

1 Atom-diatom collision

Minimum translational energy required:

$$E_t = G = \frac{1 - \sqrt{\alpha}}{(1 + \sqrt{\alpha}) \cos^2 \gamma_1 \cos^2 \gamma_2} \left(\frac{\sqrt{D - E_v \sin^2 \varphi} + \sqrt{E_v} \cos \varphi}{(1 - \sqrt{\alpha}) \cos \theta} - \sqrt{E_v} \cos \theta \cos \varphi - \sqrt{E_r} \cos \beta \sin \theta \right)^2 \quad (1)$$

Simplified:

$$E_t = G = \frac{1 - \sqrt{\alpha}}{(1 + \sqrt{\alpha}) \cos^2 \gamma_1 \cos^2 \gamma_2} \left(\frac{\sqrt{D^* - E_v \sin^2 \varphi} + \sqrt{E_v} \cos \varphi}{(1 - \sqrt{\alpha}) \cos \theta} - \sqrt{E_v} \cos \theta \cos \varphi \right)^2 \quad (2)$$

Threshold line:

$$\gamma_1 = \gamma_2 = \theta = 0 \quad (3)$$

$$\cos \varphi = \begin{cases} -1 & \text{if } E_v \leq \alpha D^* \\ -\sqrt{\frac{\alpha(D^* - E_v)}{(1 - \alpha)E_v}} & \text{if } E_v > \alpha D^* \end{cases} \quad (4)$$

Threshold function:

$$E_t = F(E_v) = \begin{cases} \frac{(\sqrt{D^*} - \sqrt{\alpha E_v})^2}{1 - \alpha} & \text{if } E_v \leq \alpha D^* \\ D^* - E_v & \text{if } E_v > \alpha D^* \end{cases} \quad (5)$$

Taylor expansion of G :

1.1 For $E_v < \alpha D$

$$\begin{aligned} G_{\gamma_1, \gamma_2}^{(2)} &= 2F \\ G_{\theta}^{(2)} &= \frac{2D}{1 - \alpha} \left(1 - \sqrt{\frac{\alpha E_v}{D}} \right) \left(1 - (2 - \sqrt{\alpha}) \sqrt{\frac{E_v}{D}} \right) \\ G_{\varphi}^{(2)} &= \frac{2}{1 - \alpha} D \sqrt{\frac{\alpha E_v}{D}} \left(1 - \sqrt{\frac{\alpha E_v}{D}} \right) \left(1 - \sqrt{\frac{E_v}{\alpha D}} \right) \\ G_{\varphi}^{(4)} &= 6D\alpha(1 - \alpha) \end{aligned} \quad (6)$$

1.2 For $E_v > \alpha D$

Follow the similar procedure,

$$\begin{aligned} G_{\gamma_1, \gamma_2}^{(2)} &= 2F \\ G_{\theta}^{(2)} &= \frac{1 - \sqrt{\alpha}}{1 + \sqrt{\alpha}} \cdot 2F \\ G_{\varphi}^{(2)} &= 2(E_v - \alpha D) \end{aligned} \quad (7)$$

1.3 Monte Carlo Process

We can also get the probability by **Monte Carlo sampling**, which should be more accurate and we won't have any singularity:

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1: procedure CHECK_REACTION( $E_t, E_r, E_v$ )
2:   Generate phase angles  $\gamma_1, \gamma_2, \theta, \varphi$  randomly with suitable p.d.f
3:   Compute effective dissociation energy  $D_{ef} = D_{ef}(E_r)$ 
4:   Compute threshold of reaction  $E_{th} = F(\gamma_1, \gamma_2, \theta, \varphi, D_{ef}, E_v)$ 
5:   if  $E_t \geq E_{th}$  then
6:     Reaction occurs (i.e.  $P = 1$ )
7:   else
8:     Reaction doesn't occur (i.e.  $P = 0$ )
9:   end if
10: end procedure

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2 Derivation for diatom-diatom collision

A different set of geometry angles are used here. These angles are fully decoupled.

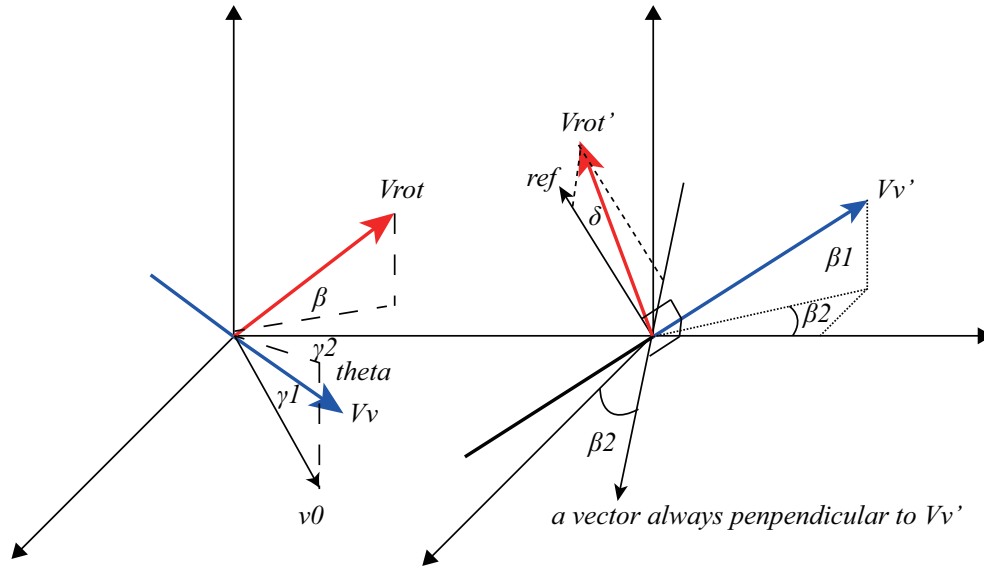


Figure 1: Collision geometry

Assume a collision between diatom($N_1 N_2$) and diatom($N_3 N_4$), N_2 and N_3 are the atoms which collide. A body fitted right-hand-side coordinate system is formulated by unit vectors:

$$\begin{aligned}
\hat{v}'_x &= [\cos \beta_2, \sin \beta_2, 0]^T \\
\hat{v}'_v &= [-\cos \beta_1 \sin \beta_2, \cos \beta_1 \cos \beta_2, \sin \beta_1]^T \\
\hat{v}'_{ref} &= [\cos \beta_2, \sin \beta_2, 0]^T \times \hat{v}'_v = [\sin \beta_1 \sin \beta_2, -\sin \beta_1 \cos \beta_2, \cos \beta_1]
\end{aligned} \tag{8}$$

Two rotational operation can transform the coordinates from original coordinates to the new one:

$$\begin{bmatrix} x' \\ y' \\ z' \end{bmatrix} = R_x(\beta_1) \cdot R_z(\beta_2) \begin{bmatrix} x \\ y \\ z \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos \beta_1 & \sin \beta_1 \\ 0 & -\sin \beta_1 & \cos \beta_1 \end{bmatrix} \cdot \begin{bmatrix} \cos \beta_2 & \sin \beta_2 & 0 \\ -\sin \beta_2 & \cos \beta_2 & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} x \\ y \\ z \end{bmatrix} \tag{9}$$

Thus we can get:

$$\begin{bmatrix} x \\ y \\ z \end{bmatrix} = R_z(-\beta_2) \cdot R_x(-\beta_1) \begin{bmatrix} x' \\ y' \\ z' \end{bmatrix} = \begin{bmatrix} \cos \beta_2 & -\cos \beta_1 \sin \beta_2 & \sin \beta_1 \sin \beta_2 \\ \sin \beta_2 & \cos \beta_1 \cos \beta_2 & -\cos \beta_2 \sin \beta_1 \\ 0 & \sin \beta_1 & \cos \beta_1 \end{bmatrix} \begin{bmatrix} x' \\ y' \\ z' \end{bmatrix} = A \begin{bmatrix} x' \\ y' \\ z' \end{bmatrix} \tag{10}$$

Then we have:

$$\begin{aligned}
\hat{v}_v &= A \begin{bmatrix} 0 & 1 & 0 \end{bmatrix}^T \\
\hat{v}_{ref}' &= A \begin{bmatrix} 0 & 0 & 1 \end{bmatrix}^T \\
\hat{v}_r' &= A \begin{bmatrix} -\sin \delta & 0 & \cos \delta \end{bmatrix}^T = \begin{bmatrix} -\cos \beta_2 \sin \delta + \sin \beta_1 \sin \beta_2 \cos \delta \\ -\sin \beta_2 \sin \delta - \sin \beta_1 \cos \beta_2 \cos \delta \\ \cos \beta_1 \cos \delta \end{bmatrix}
\end{aligned} \tag{11}$$

Velocity vector for diatom(N_1N_2)-diatom(N_3N_4) collision:

$$\vec{v}_2^T = \begin{bmatrix} -\cos \beta \cos \theta & \sin \theta & \cos \gamma_1 \sin \gamma_2 \\ \cos \beta \sin \theta & \cos \theta & \cos \gamma_1 \cos \gamma_2 \\ \sin \beta & 0 & -\sin \gamma_1 \end{bmatrix} \begin{bmatrix} v_r \\ v_v \\ v \end{bmatrix} \tag{12}$$

$$\vec{v}_3^T = \begin{bmatrix} -\cos \beta_2 \sin \delta + \sin \beta_1 \sin \beta_2 \cos \delta & -\cos \beta_1 \sin \beta_2 & -\cos \gamma_1 \sin \gamma_2 \\ -\sin \beta_2 \sin \delta - \sin \beta_1 \cos \beta_2 \cos \delta & \cos \beta_1 \cos \beta_2 & -\cos \gamma_1 \cos \gamma_2 \\ \cos \beta_1 \cos \delta & \sin \beta_1 & \sin \gamma_1 \end{bmatrix} \begin{bmatrix} v_r' \\ v_v' \\ \frac{m}{M}v \end{bmatrix} \tag{13}$$

Pre-collision component of velocity on y -axis:

$$\begin{aligned}
v_{2y} &= v \cos \gamma_1 \cos \gamma_2 + v_r \cos \beta \sin \theta + v_v \cos \theta \\
v_{3y} &= -\frac{m}{M}v \cos \gamma_1 \cos \gamma_2 - v_r' (\sin \beta_1 \cos \beta_2 \cos \delta + \sin \beta_2 \sin \delta) + v_v' \cos \beta_1 \cos \beta_2
\end{aligned} \tag{14}$$

The minimum velocity v to make post-vibrational energy equal to D :

$$\begin{aligned}
v &= \frac{1}{\cos \gamma_1 \cos \gamma_2} \left[\frac{1}{\cos \theta} \left(\frac{\sqrt{D - mv_0^2 \sin^2 \varphi_0}}{\sqrt{m}} + \frac{m + M \sin^2 \theta}{M + m} v_0 \cos \varphi_0 \right) \right. \\
&\quad - \frac{M}{m + M} (v_r' (\sin \beta_1 \cos \beta_2 \cos \delta + \sin \beta_2 \sin \delta) - v_1 \cos \varphi_1 \cos \beta_1 \cos \beta_2) \\
&\quad \left. - \frac{M}{m + M} (v_r \cos \beta \sin \theta) \right]
\end{aligned} \tag{15}$$

Noted that the following term is the projection of velocity on y axis:

$$\boxed{v_r' (\sin \beta_1 \cos \beta_2 \cos \delta + \sin \beta_2 \sin \delta) - v_1 \cos \varphi_1 \cos \beta_1 \cos \beta_2} \tag{16}$$

Then we can get the threshold $E_t = \frac{2}{\mu}(mv)^2$:

$$\begin{aligned}
E_t &= \frac{2m^2/\mu}{\cos^2 \gamma_1 \cos^2 \gamma_2} \left[\frac{M}{(m + M)\sqrt{m}} \left(\frac{\sqrt{D - E_v \sin^2 \varphi_0} + \sqrt{E_v} \cos \varphi_0}{\cos \theta (M/(m + M))} - \sqrt{E_v} \cos \varphi_0 \cos \theta - \sqrt{E_r} \cos \beta \sin \theta \right) \right. \\
&\quad \left. - \frac{\sqrt{M}}{m + M} \left(\sqrt{E_r'} (\cos \delta \cos \beta_2 \sin \beta_1 + \sin \beta_2 \sin \delta) - \sqrt{E_v'} \cos \varphi_1 \cos \beta_1 \cos \beta_2 \right) \right]^2
\end{aligned} \tag{17}$$

Again, define $\alpha = (m/(M + m))^2$, then we have:

$$\frac{m}{M + m} = \sqrt{\alpha}; \quad \frac{M}{M + m} = 1 - \sqrt{\alpha} \tag{18}$$

$$\frac{m}{M} = \frac{\sqrt{\alpha}}{1 - \sqrt{\alpha}}; \quad \frac{M}{m} = \frac{1 - \sqrt{\alpha}}{\sqrt{\alpha}}; \tag{19}$$

Then:

$$E_t = \frac{1 - \sqrt{\alpha}}{\cos^2 \gamma_1 \cos^2 \gamma_2} \left[\frac{\sqrt{D - E_v \sin^2 \varphi_0} + \sqrt{E_v} \cos \varphi_0}{\cos \theta (1 - \sqrt{\alpha})} - \sqrt{E_v} \cos \varphi_0 \cos \theta - \sqrt{E_r} \cos \beta \sin \theta \right. \\ \left. - \left(\frac{\sqrt{\alpha}}{1 - \sqrt{\alpha}} \right)^{1/2} \left(\sqrt{E'_r} (\cos \delta \cos \beta_2 \sin \beta_1 + \sin \beta_2 \sin \delta) - \sqrt{E'_v} \cos \varphi_1 \cos \beta_1 \cos \beta_2 \right) \right]^2 \quad (20)$$

Again, we use $D_{eff} = D - E_r + \frac{2E_r^{3/2}}{3(3bD)^{1/2}}$ to replace E_r

$$E_t = \frac{1 - \sqrt{\alpha}}{\cos^2 \gamma_1 \cos^2 \gamma_2} \left[\frac{\sqrt{D_{eff} - E_v \sin^2 \varphi_0} + \sqrt{E_v} \cos \varphi_0}{\cos \theta (1 - \sqrt{\alpha})} - \sqrt{E_v} \cos \varphi_0 \cos \theta \right. \\ \left. - \left(\frac{\sqrt{\alpha}}{1 - \sqrt{\alpha}} \right)^{1/2} \left(\sqrt{E'_r} (\cos \delta \cos \beta_2 \sin \beta_1 + \sin \beta_2 \sin \delta) - \sqrt{E'_v} \cos \varphi_1 \cos \beta_1 \cos \beta_2 \right) \right]^2 \quad (21)$$

The term $[\cos \delta \cos \beta_2 \sin \beta_1 + \sin \beta_2 \sin \delta]$ can be replaced by $\cos \alpha_1 \cos \alpha_2$, in which α_1 and α_2 are azimuth and polar angle for \vec{v}_r

The original one in the paper:

$$E_t = \frac{1 - \sqrt{\alpha}}{\cos^2 \gamma_1 \cos^2 \gamma_2} \left[\frac{\sqrt{D_{eff} - E_v \sin^2 \varphi_0} + \sqrt{E_v} \cos \varphi_0}{\cos \theta (1 - \sqrt{\alpha})} - \sqrt{E_v} \cos \varphi_0 \cos \theta \right. \\ \left. - \left(\frac{\sqrt{\alpha}}{1 - \sqrt{\alpha}} \right)^{1/2} \left(\sqrt{E'_r} (\cos \delta \cos \beta_2 \sin \beta_1 + \sin \beta_2 \sin \delta) + \sqrt{E'_v} \cos \varphi_1 \cos \beta_1 \cos \beta_2 \right) \right]^2 \quad (22)$$

Optimum configuration and threshold function are same as the ones in original paper.

$$\gamma_1 = \gamma_2 = \theta = \beta_1 = \varphi_1 = 0; \quad \delta = \frac{\pi}{2}; \quad \beta_2 = \pi - \arctan(\sqrt{E'_r/E'_v}) \quad (23)$$

3 DSMC recipe

There are 8 angles to be sampled. The range of sampling are:

$$\begin{aligned} \text{Phase angle : } \varphi_0, \varphi_1 &\in [0, 2\pi] \\ \text{Polar angle : } \gamma_2, \beta_2 &\in [0, 2\pi] \\ \text{Azimuth angle : } \gamma_1, \beta_1 &\in [0, \pi] \\ \text{Reference angle : } \theta, \delta &\in [0, 2\pi] \end{aligned} \quad (24)$$

The region can be reduced by considering terms in Eq. 21.

First, the phase angles only appear in $\sin^2 \varphi$ or $\cos \varphi$, thus:

$$\text{Phase angle : } \varphi_0, \varphi_1 \in [0, \pi] \quad (25)$$

Next, polar angle γ_2 appears as $\cos^2 \gamma_2$. The reason is that only projection of velocity influences, thus $\gamma_2 \in [0, \pi]$ has no difference compared to $\gamma_2 \in [\pi, 2\pi]$

$$\text{Polar angle : } \gamma_2 \in [0, \pi] \quad (26)$$

Next, if we expand Eq. 21, we will find that θ only appears in $\cos \theta, \cos^2 \theta, \cos^3 \theta, \cos^4 \theta$. Thus In summary:

$$\begin{aligned} \varphi_0, \varphi_1, \gamma_2, \beta_1, \gamma_1 &\in [0, \pi] \\ \beta_2, \theta, \delta &\in [0, 2\pi] \end{aligned} \quad (27)$$

4 Matlab recipe

We can also obtain the same results by Monte-Carlo sampling in Matlab.

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1: for  $E_v = E_v(0), \dots, E_v(end)$  do
2:   Sample  $E_t$  from  $f(\frac{E_t}{T}) = \frac{1}{\Gamma[5/2 - \bar{\omega}]} \left(\frac{E_t}{T}\right)^{3/2 - \bar{\omega}} \exp(-\frac{E_t}{T})$ 
3:   Sample  $E_r, E'_r$  from  $f(\frac{E_r}{T}) = \exp(-\frac{E_r}{T})$ 
4:   Sample  $E'_v$  from  $P(E'_v) = \frac{\exp(-E'_v/T_v)}{\sum_j \exp(-E'_v(j)/kT_v)}$ 
5:   Sample angles
6:   Calculate reaction probability  $P(v)$ 
7: end for
8: Calculate VHS collision rates  $k_{coll}(T)$ 
9: Reaction rates  $k(T, T_v) = k_{coll}(T) \frac{\sum_j P(j) \exp(-E_v(j)/T_v)}{\sum_j \exp(-E_v(j)/kT_v)}$ 

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This method is much faster than DSMC (2 min v.s. 2 hours). It can also obtain rates for extreme low temperature since vibrational state-specific rates are directly calculated with the method.

Appendix:

1. Volume 1

$$\sum_{i=1}^n \left(\frac{x}{R_i} \right)^2 = 1 \quad (28)$$

$$V = \frac{\Pi^{n/2} \prod_i R_i}{\Gamma[n/2 + 1]} \quad (29)$$

2. Volume 2

$$\sum_{i=1}^{n-1} \left(\frac{x}{R_i} \right)^2 + \left(\frac{x}{R_n} \right)^4 = 1 \quad (30)$$

$$V = \frac{2\pi^{n/2-1} \Gamma[\frac{5}{4}]}{\Gamma\left[\frac{3}{4} + \frac{n}{2}\right]} \prod_i R_i \quad (31)$$