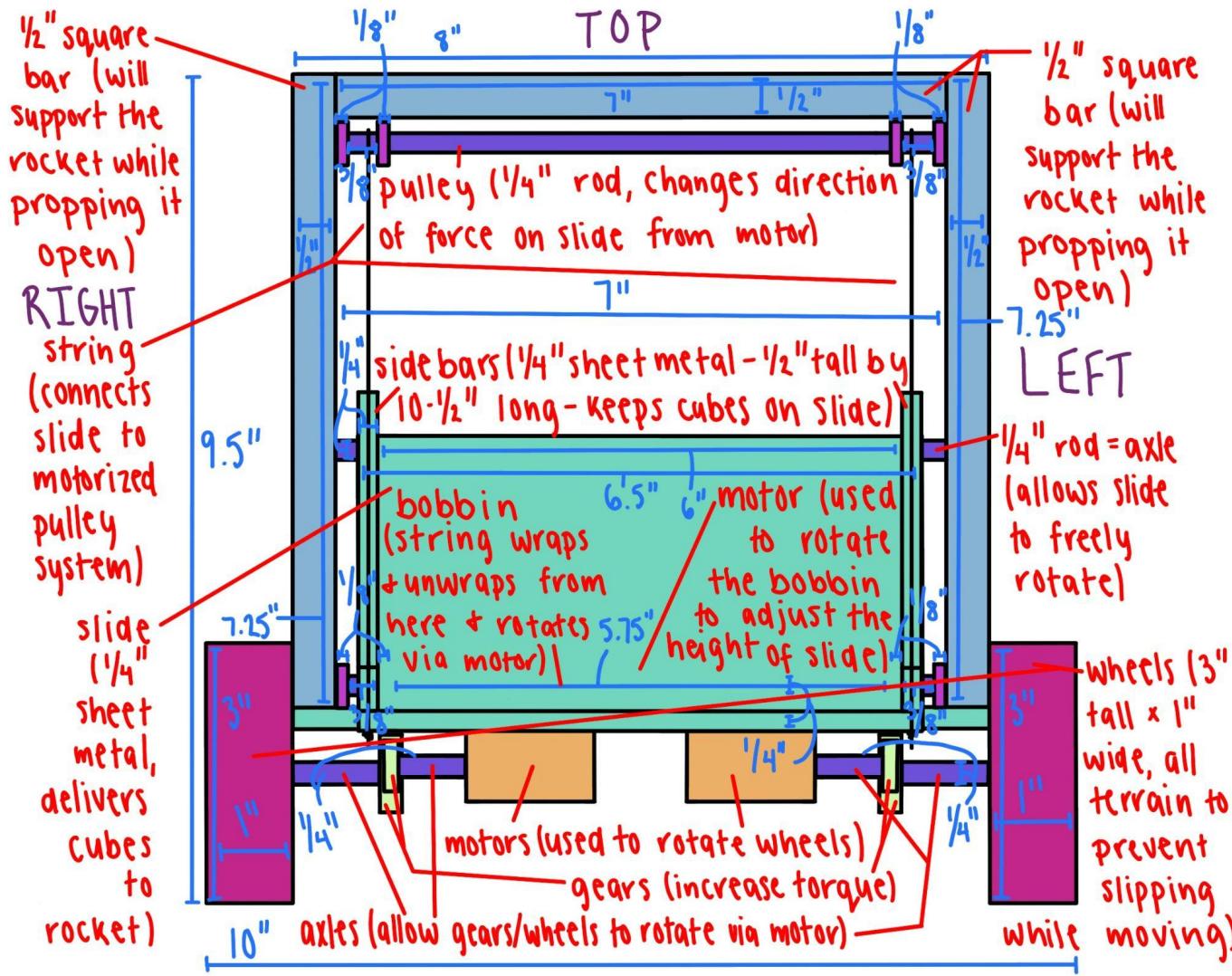


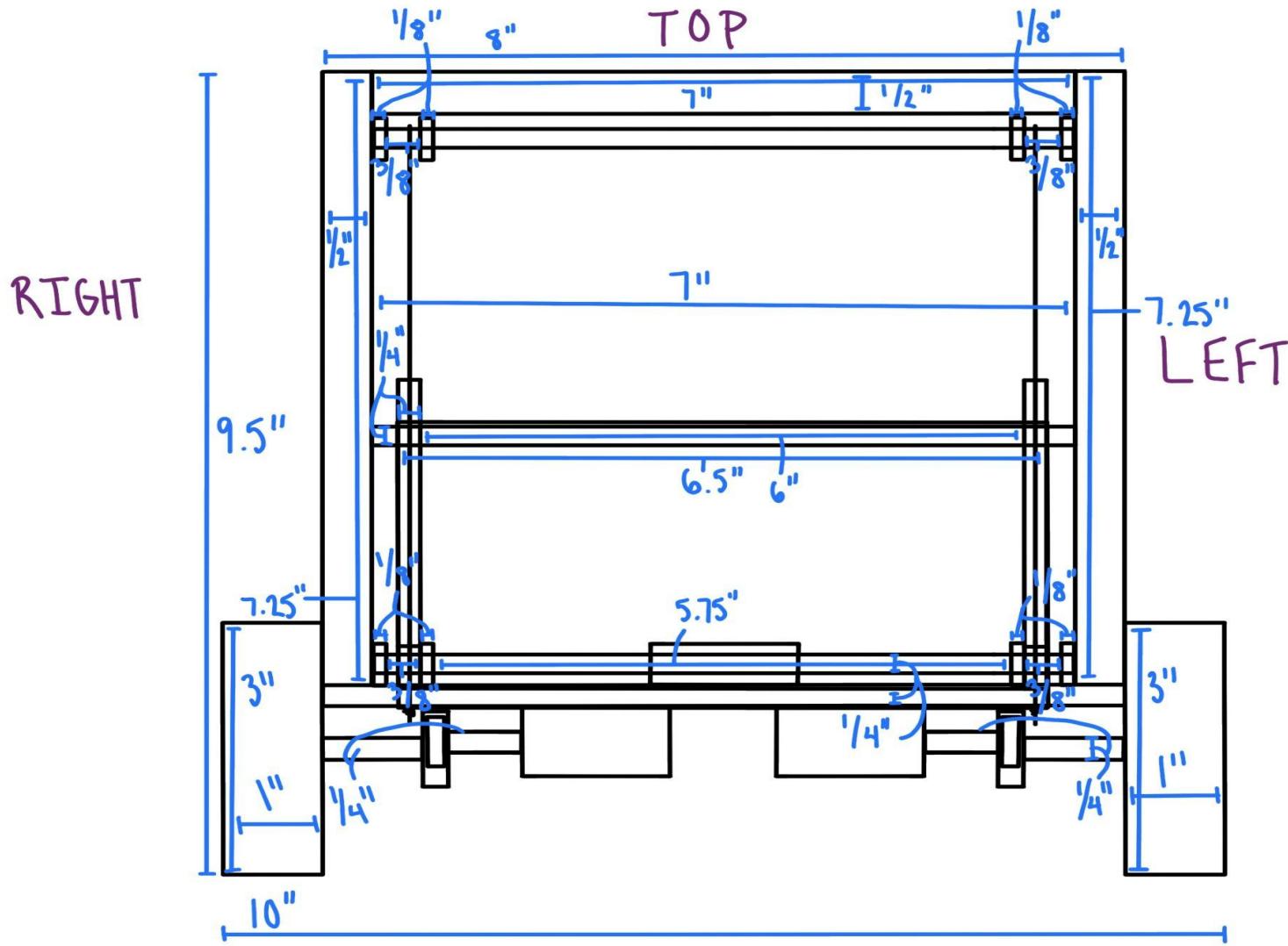


# Concept Sketches

Front View







# Decision Variables

## Ramp Angle and Material

- Ramp angle must be large enough to slide cubes (FR), but low enough to meet height limitations
- Determined by empirical testing
  - Ease of test setup
  - Coefficient of friction is “unknown”
- Conclusion: Delrin has least coefficient of friction and 30 degrees of incline is more than sufficient

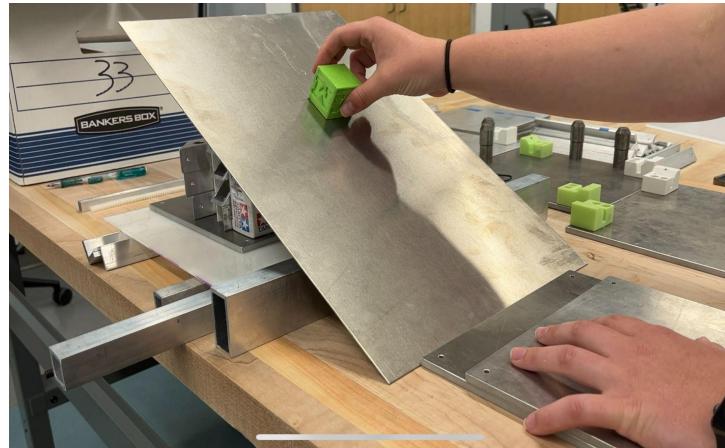
## Motor Choices

- Motors must have sufficient torque for respective applications (FR)
- Determined by FPAs
  - Statically determinate- 3 equations, 3 unknowns
- Conclusion: Double gearbox motor for pulley, metal motors for wheels

## Why Banebots Wheels and Caster Balls?

- Movement and maneuverability (most critical subsystem)
- Determined by engineering intuition
- Conclusion: Driven wheels in the front, caster balls in the rear

# Empirical Testing: Optimal Ramp Angle and Material

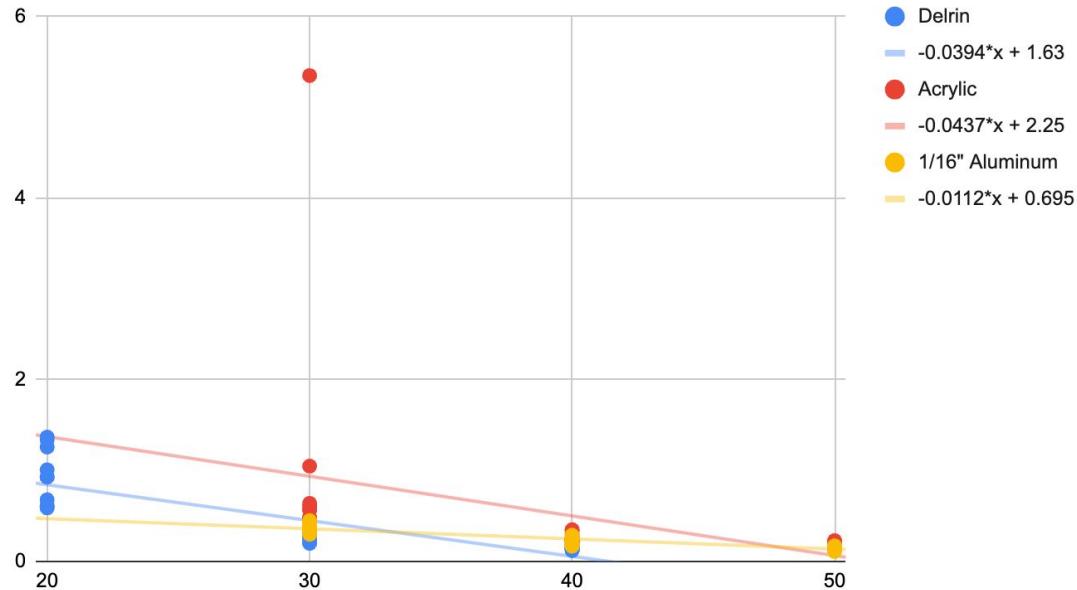


Top Left: Acrylic  
Bottom Left: Delrin  
Right: Aluminum

# Empirical Testing: Optimal Ramp Angle and Material

- Conclusion: Delrin around 25-30 degrees

Angle, Delrin, Acrylic and 1/16" Aluminum



\* Some of the cubes did not slide at 20 degrees for Delrin

# First Principles Analysis: Pulley Problem

$$\sum F_y = 0 = \cos(49.77) - W + C_y$$

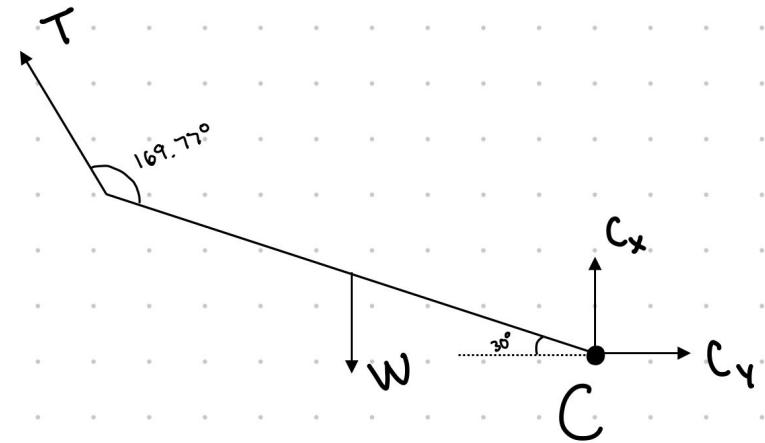
$$\sum F_x = 0 = -T \sin(49.77) + C_x$$

$$\sum M = 0 = -T \cos(49.77)(7.375 \cos(30)) - T \sin(49.77)(7.375 \sin(30)) + W(3.6875 \cos(30))$$

$$\sum M = 0 = -1.3098T + 3.1935W$$

$$T = 1.7067 \text{ lb}$$

$$T_{out} = 1.7067(0.25) = 0.4267 \text{ lb} \cdot \text{in} = 6.827 \text{ oz} \cdot \text{in}$$



# First Principles Analysis: Incline Torque Requirement

$$\sum F_x = 0 = F_W - F_g \sin(\theta)$$

$$\sum F_y = 0 = -F_g \cos(\theta) + N_1 + N_2$$

$$\sum M_O = 0 = (-N_2 \cdot d_{wheelbase}) + (F_g \cos(\theta) \cdot d_{COM}) + (F_g \sin(\theta) \cdot h)$$

Approx. Weight  $\cong 7 \text{ lbs.}$

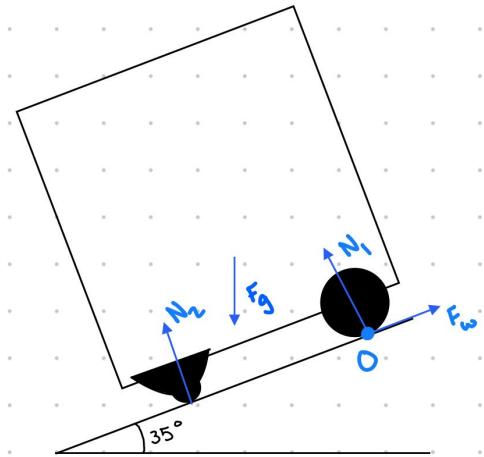
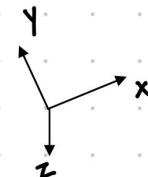
$$F_g = 7 \text{ lbf}$$

$$F_W = F_g \sin(\theta) = 7 \text{ lbf} \cdot \sin(45 \text{ deg}) = 4.1015 \text{ lbf}$$

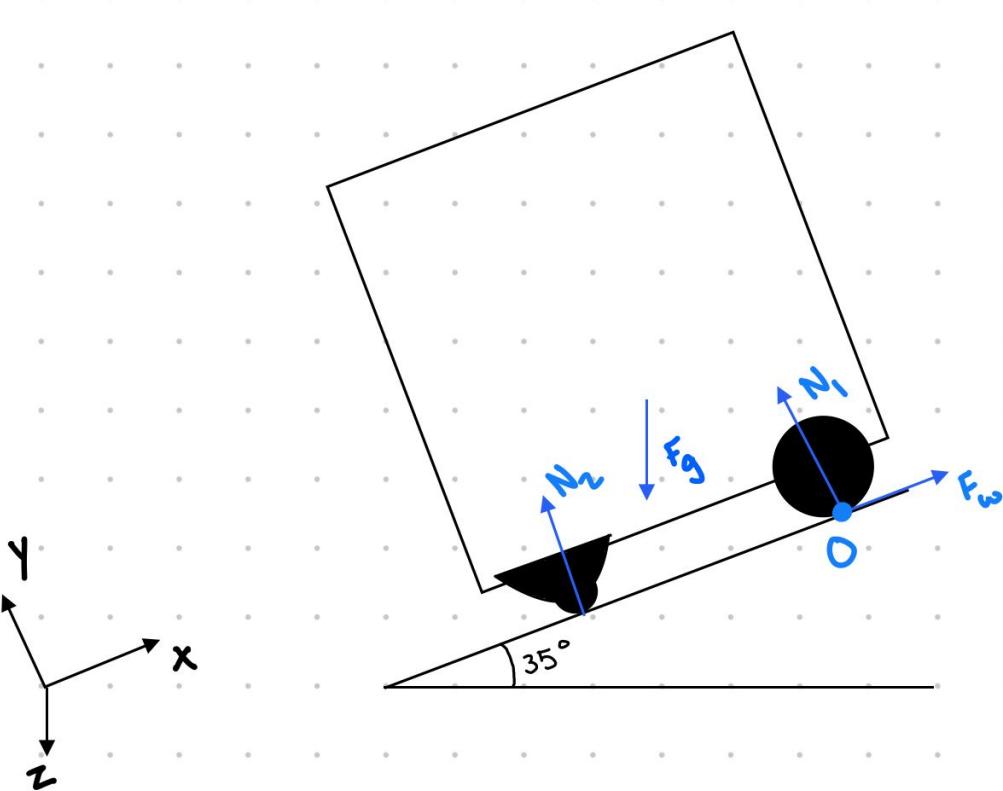
$$T_{total, out} = F_W \times r_{wheel} = 4.1015 \text{ lbf} \times 1.4375 \text{ in} = 5.8816129 \text{ lb} \cdot \text{in}$$

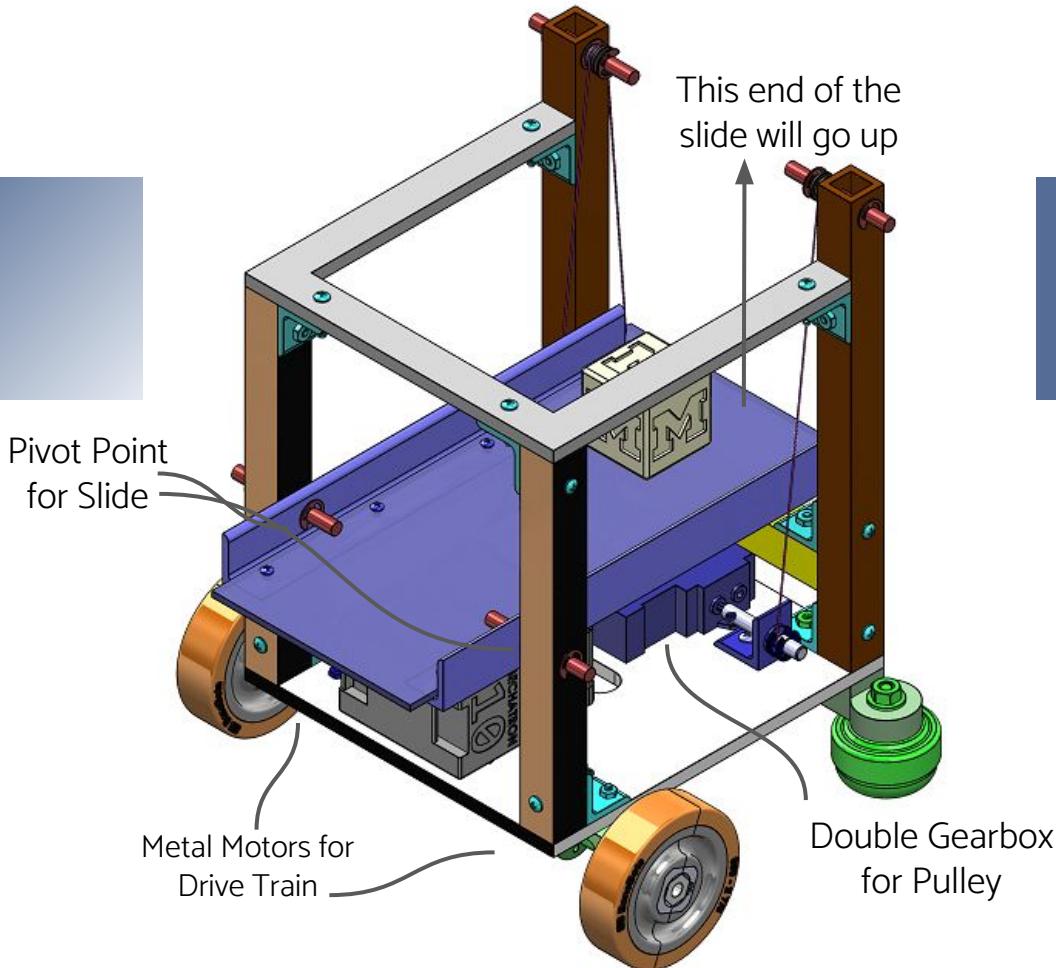
$$T_{wheel} = T_{total, out} / 2 = 2.8858 \text{ lb} \cdot \text{in}$$

$$T_{wheel, sf} = T_{wheel} \times S.F. = 5.8816129 \text{ lb} \cdot \text{in} (\text{with a safety factor} = 2)$$



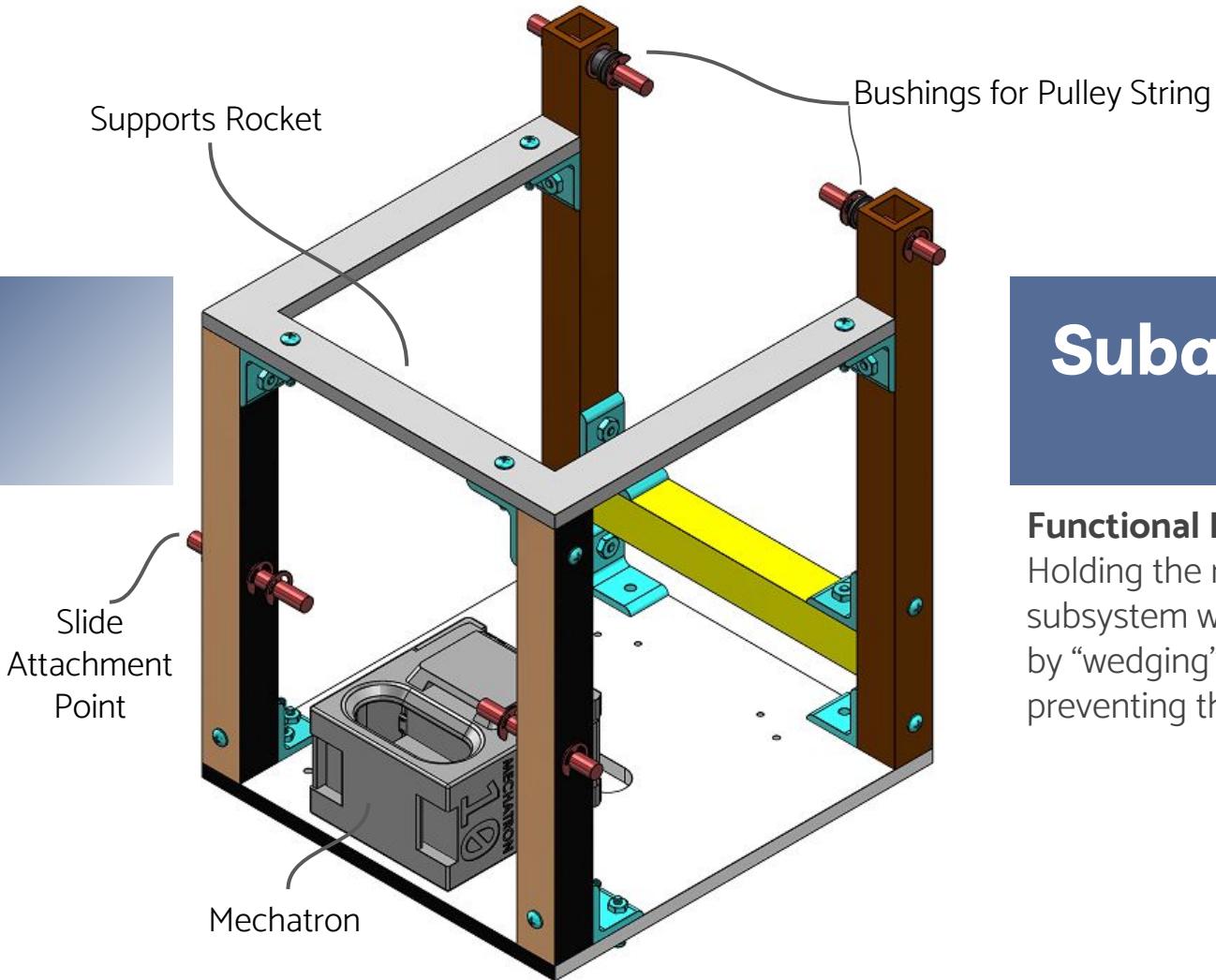
# First Principles Analysis: Incline Torque Requirement





## Final RMP: Full Assembly

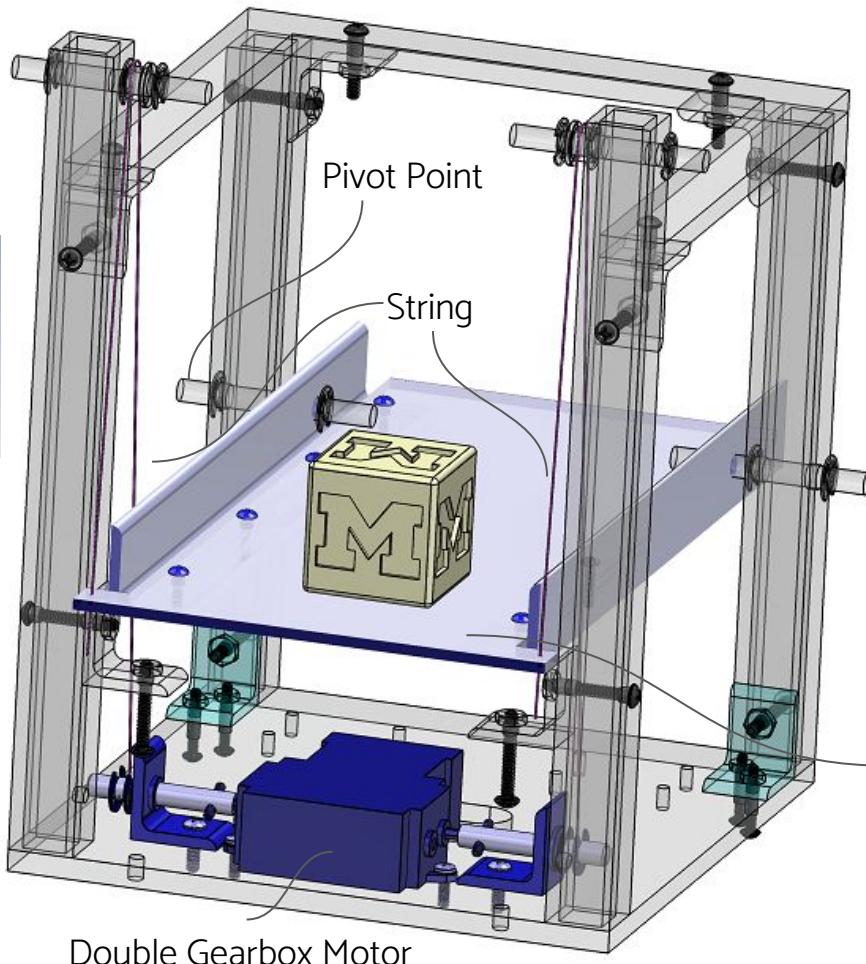
- We chose the final design concept because it was the design with the highest score from the Pugh chart
- The redesigns that we made were done with the purpose of increasing the manufacturability and creativity of the design
- Additionally, the highest ranking design contained many elements from our other designs and thus will effectively achieve the functional requirements.



## Subassembly 1: Chassis

### Functional Requirement:

Holding the rocket open. This subsystem will fulfill this requirement by “wedging” open the rocket doors, preventing them from closing.



## Subassembly 2: Slide

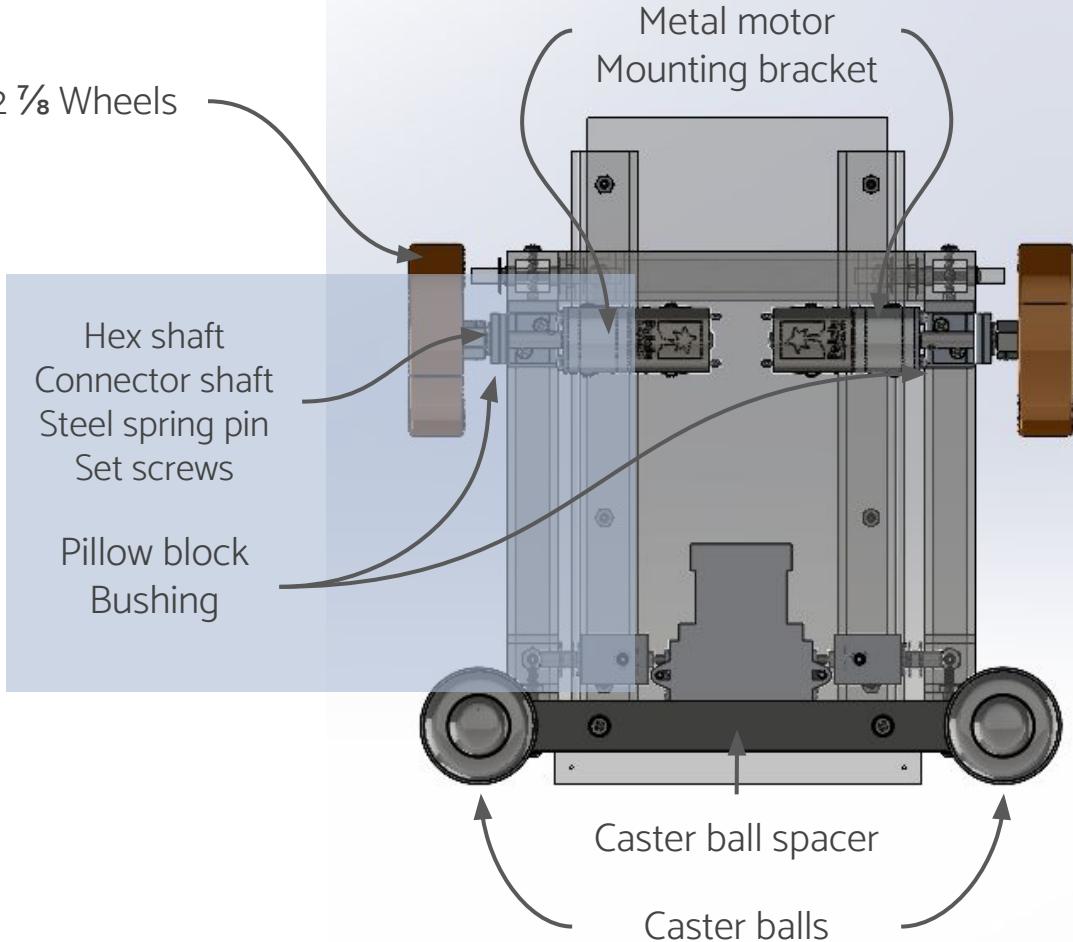
### Functional Requirement:

Depositing Cubes into Rocket. The depositing cube mechanism consists of a pivoting ramp that effectively acts as a slide for cubes into the rocket.

## **Subassembly 3: Most Critical**

- Movement and maneuverability
- Most complex
- Many failure modes

Banebots 2  $\frac{7}{8}$  Wheels

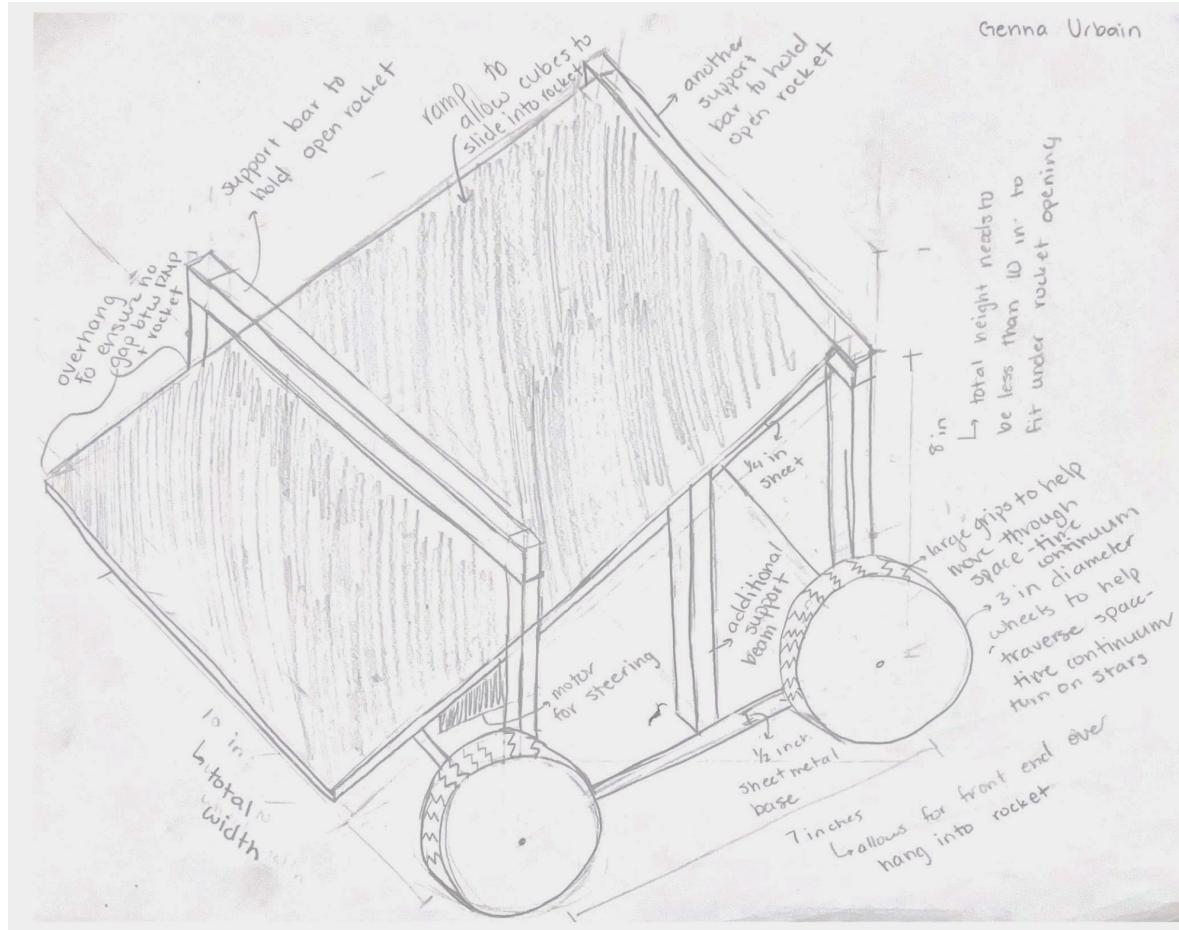


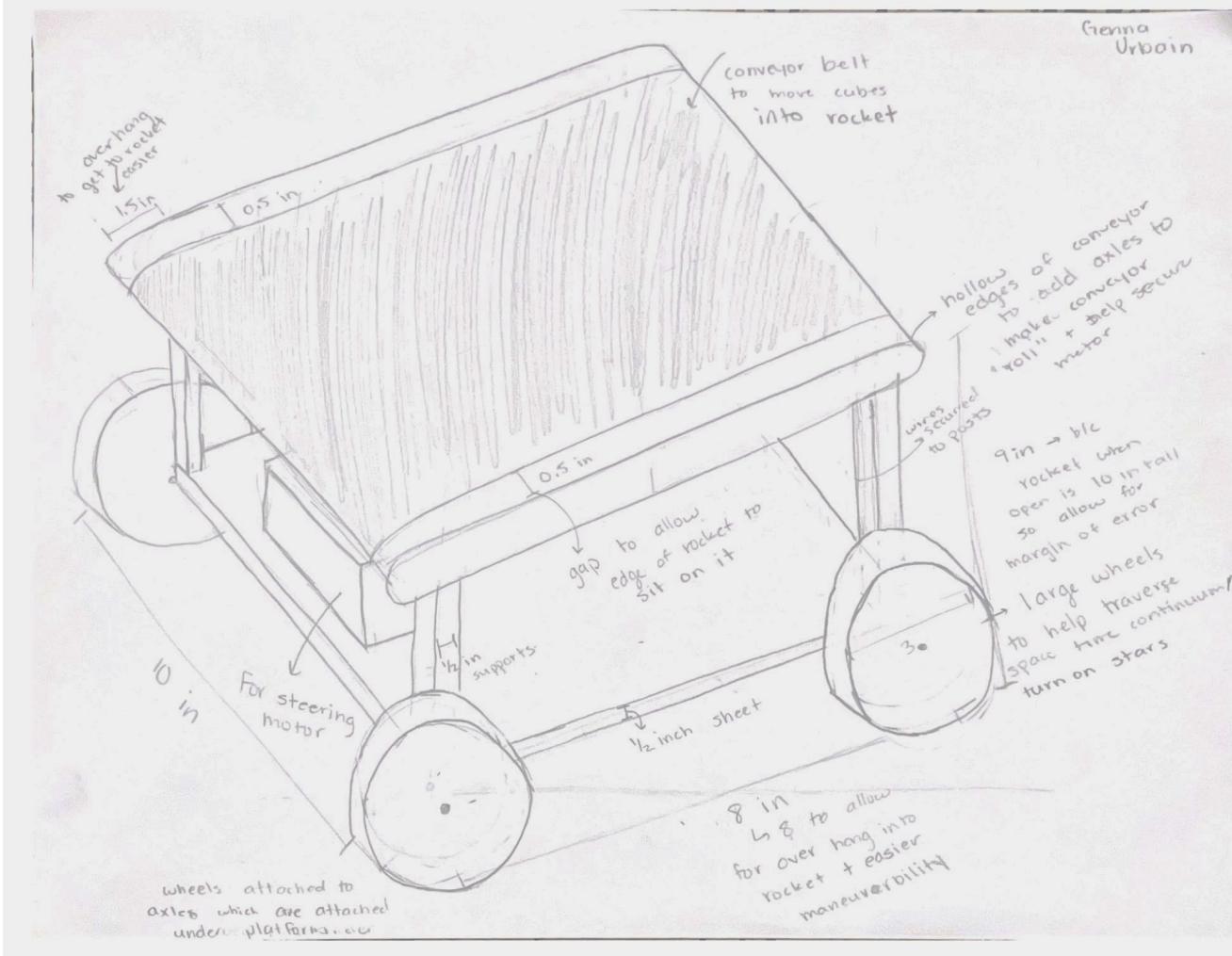
# Concluding Issues

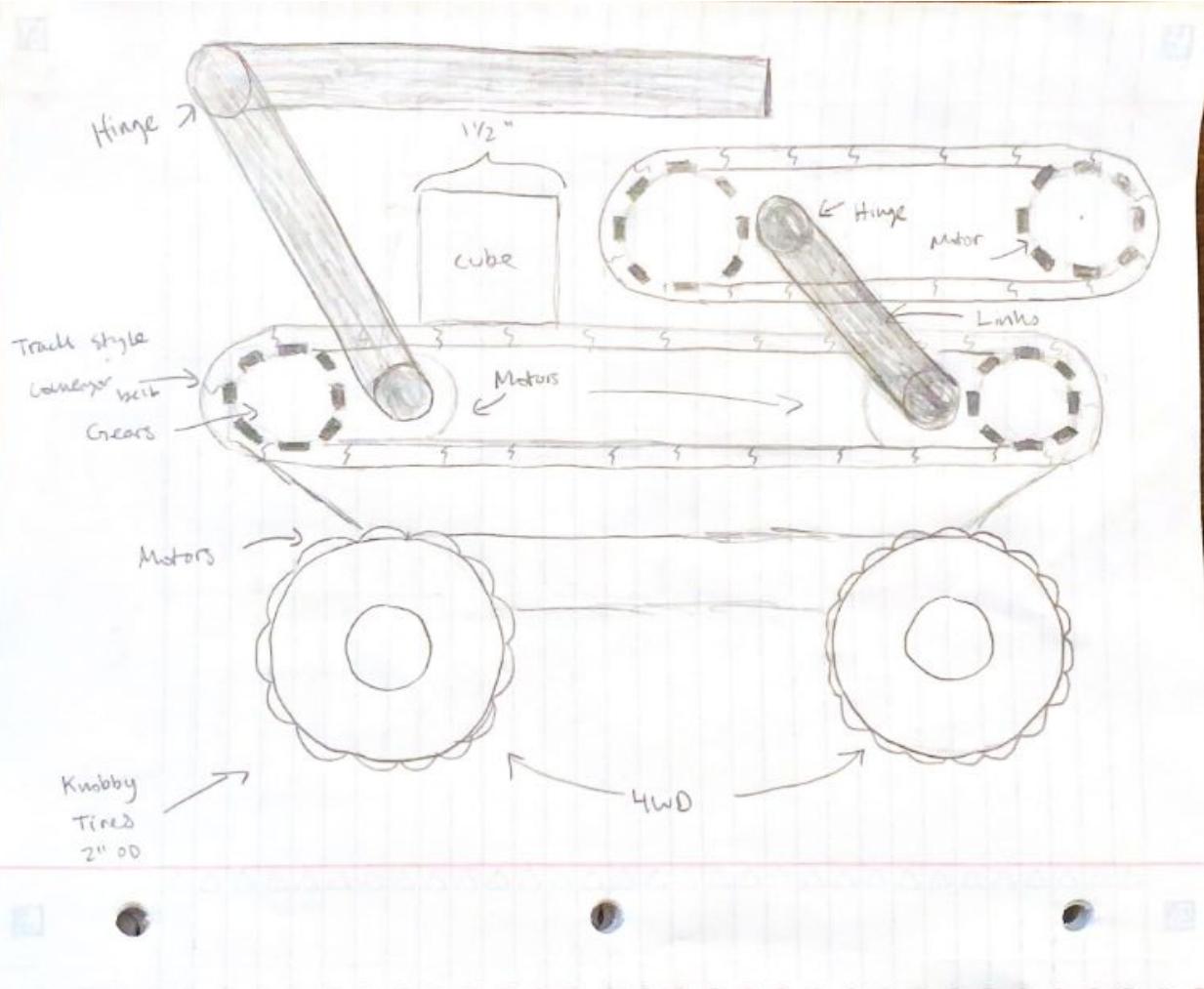
- Special Materials/Components:
  - May have to use 6-32 1.25" screws
- Expected Design and Manufacturing Challenges
  - Long wait times for waterjet (for base plate and top support)
  - Imprecise milling on parts leading to assembly failure
- Risks of Strategy/Design
  - If for some reason, the double gearbox cannot pull up the slide properly, then the RMP will not be able to deposit cubes
  - Not being able to trade enough materials in order to get the materials needed
  - Caster ball spacer may have too much stress

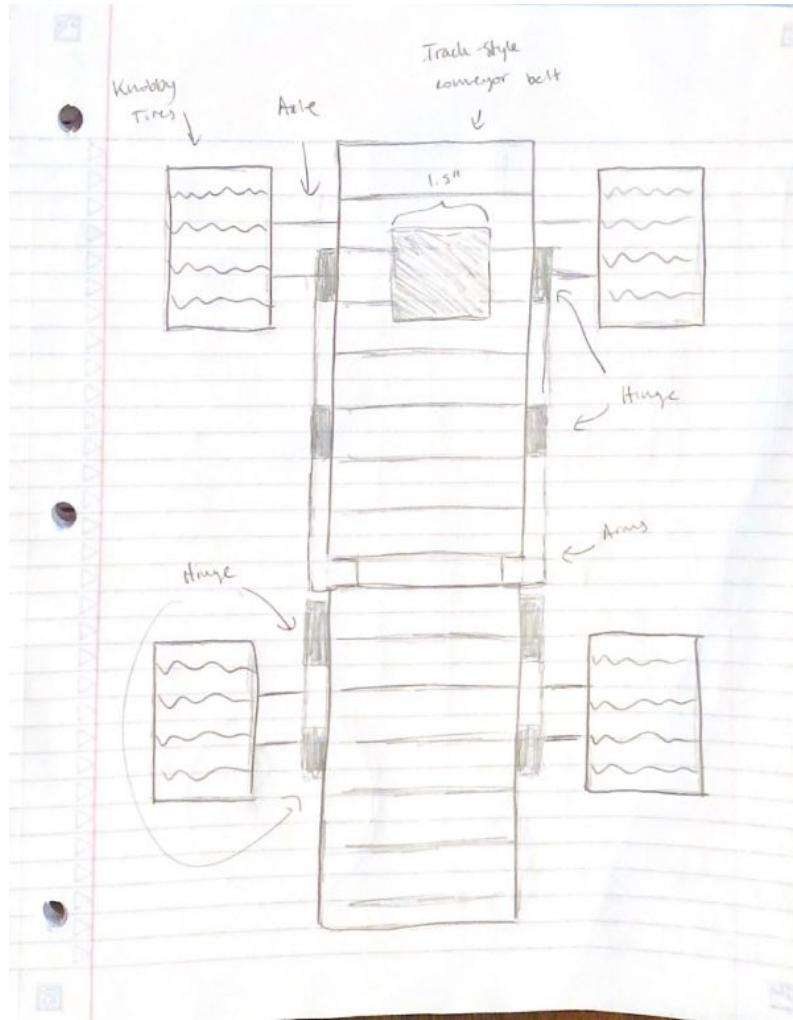
# Appendix

# Preliminary Design Concept Sketches:

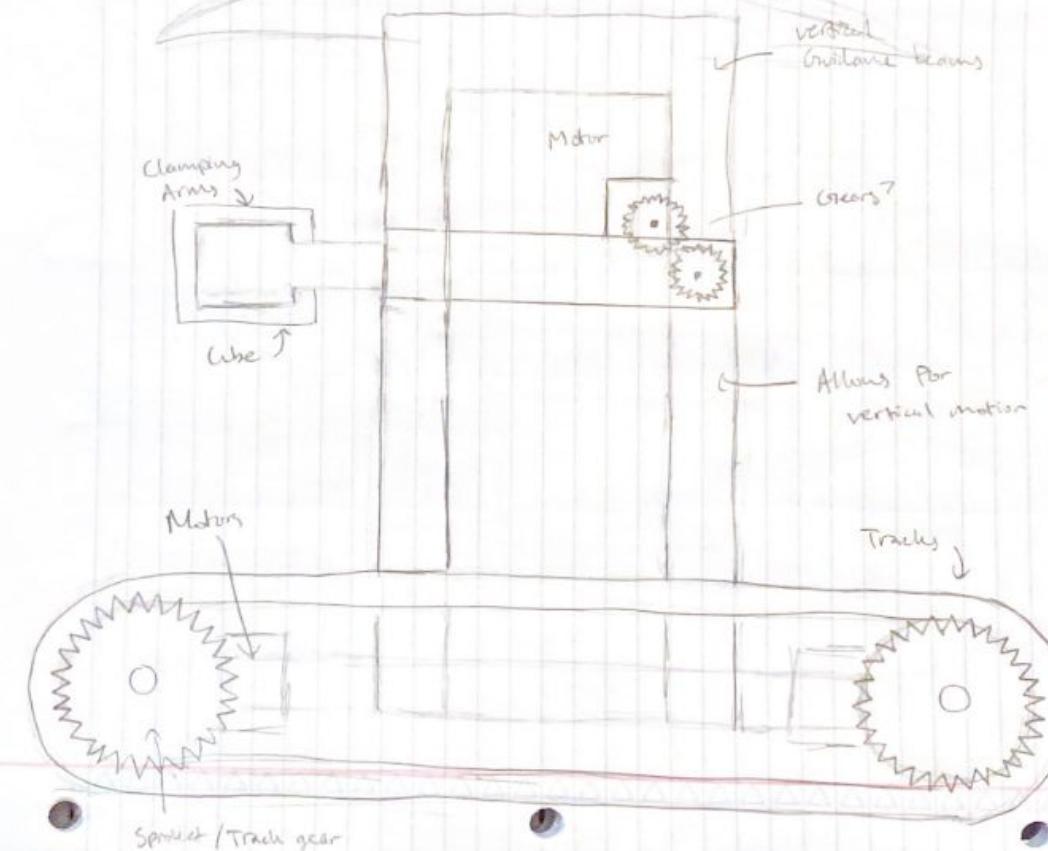


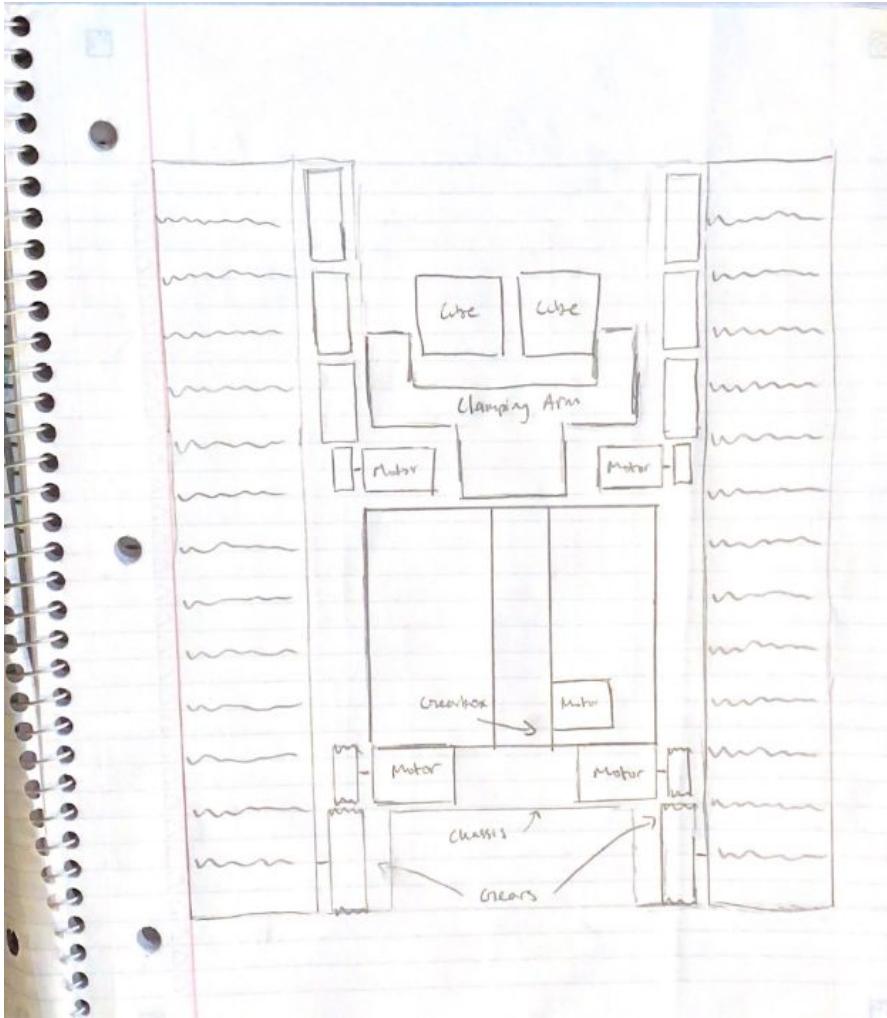


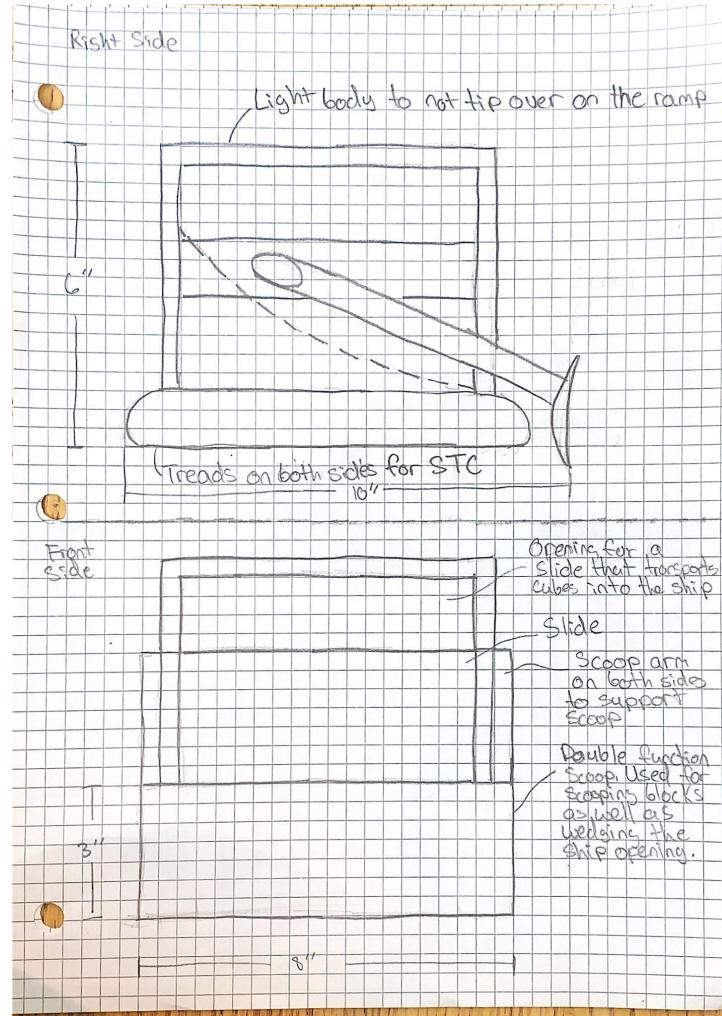


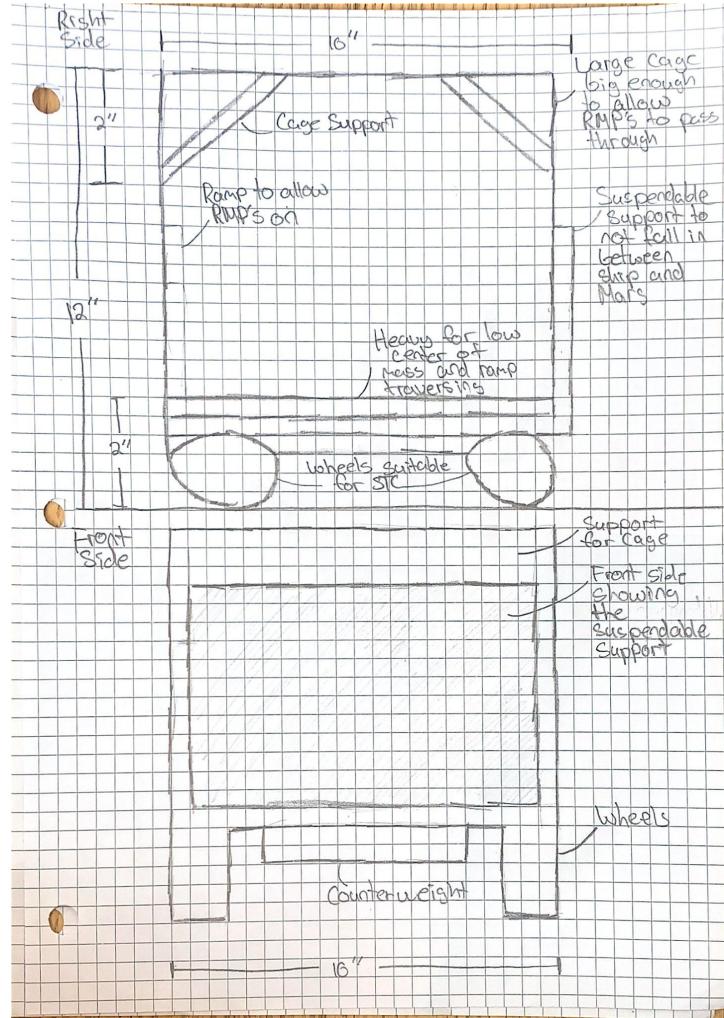


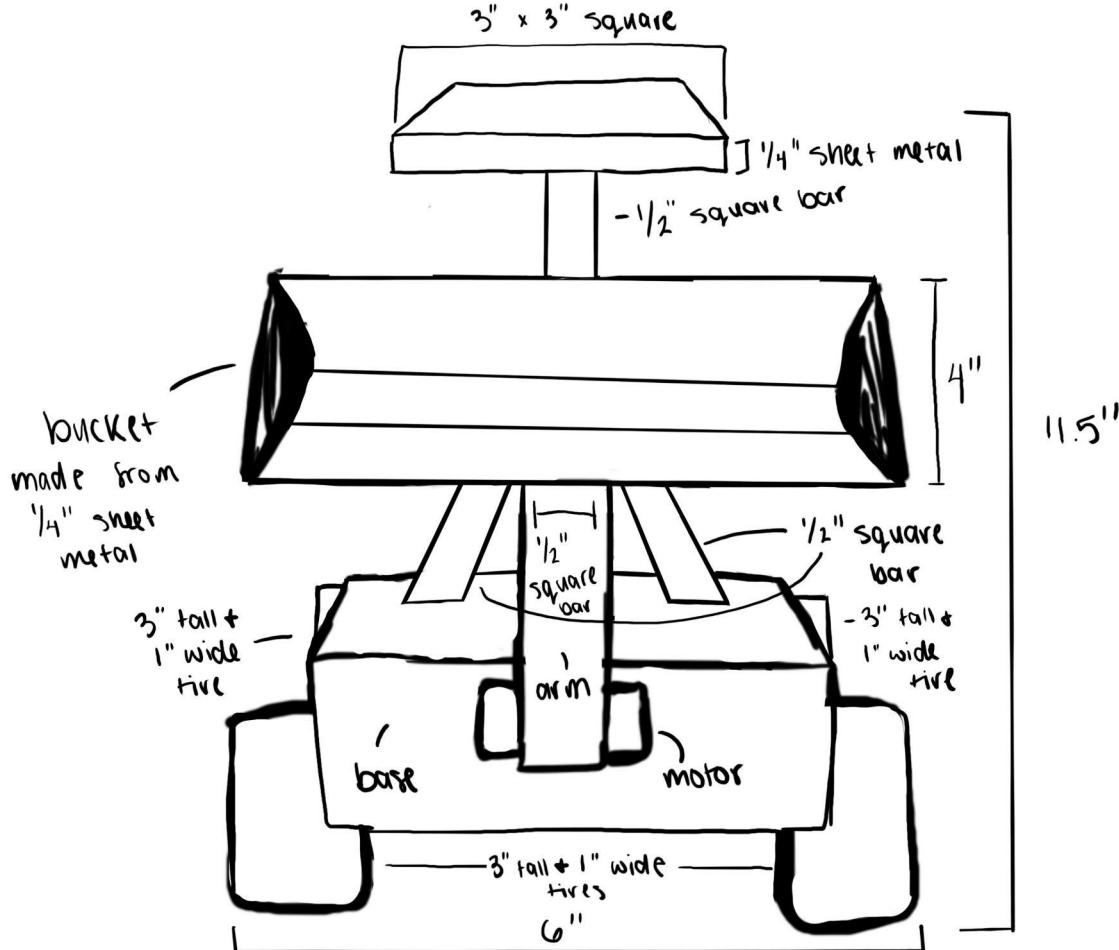
Gullwing Dome on top ↗

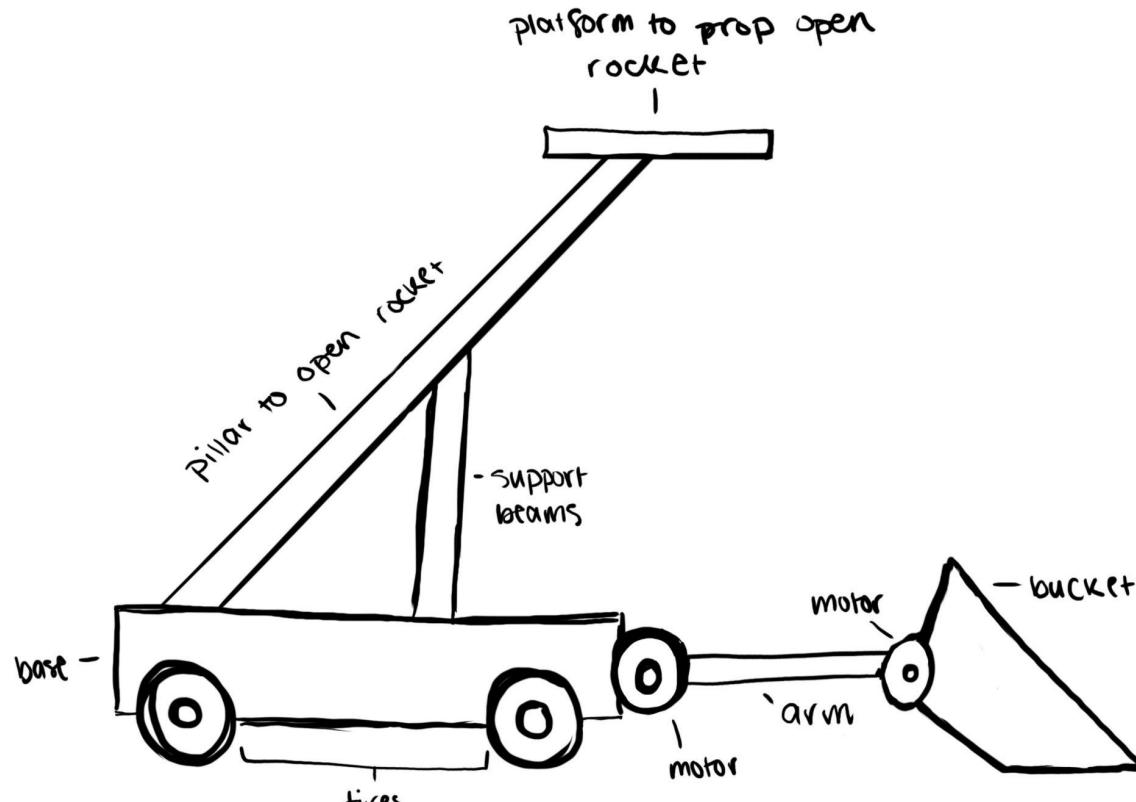




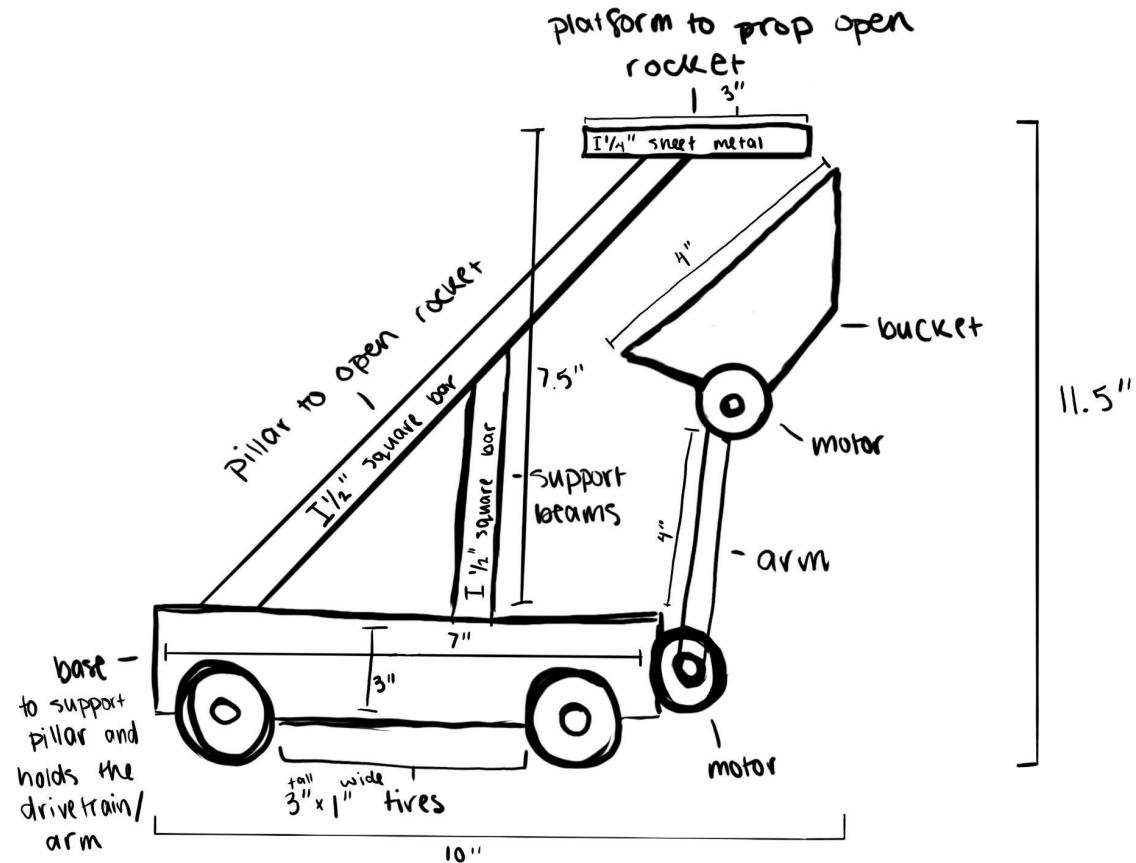




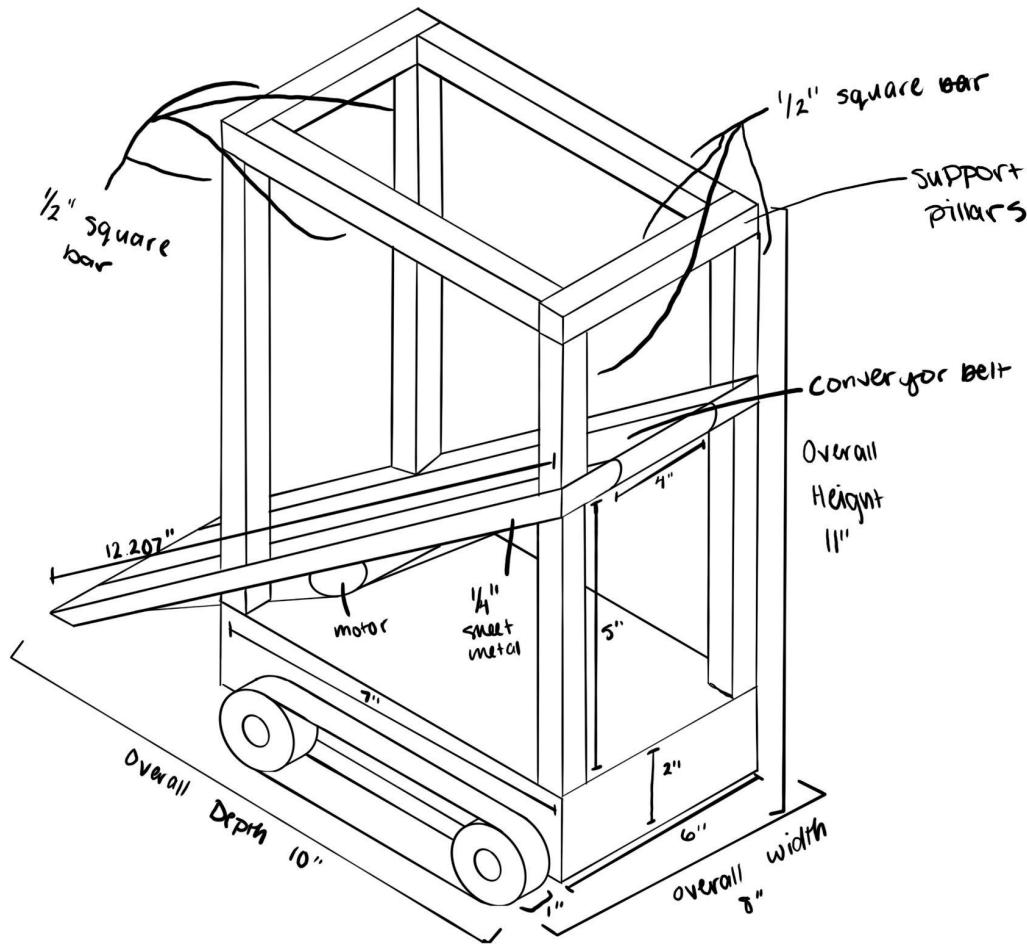




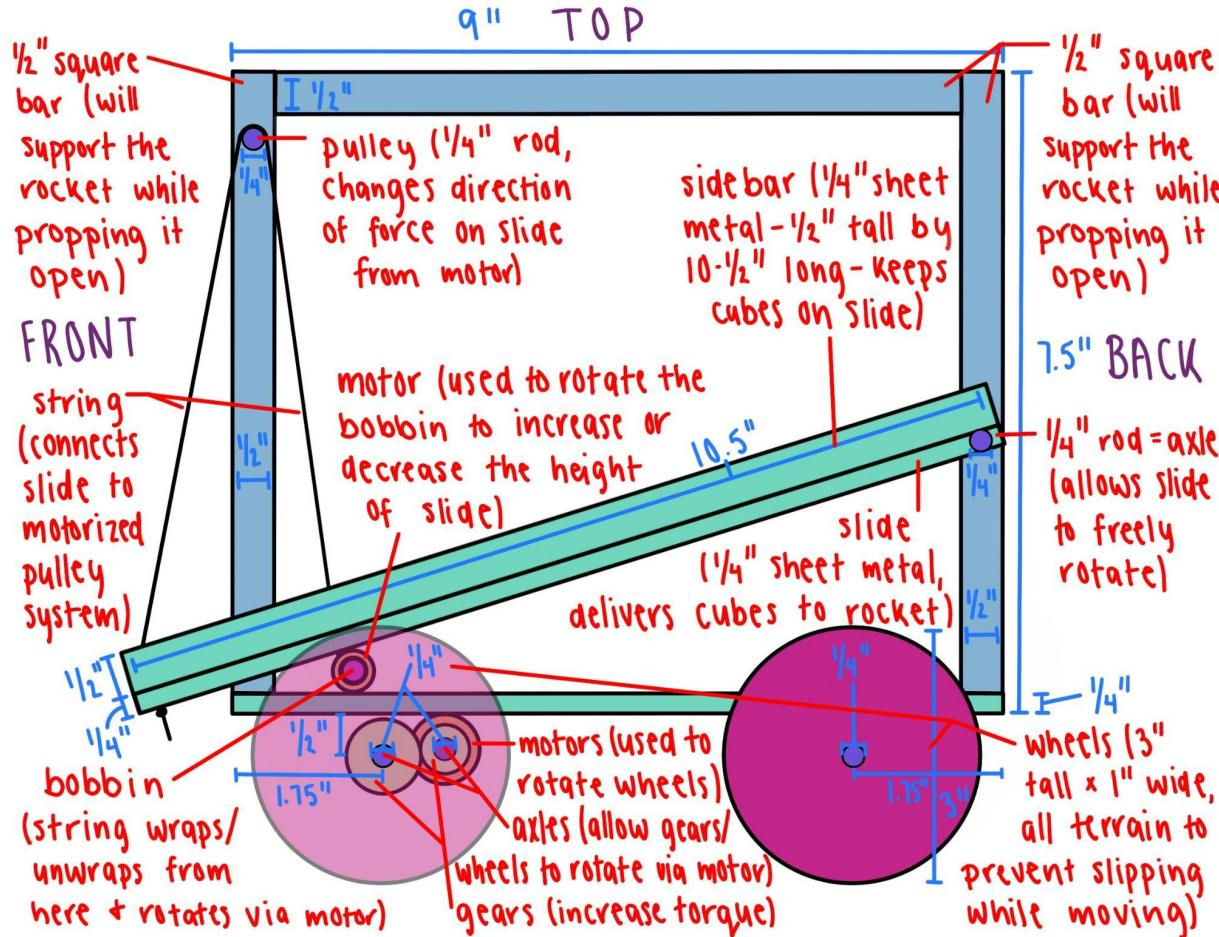
Working position

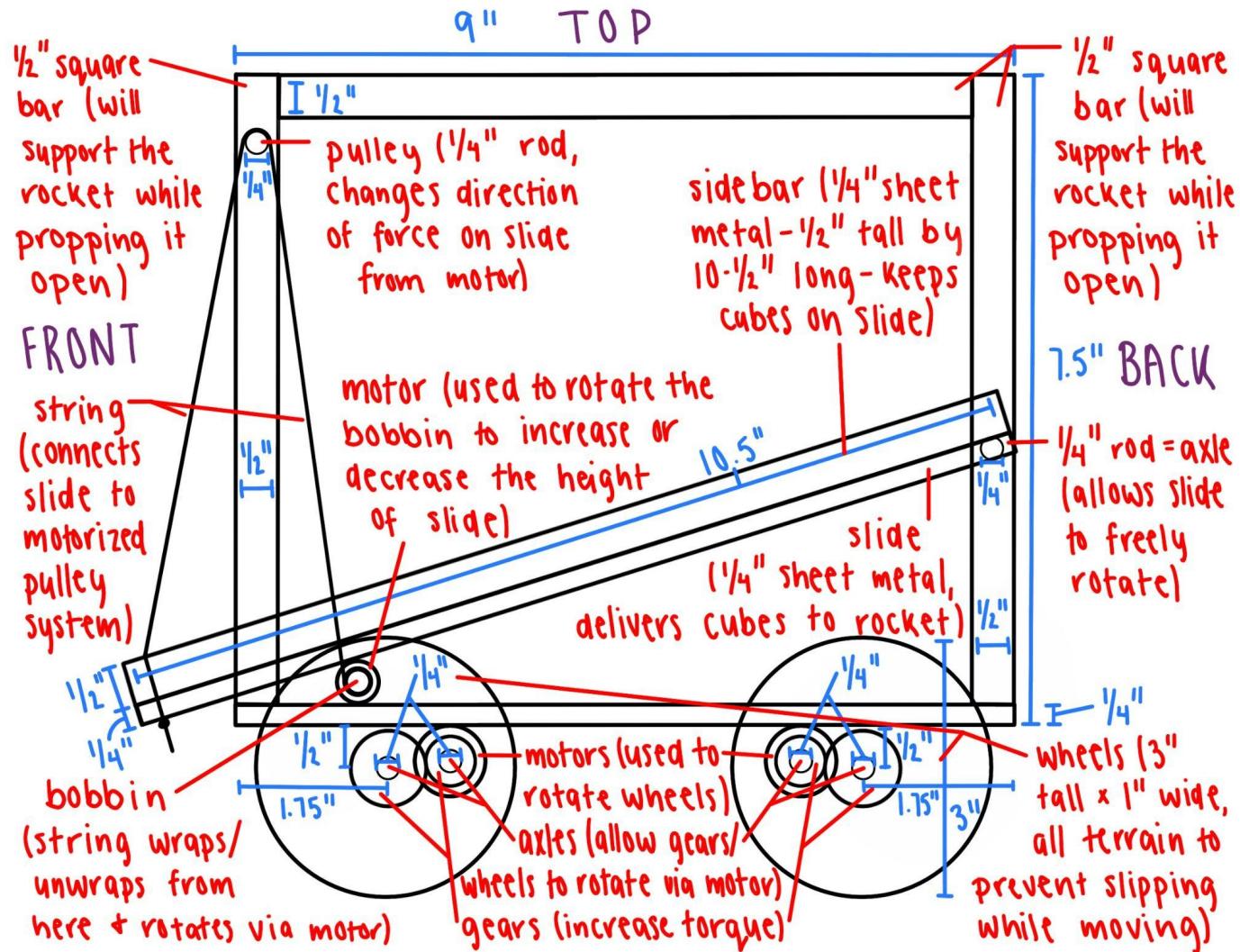


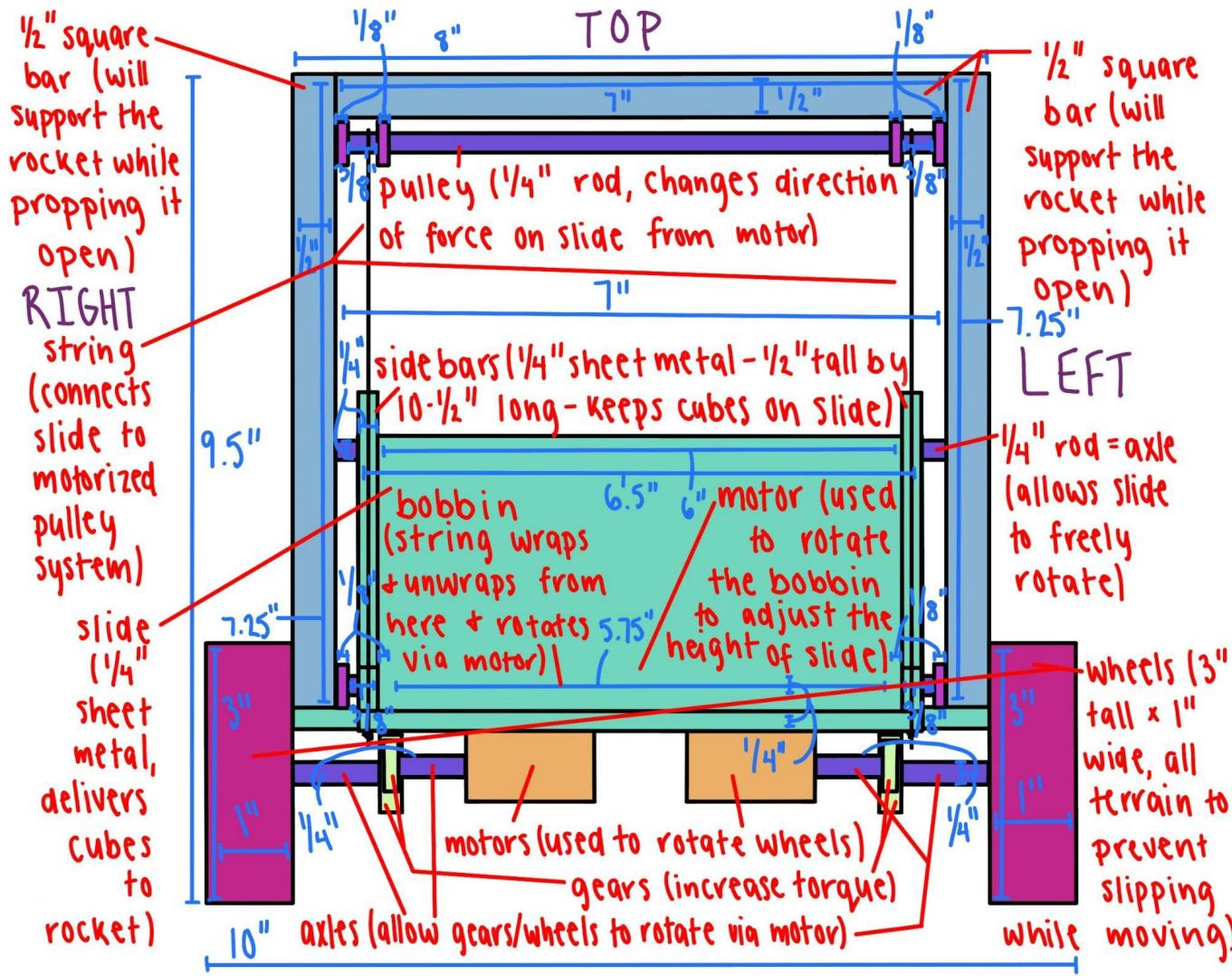
Starting position

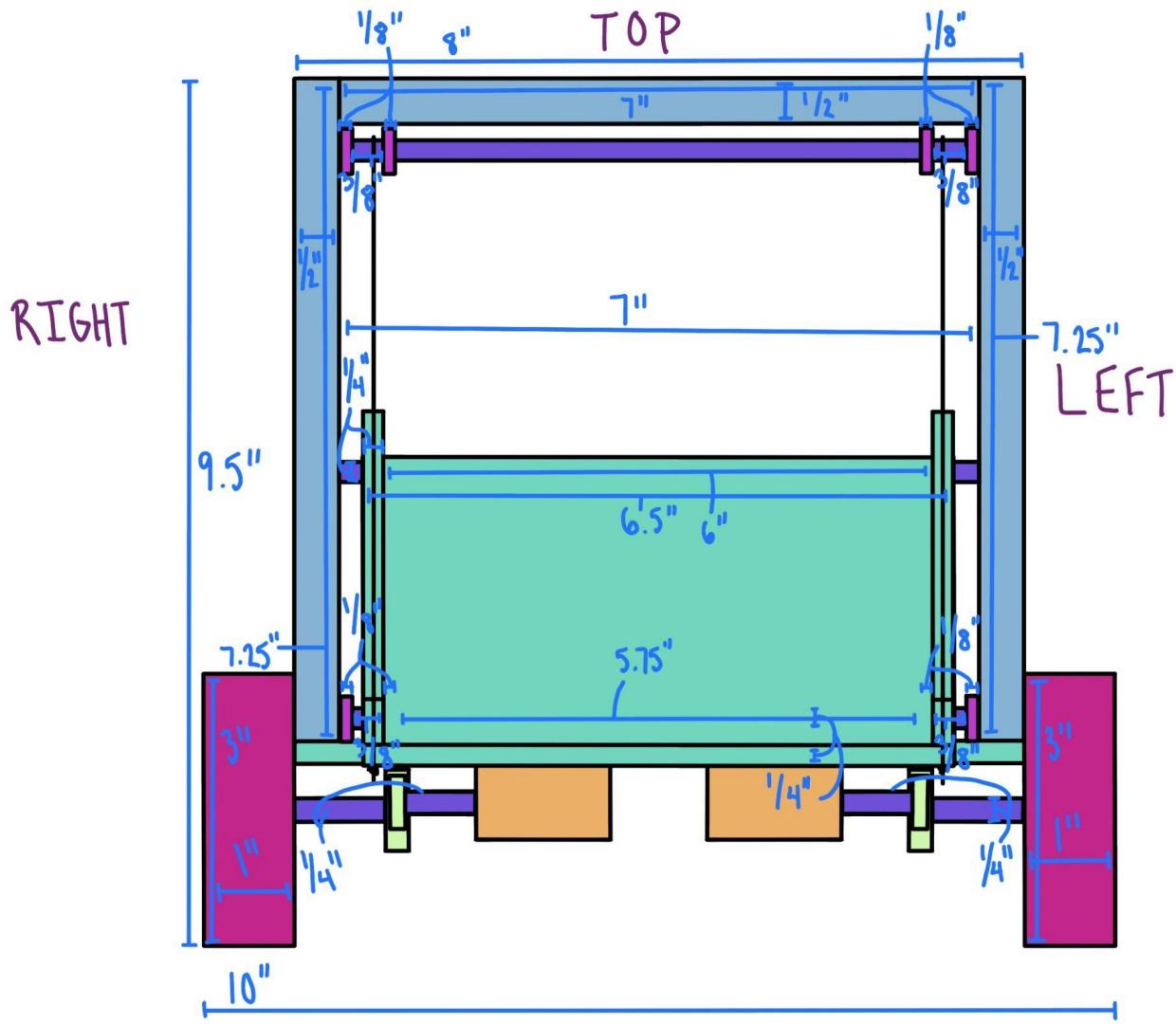


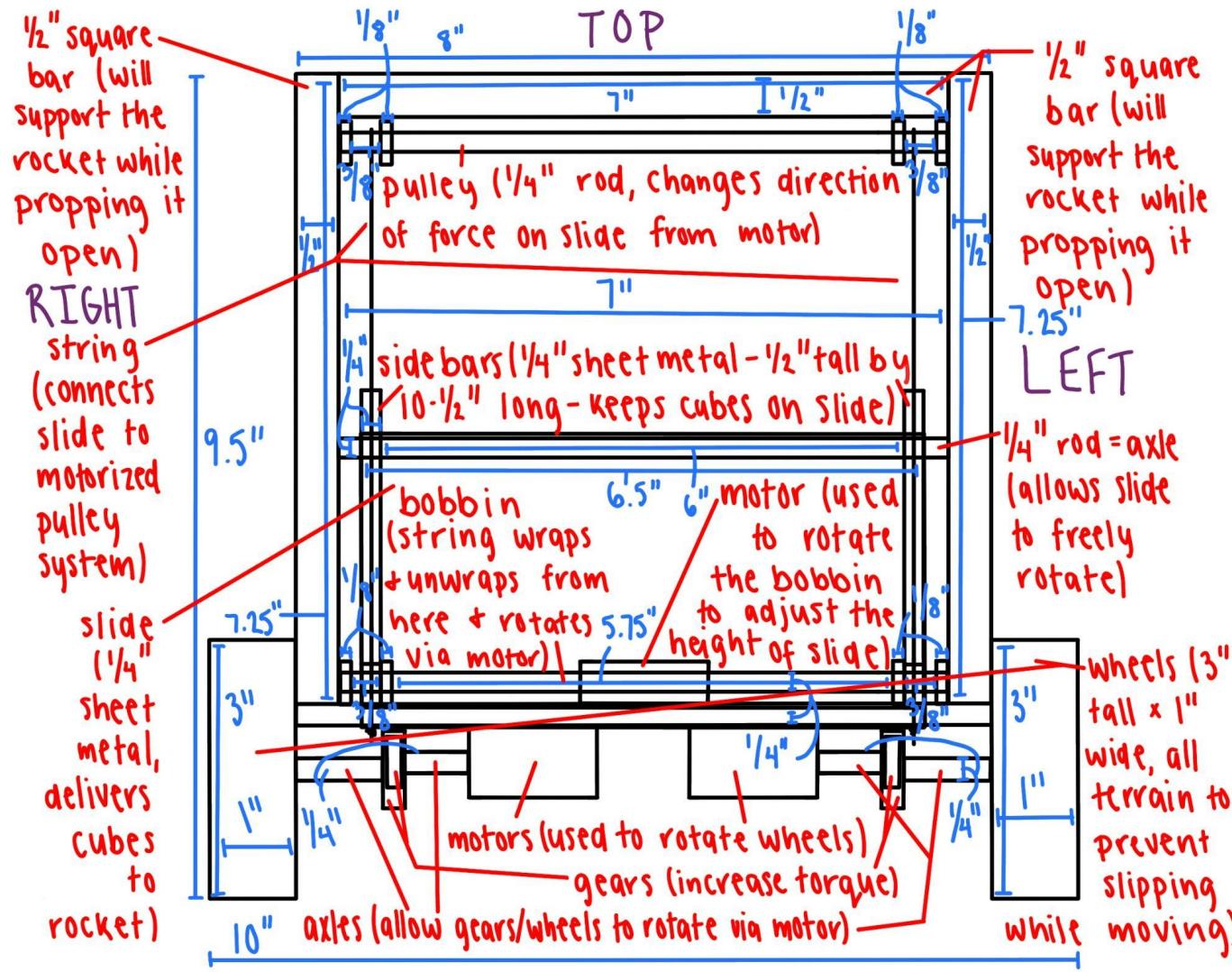
# More RMP Final Concept Sketches:







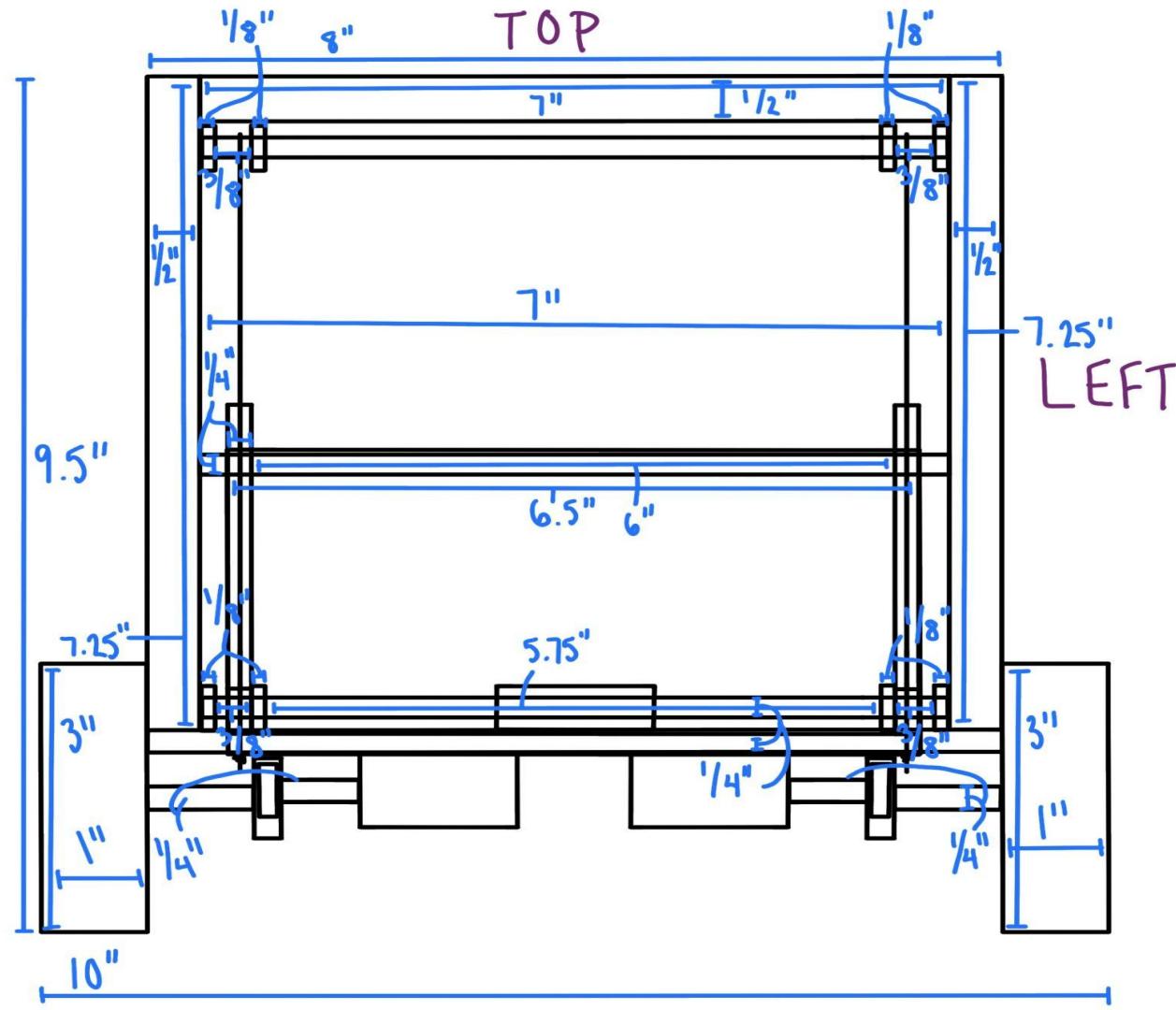


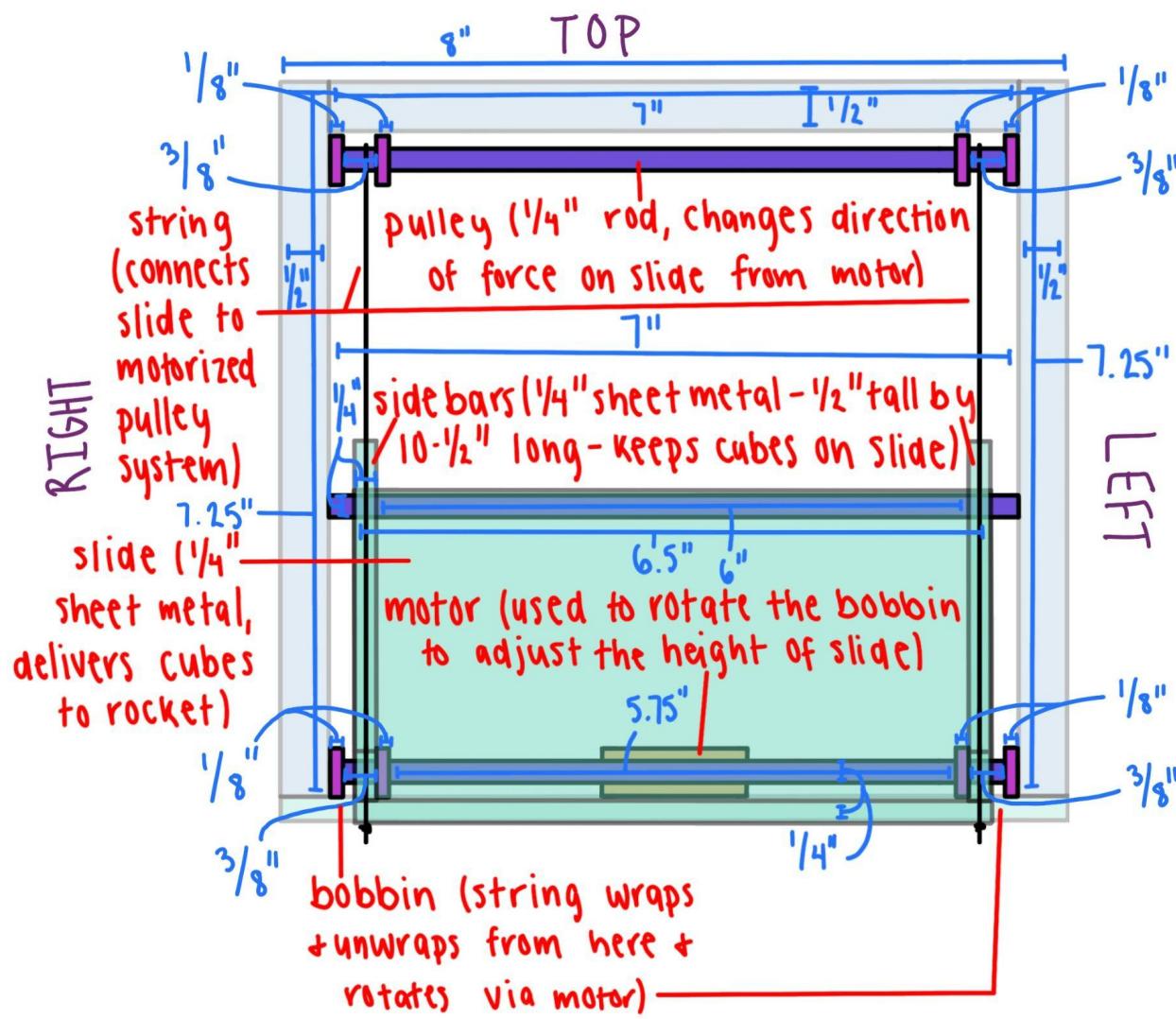


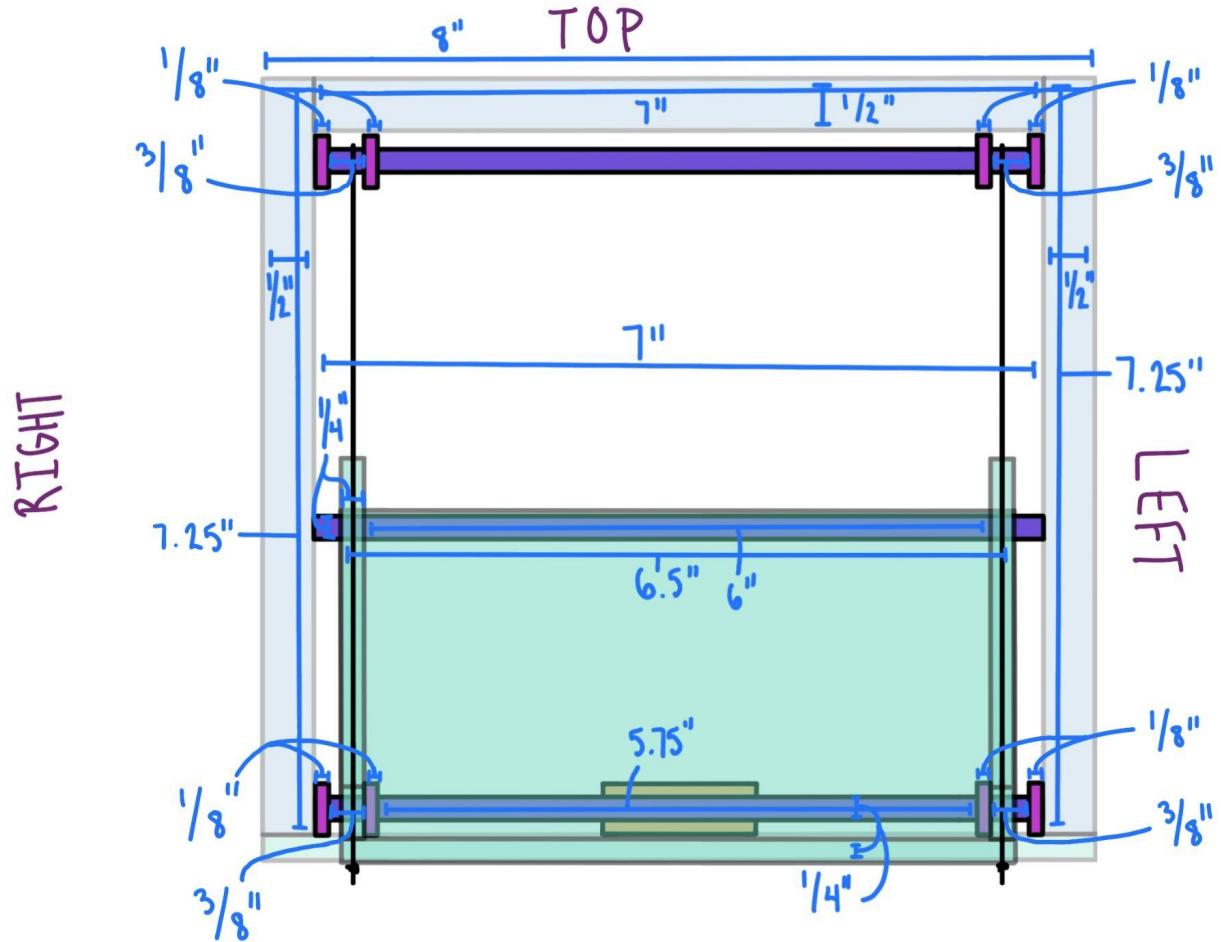
RIGHT

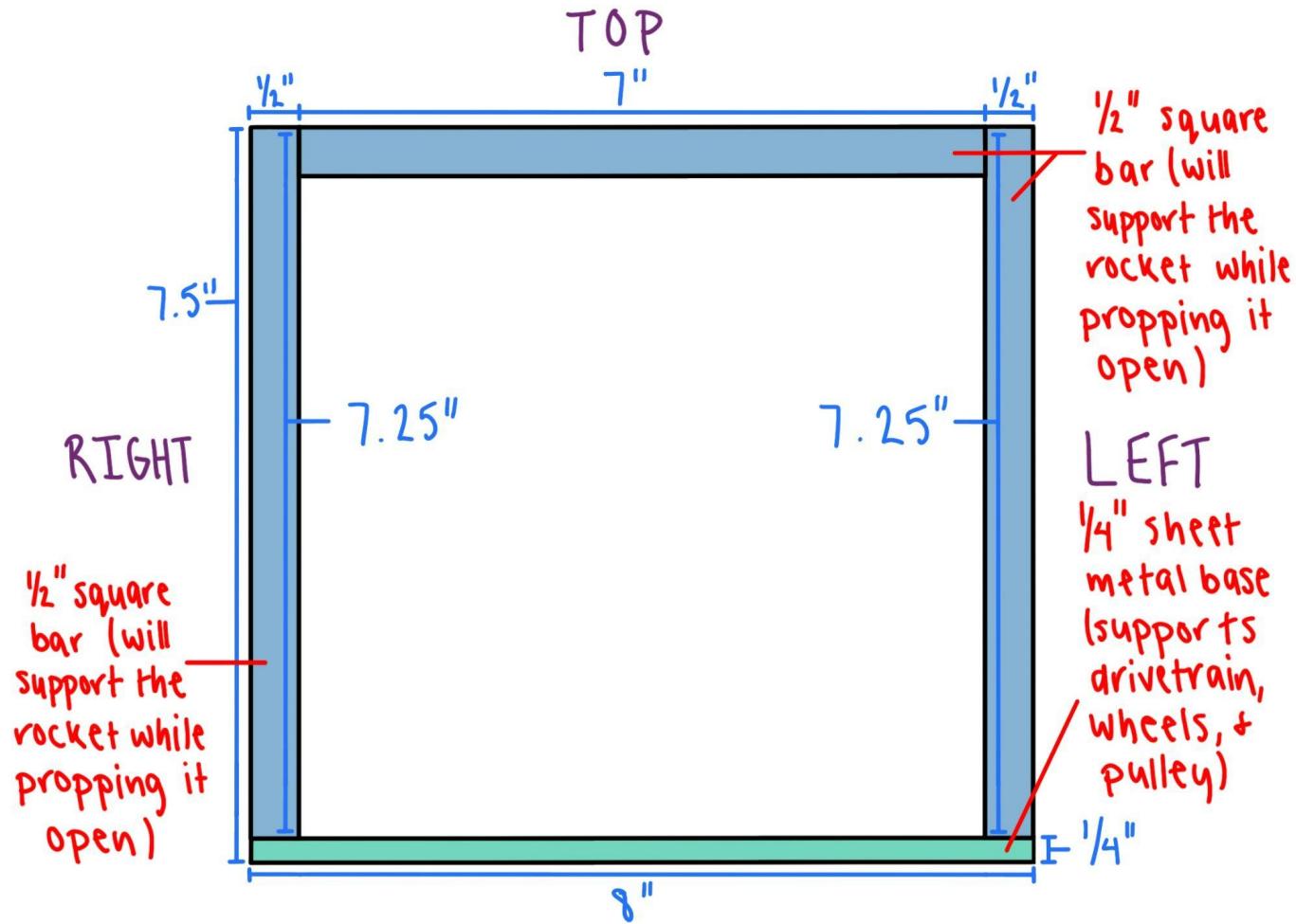
TOP

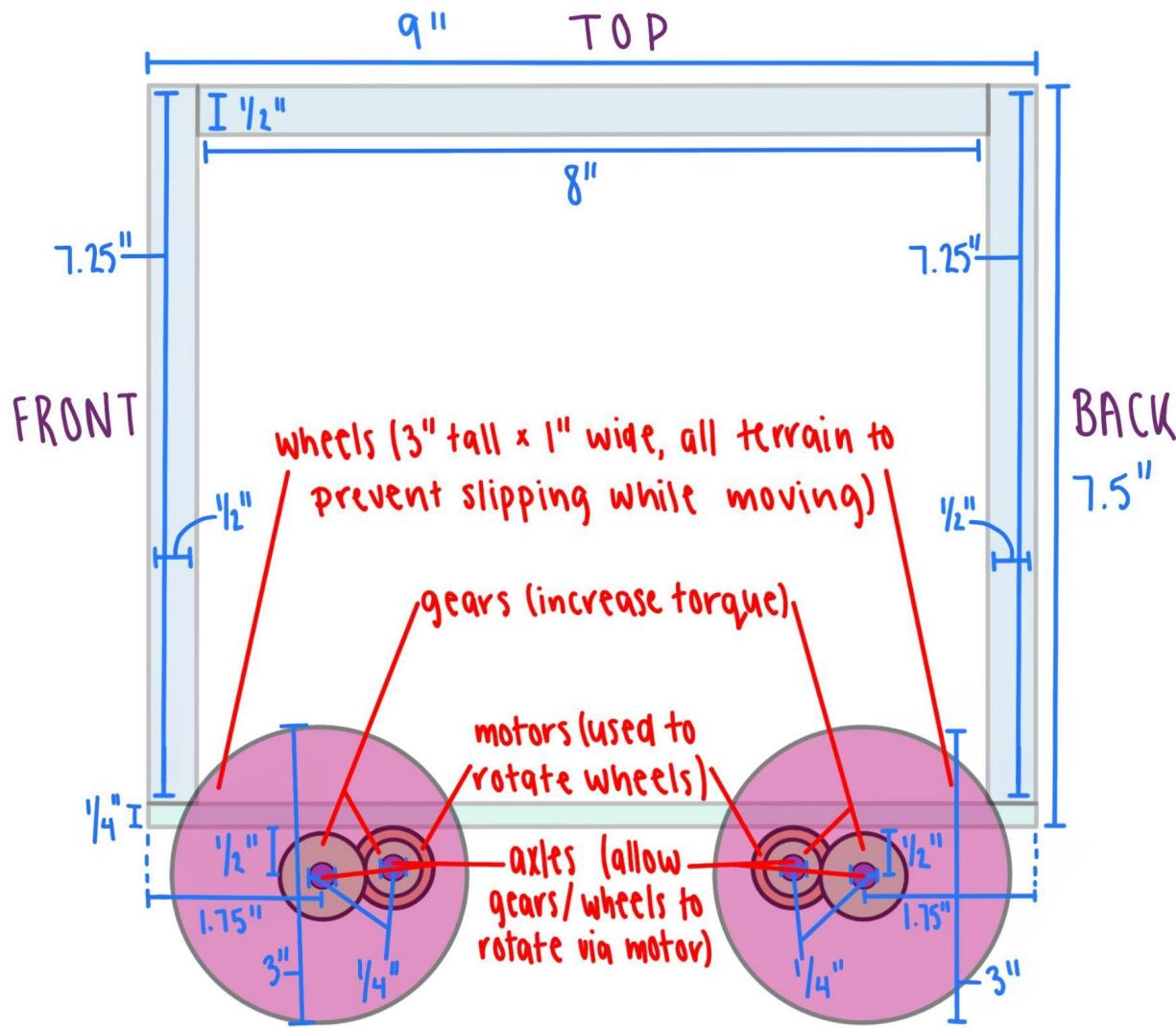
LEFT









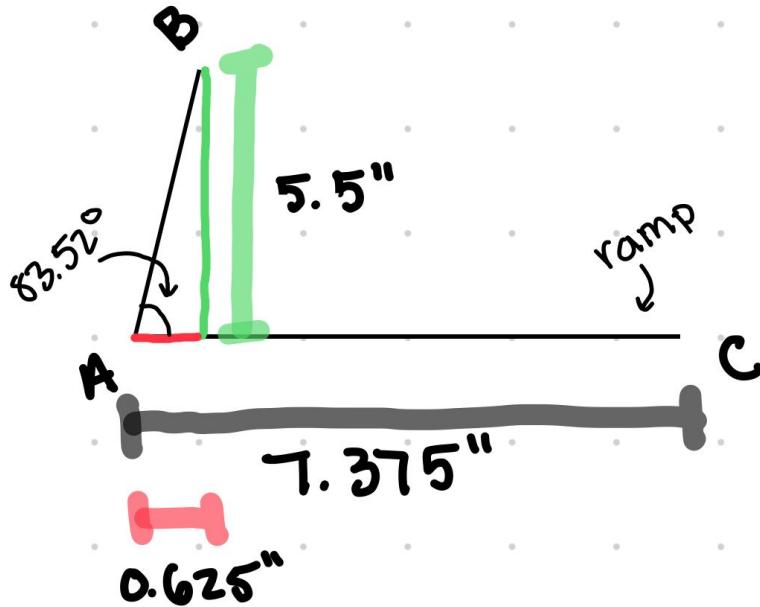


# Empirical Testing Data

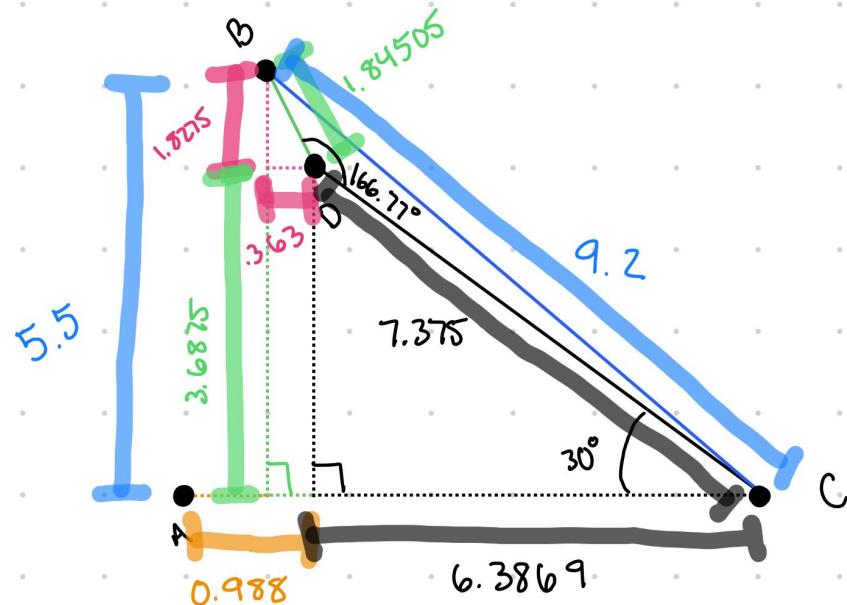
Material	Delrin			Acrylic			1/16 in Sheet Metal			
	Angle	20 degrees	30 degrees	40 degrees	30 degrees	40 degrees	50 degrees	30 degrees	40 degrees	50 degrees
Trial 1		0.93	0.33	0.15	5.35	0.35	0.18	0.43	0.25	0.16
Trial 2		1.37	0.2	0.12	0.57	0.24	0.17	0.31	0.29	0.17
Trial 3		0.68	0.26	0.15	0.64	0.19	0.16	0.45	0.25	0.17
Trial 4		1.34	0.21	0.13	0.57	0.23	0.2	0.3	0.17	0.17
Trial 5		0.61	0.3	0.16	0.38	0.2	0.19	0.33	0.19	0.15
Trial 6		1.01	0.28	0.17	0.48	0.31	0.21	0.43	0.17	0.11
Trial 7		0.61	0.29	0.13	0.61	0.34	0.23	0.34	0.25	0.13
Trial 8		1.26	0.3	0.14	0.48	0.22	0.21	0.4	0.27	0.15
Trial 9		0.59	0.25	0.16	0.46	0.28	0.15	0.37	0.2	0.16
Trial 10		0.93	0.32	0.14	1.05	0.25	0.16	0.37	0.19	0.13

# First Principles Analysis: Incline Torque Requirement

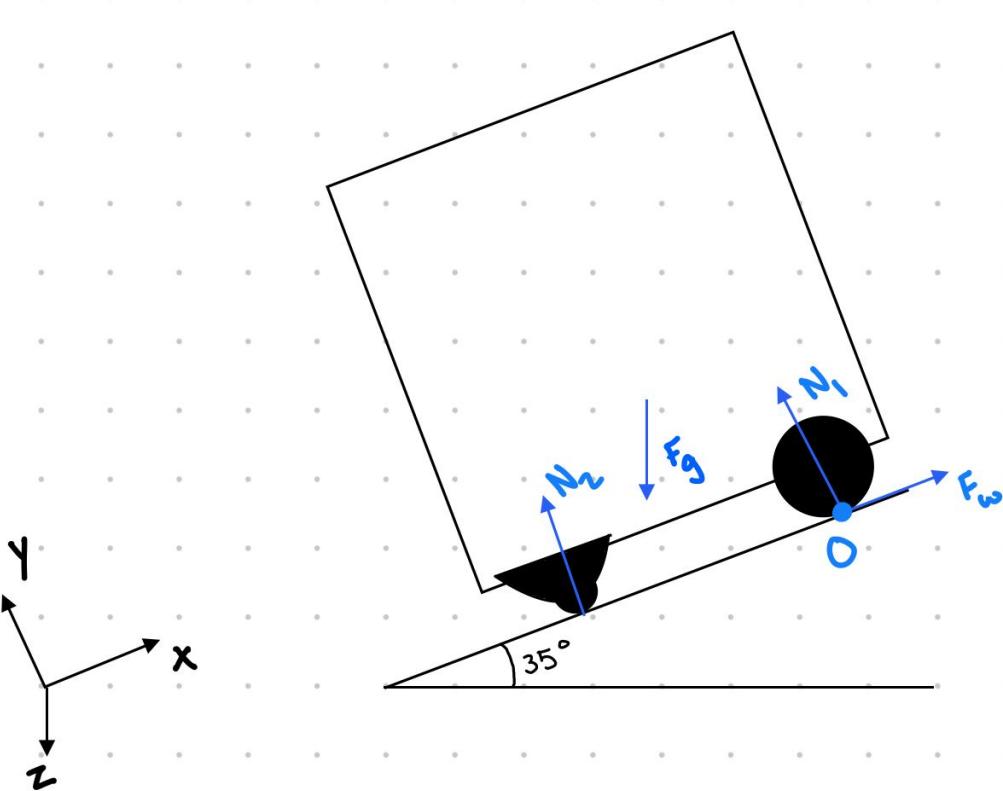
State 1:



State 2:



# First Principles Analysis: Incline Torque Requirement



# Metal Motor Analysis

Gear Ratio(@98.78)	Theoretical Torque Output(oz*in)	Angular Speed(RPM)	Angular Speed(Rad/s)	Linear Speed(IN/S)
1	210	99	10.362	0.8154894
0.2	42	495	51.81	4.077447
0.25	52.5	396	41.448	3.2619576
0.33	69.3	300	31.4	2.47118
0.5	105	198	20.724	1.6309788
2	420	49.5	5.181	0.4077447
3	630	33	3.454	0.2718298
4	840	24.75	2.5905	0.20387235
5	1050	19.8	2.0724	0.16309788

$$T = 1.7067 \text{ lb}$$

$$T_{out} = 1.7067(0.25) = 0.4267 \text{ lb} \cdot \text{in} = 6.827 \text{ oz} \cdot \text{in}$$

# Double Gearbox Motor Analysis

Gear Ratio	Torque Output(oz*in)	Angular Speed(RPM)	Angular Speed(Rad/s)	Linear Speed(IN/S)
12.7	1.27	968.503937	101.3700787	5.990971654
38	3.8	323.6842105	33.87894737	2.002245789
115	11.5	106.9565217	11.19478261	0.6616116522
344	34.4	35.75581395	3.74244186	0.221178314

$$T = 1.7067 \text{ lb}$$

$$T_{out} = 1.7067(0.25) = 0.4267 \text{ lb} \cdot \text{in} = 6.827 \text{ oz} \cdot \text{in}$$

# Planetary Motor Analysis

Gear Ratio	Torque Output(oz*in)	Angular Speed(RPM)	Angular Speed(Rad/s)	Linear Speed(IN/S)
4	0.96	1700	177.9333333	14.00335333
5	1.2	1360	142.3466667	11.20268267
16	3.84	425	44.48333333	3.500838333
20	4.8	340	35.58666667	2.800670667
25	6	272	28.46933333	2.240536533
80	19.2	85	8.896666667	0.7001676667
100	24	68	7.117333333	0.5601341333
400	96	17	1.779333333	0.1400335333

# **Motor and Wheel Assembly Closeup**

