



Velo & Velo Upgrade Parallel Session

107<sup>th</sup> LHCb Week

## End of Life Radiation damage estimation for Velo

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# •Current condition & Scenarios

## Replacement w/wo cooling

2022

### **Current Status**

#### **Luminosity** (Nathan)

- 0.793 fb<sup>-1</sup> VELO open (31 mm)
- 0.264 fb<sup>-1</sup> VELO closed (1 mm)

#### **Annealing budget** (TIBER Data)

- -20°C for irradiation
- 3h at -10°C (17<sup>th</sup> and 22<sup>nd</sup> of November)

2023

#### **Luminosity**

- 0 fb<sup>-1</sup> VELO open (31 mm)

#### **Annealing budget** (TIBER Data)

- 21°C since the foil incident (28 days, since 10/2)

*Foil Replacement with cooling  
(120 days at -20°C)*

**2023**

- 1 fb<sup>-1</sup> VELO @ 11 mm → -20°C (April to November)

- 120 days (November to April 2024) @ -20°C

- 4 days @ 21°C (maintenance)

#### **2024 – 2025 (per year)**

- 5.5 fb<sup>-1</sup> VELO @ 0 mm → -20°C
- 4 days @ 21°C (maintenance)

#### **2026 – 2028 (per year)**

- 0 fb<sup>-1</sup> VELO @ 0 mm → -20°C
- 4 days @ 21°C (maintenance)

#### **2029 – 2032 (per year)**

- 7 fb<sup>-1</sup> VELO @ 0 mm → -20°C
- 4 days @ 21°C (maintenance)

*Foil Replacement with cooling,  
high 2023 luminosity  
(120 days at -20°C)*

#### **Same but.....**

- 4 fb<sup>-1</sup> VELO @ 11 mm → -20°C (April to November)

*Foil Replacement without cooling  
(120 days at 21°C)*

#### **Same but.....**

- 120 days (November to April 2024) @ 21°C

*Foil Replacement without cooling,  
high 2023 luminosity  
(120 days at 21°C)*

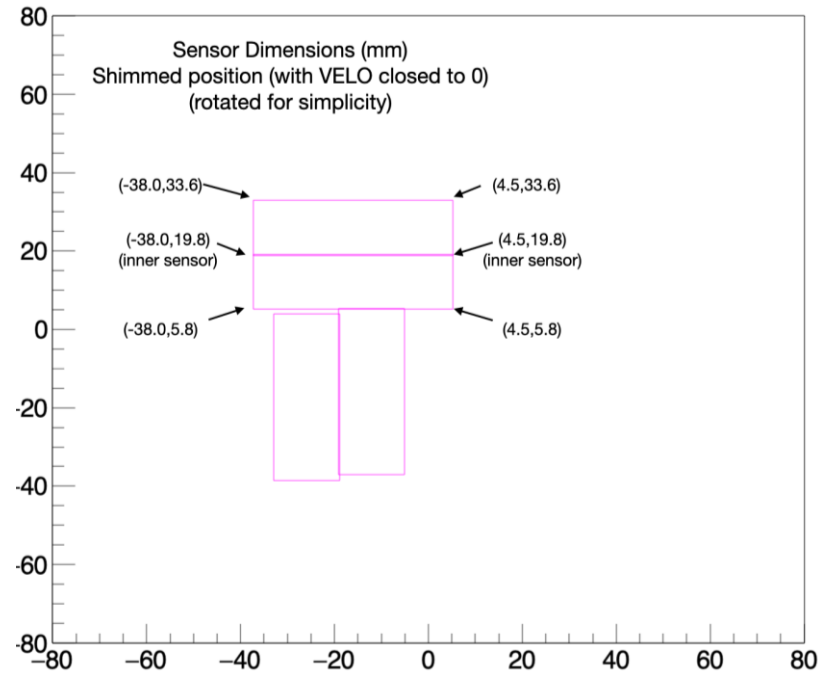
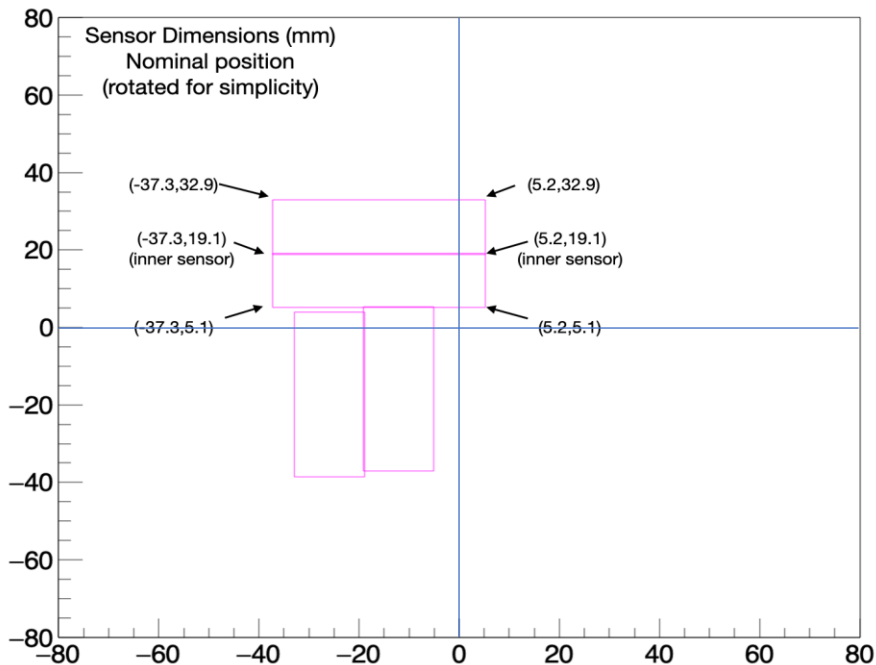
#### **Same but.....**

- 4 fb<sup>-1</sup> VELO @ 11 mm → -20°C (April to November)
- 120 days (November to April 2024) @ 21°C

**Baseline Scenario: No incident, Shims for 2023, 4fb<sup>-1</sup> @ 2023, same afterwards**

# •Velo Coordinate System

## Module positions and radial distances



$$\Phi_{mv.} = \tan^{-1} \frac{|y_0 - y_n|}{|x_0 - x_n|} \xleftrightarrow{\Phi_{mv.}=45^\circ}$$

$$|y_0 - y_n| = |x_0 - x_n| \xleftrightarrow{y \uparrow, x \downarrow}$$

$$y_n = x_0 + y_0 - x_n$$

$$R = \sqrt{|x_0 - x_n|^2 + |y_0 - y_n|^2} \xleftrightarrow{y \uparrow, x \downarrow}$$

$$R = \sqrt{(x_0 - x_n)^2 + (y_n - y_0)^2} \xleftrightarrow{y_n = x_0 + y_0 - x_n}$$

$$R = \sqrt{2}(x_0 - x_n) \Leftrightarrow$$

$$x_n = x_0 - \frac{R}{\sqrt{2}}$$

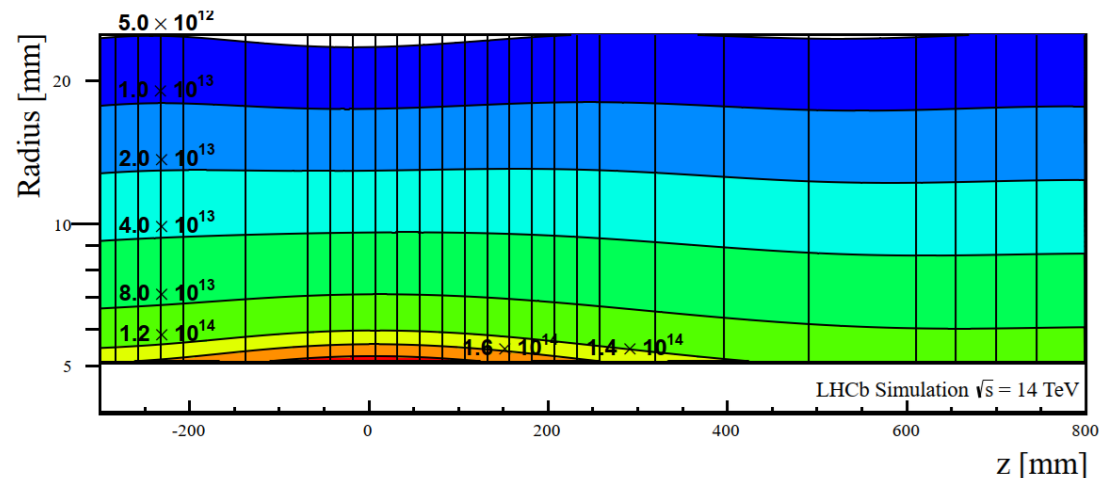
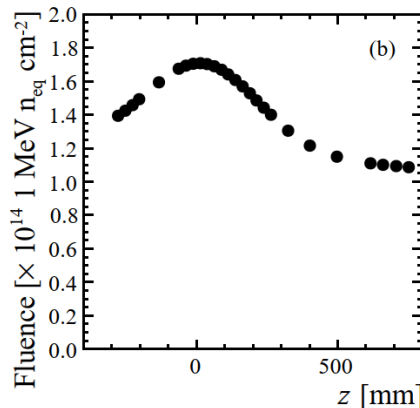
- Rotated cartesian coordinate system
- Assume only lateral movement with respect to the bam axis
- $\Phi_{mv.} = 45^\circ$
- Distances converted to coordinates for fluence estimation
- Mean per ladder fluence estimation using numerical integration assuming uniform per pixel fluence
- Number of steps equal to number of per module pixels

# •Fluence Estimation

## 7<sup>th</sup> order polynomial fit

$$\Phi(R,z) = \underbrace{(a_0 + a_1 \times z + a_2 \times z^2 + a_3 \times z^3 + a_4 \times z^4 + a_5 \times z^5 + a_6 \times z^6)}_{A(z)} \times L \times R^{-\overbrace{(k_0 + k_1 \times z + k_2 \times z^2 + k_3 \times z^3 + k_4 \times z^4 + k_5 \times z^5 + k_6 \times z^6)}^{k(z)}}$$

- Exponential dependence with radius from beam axis on a dedicated z position ( $A \times R^{-k}$ )
- 7<sup>th</sup> order approximation through polynomial fit from Fluka simulations
- R in centimeters, luminosity in  $\text{fb}^{-1}$
- Fit factors estimated for fluence units of  $10^{13} \text{ n}_{\text{eq}}/\text{cm}^2$



Alpha Factors		Kappa Factors	
$\alpha_0$	3.63	$k_0$	2.3
$\alpha_1$	$2.72 \times 10^{-4}$	$K_1$	$-1.22 \times 10^{-4}$
$\alpha_2$	$-3.30 \times 10^{-6}$	$K_2$	$-5.11 \times 10^{-6}$
$\alpha_3$	$-3.43 \times 10^{-9}$	$K_3$	$6.22 \times 10^{-9}$
$\alpha_4$	$6.36 \times 10^{-12}$	$K_4$	$2.79 \times 10^{-11}$
$\alpha_5$	$1.94 \times 10^{-15}$	$K_5$	$-6.87 \times 10^{-14}$
$\alpha_6$	$1.63 \times 10^{-18}$	$k_6$	$4.18 \times 10^{-17}$

Single Pixel

$$\left\{ \begin{array}{l} \Phi(z)_{\text{pixel}} = A(z) \times L \times \left( \sqrt{x_{\langle \text{pix.} \rangle}^2 + y_{\langle \text{pix.} \rangle}^2} \right)^{-k(z)} \\ x_{\langle \text{pix.} \rangle}, y_{\langle \text{pix.} \rangle} = x_i, y_i + \sqrt{N_{\text{pixels}} / S_{\text{ladder}}} \\ \delta \Phi(z)_{\text{pixel}} = \sqrt{\frac{1}{2} \times (|\Phi(z)_{\text{pixel}} - \Phi(z)_i|^2 + |\Phi(z)_{\text{pixel}} - \Phi(z)_{i+1}|^2)} \end{array} \right.$$

# •Fluence Estimation

## 2D Trapezoidal model for Ladders

D. Kaffer, [Numerical Techniques for the Evaluation of Multi-Dimensional Integral Equations](#)

$$\langle \Phi(z) \rangle = \frac{1}{S_{ladder}} \times \underbrace{\iint_{ladder} A(z) \times L \times \sqrt{x^2 + y^2}^{-k(z)} dx dy}$$

$$\frac{h_x h_y}{4} \times \left( \Phi(x_0, y_0) + \Phi(x_f, y_0) + \Phi(x_f, y_f) + 4 \times \sum_{i=2}^{n_y} \sum_{j=2}^{n_x} \Phi(x_j, y_i) + 2 \times \sum_{i=2}^{n_y} [\Phi(x_0, y_i) + \Phi(x_f, y_i)] + 2 \times \sum_{j=2}^{n_x} [\Phi(x_j, y_0) + \Phi(x_j, y_f)] \right)$$

### 2D trapezoidal integration rule (uniform pixel fluence approximation)

- $(x_0, y_0)$  Coordinates of closer pixel to beam
- $(x_f, y_f)$  Coordinates of furthest pixel from beam
- $(x_0, y_f)$  Vertically furthest pixel from beam
- $(x_f, y_0)$  Horizontally furthest pixel from beam
- $n_y$  Number of pixel rows
- $n_x$  Number of pixel columns
- $h_x$  Pixel width
- $h_y$  Pixel height

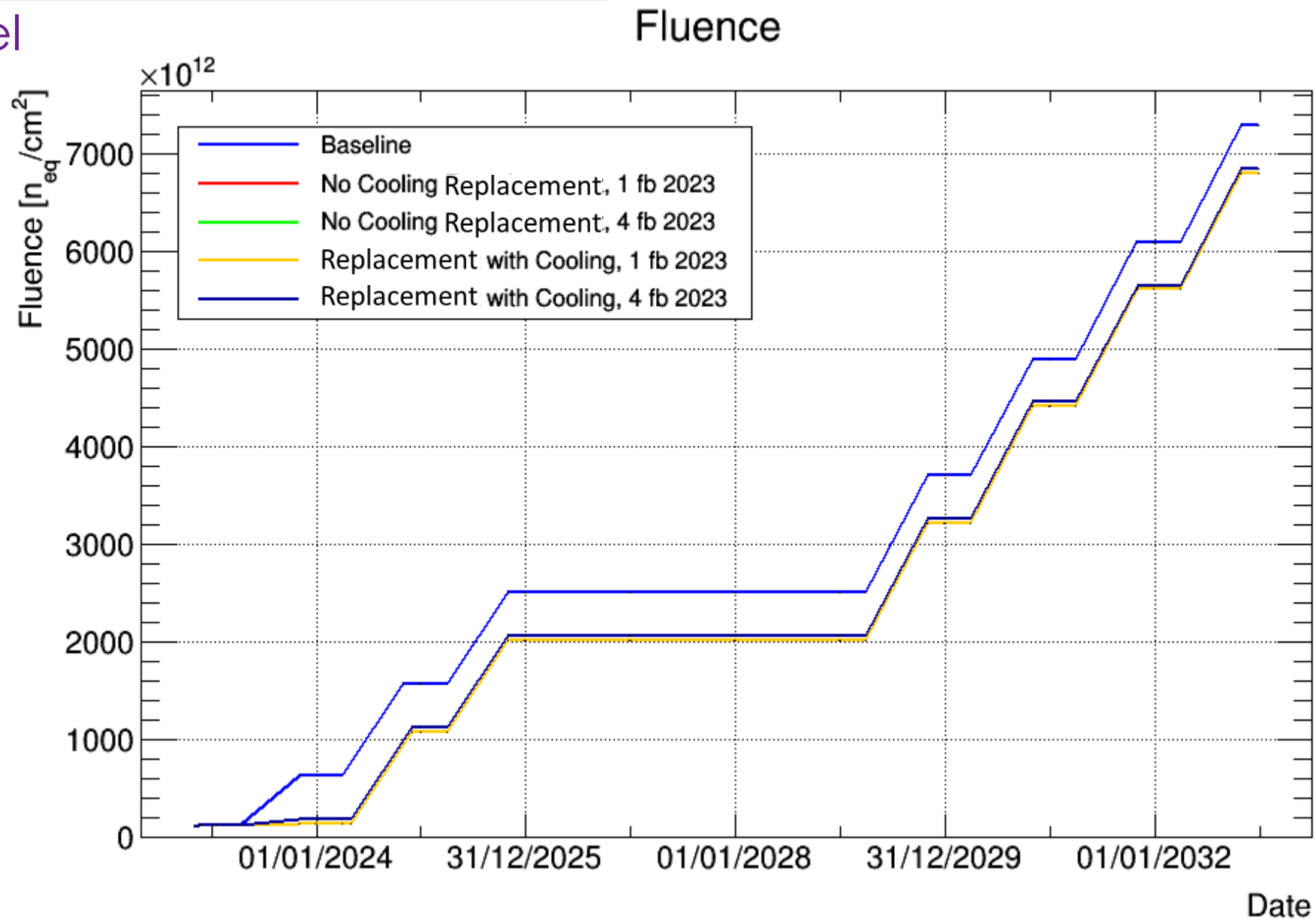
### Fluence uncertainty approximation

$$\delta \langle \Phi(z) \rangle \frac{1}{N_{pix.}} \times \sqrt{\sum \underbrace{(\delta \Phi(z)_{pixel})_i^2}_{\text{Single Pixel fluence uncertainty}}}$$

Single Pixel fluence uncertainty

# •Fluence Estimation

Hottest Pixel



# •Leakage Current modeling

## Hamburg Model

$$I_n(T_{\text{ref}}) \equiv I_n^{\text{exp}} + I_n^{\text{log}} = \sum_{i=1}^n \delta\Phi_i^{\text{eq}} \cdot \alpha_l \cdot \exp\left(-\frac{t_{n,i}^{\text{l}}}{\tau_l(T_{\text{ref}})}\right) + \sum_{i=1}^n \delta\Phi_i^{\text{eq}} (\alpha_0^* - \beta \ln(t_{n,i}^{\text{log}}/t_0)) \quad (\text{A.1})$$

$$t_{n,i}^{\text{l}} = \sum_{j=i}^n \delta t_j \frac{\tau_l(T_{\text{ref}})}{\tau_l(T_j)}, \quad t_{n,i}^{\text{log}} = \sum_{j=i}^n \delta t_j \Theta_A(T_j) \quad (\text{A.2})$$

$$\frac{1}{\tau_l(T)} = k_{0l} \cdot \exp\left(-\frac{E_l}{k_B T}\right), \quad \Theta_A(T) = \exp\left(-\frac{E_l^*}{k_B} \left[\frac{1}{T} - \frac{1}{T_{\text{ref}}}\right]\right) \quad (\text{A.3})$$

$$A = \pi r^2$$

$$\begin{aligned} \alpha_I &= (1.23 \pm 0.06) \times 10^{-17} \text{ A/cm} \\ k_{0I} &= 1.2_{-1.0}^{+5.3} \times 10^{13} \text{ s}^{-1} \\ E_I &= 1.11 \pm 0.05 \text{ eV} \\ \alpha_0^* &= 7.07 \times 10^{-17} \text{ A/cm} \\ \beta &= 3.29 \times 10^{-18} \text{ A/cm} \\ E_I^* &= 1.30 \pm 0.14 \text{ eV} \\ t_0 &= 1 \text{ min} \\ T_{\text{ref}} &= 21^\circ\text{C} \end{aligned}$$

M. Moll, Thesis, Universität Hamburg (1999), O. Krasel, Thesis, Universität Dortmund (2004)

**Leakage Current scaling**  
( $E_{\text{eff.}} = 1.214 \pm 0.014 \text{ eV}$ )

$$\left\{ \begin{aligned} I(T) &\propto T^2 e^{-\frac{E_{\text{eff.}}}{2k_B T}} \\ I(T_R) &\propto T_R^2 e^{-\frac{E_{\text{eff.}}}{2k_B T_R}} \end{aligned} \right. \rightarrow I(T) = I(T_R) \times \left(\frac{T}{T_R}\right)^2 \times e^{-\frac{E_{\text{eff.}}}{2k_B} \left(\frac{1}{T} - \frac{1}{T_R}\right)}$$

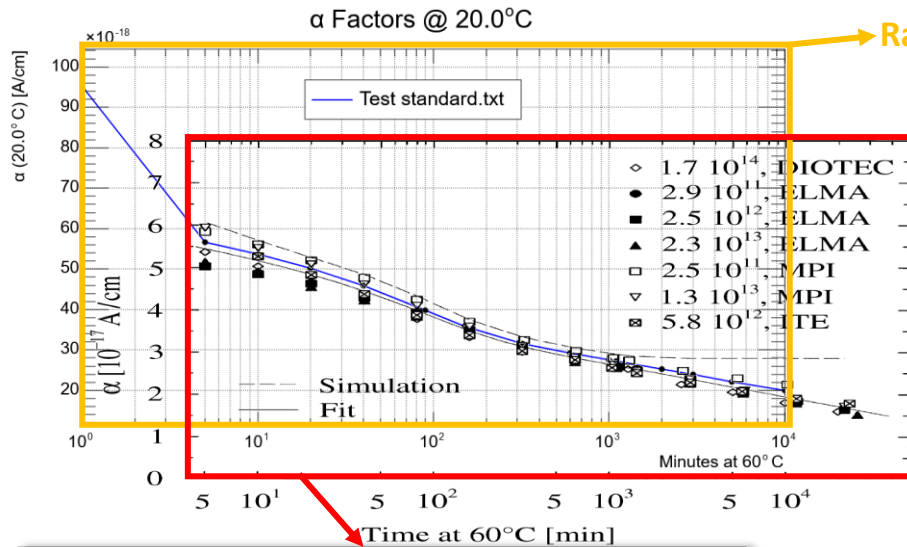
**Depletion Voltage estimation**

$$\left\{ \begin{aligned} \text{Depletion Voltage: } V_{FD} &= \frac{D^2}{2\varepsilon_{Si}\mu\rho} \\ \text{Bulk Resistivity: } \rho &= \frac{1}{e\mu N_{\text{eff}}} \end{aligned} \right. \rightarrow V_{FD} = \frac{e|N_{\text{eff}}|D^2}{2\varepsilon_0\varepsilon_{r,Si}}$$



# • Leakage Current modeling

## Validation Tests I – Standard Annealing Experiment

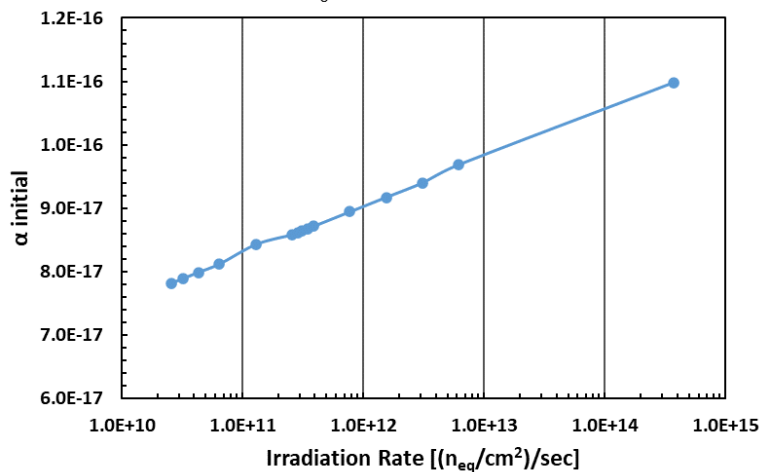


RadDamage Code

- A  $3 \text{ fb}^{-1}$  exposure in a 60-minute interval at  $-20^\circ\text{C}$  was simulated, corresponding to an equivalent fluence of  $3.74 \times 10^{14} \text{ n}_{\text{eq}}/\text{cm}^2$  for the hottest pixel
- Consecutive annealing steps at  $60^\circ\text{C}$  are performed and leakage current is evaluated at  $21^\circ\text{C}$  ( $T_{\text{ref}}$ )
- Leakage current scaled to  $20^\circ\text{C}$  and corresponding  $\alpha$  factors estimated
- Results in perfect agreement with ROSE collaboration measurements (material and fluence independent)
- Zero annealing time predictions are non-defined by the model as the original parametrization assumes adiabatic irradiation only valid at an infinitely low-rate irradiation

M. Moll, E. Fretwurst, G. Lindstrom, "Leakage Current of Hadron Irradiated Silicon Sensors – Material Dependence"

$\alpha_0$  vs Irradiation Rate



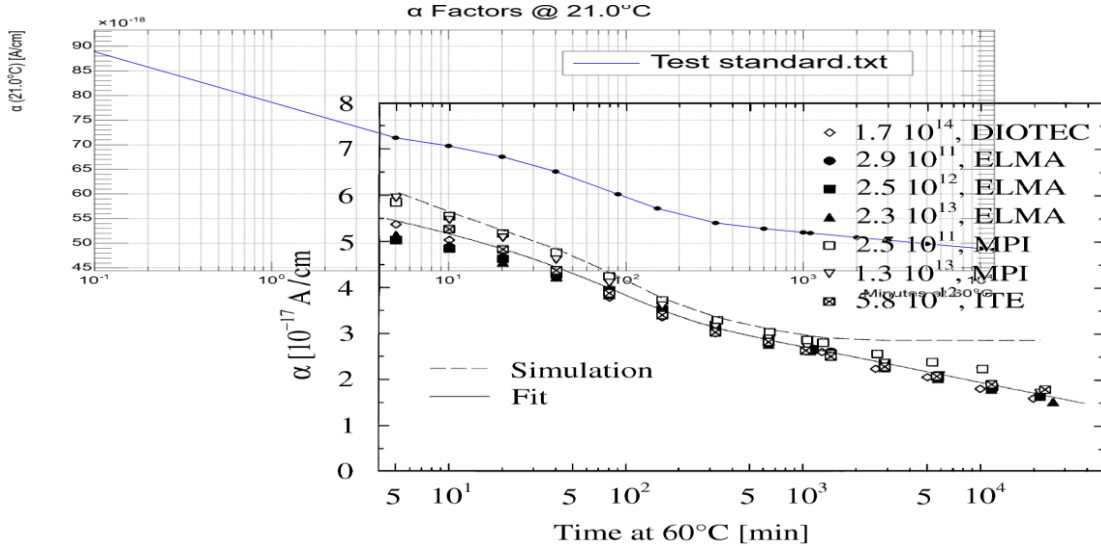
Rate ( $\text{n}_{\text{eq}}/\text{cm}^2 \times \text{min}^{-1}$ )	$\alpha_0$
3.74E+14	1.10E-16
6.23E+12	9.69E-17
3.11E+12	9.40E-17
1.56E+12	9.17E-17
7.79E+11	8.95E-17
3.89E+11	8.72E-17
3.46E+11	8.68E-17
3.11E+11	8.64E-17
2.87E+11	8.62E-17
2.60E+11	8.58E-17
1.30E+11	8.43E-17
6.49E+10	8.13E-17
4.33E+10	7.99E-17
3.24E+10	7.90E-17
2.60E+10	7.82E-17

- Standard fluence of  $3.74 \times 10^{14} \text{ n}_{\text{eq}}/\text{cm}^2$  at  $-20^\circ\text{C}$  was administered in varied time intervals, ranging from 1 to 14400 minutes
- $\alpha_0$  estimated for each case, with values converging to model predictions at  $t_{\text{irad}} \gg t_{\text{anneal}}$
- Behavior justified by the differential nature of annealing estimation performed by the code, both annealing and irradiation are performed simultaneously



# •Leakage Current modeling

## Validation Tests II – ln vs log base terme



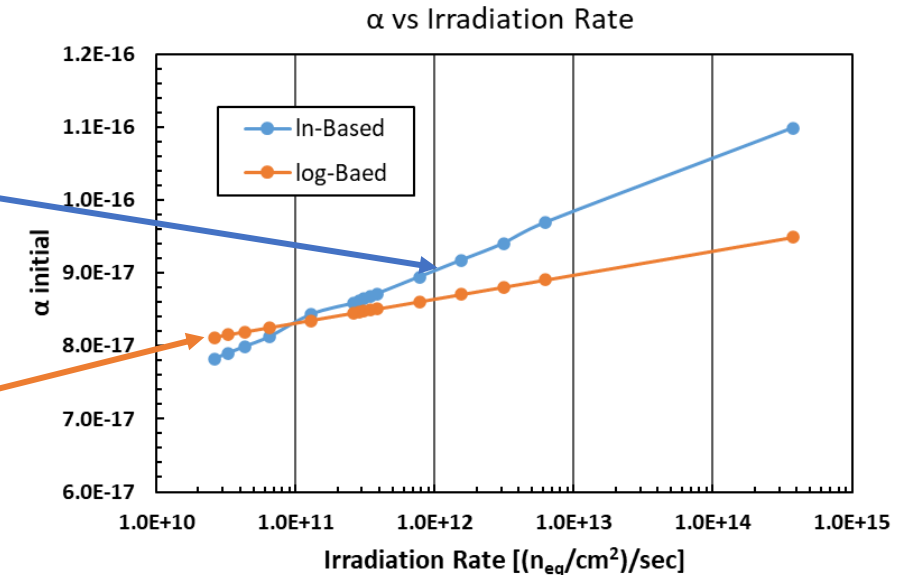
- In several papers, the logarithmic term of the leakage current model is incorrectly represented with a base-10 logarithm instead of a natural-based logarithm  
e.g.: [JINST 14 \(2019\) P06012](#) - page 5,  
[arXiv:2203.06216v4 \[physics.ins-det\]](#) 29 Dec 2022 - page 11
- Repeating simulation for the standard experiment and comparing with bibliographic data demonstrates the magnitude of the disagreement
- Same exercise can be repeated for the  $\alpha_0$  estimation, where in this case the irradiation rate dependence becomes less pronounced and can even some times be completely neglected

Correct

$$\frac{I_n}{V} = \sum_{i=1}^n \delta\Phi_i^{eq} \times \left[ a_0^* + a_I \times e^{-\left(\sum_{j=i}^n \frac{\delta t_j}{\tau_I(T_j)}\right)} - \beta \times \ln \sum_{j=i}^n \frac{\delta t_j}{60} \times \theta_A(T_j) \right]$$

Wrong

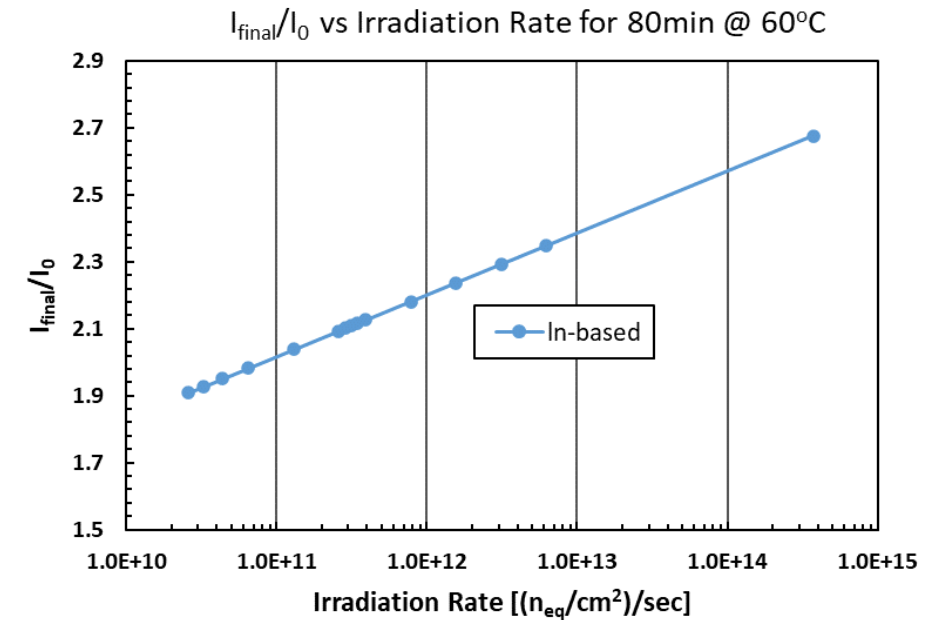
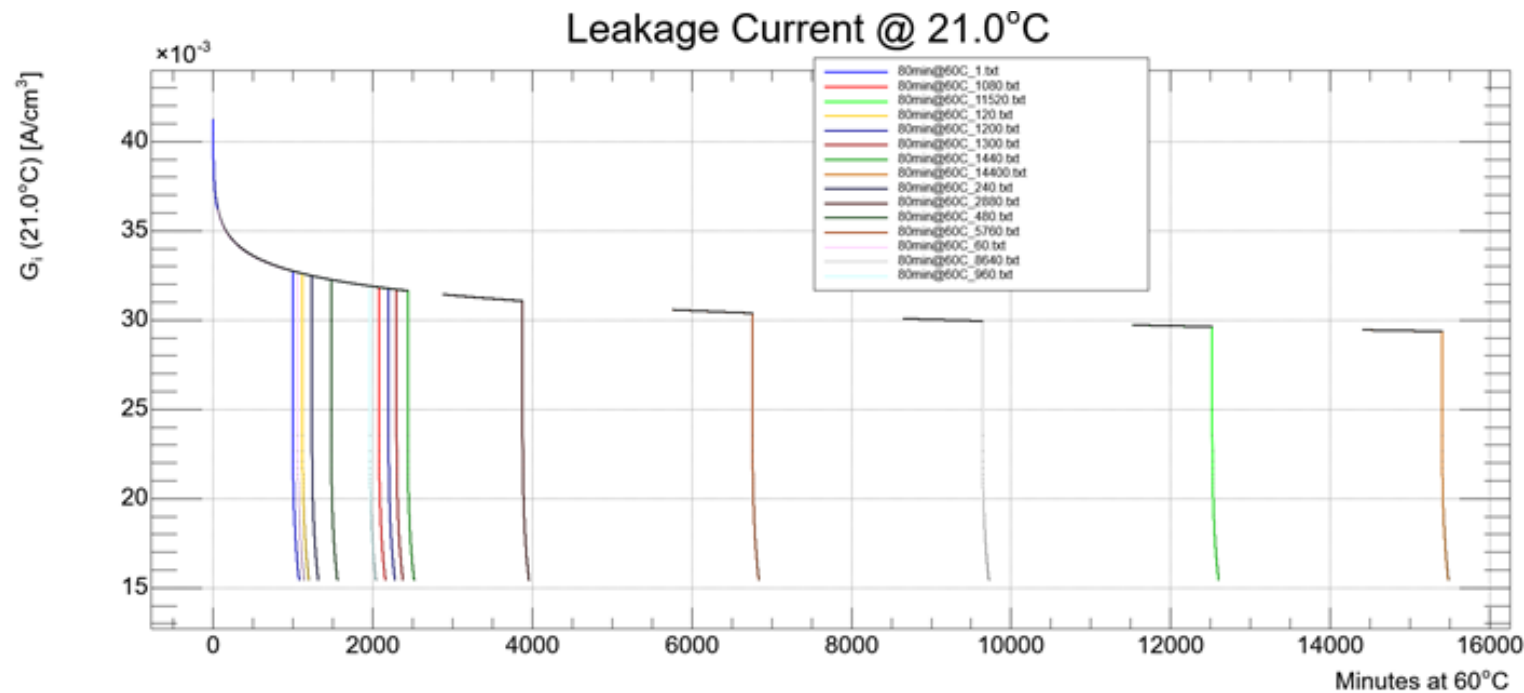
$$\frac{I_n}{V} = \sum_{i=1}^n \delta\Phi_i^{eq} \times \left[ a_0^* + a_I \times e^{-\left(\sum_{j=i}^n \frac{\delta t_j}{\tau_I(T_j)}\right)} - \beta \times \log \sum_{j=i}^n \frac{\delta t_j}{60} \times \theta_A(T_j) \right]$$



# •Leakage Current modeling

## Validation Tests III – Long term annealing

- Since initial  $\alpha$  is irradiation rate dependent, so will  $I_{\text{final}}/I_0$
- In the standard experiment ( $3.74 \times 10^{14} \text{ n}_{\text{eq}}/\text{cm}^2$  @  $-20^\circ\text{C}$ ), the  $I_{\text{final}}/I_0$  is represented for various irradiation rates after an annealing of 80 min at  $60^\circ\text{C}$
- Although factors seem to change with respect to the initial time of irradiation, this is of low consequence.

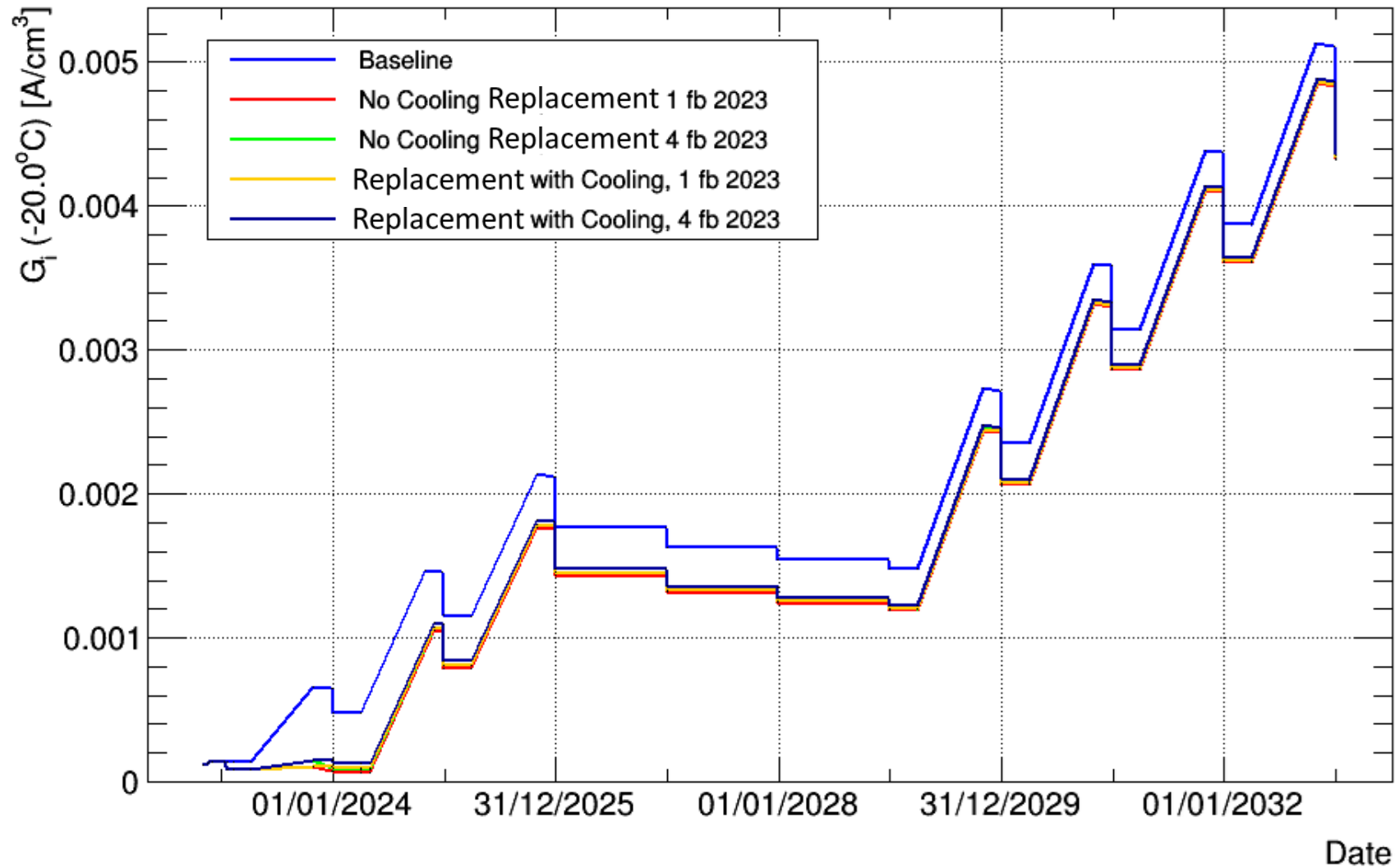


- Final leakage current for all cases is the same, no matter of the irradiation rate
- For all scenarios, independent of the irradiation rate, after 80 min at  $60^\circ\text{C}$  we end up at the same value of leakage current. The current just after the irradiation though - the starting point - is not the same and may vary up to 25%.

# •Leakage Current modeling

Hottest pixel ( $\sim 7.4 \times 10^{15} n_{eq}/cm^2$ )

Leakage Current @ -20.0°C



# •N<sub>eff</sub> – Dynamic Model

## Differential equations on Effective dopant

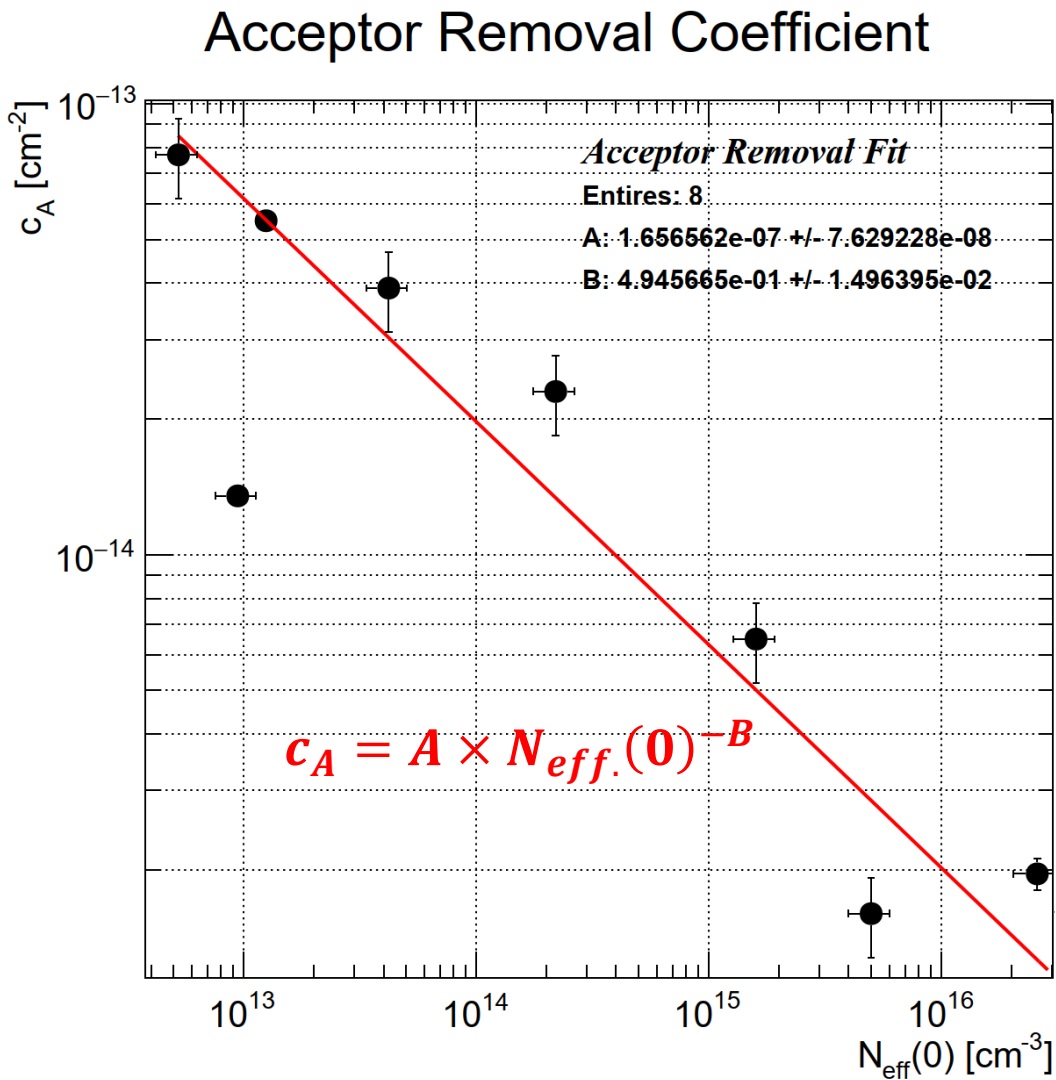
G. Lindstrom et al., NIM A 466(2001) 308-326  
[“Radiation damage in silicon detectors”](#)

Radiation damage modeling		
Irradiation Related part	Constant Damage Terms	<b>Acceptor Introduction</b> $\frac{dN_{acc.}^{con.}(t)}{dt} = g_{C_A} \times \Phi_{eq}(t)$
		<b>Donor Introduction</b> $\frac{dN_{don.}^{con.}(t)}{dt} = g_{C_D} \times \Phi_{eq}(t)$
		<b>Acceptor Removal</b> $\frac{dN_{acc.}^{rem.}(t)}{dt} = -c_{C_A} \times \Phi_{eq}(t) \times N_{acc.}^{rem.}(t)$
		<b>Donor Removal</b> $\frac{dN_{don.}^{rem.}(t)}{dt} = -c_{C_D} \times \Phi_{eq}(t) \times N_{acc.}^{rem.}(t)$
Annealing Related part	Short term annealing	<b>Acceptor Reduction</b> $\frac{dN_{acc.}^{short.}(t)}{dt} = g_A \times \Phi_{eq}(t) - k_A(T) \times N_{acc.}^{short.}(t)$
	Long term annealing	<b>Max Introdutable Acceptors</b> $\frac{dN_{acc.}^{Max.long.}(t)}{dt} = g_Y \times \Phi_{eq}(t) - k_Y(T) \times N_{acc.}^{Max.long.}(t)$
		<b>Acceptor Introduction</b> $\frac{dN_{acc.}^{long.}(t)}{dt} = k_Y(T) \times N_{acc.}^{Max.long.}(t)$

# •N<sub>eff</sub> – Dynamic Model

Radiation damage modeling		
Constant Damage Terms	Acceptor Introduction	$N_{acc.}^{con.}(t) = g_{c_A} \times \int_0^t \Phi_{eq.}(\tau) \partial \tau$
	Donor Introduction	$N_{don.}^{con.}(t) = g_{c_D} \times \int_0^t \Phi_{eq.}(\tau) \partial \tau$
	Acceptor Removal	$N_{acc.}^{rem.}(t) = f_{c_A} \times N_{eff.}(0) \left( 1 - e^{-c_{c_A} \int_0^t \Phi_{eq.}(\tau) \partial \tau} \right)$
	Donor Removal	$N_{don.}^{rem.}(t) = f_{c_D} \times N_{eff.}(0) \left( 1 - e^{-c_{c_D} \int_0^t \Phi_{eq.}(\tau) \partial \tau} \right)$
Short term annealing	Acceptor Reduction	$N_{acc.}^{short.}(t_i) = g_A \times \int_{t_{i-1}}^{t_i} \Phi_{eq.}(\tau) \partial \tau / \delta t \times \frac{(1 - e^{-k_a(T_i) \times \delta t})}{k_a(T_i)} + N_{acc.}^{short.}(t_{i-1}) \times e^{-k_a(T_i) \times \delta t}$
Long term annealing	Max Introdutable Acceptors	$N_{acc.}^{Max. long.}(t_i) = g_Y \times \int_{t_{i-1}}^{t_i} \Phi_{eq.}(\tau) \partial \tau / \delta t \times \frac{(1 - e^{-k_Y(T_i) \times \delta t})}{k_Y(T_i)} + N_{acc.}^{Max. long.}(t_{i-1}) \times e^{-k_Y(T_i) \times \delta t}$
	Acceptor Introduction	$N_{acc.}^{long.}(t_i) = N_{acc.}^{long.}(t_{i-1}) + g_Y(T) \times \frac{\int_{t_{i-1}}^{t_i} \Phi_{eq.}(\tau) \partial \tau}{k_Y(T) \delta t} \times (k_Y(T) \times t + e^{-k_Y(T)t} - 1) + N_{acc.}^{Max. long.}(t_i) \times (1 - e^{-k_Y(T)t})$

# •Acceptor Removal Fit



## Current Velo

200 μm thick, non-oxygenated, n-in-p, FZ, 3 – 8 kΩ × cm

Acceptor removal part

$$N_C.(\Phi_{eq.}) = -f_c \times N_{eff.}(0) (1 - e^{-c_A \Phi_{eq.}})$$

Original doping concentration

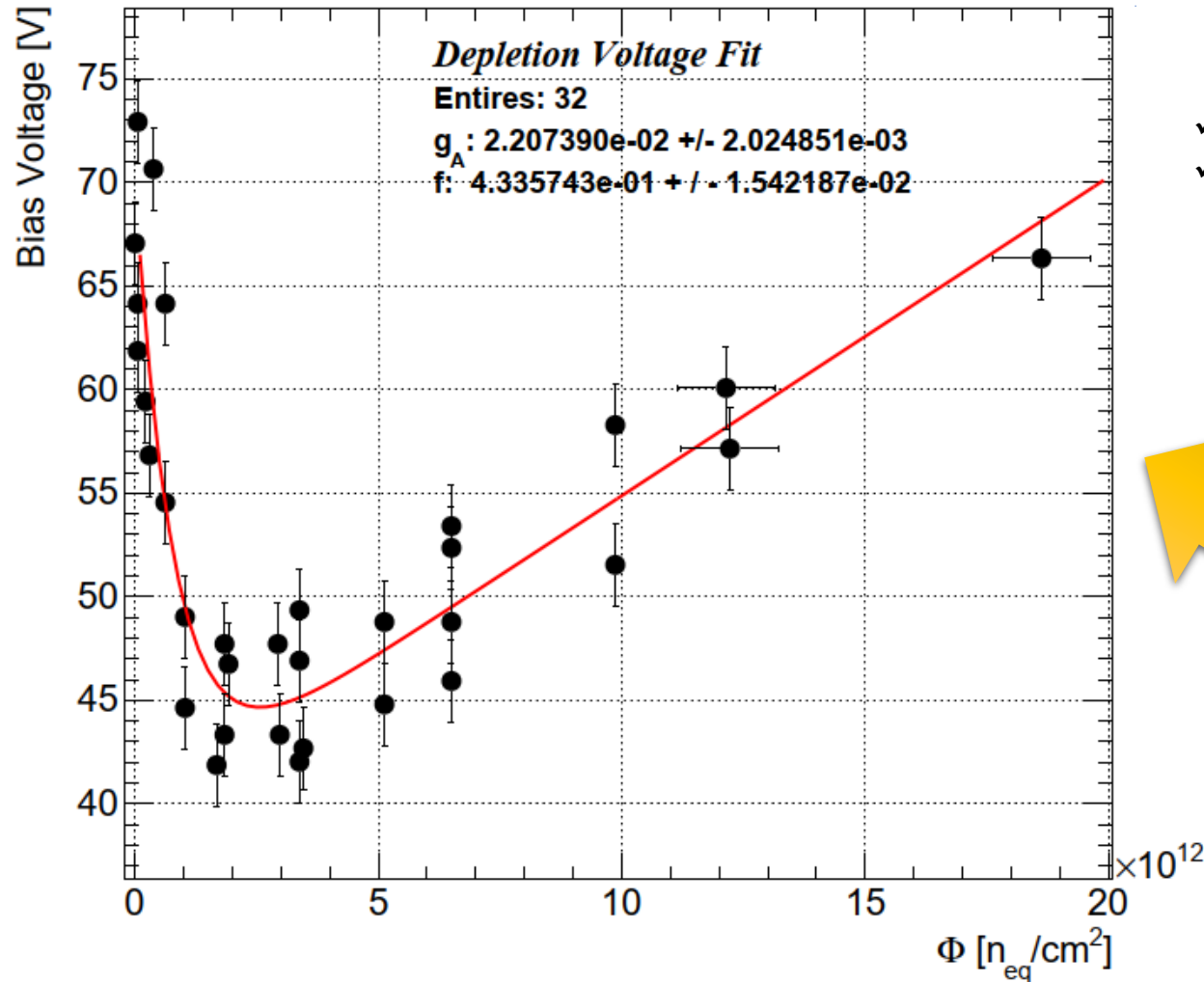
Removable Fraction

Acceptor Removal Coefficient

$N_{eff}(0)$ [cm <sup>-3</sup> ]		$c_A$ [cm <sup>-2</sup> ]	Sensor Type	Reference
Method	Value			
SiMS	$5 \times 10^{15} (\pm 20\%)$	$16 \times 10^{-16} (\pm 20\%)$	LGAD	G. Kramberger et al., JINST Vol. 10 (2015) P07006.
	$(2.59 \pm 0.54) \times 10^{16}$	$(19.6 \pm 1.6) \times 10^{-16}$		E. – L. Gkougkousis et al. J. Phys.: Conf. Ser. 2374 012175
CV Meas.	$(9.44 \pm 0.07) \times 10^{12}$	<b><math>(1.35 \pm 0.03) \times 10^{-14}</math></b>	Pad Diodes - MCz	K. Kaska, PhD Thesis, Technical University Vienna, 2014
	$(12.49 \pm 0.74) \times 10^{12}$	$(5.5 \pm 0.04) \times 10^{-14}$	Epi 150 μm pad diodes	
Resistivity	$1.6 \times 10^{15} (\pm 20\%)$	$6.5 \times 10^{-15} (\pm 20\%)$	Epi 50 μm pad diodes	P. D. de Almeida, "Measurement of the acceptor removal rate in silicon pad diodes," 30th RD50 Workshop, <a href="https://indico.cern.ch/event/637212/contributions/2608666/">https://indico.cern.ch/event/637212/contributions/2608666/</a>
	$2.2 \times 10^{14} (\pm 20\%)$	$2.3 \times 10^{-14} (\pm 20\%)$		
	$4.21 \times 10^{13} (\pm 20\%)$	$3.9 \times 10^{-14} (\pm 20\%)$		
	$5.25 \times 10^{12} (\pm 20\%)$	$7.7 \times 10^{-14} (\pm 20\%)$		

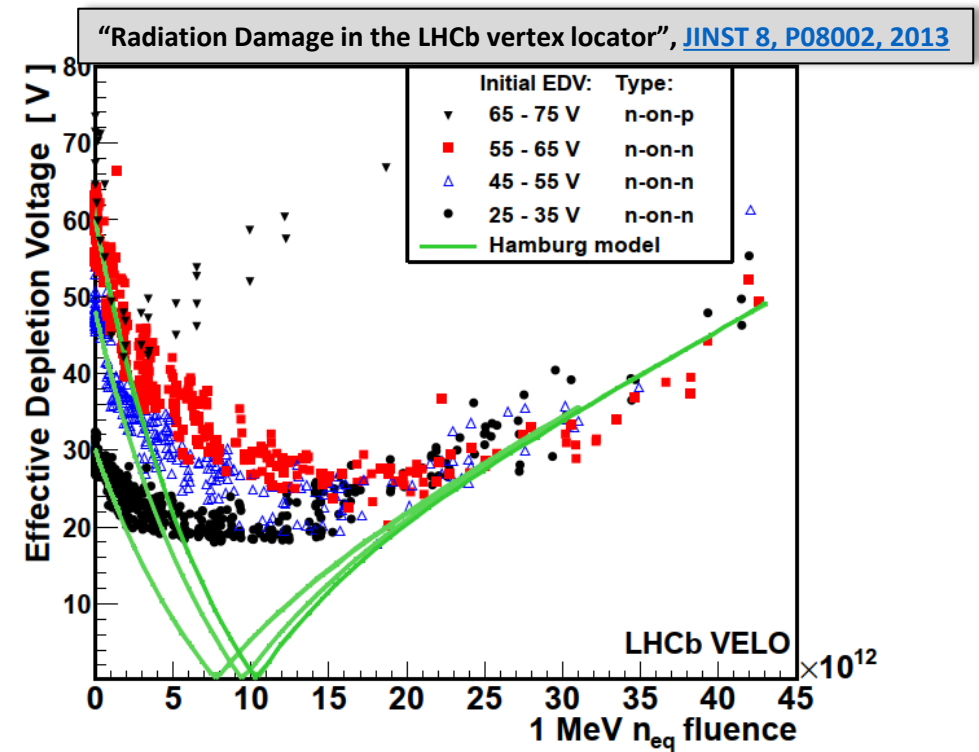
# •Re-introduction coefficient

## Re-Introduction Rates



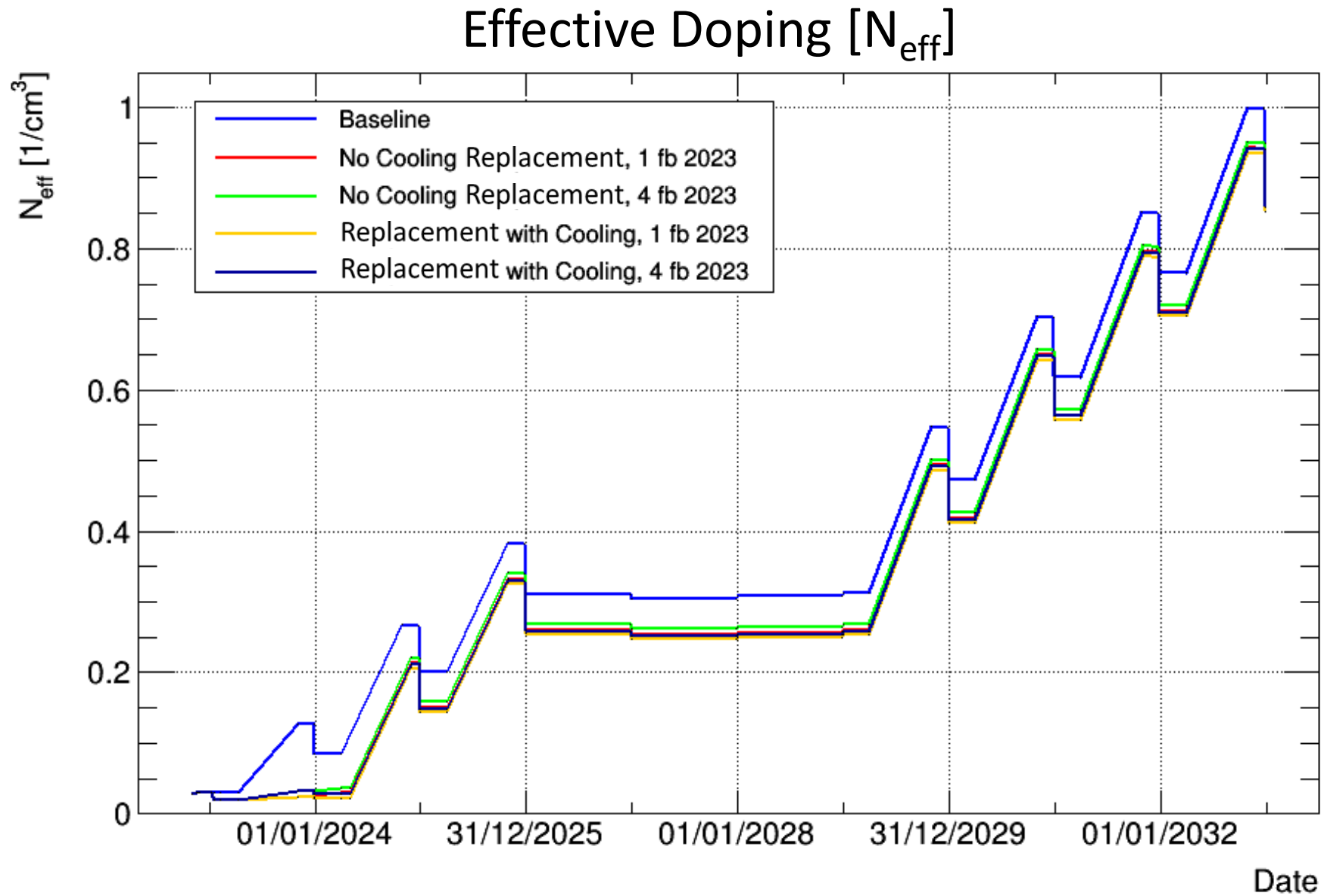
$$N_C(\Phi_{eq.}) = \underbrace{g_c}_{\text{Re-Introduction rate } g_c} \times \Phi_{eq.} - \underbrace{f_c}_{\text{Removable Fraction}} \times \underbrace{N_{eff.}(0)}_{\text{Original doping concentration}} (1 - e^{-\underbrace{c_A}_{\text{Acceptor Removal Coefficient}} \Phi_{eq.}})$$

$\checkmark > 0$  primarily acceptor introduction  
 $\checkmark < 0$  primarily donor introduction





# • $N_{\text{eff}}$ – Dynamic Model



# •Code Structure

## Run Time Interaction

Acceptor removal Fit from bibliography (data in Share\AcceptorRemoval.txt) to establish the equation for calculation he removal coefficient with respect to  $N_{\text{eff}}(0)$

Fit using data in Share\VDepVelo1.txt to determine the re-introduction rates to be used for the calculations of the  $N_{\text{eff}}$

Folder where scenario files will be searched, all present files will be treated as different scenarios

Processed scenario

Printing final values of the final scenario for control and debug purposes. Not really needed, can be expanded to every included scenario

```
(RadDamage *) 0x234a172f150
FCN=89.5311 FROM MINOS STATUS=SUCCESSFUL 44 CALLS 384 TOTAL
EDM=1.10201e-07 STRATEGY= 1 ERROR MATRIX ACCURATE

EXT PARAMETER STEP FIRST
NO. NAME VALUE ERROR SIZE DERIVATIVE
1 Factor 1.65656e-07 7.61792e-08 -8.54537e-06 4.37059e-02
2 Exponent 4.94566e-01 1.49418e-02 1.49418e-02 -5.01063e-02
FCN=89.5311 FROM MINOS STATUS=SUCCESSFUL 44 CALLS 384 TOTAL
EDM=1.10201e-07 STRATEGY= 1 ERROR MATRIX ACCURATE
```

```
EXT PARAMETER STEP FIRST
NO. NAME VALUE ERROR SIZE DERIVATIVE
1 Factor 1.65656e-07 7.61792e-08 -8.54537e-06 4.37059e-02
2 Exponent 4.94566e-01 1.49418e-02 1.49418e-02 -5.01063e-02
FCN=95.3134 FROM MINOS STATUS=SUCCESSFUL 52 CALLS 399 TOTAL
EDM=1.29973e-08 STRATEGY= 1 ERROR MATRIX ACCURATE

EXT PARAMETER STEP FIRST
NO. NAME VALUE ERROR SIZE DERIVATIVE
1 g_{A} 2.20738e-02 2.02334e-03 -7.98061e-04 -2.29641e-03
2 f 4.33574e-01 1.54399e-02 -1.73868e-03 -1.82045e-02
3 c_{A} 1.25261e-12 1.33921e-13 1.33921e-13 -8.72214e-04
```

```
1: C:/Users/Vagelis/Desktop/VELOU1Radiation/RadDamage/Backup/Scenarios/*.*
```

```
RadDamage::Calculate INFO: Profile successfully read from file: "Test standard.txt". Profile Legnth: 16
<=====> :100%. Processed entries: 16 / 16
```

```
0.000421523 8.65308e-05 4.87136
```

```
RadDamage::Calculate INFO: Processing finished, writing data...
```

```
Final Effective Doping [N_{eff}] is: 2.18777e+13
```

```
Final Donors [N_{don.}] is: 0
```

```
Final Acceptors [N_{acc.}] is: 2.18777e+13
```

```
Final Depletion Voltage is: 677.876
```

```
Final #alpha Factors @ 21.0^{o}C is: 1.98917e-17
```

```
Final Leakage Current per module @ 21.0^{o}C is: 0.000884688
```

```
Final Leakage Current per module @ -20.0^{o}C is: 1.02972e-05
```

```
Final Leakage Current @ 21.0^{o}C is: 0.00743435
```

```
Final Leakage Current @ -20.0^{o}C is: 8.65308e-05
```

```
Final Power Consumption @ 21.0^{o}C is: 5.03957
```

```
Final Power Consumption @ -20.0^{o}C is: 0.0586571
```

```
Final Temperature is: 333.15
```

```
Final Fluence is: 3.73742e+14
```

# •Conclusions

## Outlook and next steps

- Introduction of asymmetric band uncertainties (currently underway)
- Validation against data (mainly  $\alpha$  factors and  $N_{\text{eff}}$ )
- Re-optimization of fitting parametrization from data
- Direct link to TIMBER and to luminosity monitor for automatization
- Expand to n-in-p type sensors (intrinsically supported, treated indifferently in re-introduction rate fit level)

