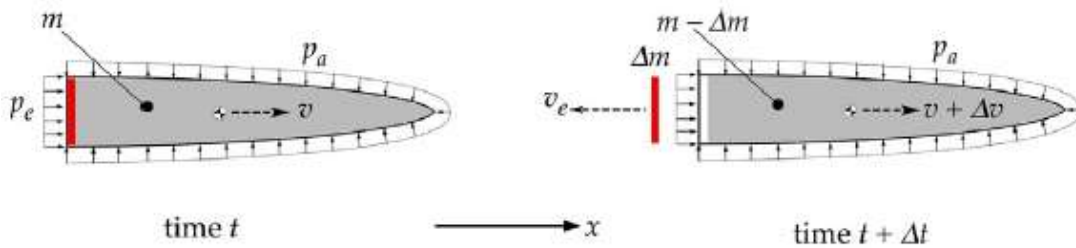


Orbital Manoeuvres

- Orbital manoeuvres transfer a spacecraft from one orbit to another.
- Changing of orbits requires the firing of on-board rocket engines.
- Impulsive manoeuvres are those in which brief firings of on-board rocket motors change the magnitude and the direction of the velocity vector instantaneously.

The Thrust Equation



- According to Newton's second law of motion:

(Momentum of system at $t + \Delta t$) - (momentum of system at t) =
Net external impulse

$$[(m - \Delta m)(v + \Delta v)\hat{i} + \Delta m(-v_e\hat{i})] - mv\hat{i} = (p_e - p_a)A_e\Delta t\hat{i}$$

$$- \frac{dm}{dt} = -\dot{m}_e$$

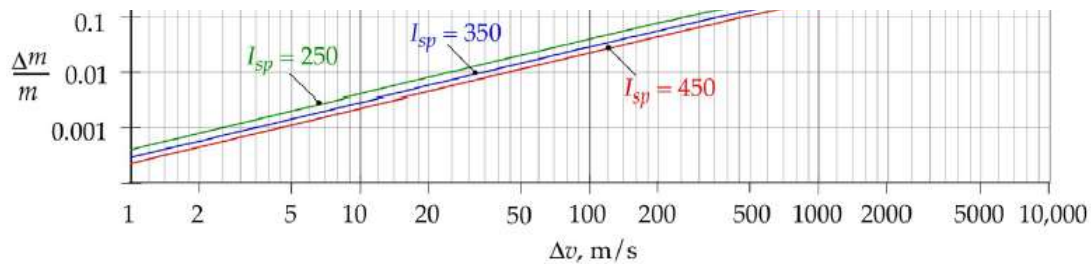
... ..

- $m(t) = m_0 - \dot{m}_e t$ (assuming m_e is a constant)
- $\Delta m = \dot{m}_e \Delta t$
- $[(m - \dot{m}_e \Delta t)(v + \Delta v)\hat{i} + \dot{m}_e \Delta t(-v_e \hat{i})] - mv\hat{i} = (p_e - p_a)A_e \Delta t \hat{i}$
- $m \Delta v \hat{i} - \dot{m}_e \Delta t (v_e + v) \hat{i} - \dot{m}_e \Delta t \Delta v \hat{i} = (p_e - p_a)A_e \Delta t \hat{i}$
- $m \frac{dv}{dt} - \dot{m}_e \underbrace{C_a}_{\substack{\downarrow \\ v_e + v}} = (p_e - p_a)A_e$
- $m \frac{dv}{dt} = \dot{m}_e C_a + (p_e - p_a)A_e$
- $T = \dot{m}_e \left[C_a + \frac{(p_e - p_a)A_e}{\dot{m}_e} \right] = \dot{m}_e C$
- Specific impulse :

$$I_{sp} = \frac{T}{\dot{m}_e g_0} \left(\frac{\text{Thrust}}{\text{Sea-level weight-rate of consumption}} \right)$$

Table 6.1 Some typical specific impulses	
Propellant	I_{sp} (s)
Cold gas	50
Monopropellant hydrazine	230
Solid propellant	290
Nitric acid/monomethylhydrazine	310
Liquid oxygen/liquid hydrogen	455
Ion propulsion	>3000





$$- c = I_{sp} g_0$$

Rocket Performance

$$- T = - I_{sp} g_0 \frac{dm}{dt}$$

$$- m \frac{dv}{dt} = - I_{sp} g_0 \frac{dm}{dt}$$

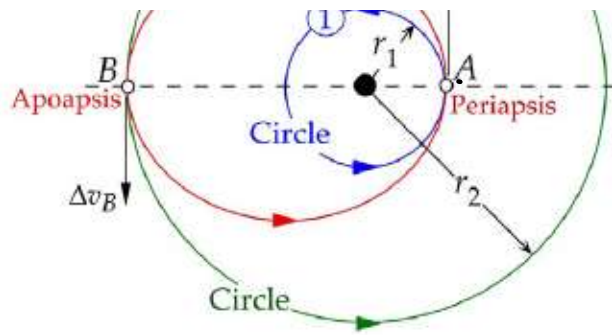
$$- \Delta v = I_{sp} g_0 \ln \left(\frac{m_0}{m_f} \right)$$

$$- \frac{\Delta m}{m} = \frac{m_0 - m_f}{m_0} = 1 - \frac{m_f}{m_0} = 1 - e^{\frac{-\Delta v}{I_{sp} g_0}}$$

Hohmann Transfer [Walter Hohmann (1880-1945)]

- The most energy-efficient two-impulse manoeuvre for transferring between two co-planar circular orbits sharing a common focus.





$$- \Delta v_{total} = \Delta v_A + \Delta v_B$$

$$- ||e|| = \frac{r_a - r_p}{r_a + r_p}$$

$$- r_p = \frac{||h||^2}{\mu} \frac{1}{1 + ||e||}$$

$$- r_p = \frac{||h||^2}{\mu} \frac{r_a + r_p}{2r_a}$$

$$- ||h|| = \sqrt{2\mu} \sqrt{\frac{r_a r_p}{r_a + r_p}} \quad (||h|| = ||r|| v_{\perp})$$

$$- ||h|| = \sqrt{\mu ||r||} \quad (\text{circular orbit})$$

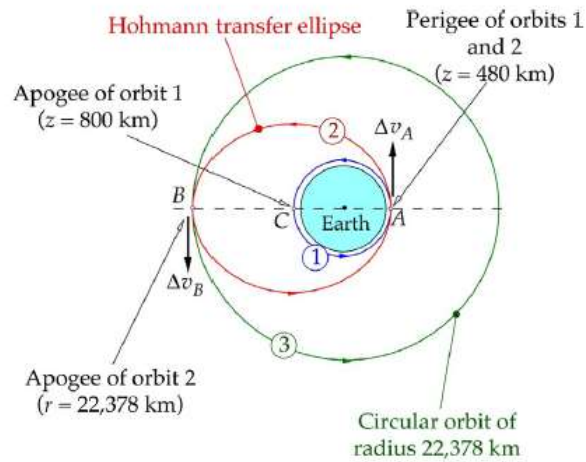
$$- ||v|| = \sqrt{2\mu} \sqrt{\frac{1}{||r||} - \frac{1}{2a}}$$

Example

A 2000-kg spacecraft is in a 480 km by 800 km earth orbit (orbit 1 in Fig. 6.3). Find

- The Δv required at perigee A to place the spacecraft in a 480 km by 16,000 km transfer ellipse (orbit 2).
- The Δv (apogee kick) required at B of the transfer orbit to establish a circular orbit of 16,000 km altitude (orbit 3).
- The total required propellant if the specific impulse is 300 s.

(c) The total required propellant if the specific impulse is 300 s



Details

Orbit 1: $r_p = 6378 + 480 \text{ km}$, $r_a = 6378 + 800 \text{ km}$

Orbit 2: $r_p = 6378 + 480 \text{ km}$, $r_a = 6378 + 16000 \text{ km}$

Orbit 3: $r_p = r_a = 6378 + 16000 \text{ km}$

(a) $V_A)_1 = \frac{\|h_1\|}{r_A}$, $V_A)_2 = \frac{\|h_2\|}{r_A}$

$$\Delta V_A = V_A)_2 - V_A)_1$$

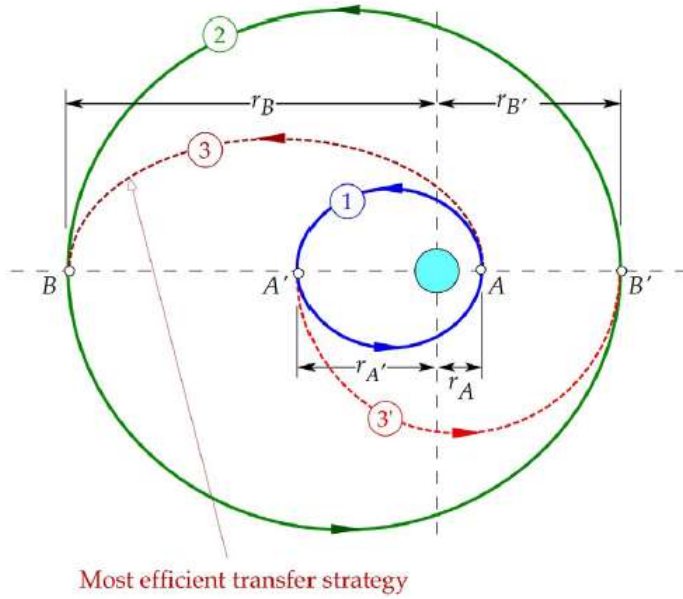
(b) $V_B)_2 = \frac{\|h_2\|}{r_B}$, $V_B)_3 = \frac{\|h_3\|}{r_B}$

$$\Delta V_B = V_B)_3 - V_B)_2$$

(c) $\Delta V_{\text{total}} = |\Delta V_A| + |\Delta V_B|$

$$\underline{\Delta m} = 1 - e^{\frac{-\Delta V_{\text{total}}}{I_{sp} g_0}}$$

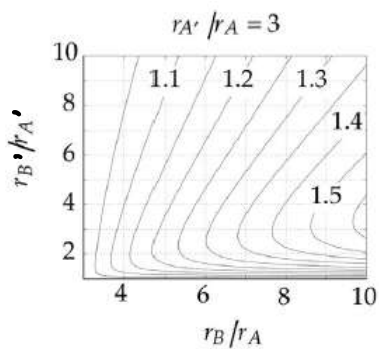
The diagram illustrates the most efficient transfer strategy between two circular orbits. A central cyan circle represents the primary body. Two concentric dashed circles represent the initial and target orbits. The initial orbit has radius r_A and the target orbit has radius r_B . A blue solid circle with radius $r_{A'}$ represents the transfer orbit. The transfer orbit is tangent to the initial orbit at point A and the target orbit at point B. The transfer orbit is divided into two segments: a blue solid segment (labeled 1) and a red dashed segment (labeled 3). The blue segment is the most efficient transfer strategy. The red dashed segment is labeled 3'.



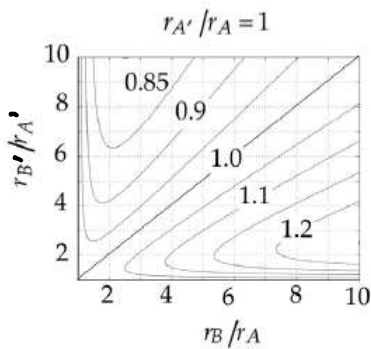
$$- \Delta V_{\text{total}})_3 = \Delta V_A + \Delta V_B, \quad \Delta V_{\text{total}})_3 = \Delta V_{A'} + \Delta V_{B'}$$

$$- \Delta V_A = |V_A)_3 - V_A)_1|, \Delta V_B = |V_B)_2 - V_B)_3|$$

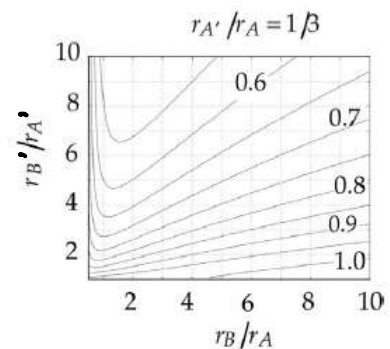
$$- \Delta V_{A'} = |V_{A'}'_{3'} - V_{A'}'_{1}|, \Delta V_{B'} = |V_{B'}'_{2} - V_{B'}'_{3'}|$$



(a) A is periapsis of orbit 1



(b) Orbit 1 is circular

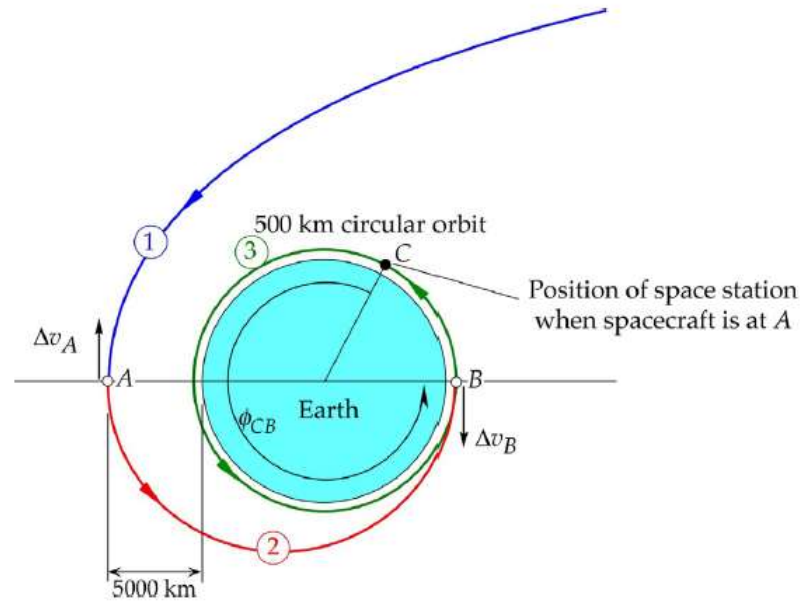


(c) A is apoapsis of orbit 1

Example

A spacecraft returning from a lunar mission approaches earth on a hyperbolic trajectory. At its closest approach A it is at an

altitude of 5000 km, traveling at 10 km/s. At A retrorockets are fired to lower the spacecraft into a 500-km-altitude circular orbit, where it is to rendezvous with a space station. Find the location of the space station at retrofire so that rendezvous will occur at B (Fig. 6.6).



Details

$$r_A = 5000 + 6378 \text{ km}, \quad r_B = 500 + 6378 \text{ km}$$

$$a = \frac{1}{2} (r_A + r_B)$$

$$T_2 = \frac{2\pi}{\sqrt{\mu}} a^{3/2}$$

$$T_3 = \frac{2\pi}{\sqrt{\mu}} r_B^{3/2}$$

$$\Delta t_{CB} = \frac{T_2}{2}$$

$$\frac{\phi_{CB}}{\Delta t_{CB}} = \frac{360^\circ}{T_3}$$