# AE 242 Aerospace Measurements Laboratory

a<sub>2</sub> a<sub>1</sub>, a<sub>0</sub> and b<sub>0</sub> are non zero in the generalised equation. Any instrument which can be represented using this equation is a second - order instrument.

$$\mathbf{a}_{2} \frac{\mathbf{d}^{2} \mathbf{q}_{0}}{\mathbf{d} \mathbf{t}^{2}} + \mathbf{a}_{1} \frac{\mathbf{d} \mathbf{q}_{0}}{\mathbf{d} \mathbf{t}} + \mathbf{a}_{0} \mathbf{q}_{0} = \mathbf{b}_{0} \mathbf{q}_{i}$$
Roots of this equation can be imaginary, complex, real

Above equation can be written as

$$\mathbf{K} = \frac{\mathbf{b}_{\scriptscriptstyle 0}}{\mathbf{a}_{\scriptscriptstyle 0}}$$

$$\boldsymbol{\omega}_{\scriptscriptstyle \mathrm{n}} = \sqrt{\frac{\mathbf{a}_{\scriptscriptstyle \mathrm{0}}}{\mathbf{a}_{\scriptscriptstyle \mathrm{0}}}}$$

$$\left(\frac{\mathbf{D}^{2}}{\boldsymbol{\omega}_{n}^{2}} + \frac{2\boldsymbol{\xi}\mathbf{D}}{\boldsymbol{\omega}_{n}} + 1\right)\mathbf{q}_{0} = \mathbf{K}\mathbf{q}_{i}$$

$$\boldsymbol{\xi} = \frac{\mathbf{a}_{1}}{2\sqrt{\mathbf{a}_{0}\mathbf{a}_{2}}}$$

Static sensitivity

Undamped natural frequency

Damping ratio

Transfer function

$$\frac{\mathbf{q}_{0}}{\mathbf{q}_{i}}(\mathbf{D}) = \frac{\mathbf{K}}{\mathbf{D}^{2}/\boldsymbol{\omega}_{n}^{2} + 2\boldsymbol{\xi}\mathbf{D}/\boldsymbol{\omega}_{n} + 1}$$

# Second-order system – an example

#### Force measuring spring

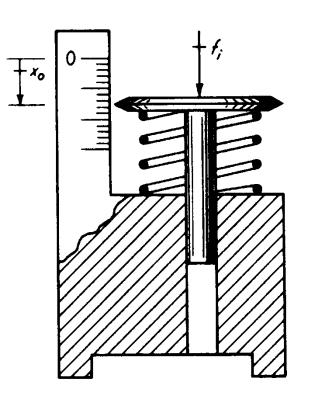
Total mass – M

Spring constant – K<sub>s</sub>

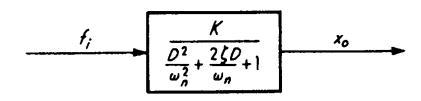
Damping - B

$$(\mathbf{M}\mathbf{D}^2 + \mathbf{B}\mathbf{D} + \mathbf{K}_{s})\mathbf{X}_{0} = \mathbf{f}_{s}$$

$$\mathbf{K} = \frac{1}{\mathbf{K}_{s}} \qquad \boldsymbol{\omega}_{n} = \sqrt{\frac{\mathbf{K}_{s}}{\mathbf{M}}} \qquad \boldsymbol{\xi} = \frac{\mathbf{B}}{2\sqrt{\mathbf{K}_{s}\mathbf{M}}}$$



 $\omega_{\text{n}}$  is direct indication of speed of response



$$\left(\frac{D^2}{\omega_n^2} + \frac{2D\zeta}{\omega_n} + 1\right)q_o = Kf_i$$
 Two roots of the characteristic equation 
$$-\zeta\omega_n + \omega_n\sqrt{\zeta^2 - 1} \text{ and } -\zeta\omega_n - \omega_n\sqrt{\zeta^2 - 1}$$

$$-\zeta\omega_n + \omega_n\sqrt{\zeta^2 - 1}$$
 and  $-\zeta\omega_n - \omega_n\sqrt{\zeta^2 - 1}$ 

Undamped :  $\zeta = 0$ , roots =  $\pm i\omega$ .

$$\frac{q_0/K}{q_{is}} = 1 - \sin(\omega_n t + \phi)$$

Initial conditions are zero

$$q_0 = \dot{q}_0 = 0$$

Underdampe d:  $0 < \zeta < 1.0$ , roots  $= -\zeta \omega_n \pm i\omega_n \sqrt{1 - \zeta^2}$ 

$$\frac{q_0/K}{q_{is}} = 1 - \frac{e^{-\zeta \omega_n t}}{\sqrt{1-\zeta^2}} \sin\left(\omega_n \sqrt{1-\zeta^2}t + \phi\right)$$

$$\left(\frac{D^2}{\omega_n^2} + \frac{2D\zeta}{\omega_n} + 1\right)q_o = Kf_i \text{ Over damped: } \zeta > 1.0, \text{ roots} = \omega_n\left(-\zeta \pm \sqrt{\zeta^2 - 1}\right) = \frac{1}{\tau_1}, \frac{1}{\tau_2}$$

Two roots of the characteristic equation

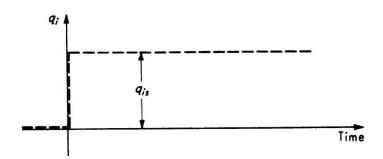
$$\frac{q_0/K}{q_{is}} = \left(1 - \frac{\zeta + \sqrt{\zeta^2 - 1}}{2\sqrt{\zeta^2 - 1}}e^{-t/\tau_1} + \frac{\zeta - \sqrt{\zeta^2 - 1}}{2\sqrt{\zeta^2 - 1}}e^{-t/\tau_2}\right)$$

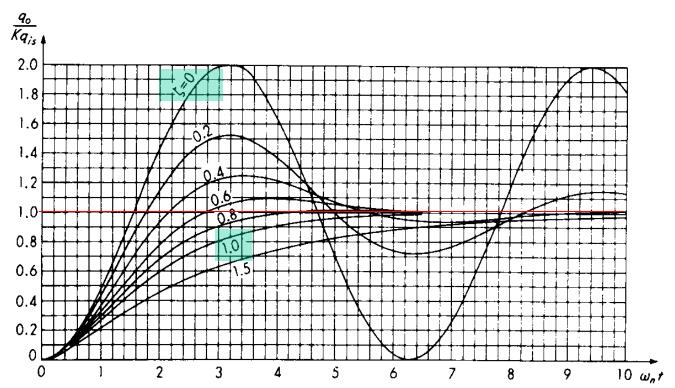
Crtically damped :  $\zeta = 1.0$ , roots =  $\omega_n$ 

$$\frac{q_0/K}{q_{is}} = \left(1 - (1 + \omega_n t)e^{-\omega_n t}\right)$$

### Second-order system – Step response

$$\left(\frac{\mathbf{D}^{2}}{\boldsymbol{\omega}_{n}^{2}} + \frac{2\boldsymbol{\xi}\mathbf{D}}{\boldsymbol{\omega}_{n}} + 1\right)\mathbf{q}_{0} = \mathbf{K}\mathbf{q}_{is}$$





Observe the time response for different damping ratio.

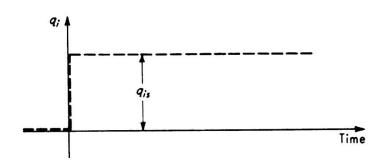
# Second-order system – Step response

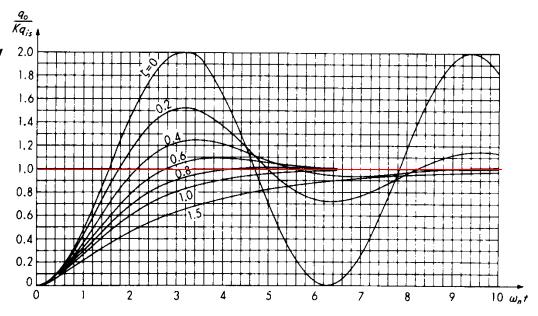
$$\left(\frac{\mathbf{D}^{2}}{\boldsymbol{\omega}_{n}^{2}} + \frac{2\boldsymbol{\xi}\mathbf{D}}{\boldsymbol{\omega}_{n}} + 1\right)\mathbf{q}_{0} = \mathbf{K}\mathbf{q}_{is}$$

Under damping – Damping ratio less than 1. This will always give overshoot before reaching steady state

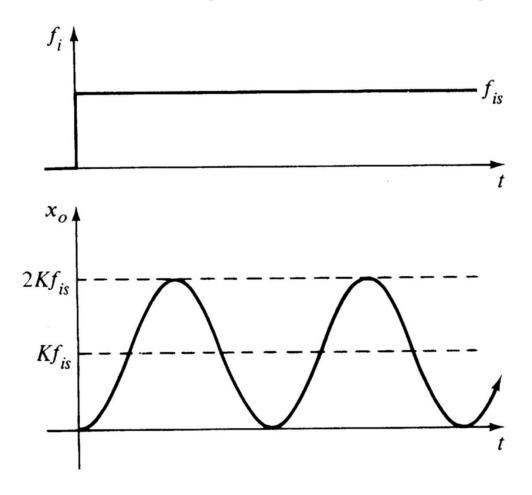
Critical damping – Damping ratio equal to 1. this will take minimum time to achieve steady state output without overshoot

Over damping – Damping ratio greater than 1.this will take more time to achieve steady state compared to critical damping output without overshoot





#### Second order systems - Step input



Step response of undamped second order system  $\zeta = 0$ 

#### Second order systems - Step input

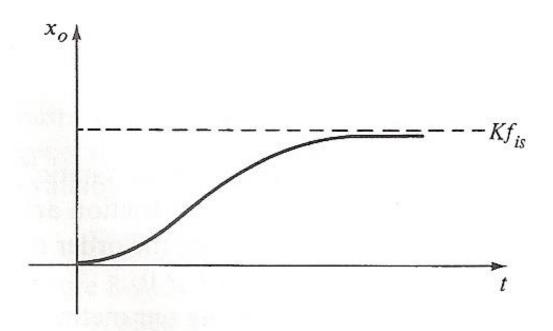


Figure 8-10 Step response of critically damped second-order system.

Step response of critically second order system  $\zeta = 1$ 

$$q_{o} = Kq_{is}(1 - (1 + \omega_{n}t)e^{-\omega_{n}t})$$

#### Second order systems - ramp input

$$\left(\frac{D^2}{\omega_n^2} + \frac{2D\zeta}{\omega_n} + 1\right) q_O = K\dot{q}_{is}t \qquad -\zeta\omega_n + \omega_n\sqrt{\zeta^2 - 1} \quad \text{and} \quad -\zeta\omega_n - \omega_n\sqrt{\zeta^2 - 1}$$

Two roots of the characteristic equation

Underdamped: 
$$0 < \zeta < 1.0$$
, roots  $= -\zeta \omega_n \pm i\omega_n \sqrt{1 - \zeta^2}$ 

$$\frac{q_0}{K} = \dot{q}_{is}t - \frac{2\zeta \dot{q}_{is}}{\omega_n} \left[ 1 - \frac{e^{-\zeta \omega_n t}}{\sqrt{1 - \zeta^2}} \sin\left(\omega_n t \sqrt{1 - \zeta^2} + \phi\right) \right]$$

$$-\zeta\omega_n + \omega_n\sqrt{\zeta^2 - 1}$$
 and  $-\zeta\omega_n - \omega_n\sqrt{\zeta^2 - 1}$ 

Critically damped : 
$$\zeta = 1.0$$
, roots =  $-\omega_n$ 

$$\left| \frac{q_0}{K} = \dot{q}_{is}t - \frac{2\dot{q}_{is}}{\omega_n} \left[ 1 - e^{-\omega_n t} \left( 1 + \frac{\omega_n t}{2} \right) \right] \right|$$

Over damped case

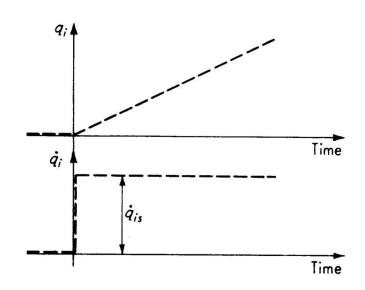
$$\frac{q_{0}}{K} = \dot{q}_{is}t - \frac{2\zeta\dot{q}_{is}}{\omega_{n}} \left(1 + \frac{2\zeta^{2} - 1 - 2\zeta\sqrt{\zeta^{2} - 1}}{4\zeta\sqrt{\zeta^{2} - 1}} e^{\left(-\zeta + \sqrt{\zeta^{2} - 1}\right)\omega_{n}t} + \frac{-2\zeta^{2} - 1 - 2\zeta\sqrt{\zeta^{2} - 1}}{4\zeta\sqrt{\zeta^{2} - 1}} e^{\left(-\zeta + \sqrt{\zeta^{2} - 1}\right)\omega_{n}t}\right)$$

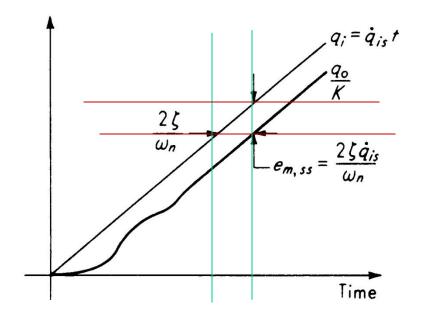
#### Second-order system – Ramp response

Steady state error  $2\xi\dot{\mathbf{q}}_{\scriptscriptstyle \mathrm{is}}/\boldsymbol{\omega}_{\scriptscriptstyle \mathrm{n}}$ 

Time lag  $2\xi/\omega_{n}$ 

Steady state error can be reduced by reducing  $\xi$  and increasing  $\omega_n$  This will increase the oscillations in the output





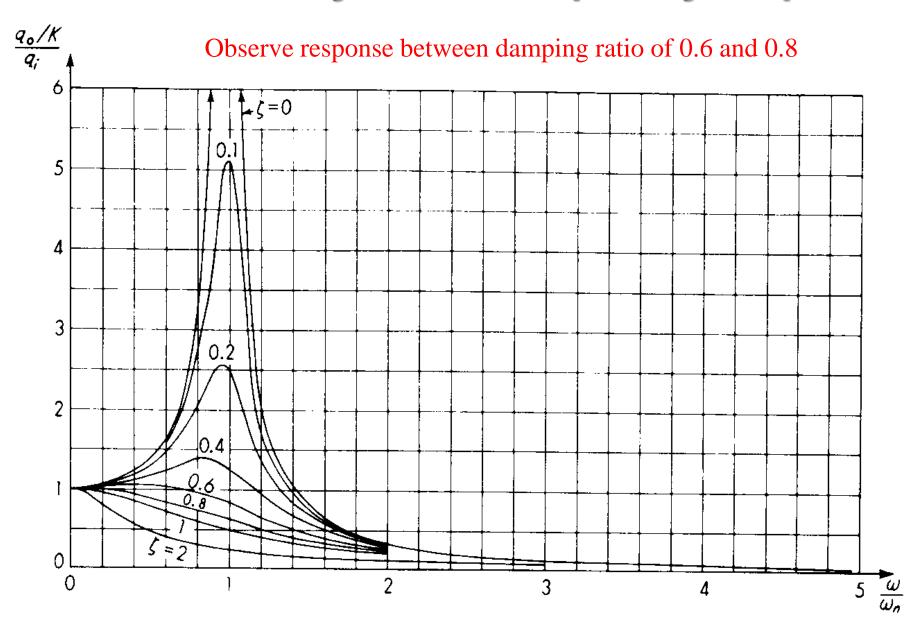
$$\left(\frac{D^2}{\omega_n^2} + \frac{2D\zeta}{\omega_n} + 1\right)q_o = Kq_i \sin(\omega t) \qquad \frac{q_0}{q_i}(i\omega) = \frac{K}{(i\omega/\omega_n)^2 + 2\zeta i\omega/\omega_n + 1}$$

$$\frac{q_0/K}{q_i}(i\omega) = \frac{1}{\sqrt{\left[1 - (\omega/\omega_n)^2\right]^2 + 4\zeta^2(\omega/\omega_n)^2}} \angle \phi$$

$$\phi = \tan^{-1} \frac{2\zeta}{\omega/\omega_n - \omega_n/\omega}$$

Output is dependent on input frequency. It will peak close to natural frequency upto some damping ratio. Phase difference is also dependent on the input frequency.

#### Second-order system – frequency response



#### Second-order system – frequency response

Amplitude ratio strongly related to small and large damping ratio.

Flat response for damping of 0.6- 0.7

Linear variation of phase for above damping

Damping in the above range is a good choice for second order system

Frequency up to 0.4 of natural frequency

