

1. a.  $I_{D1} = I_{REF} = 25 \mu A$

$$I_{D1} = \frac{K'_n}{2} \left( \frac{W}{L} \right)_1 (V_{GSN} - V_{TN})^2$$

$$I_{D2} = \frac{K'_n}{2} \left( \frac{W}{L} \right)_2 (V_{GSN} - V_{TN})^2$$

$$I_{D3} = \frac{K'_n}{2} \left( \frac{W}{L} \right)_3 (V_{GSN} - V_{TN})^2$$

$$\frac{I_{D1}}{I_{D2}} = \frac{\left( \frac{W}{L} \right)_1}{\left( \frac{W}{L} \right)_2} \quad \frac{I_{D3}}{I_{D1}} = \frac{\left( \frac{W}{L} \right)_3}{\left( \frac{W}{L} \right)_1}$$

$$\therefore I_{D2} = 2 I_{D1} = 50 \mu A$$

$$I_{D3} = 5 I_{D1} = 125 \mu A$$

$$I_{D4} = I_{REF} = 25 \mu A$$

$$I_{D4} = \frac{K'_p}{2} \left( \frac{W}{L} \right)_4 (V_{GSP} - V_{TP})^2 \quad I_{D5} = \frac{K'_p}{2} \left( \frac{W}{L} \right)_5 (V_{GSP} - V_{TP})^2$$

$$\therefore \frac{I_{D5}}{I_{D4}} = \frac{\left( \frac{W}{L} \right)_5}{\left( \frac{W}{L} \right)_4} \quad \therefore I_{D5} = 25 \mu A$$

b.  $I_{D1} = \frac{K'_n}{2} \left( \frac{W}{L} \right)_1 (V_{GSN} - V_{TN})^2$

$$\Downarrow$$

$$25 \mu A = \frac{25 \mu A / V^2}{2} \times 5 \times (V_{GSN} - 1)^2 \quad \text{also } V_{GSN} - V_{TN} > 0$$

$$\therefore V_{GSN} = 1.63 V$$

$$I_{D4} = \frac{K'_p}{2} \left( \frac{W}{L} \right)_4 (V_{GSP} - V_{TP})^2$$

$$\Downarrow$$

$$25 \mu A = \frac{10 \mu A / V^2}{2} \times 5 \times (V_{GSP} + 1)^2 \quad \text{also } V_{GSP} - V_{TP} < 0$$

$$\therefore V_{GSP} = -2 V$$

$$R = \frac{(V_{DD} + V_{GSP}) - (V_{SS} + V_{GSN})}{I_{REF}} = 0.255 \mu \Omega$$

2. a. From problem 1 we know that  $V_{GSN} = 1.63V$   $V_{GSP} = -2V$

$$V_{SD6} = V_{DD} + V_{GSP} - (V_{SS} + V_{GSN})$$
$$= 5V - 2V + 5V - 1.63V = 6.37V$$

$$V_{GS6} = V_{DS6} = -6.37V$$

$$I_{D6} = I_{REF} = 25\mu A = \frac{K'_p}{2} \left(\frac{W}{L}\right)_6 (V_{GS6} - V_{TP})^2$$

$$\left(\frac{W}{L}\right)_6 = \frac{I_{D6}}{\frac{K'_p}{2} (V_{GS6} - V_{TP})^2} = \frac{25\mu A}{\frac{1}{2} \times 10\mu A/V^2 \times (-6.37V + 1V)^2} = \frac{1}{5.77}$$

b. If  $M_6$  is implemented as a diode-connected nFET

$$V_{DS6} = 6.37V \quad V_G = V_D \quad V_{GS6} = 6.37V$$

$$\left(\frac{W}{L}\right)_6 = \frac{I_{D6}}{\frac{K'_n}{2} (V_{GS6} - V_{TN})^2} = \frac{25\mu A}{\frac{1}{2} \times 25\mu A/V^2 \times (6.37V - 1V)^2} = \frac{1}{14.42}$$

c. Assume  $W$  is fixed,  $L_n > L_p$ , so nFET would take up the most area.

3. a.  $V_{EQ} = \frac{R_1}{R_1 + R_2} V_{GG} = 3V$   $R_{EQ} = \frac{R_1 R_2}{R_1 + R_2} = 210k\Omega$

b.  $V_{GS} = V_{EQ} = 3V > V_T$  Assume MOSFET operates in saturation

$$I_D = \frac{K_n}{2} (V_{GS} - V_T)^2 = \frac{25\mu A/V^2}{2} \times (3 - 1)^2 = 50\mu A$$

$$V_{DS} = V_{DD} - I_D R_D = 10V - 0.05mA \cdot 100k\Omega = 5V$$

$\therefore V_{DS} > V_{GS} - V_T$ , the MOSFET indeed operates in saturation and the assumption is correct.

c. Now the new value of  $K_n$  is  $K_{n1} = 20\mu A/V^2$

$$I_{D1} = \frac{K_{n1}}{2} (V_{GS} - V_T)^2 = \frac{20\mu A/V^2}{2} \times (3V - 1V)^2 = 40\mu A$$

$$V_{DS1} = V_{DD} - I_{D1} R_D = 10V - 0.04 \text{ mA} \times 100 \text{ k}\Omega = 6V$$

$$I_D \text{ decreases by } \frac{\Delta I_D}{I_D} = \frac{50 \mu\text{A} - 40 \mu\text{A}}{50 \mu\text{A}} = 20\%$$

$$V_{DS} \text{ increases by } \frac{\Delta V_{DS}}{V_{DS}} = \frac{6V - 5V}{5V} = 20\%$$

$$4. \quad a. \quad V_{EQ} = V_{DD} \cdot \frac{R_1}{R_1 + R_2} = 10V \cdot \frac{1 \text{ M}\Omega}{2.5 \text{ M}\Omega} = 4V$$

$$R_{EQ} = \frac{R_1 R_2}{R_1 + R_2} = 0.6 \text{ M}\Omega$$

$$b. \quad I_D = \frac{V_{EQ} - V_{GS}}{R_S} = \frac{K_n}{2} (V_{GS} - V_T)^2 \text{ with the assumption of saturation}$$

plugging the numbers, we have

$$\frac{25}{2} (V_{GS} - 1)^2 \times 10^{-3} = \frac{4 - V_{GS}}{39}$$

↓

$$V_{GS} = -2.71V \text{ or } V_{GS} = 2.66V \quad \text{Since } V_{GS} > V_T, \quad V_{GS} = 2.66V$$

$$I_D = \frac{V_{EQ} - V_{GS}}{R_S} = \frac{4V - 2.66V}{39 \text{ k}\Omega} = 34.4 \mu\text{A}$$

$$V_{DS} = V_{DD} - I_D R_D - I_D R_S = 6.08V$$

$V_{DS} > V_{GS} - V_T$ , so the transistor operates in saturation and the assumption is correct.

c. With the new value  $K_{n1} = 20 \mu\text{A}/\text{V}^2$ , we have

$$\frac{20}{2} (V_{GS1} - 1)^2 \times 10^{-3} = \frac{4 - V_{GS1}}{39}$$

↓

$$V_{GS1} = -3.34V \text{ or } V_{GS1} = 2.77V \quad \text{Since } V_{GS} > V_T, \quad V_{GS} = 2.77V$$

$$I_{D1} = \frac{V_{EQ} - V_{GS1}}{R_S} = \frac{4V - 2.77V}{39 \text{ k}\Omega} = 31.5 \mu\text{A}$$

$$V_{DS1} = V_{DD} - I_{D1} R_D - I_{D1} R_S = 6.41V$$

$$I_D \text{ decreases by } \frac{\Delta I_D}{I_D} = \frac{34.4 \mu\text{A} - 31.5 \mu\text{A}}{34.4 \mu\text{A}} = 8.4\%$$

$$V_{DS} \text{ increases by } \frac{\Delta V_{DS}}{V_{DS}} = \frac{6.41V - 6.08V}{6.08V} = 5.4\%$$

5. Since  $I_G = 0$ ,  $V_G = V_D$ , the MOSFET operates in saturation

$$I_D = \frac{K_n}{2} (V_{GS} - V_T)^2 \quad I_D = \frac{V_{DD} - V_{DS}}{R_D} = \frac{V_{DD} - V_{GS}}{R_D}$$

$$\therefore \frac{250}{2} (V_{GS} - 1)^2 = \frac{3.3 - V_{GS}}{10} \times 10^3$$

$$\Downarrow$$
$$V_{GS} = 0.81 V \text{ or } V_{GS} = 2.01 V \quad \text{Since } V_{GS} > V_T \quad V_{GS} = 2.01 V$$

$$V_{DS} = V_{GS} = 2.01 V \quad I_D = \frac{3.3 V - 2.01 V}{10 k\Omega} = 0.129 \text{ mA}$$

a. Now the new value of  $K_n$  is  $K_{n1} = 200 \mu A/V^2$

$$\frac{200}{2} (V_{GS1} - 1)^2 = \frac{3.3 - V_{GS1}}{10} \times 10^3$$

$$\Downarrow$$
$$V_{GS1} = -1.097 V \text{ or } V_{GS1} = 2.097 V$$

$$\text{To make } V_{GS1} > V_T, \quad V_{GS1} = 2.097 V \quad V_{DS1} = V_{GS1} = 2.097 V$$

$$I_{D1} = \frac{(3.3 - 2.097) V}{10 k\Omega} = 0.120 \text{ mA}$$

$$I_D \text{ decreases by } \frac{\Delta I_D}{I_D} = \frac{0.129 \text{ mA} - 0.120 \text{ mA}}{0.129 \text{ mA}} = 7.0\%$$

$$V_{DS} \text{ increases by } \frac{\Delta V_{DS}}{V_{DS}} = \frac{2.097 V - 2.01 V}{2.01 V} = 4.3\%$$

6. In problem 3, the simple biasing scheme is sensitive to the variation in  $K_n$ . Since  $I_D = \frac{K_n}{2} (V_{GS} - V_T)^2$ ,  $V_{DS} = V_{DD} - I_D R_D$ ,

the variation percentage of  $I_D$  and  $V_{DS}$  is same as that of  $K_n$  with  $V_{GS}$  fixed in this case.

The biasing techniques in problem 4 and 5 are less sensitive to variations in device parameters since the operating point is stabilized by negative feedback.

In the case of problem 4, suppose for some reason  $I_D$  begins to increase, the voltage drop on  $R_S$  would increase, which results in a decrease in  $V_{GS}$  since  $V_{DD}$  is fixed. And the decrease in  $V_{GS}$  will tend to restore  $I_D$  back to its original value.

In the case of problem 5, suppose  $I_D$  increases for some reason. As a result,  $V_{DS}$  will decrease and so will  $V_{GS}$  since  $V_{GS} = V_{DS}$ . The decrease in  $V_{GS}$  will tend to make  $I_D$  decrease to its original value.