

Module 4: Water in soils (part 2)

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COURSE CONTENTS AND SCHEDULE

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Tentative schedule

| Day | Date | Topic | Lab. |
|-----|-----------|--|-----------------------------|
| W | 1/19/2022 | Class introduction, syllabus, policies | Soil components |
| F | 1/21/2022 | Invited speaker: Topic TBD | Grain size dist. |
| M | 1/24/2022 | Introduction: The geological cycle, soil origin | |
| W | 1/26/2022 | Introduction: Site investigation | |
| F | 1/28/2022 | Index properties: Phase relationships | |
| M | 1/31/2022 | Index properties: Grain size distribution, Atterberg limits | Atterberg limits |
| W | 2/2/2022 | Index properties: Soil classification | |
| F | 2/4/2022 | Compaction | |
| M | 2/7/2022 | Quiz 1: Introduction, index properties, compaction, in-situ testing | Visual classification |
| W | 2/9/2022 | Water in soils: Groundwater table, pore pressure, total and effective stresses | |
| F | 2/11/2022 | Water in soils: Darcy's law | |
| M | 2/14/2022 | Water in soils: Permeability and hydraulic conductivity | Compaction |
| W | 2/16/2022 | Water in soils: One-dimensional seepage | |
| F | 2/18/2022 | Water in soils: 2D-3D seepage, flow nets, pore pressure, uplift force, seepage force | |
| M | 2/21/2022 | President's day: no class | In-situ density |
| W | 2/23/2022 | Water in soils: piping | |
| F | 2/24/2022 | Quiz 2: Water in soils | Permeability |
| M | 2/28/2022 | Induced stress: Approximations, Boussinesq's elastic solution | |
| W | 3/2/2022 | Induced stress: Boussinesq's elastic solution, superposition | |
| F | 3/4/2022 | Induced stress: Stress tensor, elastic deformations | |
| M | 3/7/2022 | Consolidation: Oedometer test, primary and secondary consolidation | Site investigation |
| W | 3/9/2022 | Consolidation: Preconsolidation pressure, OCR | |
| F | 3/11/2022 | Consolidation: Primary consolidation parameters | |
| M | 3/14/2022 | Spring break: no class | |
| W | 3/16/2022 | Spring break: no class | |
| F | 3/18/2022 | Spring break: no class | |
| M | 3/21/2022 | Consolidation: rate of consolidation | Bonus |
| W | 3/23/2022 | Consolidation: preloading, radial consolidation | |
| F | 3/25/2022 | Quiz 3: Induced stress and consolidation | Consolidation |
| M | 3/28/2022 | State of stress: 2D stresses and Mohr's circle | |
| W | 3/30/2022 | State of stress: principal stresses, stress invariants, rotations | |
| F | 4/1/2022 | State of stress: Usage of Mohr's circle | |
| M | 4/4/2022 | State of stress: stress paths, simple shear, triaxial compression | Settlement estimates |
| W | 4/6/2022 | Quiz 4: State of stress | |
| F | 4/8/2022 | Shear strength: Mohr-Coulomb failure criteria | |
| M | 4/11/2022 | Shear strength: drained and undrained behavior | Unconfined compression test |
| W | 4/13/2022 | Shear strength: Shear strength of clays | |
| F | 4/15/2022 | Shear strength: Shear strength of sands | |
| M | 4/18/2022 | Quiz 5: Shear strength | Direct shear |
| W | 4/20/2022 | Lateral earth pressure: at-rest, passive, and active conditions ² | |
| F | 4/22/2022 | Intro to slope stability ² | |
| M | 4/25/2022 | Intro to bearing capacity ² | Direct shear |
| W | 4/27/2022 | Maine's day: no class | |
| F | 4/29/2022 | Classes end: Q&A session | |
| M | 5/2/2022 | Final exam (1:30 PM- 3:30 PM) Williams Hall 110 | |

M: Monday - W: Wednesday - F: Friday

²This items may or may not be covered. It will be determined by how far the course has progressed.



RECAP

- We learned about capillary rise.
- We learned about shrinkage/swelling of soils due to water content changes.
- We learned about the ingredients needed for frost action in soils.
- We learned about the principle of effective stress.
- We learned how to calculate geostatic total and effective stress and pore pressure.
- Today 1D water seepage through soils.



CONTENTS

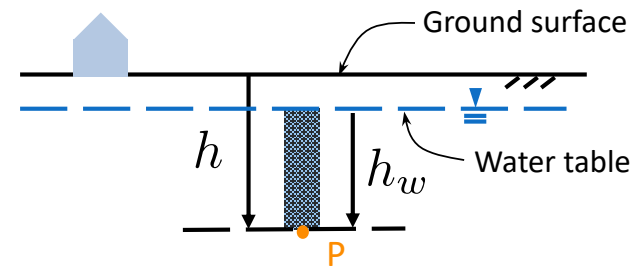
- Total head and Bernoulli's equation.
- Hydraulic gradient.
- Discharge and seepage velocity.
- Darcy's law.
- Hydraulic conductivity and permeability of soils.
- Permeability tests.
- Flow in series and parallel.

More in chapter 7 of Holtz et al. (2013)

WATER IN MOTION

- In this module, we will assume **saturated conditions** .
 - \longrightarrow all voids are fully filled with water
 - \longrightarrow water pressure $u > 0$
- In the last class, we learned how to calculate the **water pressure in saturated soils** under **static conditions** (no flow).

$$u = \gamma_w h_w$$



- In this part, we will study **what happens when WATER MOVES!**

TOTAL HEAD

From fluid mechanics, the most important variable to study the behavior of water is the **TOTAL HEAD** h , which comes from Bernoulli's equation .

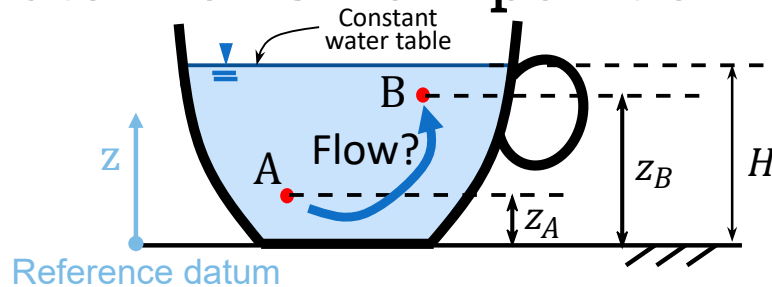
TOTAL head h measures the **total energy per unit weight of water** of a reference volume.

$$h = \frac{u}{\gamma_w} + z$$

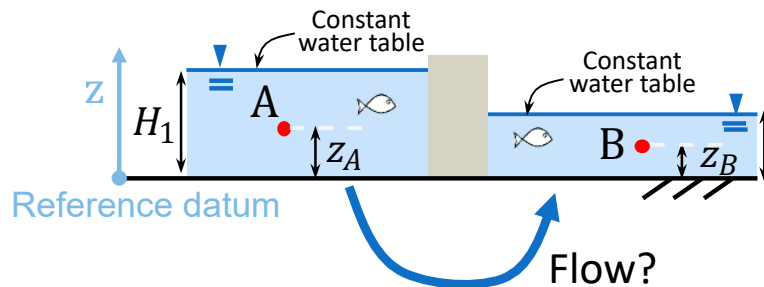
- z = elevation

WATER IN MOVEMENT

- To have flow, there needs to be a difference in total head $\Delta h \neq 0$
- Water flows from point of higher h to points of lower h .



Example: dam



HYDRAULIC GRADIENT

Is the **gradient** or change of **total head** over a length L of flow path.

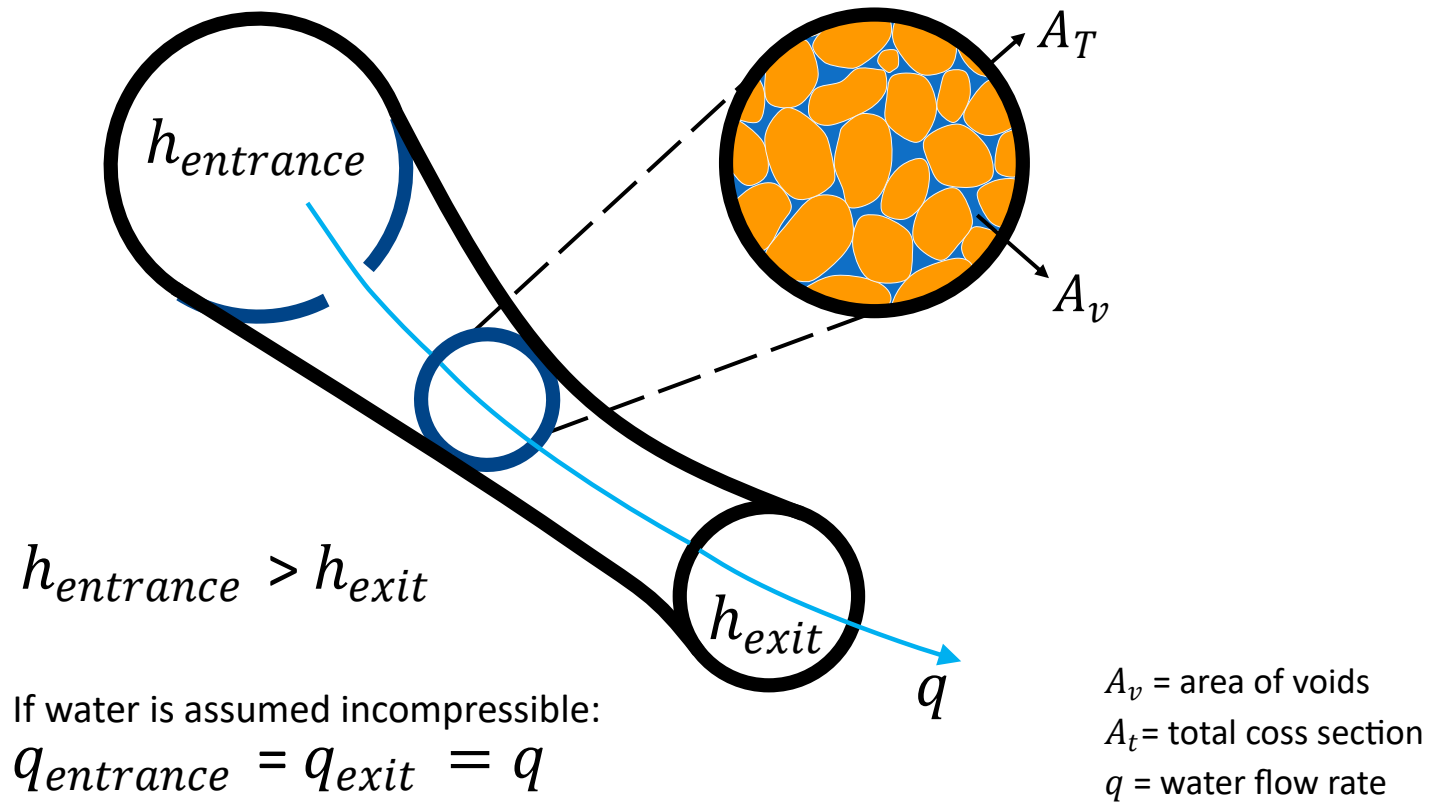
$$i = \frac{\Delta h}{L}$$

Where $\Delta h = h_a - h_b$ with $h_a > h_b$.

- $i = 0 \longrightarrow$ no flow.
- $i \neq 0 \longrightarrow$ flow between the two points.

WATER IN MOVEMENT

Flow tube or "Pipe"



TRUE SEEPAGE VELOCITY

Water flow rate q :

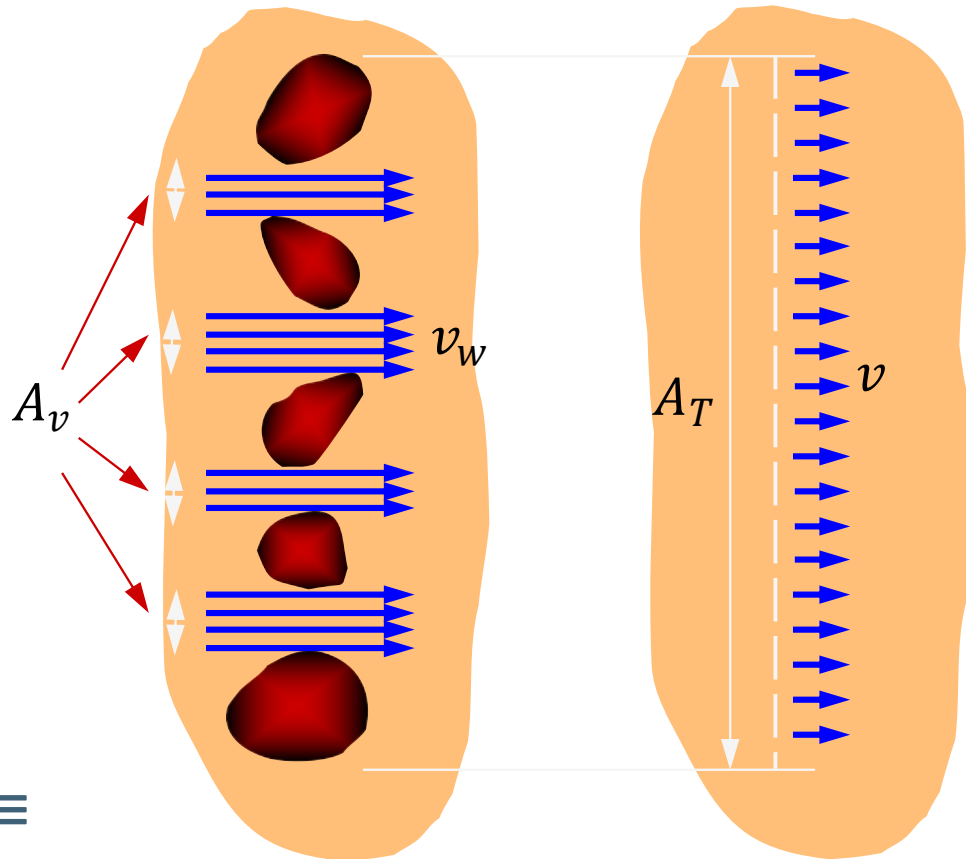
$$q = v_w A_v = v A_t$$

"Discharge" velocity (or Darcy velocity) v

$$v = v_w \frac{A_v}{A_t} = v_w n$$

- A_v = area of voids
- A_t = total area
- v_w = seepage velocity (real velocity)

Water flow
through voids



DARCY'S LAW

- Proposed by Henry Darcy (1803-1858), french engineer.
- He designed pressurized water distribution system to supply fresh water to Dijon.
- Proposed the **Darcy's law** , which describes **the flow of fluid trough porous media** based on experimental results on the flow water in sands.



Henry darcy

DARCY'S LAW

He observed that the flow rate q was:

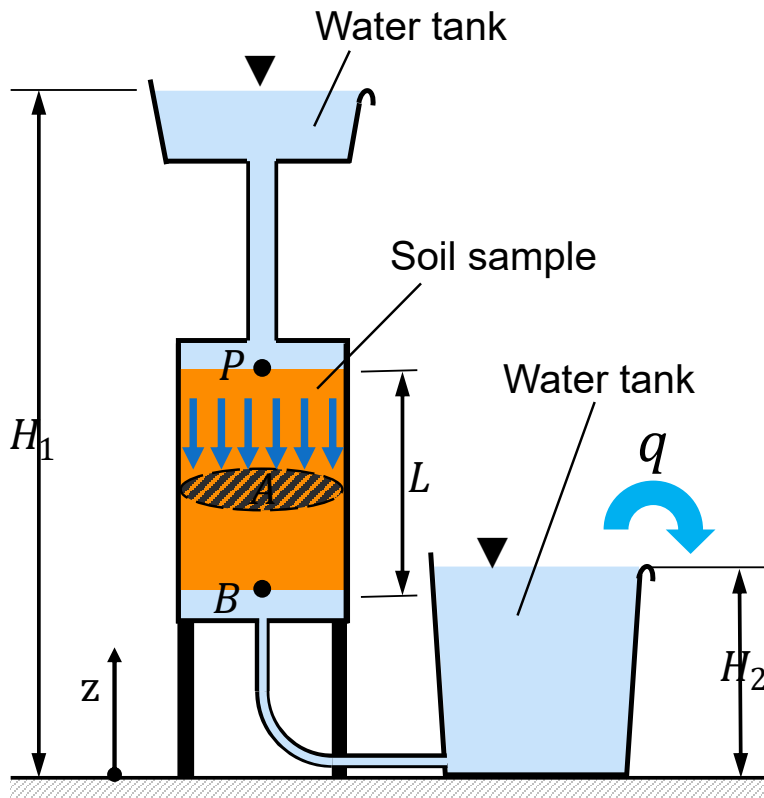
- Proportional to A and Δh .
- Inversely proportional to L .

$$q = k \frac{\Delta h}{L} A$$

$$q = kiA$$

$$q = vA$$

- k = permeability coefficient.



DARCY'S LAW

Darcy's law is valid if:

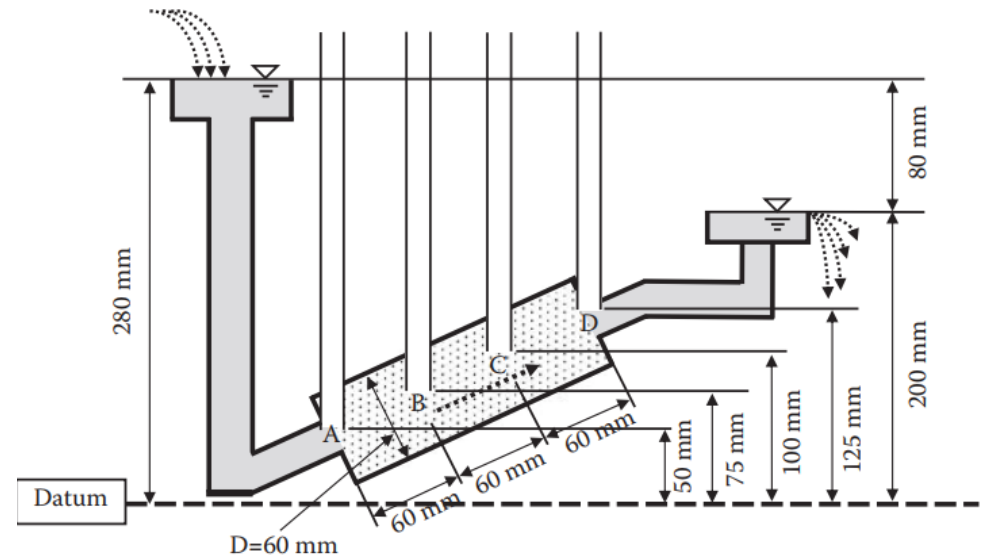
- The water flow is **slow, laminar, not turbulent** .
- Kinematic energy is negligible.
- The soil is **homogeneous** (i.e., properties do not depend on the location of measurement).
- The soil is **isotropic** (i.e., properties do not depend on the direction that you measure them).



EXAMPLE 4.3

The figure shows water flow through the soil specimen in a cylinder. The specimen's k is 3.4×10^{-4} cm/s.

1. Calculate total head, pressure head, and pore pressure at point A and B.
2. Draw the levels of water in standpipes.
3. Compute the amount of water flow q through the specimen.



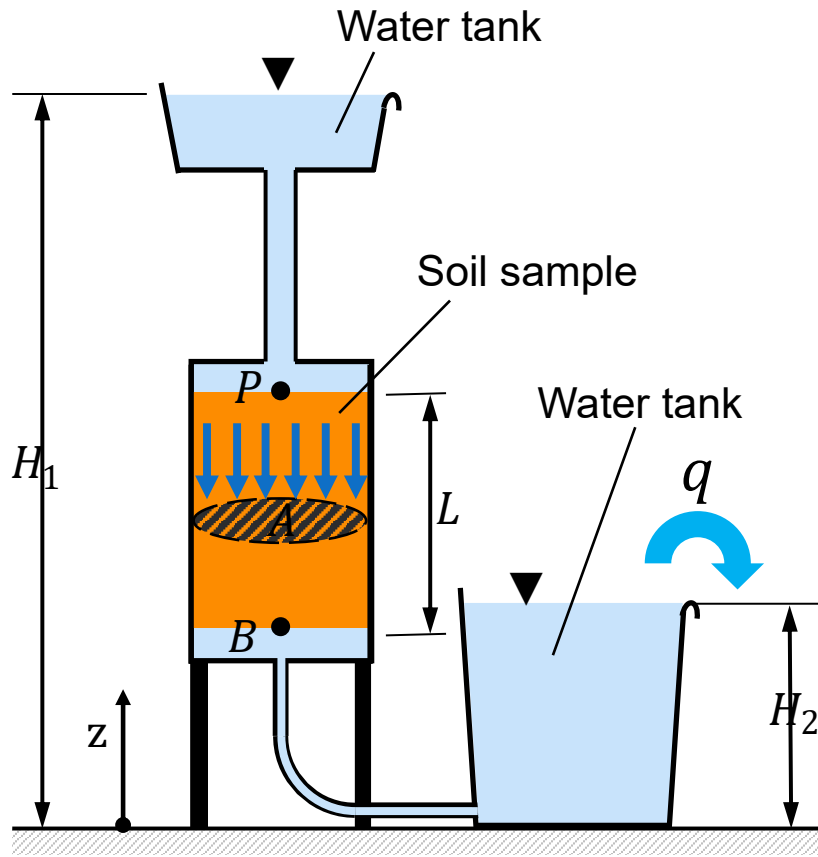
MEASUREMENT OF PERMEABILITY

Recall:

- Is the ability of water to flow through soil.
- Depends on void ratio, GSD, voids connectivity, viscosity of the fluid,...
- One of the **most variable** parameters of soils and difficult to determine in the field accurately.
- Different methods and between most popular we have:
 1. **Constant head test**
 2. **Falling head.**



CONSTANT HEAD PERMEABILITY TEST

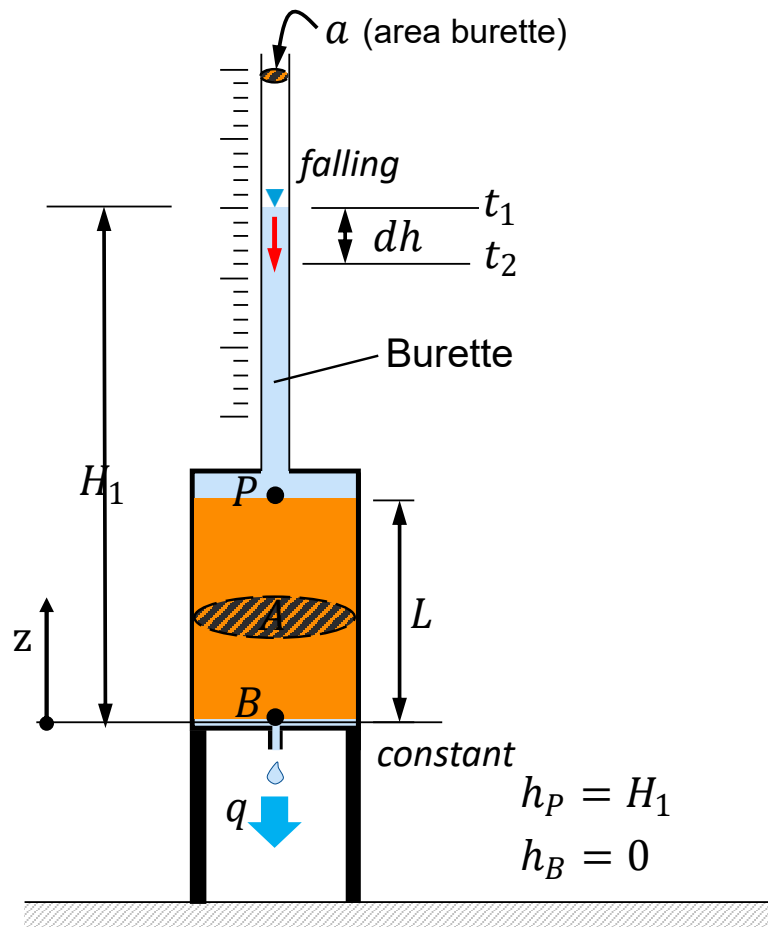


- Δh constant

$$k = \frac{QL}{A\Delta ht}$$

- t = elapsed time of measurement.
- very slow test.
- Darcy used this test in his experiments.

FALLING HEAD PERMEABILITY TEST



- Δh not constant

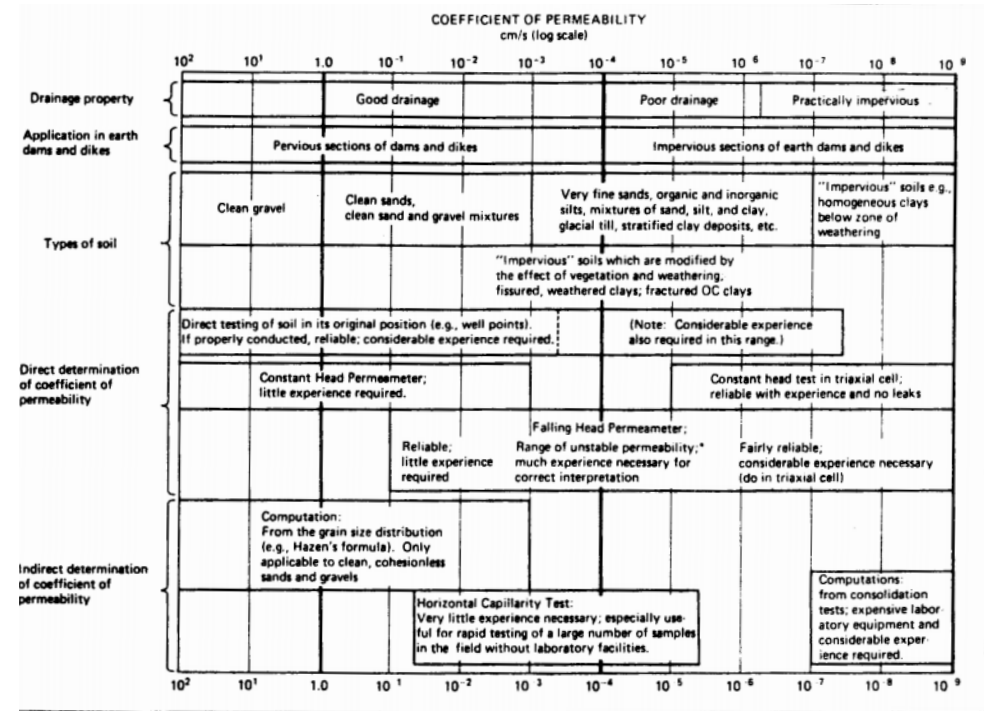
$$k = \frac{a L}{A \Delta t} \ln \left(\frac{H_1}{H_1 - \Delta h} \right)$$

- Δt = elapsed time of measurement.
- Rapid test.
- An operator is not always required in place.

PERMEABILITY OF SOILS

Rule of thumb:

1. Gravel $\longrightarrow k > 10^{-1}$ cm/s.
2. Sand $\longrightarrow 10^{-3}$ to 10^{-1} cm/s.
3. Silt $\longrightarrow 10^{-5}$ to 10^{-3} cm/s.
4. Clay $\longrightarrow 10^{-9}$ to 10^{-5} cm/s.



Due to migration of fines, channels, and air in voids.

Fig. 7.6 Permeability, drainage, soil type, and methods to determine the coefficient of permeability (after A. Casagrande, 1938, with minor additions).

Holtz et al. (2013)

PERMEABILITY OF SOILS

Empirical correlations

- Hazen's (1911) equation:

$$k[cm/s] = CD_{10}^2$$

- D_{10} in mm
- C = empirical coefficient between 0.4-10.0. 1 is a good value for clean poorly graded sands.

- Chapuis's formula

$$k[cm/s] = 2.4622 \left(D_{10}^2 \frac{e^3}{1+e} \right)$$

- Kozeny and Carman's formula:

$$k[cm/s] = \frac{\gamma_w}{\eta_w} \frac{1}{C_{k-c}} \frac{e^3}{S_s^2 (1+e)}$$

- γ_w in kN/m³
- η_w = viscosity of water 1.002×10^{-3} Ns/m²
- C_{k-c} = Kozeny-Carman's empirical constant (2 is usually used).
- S_s = specific surface 1/cm

EXAMPLE 4.4

A sample of sand, 5 cm in diameter and 15 cm long, was prepared at porosity of 60% in a constant-head apparatus. The total head was kept constant at 30 cm and the amount of water collected was 40 cm³. The test temperature was 20°. Calculate the permeability and the seepage velocity.

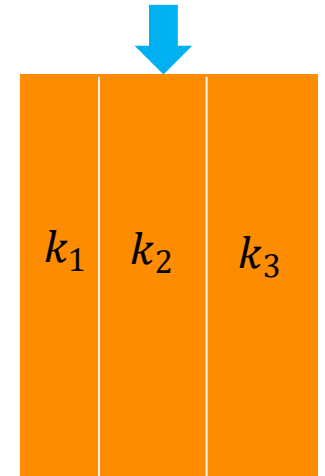
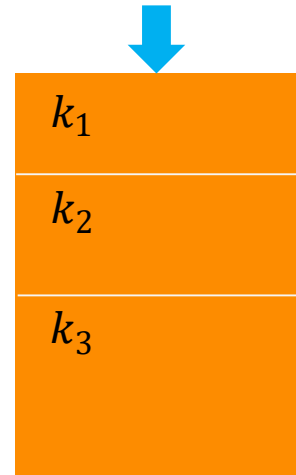


EQUIVALENT PERMEABILITY

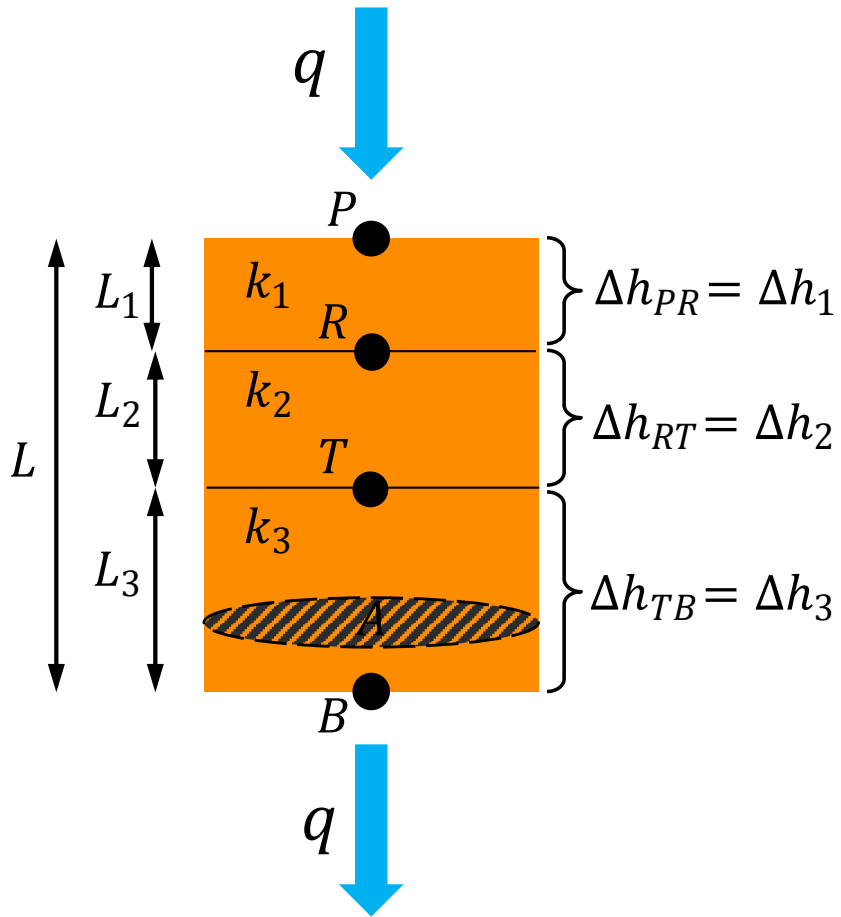
If the soil is conformed of layers with different permeability, we need to calculate an **equivalent permeability** in order to apply Darcy's law.

We will study two cases:

1. Flow is **perpendicular** to the layering.
2. Flow is **parallel** to the layering.

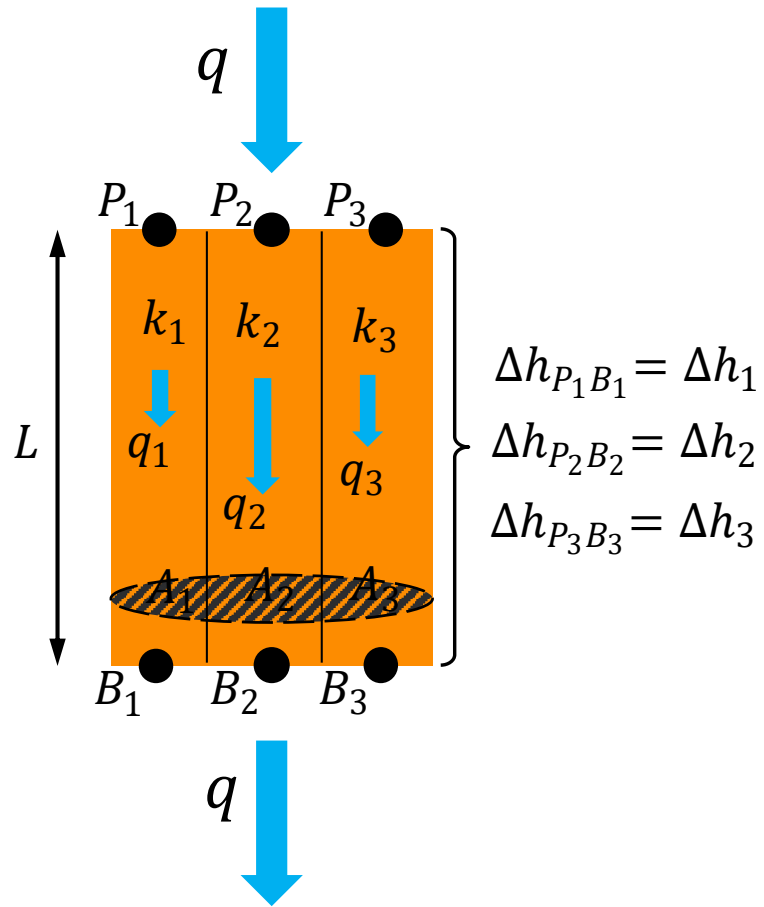


PERPENDICULAR FLOW



$$k_{eq} = \frac{L}{\sum_{i=1}^n L_i / k_i}$$

PARALLEL FLOW



$$k_{eq} = \frac{\sum_{i=1}^n k_i A_i}{A}$$

