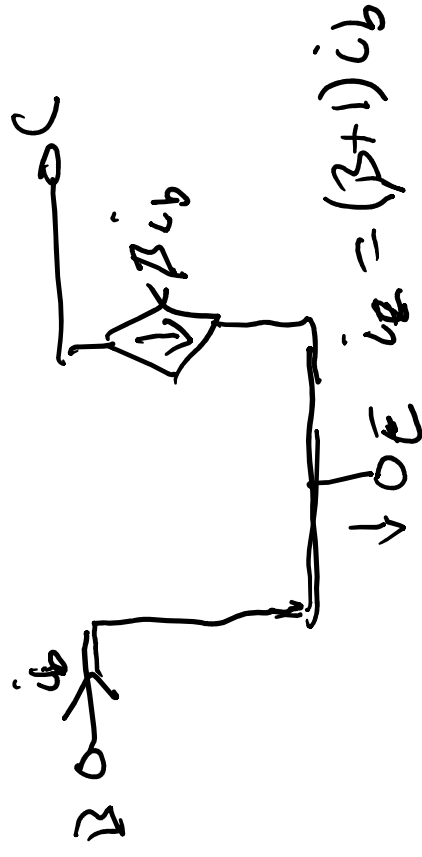
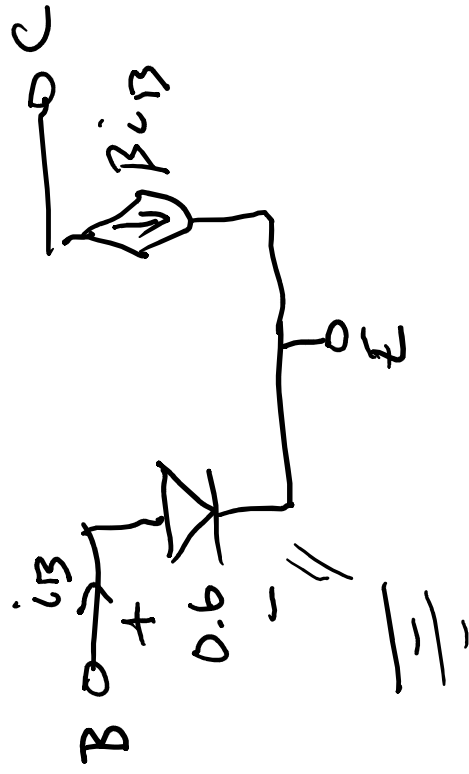


# SMALL SIGNAL MODEL FOR BJT

LARGE  
SIGNAL

$\Rightarrow$  S.S.

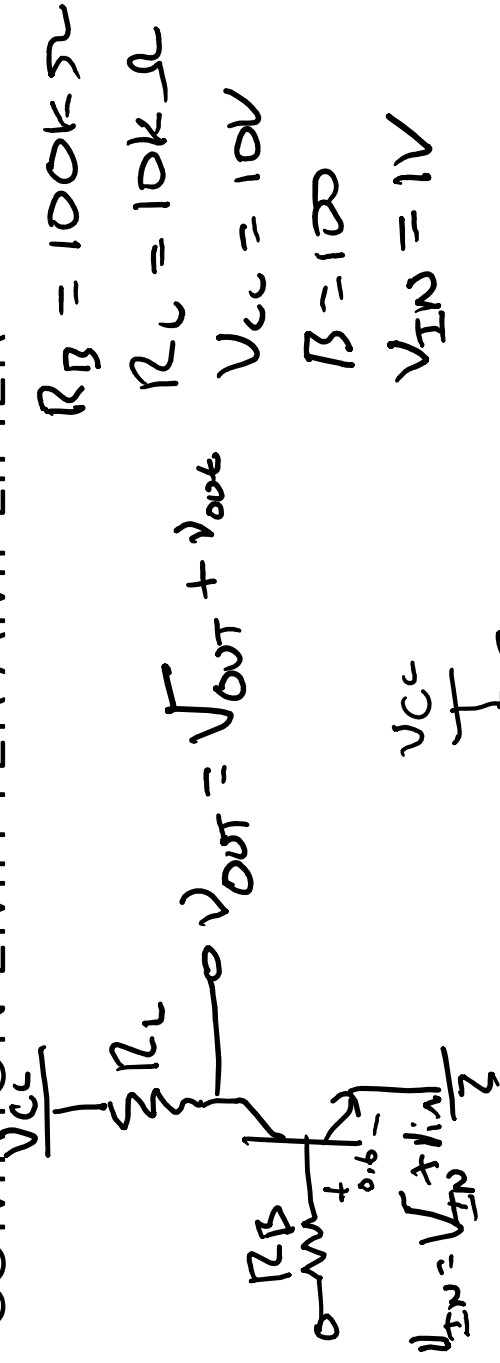


$$i_c = \beta i_b$$

$$i_c = \beta i_b$$

$$= \beta i_b$$

# COMMON EMITTER AMPLIFIER



$$I_C = I_B \beta$$

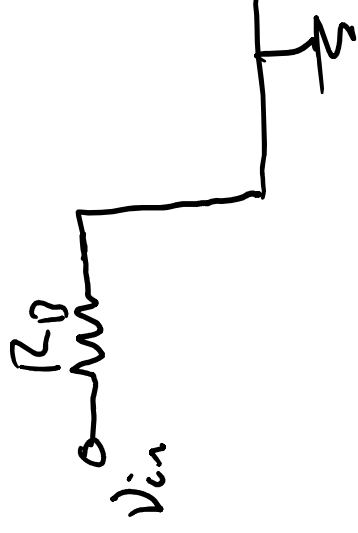
$$= 0.4mA$$

$$V_{OUT} = V_{CC} - (0.4mA)(10k\Omega)$$

$$= 6V$$

$$I_B = \frac{V_{IN} - 0.6V}{R_B}$$

$$= \frac{.4}{105} = 4\mu A$$



$$V_{out} = -\beta i_b$$

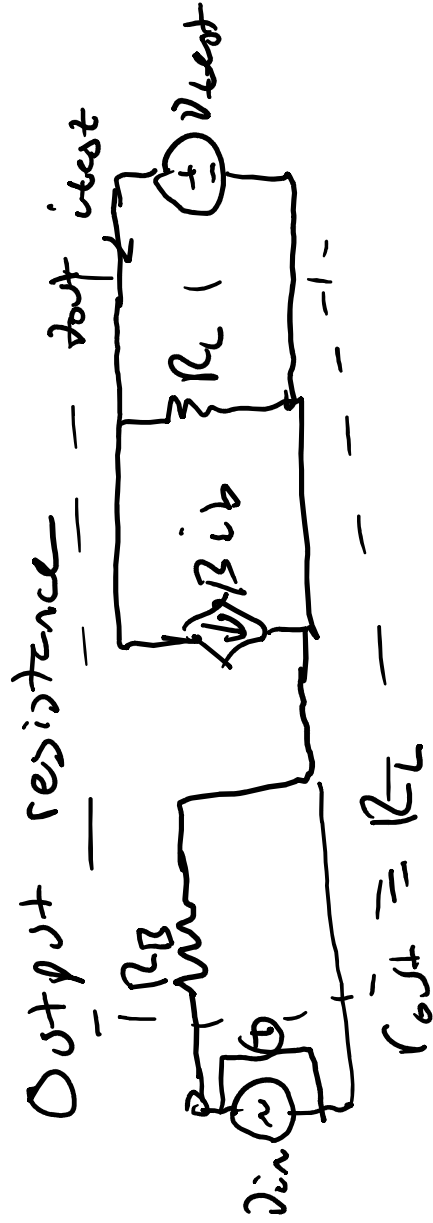
$$i_b = \frac{V_{in}}{R_B}$$

$$\frac{V_{out}}{V_{in}} = -\beta$$

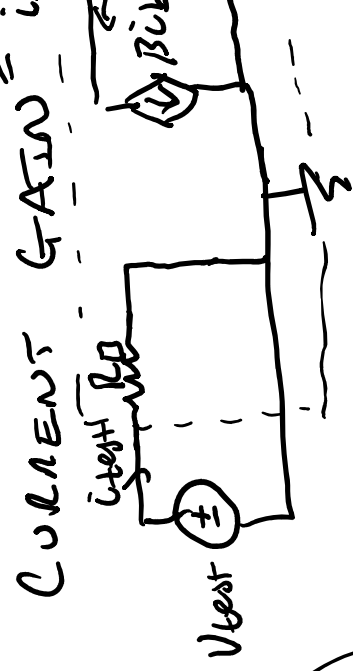
$$V_{out}$$

# INPUT & OUTPUT RESISTANCE FOR C-E AMP

Input resistance =  $R_B$



- ① Zero independent sources
- ② Apply  $V_{test}$ , measure  $i_{test}$



$$i_{test} = \frac{V_{test}}{R_B}$$

$$i_{cb} + \frac{V_{out}}{R_C} + i_{test}$$

$$V_{out} = -\beta i_b (R_C || R_L)$$

$$\beta i_b - \beta i_b \frac{R_C || R_L}{R_C || R_L}$$

$$i_b = i_{test}$$

$$\frac{i_{out}}{i_{test}} = -\beta \frac{R_C || R_L}{R_C || R_L}$$

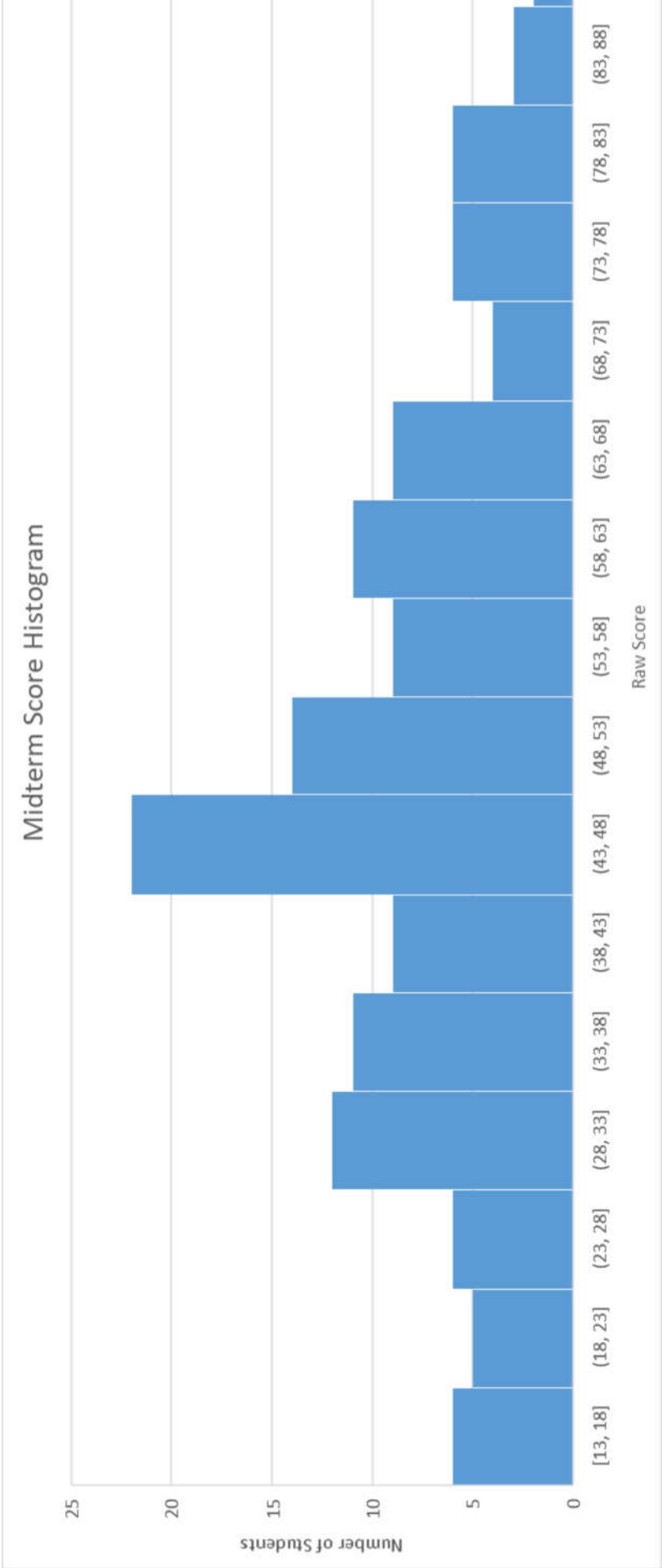
# INPUT & OUTPUT RESISTANCE FOR C-E AMP

$$\begin{aligned} \text{Power Gain} &= \frac{V_{out} \cdot i_{out}}{V_{in} \cdot i_{in}} \\ &= \left( \text{Voltage}_{Gain} \right) \times \left( \text{Current}_{Gain} \right) \\ &= -\beta \left( \frac{R_L // R_o}{R_B} \right) \left( \frac{R_L // R_o}{R_o} \right) = \beta^2 \frac{(R_L // R_o)}{R_o R_B} \end{aligned}$$

with  $R_o$

$$\frac{V_{out}}{V_{in}} = -\beta \left( \frac{R_L // R_o}{R_B} \right)$$

$$\begin{aligned} \frac{i_{out}}{i_{test}} &= -\beta \left( \frac{R_L // R_o}{R_o} \right) \\ &= -\beta \frac{\frac{R_L R_o}{R_L + R_o}}{R_o} \\ &= -\beta \frac{R_L}{R_L + R_o} \end{aligned}$$



Rough Breakdown

Grade	Range	# Students	%
A+	>86	4	3
A	68-86	19	14
B	50-68	36	26
C	32-50	52	38
D	<32	27	20

# DIFFERENTIAL AMPLIFIERS



Common  
rejection  
CMRR

DEFINE:

Difference mode component  $V_D = V_A - V_B$

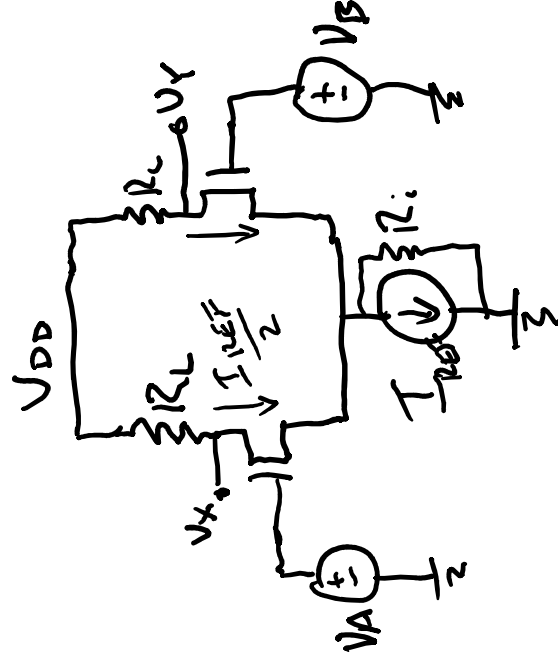
Common mode component  $V_{CM} = \frac{V_A + V_B}{2}$

$A_D = \text{DIFFERENTIAL}$

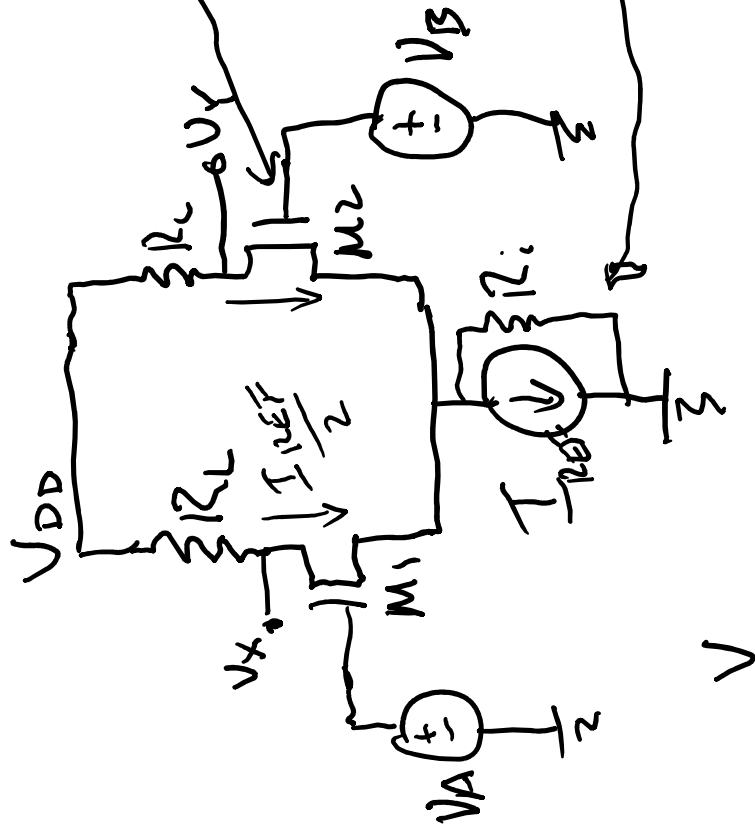
$\rightarrow \text{SIGNAL}$

$A_{CM} = \text{COMMON - MODE}$

$\rightarrow \text{NOISE}$



# DIFFERENTIAL AMPLIFIERS



SOURCE  
COUPLED  
TAIL

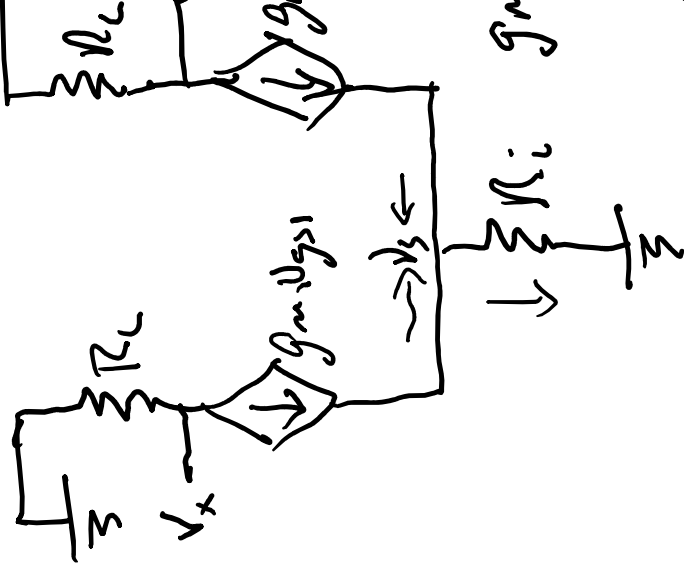
$$V_A \approx \frac{V_D}{2}$$

CURRENT  
SOURCE  
w/ finite  
output resistance

$$V_A = V_{cm} + \frac{V_D}{2}$$

$$V_B = V_{cm} - \frac{V_D}{2}$$

# DIFFERENCE



$$g_m v_{gs1} + g_m v_{gs2} = \frac{V_D}{R_i}$$

$$\frac{V_D}{2} - v_{gs1} = V_s = -\frac{V_D}{2}$$

$$g_m \left( \frac{V_D}{2} - V_s \right) + g_m \left( -\frac{V_D}{2} \right) = \frac{V_D}{R_i}$$

$$-2g_m V_s = \frac{V_D}{R_i}$$

# DIFFERENCE MODE AND COMMON MODE



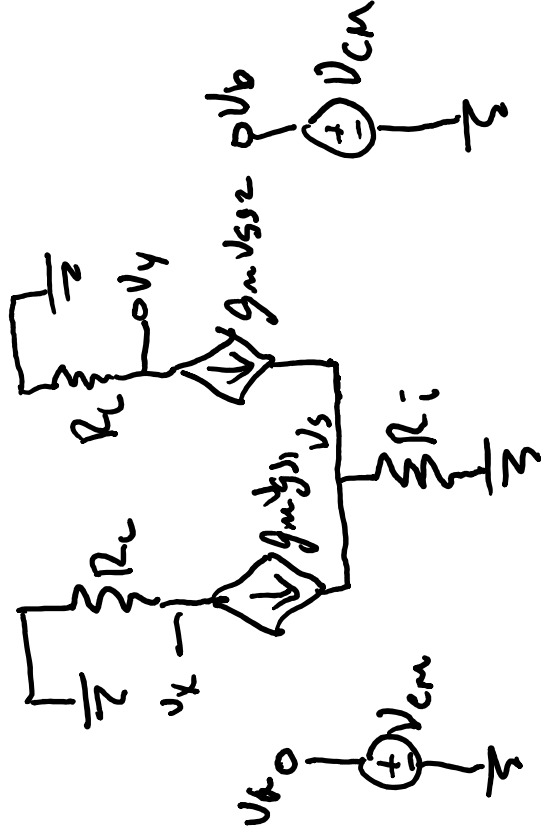
$$V_x = -\frac{g_m V_d}{2} R_L$$

$$V_y = \frac{g_m V_d}{2} R_L$$

$$V_{out} = V_x - V_y$$

$$= -g_m R_L V_d$$

## COMMON - MODE



$$V_{gs1} = V_{gs2} = V_{gs}$$

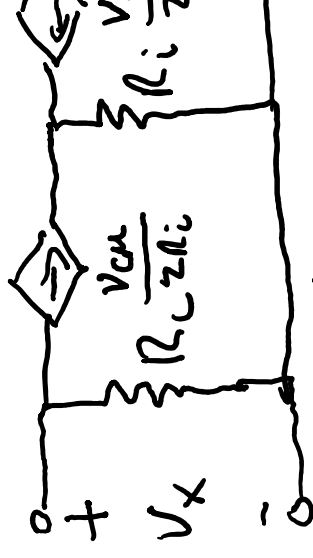
$$V_{gs} = V_{cm} - V_s$$

$$g_m V_{gs} + g_m V_{gs} = \frac{V_s}{R_i}$$

$$2g_m V_{gs} = \frac{V_{cm} - V_{gs}}{R_i}$$

$$V_{gs} = \frac{1}{2g_m R_i + 1} V_{cm}$$

$$V_{gs} \approx \frac{V_{cm}}{2g_m R_i}$$



$$V_x = V_y = -$$

$$V_{out} = V_x - V_y$$

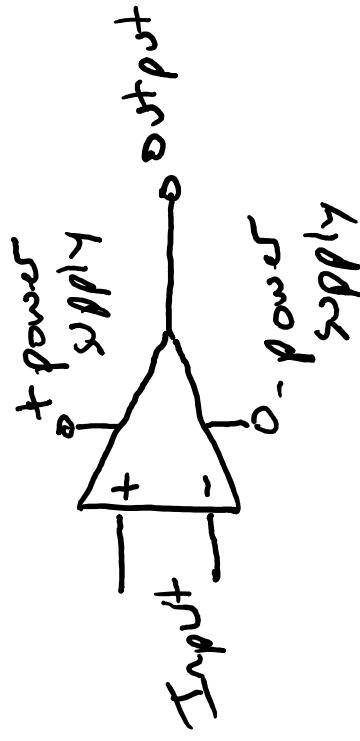
Assume  $R_i$  is large  
(good current source)  
 $2g_m R_i \gg 1$



# CHAPTER 15: OP-AMPS

multi-stage two-input differential amplifiers

Voltage controlled voltage source



IDEAL

$$R_{in} = \infty$$

$$R_{out} = 0$$

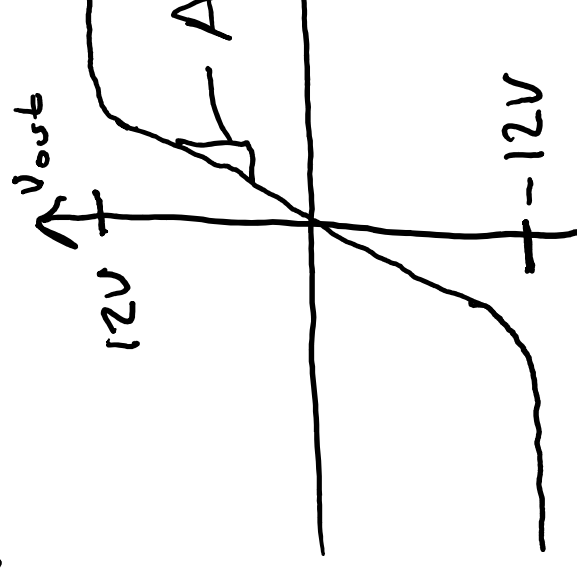
$$\rightarrow A = \infty$$

open loop gain

$$V_{out} = A(v^+ - v^-)$$

$$v^+ \xrightarrow{\dot{v}^+ = 0}$$

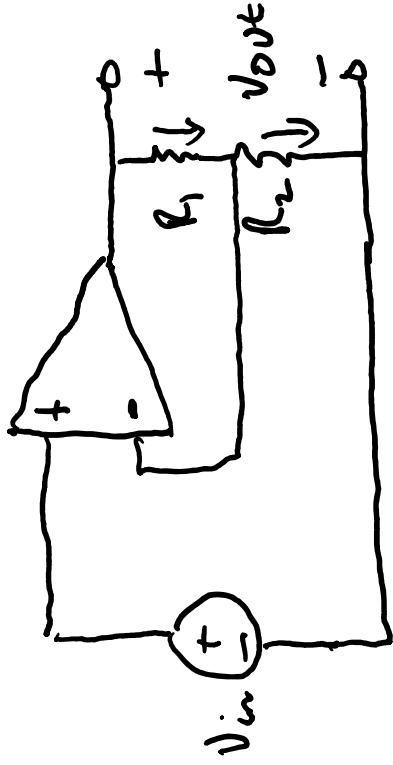
$$v^- \xrightarrow{\dot{v}^- = 0}$$



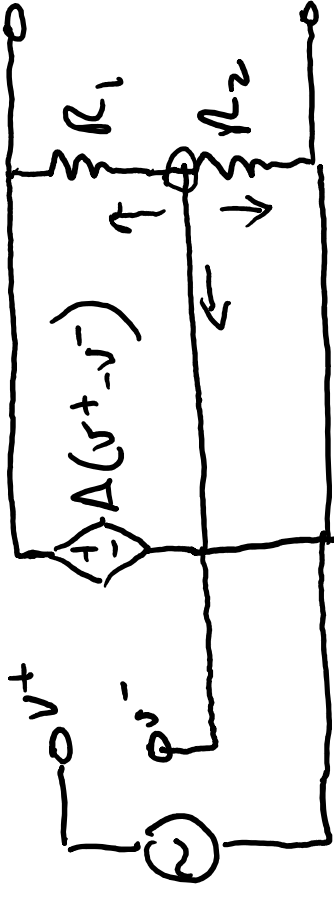
$$A = 200,000$$

input currents low

# NON INVERTING CONNECTION



$\Rightarrow v_{in}$



$$v^+ = v_{in}$$

$$v^- = \frac{R_2}{R_1 + R_2} v_{out}$$

$$\frac{v^-}{R_2} + \frac{v^- - v_{out}}{R_1} = 0$$

$$v_{out} = A(v^+ - v^-)$$

$$v^- = v^+ - \frac{v_{out}}{A}$$

$$v^+ - \frac{v_{out}}{A} = \frac{R_2}{R_1 + R_2} v_{out}$$

IDEAL with  $v^+ = v^-$

$$v^- = v_{in}$$

$$\frac{v_{in}}{R_2} = \frac{v_{out} - v_{in}}{R_1}$$

$$v_{in} R_1 = R_2 (v_{out} - v_{in})$$

$$v_{in} (R_1 + R_2) = R_2 v_{out}$$

$$v_{out} = \frac{(R_1 + R_2)}{R_2} v_{in}$$

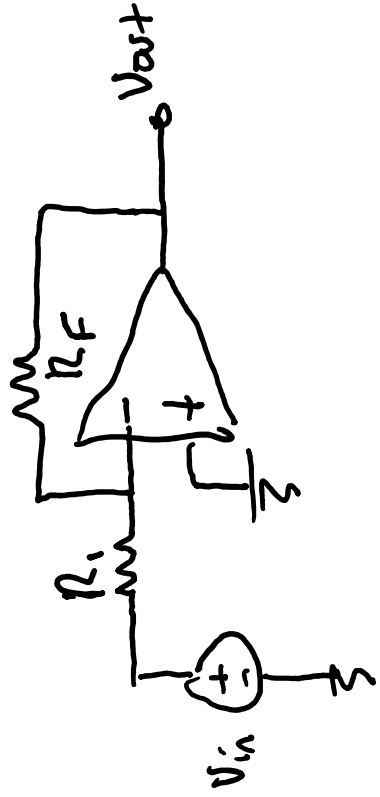
$$v_{out} = A(v^+ - v^-)$$

$$v^+ - v^- = \frac{v_{out}}{A}$$

$$A = \infty$$

$$v^+ = v^-$$

# INVERTING CONNECTION



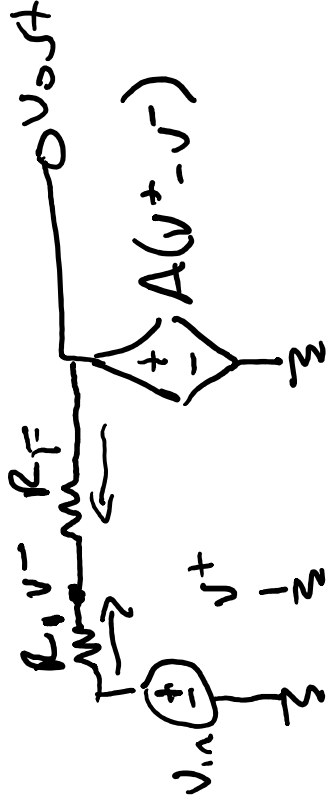
$$V^+ = 0$$

$$\frac{V_{in} - V^-}{R_i} - \frac{V^- - V_{out}}{R_F} = 0$$

$$V^- = \frac{R_F}{R_i + R_F} V_{in} + \frac{R_i}{R_i + R_F} V_{out}$$

$$V_{out} = A(V^+ - V^-) = -A V^-$$

$$\frac{-V_{out}}{A} = \frac{R_F}{R_i + R_F} V_{in} - \frac{R_i}{R_i + R_F} V_{out}$$



$$V_{out} \left( \frac{R_i}{R_i + R_F} - \frac{1}{A} \right) = \frac{R_F}{R_i + R_F} V_{in}$$

$$V_{out} = \frac{-A R_F / (R_i + R_F)}{1 + A R_i / (R_i + R_F)} V_{in}$$

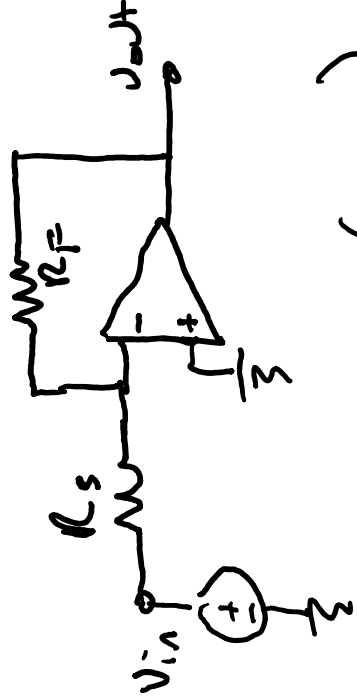
IF  $A$  is large  $\Rightarrow$  IDEAL

$$V_{out} = -\frac{R_F}{R_i} V_{in}$$

$$\text{IDEAL} \quad V^+ = 0 \quad \frac{V_{in}}{R_i} \quad \frac{V_{out}}{R_F}$$

# INVERTING OUTPUT RESISTANCE

INVERTING



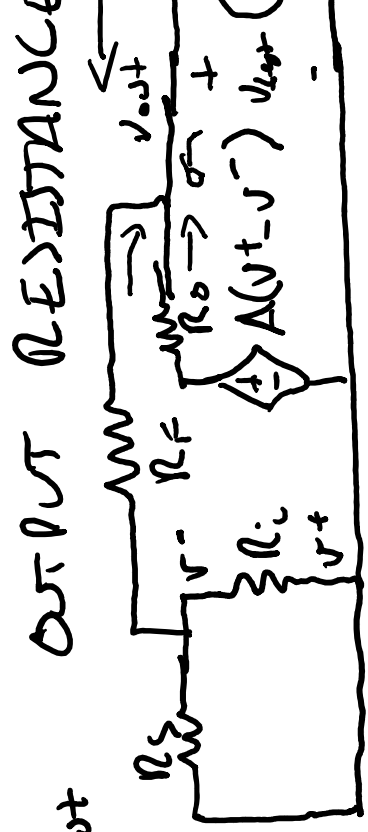
A large (or  $\infty$ )

$$G_{out} = G_o \left( 1 + \frac{A G_F}{G_F + G_S} \right)$$

$$G_{out} = G_o \left( 1 + \frac{A R_S}{R_S + R_F} \right)$$

$$R_{out} = \frac{R_o}{1 + A \left( \frac{R_S}{R_S + R_F} \right)} \quad \text{Load Gain}$$

Assume  $R_i, R_{out}$



USE CONDUCTANCES

$$G_i = \frac{1}{R_i}; G_S = \frac{1}{R_S}; G_F = \frac{1}{R_F}$$

$$v^+ = 0$$

$$v^- = \frac{G_F}{G_F + G_S + G_i} v_{test}$$

$$i_{test} + [A(v^+ - v^-) - v_{test}] G_o + (v^- -$$

$$\frac{i_{test}}{v_{test}} = G_{out} = \frac{A G_F G_o}{G_F + G_S} + G_o + \underbrace{\text{EFFECT OF FEEDBACK alone}}$$

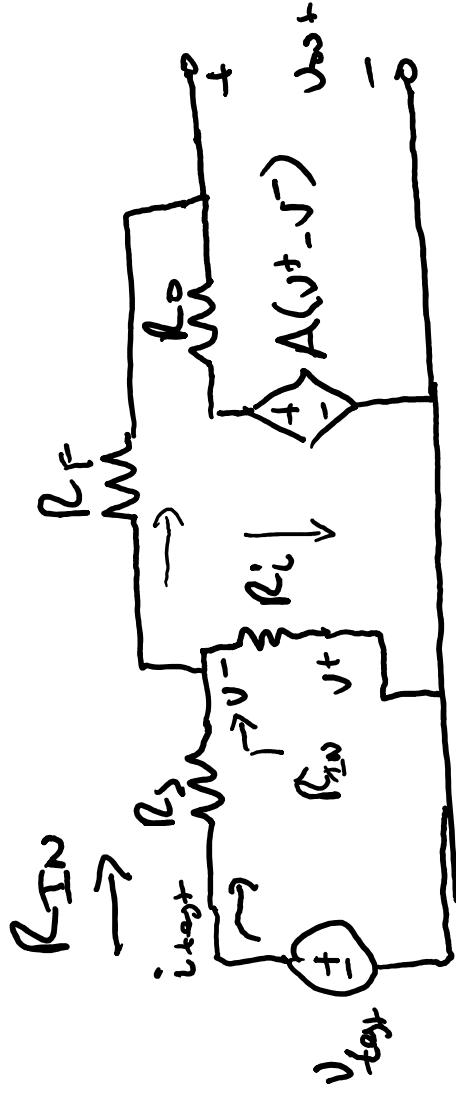
$$G = \frac{G_F G_S}{G_F + G_S}$$

$$G_T = \frac{\frac{1}{R_F} \left( \frac{1}{R_S} \right)}{\frac{1}{R_S} + \frac{1}{R_F}} = \frac{1}{R_F + R_S}$$

$$R = R_F + R_S$$

$$\frac{R_F R_S}{R_F + R_S} = (R_F // R_S)$$

# INVERTING INPUT RESISTANCE



$$R_{IN} = R_S + R'_{IN} \Rightarrow R_{EFF} \text{ to the right of } R_S$$

$$v^+ = 0$$

$$v^- = v_{test}$$

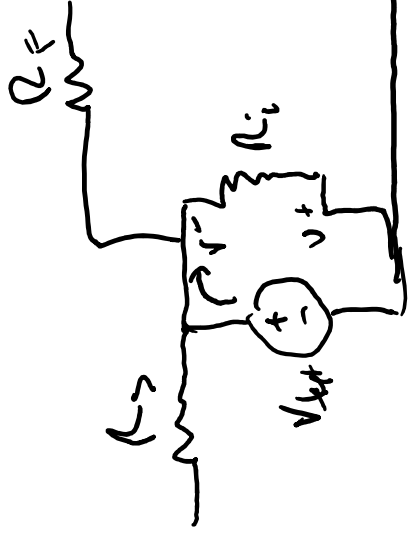
$$i_{test} = \frac{v_{test} + v_{test} - A(v^+ - v^-)}{R_F + R_O} = v_{test} \left( \frac{1}{R_i} + \frac{1}{R_F + R_O} + \frac{1}{R_O} \right)$$

$$\frac{v_{test}}{i_{test}} = R_{IN}' = \underbrace{R_i}_{\text{op-amp input}} \parallel \underbrace{(R_F + R_O)}_{R'_S} \parallel \underbrace{\left( \frac{R_F + R_O}{A} \right)}_{F/B}$$

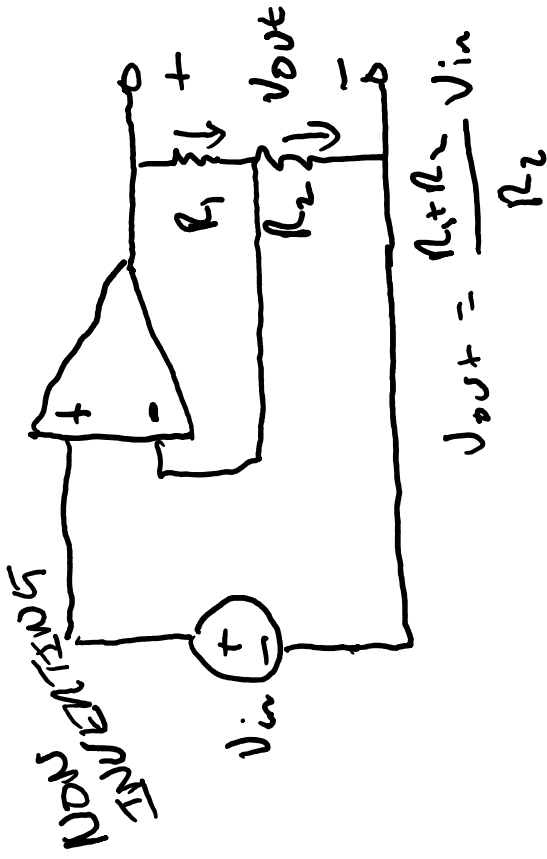
For LARGE A

$$R'_{IN} \approx \frac{R_F}{A}$$

$$R_{IN} = R_S + R'_{IN}$$



# VOLTAGE FOLLOWER



## VOLTAGE FOLLOWER

