

# Kochanek–Bartels Cubic Splines

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Given a sequence of positions  $\{P_n\}_{n=0}^{N-1}$ , the Kochanek–Bartels splines [1] provide a cubic interpolation between each pair  $P_n$  and  $P_{n+1}$  with varying properties specified at the endpoints. These properties are *tension*  $\tau$  which controls how sharply the curve bends at a control point, *continuity*  $\gamma$  which provides a smooth **visual** variation in the continuity at a control point ( $\gamma = 0$  yields derivative continuity, but  $\gamma \neq 0$  gives discontinuities), and *bias* which controls how the direction of the path at a control point by taking weighted combination of one-sided derivatives at that control point.

Using a Hermite interpolation basis  $H_0(t) = 2t^3 - 3t^2 + 1$ ,  $H_1(t) = -2t^3 + 3t^2$ ,  $H_2(t) = t^3 - 2t^2 + t$ , and  $H_3(t) = t^3 - t^2$ , a parametric cubic curve passing through points  $P_n$  and  $P_{n+1}$  with tangent vectors  $T_n$  and  $T_{n+1}$  respectively is

$$P(t) = H_0(t)P_n + H_1(t)P_{n+1} + H_2(t)T_n + H_3(t)T_{n+1} \quad (1)$$

where  $0 \leq t \leq 1$ . Catmull–Rom interpolation is the case when  $T_n = (P_{n+1} - P_{n-1})/2$ , a centered finite difference.

The equation (1) may be modified to allow specification of an “outgoing” tangent  $T_n^0$  at  $t = 0$  and an “incoming” tangent  $T_{n+1}^1$  at  $t = 1$ ,

$$P(t) = H_0(t)P_n + H_1(t)P_{n+1} + H_2(t)T_n^0 + H_3(t)T_{n+1}^1. \quad (2)$$

The paper [1] discusses various choices for the ingoing and outgoing tangents.

Tension  $\tau \in [-1, 1]$  can be introduced by using

$$T_n^0 = T_n^1 = \frac{(1-\tau)}{2} ((P_{n+1} - P_n) + (P_n - P_{n-1})).$$

If  $\tau = 0$ , then we have the Catmull–Rom spline. For  $\tau$  near 1 the curve is “tightened” at the control point while  $\tau$  near  $-1$  produces “slack” at the control point. Varying  $\tau$  changes the length of the tangent at the control point, a smaller tangent leading to a tightening and a larger tangent leading to a slackening.

Continuity  $\gamma \in [-1, 1]$  can be introduced by using

$$T_n^0 = \left( \frac{1-\gamma}{2} (P_{n+1} - P_n) + \frac{1+\gamma}{2} (P_n - P_{n-1}) \right)$$

and

$$T_{n+1}^1 = \left( \frac{1+\gamma}{2} (P_{n+1} - P_n) + \frac{1-\gamma}{2} (P_n - P_{n-1}) \right).$$

When  $\gamma = 0$ , the curve has a continuous tangent vector at the control point. As  $|\gamma|$  increases, the resulting curve has a “corner” at the control point, the direction of the corner depending on the sign of  $\gamma$ .

Bias  $\beta \in [-1, 1]$  can be introduced by using

$$T_n^0 = T_n^1 = \left( \frac{1-\beta}{2}(P_{n+1} - P_n) + \frac{1+\beta}{2}(P_n - P_{n-1}) \right).$$

When  $\beta = 0$  the left and right one-sided tangents are equally weighted (producing the Catmull–Rom spline). For  $\beta$  near  $-1$ , the outgoing tangent dominates the direction of the path of the curve through the control point (undershooting). For  $\beta$  near  $1$ , the incoming tangent dominates (overshooting).

The three effects may be combined into a single set of equations

$$T_n^0 = \frac{(1-\tau)(1-\gamma)(1-\beta)}{2}(P_{n+1} - P_n) + \frac{(1-\tau)(1+\gamma)(1+\beta)}{2}(P_n - P_{n-1}) \quad (3)$$

and

$$T_n^1 = \frac{(1-\tau)(1+\gamma)(1-\beta)}{2}(P_{n+1} - P_n) + \frac{(1-\tau)(1-\gamma)(1+\beta)}{2}(P_n - P_{n-1}). \quad (4)$$

These formulas assume a uniform spacing in time of the position samples. An adjustment can be made for nonuniform spacing. For equation (4) the multiplier is  $2\Delta_n/(\Delta_{n-1} + \Delta_n)$  and for equation (3) the multiplier is  $2\Delta_{n-1}/(\Delta_{n-1} + \Delta_n)$  where  $\Delta_n = s_{n+1} - s_n$  and  $s_n$  is the sample time for position  $P_n$ .

## References

- [1] Doris H. U. Kochanek and Richard H. Bartels, *Interpolating splines with local tension, continuity, and bias control*, ACM SIGGRAPH 1986, Course Notes 22, Advanced Computer Animation.