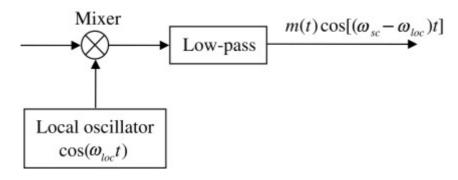
### **DSBSC**

- More effiecient
- Higher cost
- More complex

### **Coherent detection**

It will be used to detect DSBSC.



### **DSBLC**

- less efficient
- lower cost

# **Noise in AM systems**

Mean noise power in demodulator where a noise voltage is input into our demodulator

$$N_i = \lim_{T o \infty} rac{1}{T} \int_{rac{-T}{2}}^{rac{T}{2}} rac{n_i^2}{R} dt$$

If the noise is in the form of a current, then the mean noise will be

$$Ni = \lim_{T o\infty}rac{1}{T}\int_{rac{-T}{2}}^{rac{T}{2}}n_i(t)^2Rdt$$

Ususally we will assume that the noise power will flower into  $R=1\Omega$ . But it is noticable that in most cases R is matached to 50  $\Omega$ .

### random noise

$$n_i(t) = n_c \cos{(w_c t)} - n_s(t) sin(w_c t)$$

where the noise is defined in terms on in-phase and out-of-phase.

in-phase: **If two waves coincide with peaks and troughs matching they are** said to be in phase.

out-of-phase:A phrase used to characterize two or more signals whose phase relationship with each other is such that when **one is at its positive peak the other is at** (or near) its negative peak.

So the final noise will be:

$$N_i = rac{1}{2T} \int_{rac{-T}{2}}^{rac{T}{2}} n_c(t)^2 + n_s(t)^2 [1-\cos{(w_c t)}] - 2n_c(t) n_s(t) \sin{(2w_c t)} dt$$

And it bascially used the trigonometry:

$$\cos^2 lpha = rac{1 + cos 2lpha}{2}$$

where the **R** is assumed to be  $\mathbf{1}\Omega$ .

the cos and sin terms average to zero to give,

$$N_i = rac{1}{2T} \int_{rac{-T}{2}}^{rac{T}{2}} n_c^2(t) + n_s^2(t) dt = rac{1}{2} n_c \hat(t)^2 + rac{1}{2} n_s(t)^2$$

Which is the additon of two mean value of power.

If the noise is random, then the nosie spikes will occur in-phase and out-of phase with equal frequency and so we can see

$$n_c(\hat{t})^2 = n_s(\hat{t})^2 = n_i(\hat{t})^2$$

☐ Why?

# **Signal**

$$S_i = \frac{1}{T} \int_{-\frac{T}{2}}^{\frac{T}{2}} s_i(t)^2 dt$$

## **Amplitude demodulation**

$$S_i(t) = f(t)\cos\left(w_c t\right)$$

Substitute it into the original equation:

$$S_i=rac{1}{T}\int_{rac{-T}{2}}^{rac{T}{2}}f^2(t)dt$$

since the double angles was 0 during the integral.

So as shown before, accoding to DSBSC demodulation:

$$S_i(t) = f(t) \cos{(w_c t)} \ S_o(t) = si(t) \cos{(w_c t)} = Si_t cos^2(w_c t)$$

Since the  $2w_c$  term will be filtered off. Then the obtained signal will be

$$S_o=rac{1}{2}f(t)$$

☐ Why?

So the average power of the ouput signal will be

$$Sop = rac{1}{T} \int_{rac{-T}{2}}^{rac{T}{2}} (rac{1}{2} f(t))^2 = rac{1}{4} f(\hat{t})^2$$

#### No matter what is at input both noise and signal will be demodulated accodingly:

so the output noise will be  $n_o(t)=ni(t)cos(w_ct)$  which is the same as the input signal and output signal which is:

$$n_o(t) = rac{1}{2} n_c(t) [1 + cos(2w_c t)] - rac{1}{2} n_s(t) sin(2w_c t)$$

Again, after filtered off  $n_o(t)=\frac{1}{2}n_c(t)$ , so the corresponding average power will be:

$$N_o = rac{1}{T} \int_{rac{-T}{2}}^{rac{T}{2}} (rac{1}{2} n_c(t))^2 dt = rac{1}{4} n_i^{\hat{2}(t)}$$

### **Final SNR Ratio**

$$rac{S_i}{N_i} = rac{rac{1}{2}f(\hat{t})^2}{n_i(\hat{t})^2} \ rac{S_o}{N_o} = rac{rac{1}{4}f(t)^2}{rac{1}{4}n_i(t)^2}$$

Hence  $SNR_o=2SNR_i$ 

### Aim of this Course

FInd SNRi and SNRo which is SNR of input and SNR of output respectively