Given the position and velocity vectors of a spacecraft in the geocentric equitorial frame, how do we obtain the orbital elements?

- 1. Calculate the distance, $r = \sqrt{\mathbf{r} \cdot \mathbf{r}} = \sqrt{X^2 + Y^2 + Z^2}$. 2. Calculate the speed, $v = \sqrt{v \cdot v} = \sqrt{v_X^2 + v_Y^2 + v_Z^2}$. 3. Calculate the radial velocity, $v_r = \mathbf{r} \cdot \mathbf{v}/r = (Xv_X + Yv_Y + Zv_Z)/r$. Note that if $v_r > 0$, the spacecraft is flying away from perigee. If $v_r < 0$, it is flying toward
- 4. Calculate the specific angular momentum,

$$\mathbf{h} = \mathbf{r} \times \mathbf{v} = \begin{vmatrix} \hat{\mathbf{I}} & \hat{\mathbf{J}} & \hat{\mathbf{K}} \\ X & Y & Z \\ v_X & v_Y & v_Z \end{vmatrix}$$

- 5. Calculate the magnitude of the specific angular momentum, $h = \sqrt{\mathbf{h} \cdot \mathbf{h}}$. This is the first orbital element.
- 6. Calculate the inclination,

$$i = \cos^{-1}(h_Z/h)$$
 (4.7)

This is the second orbital element, Recall that i must lie between 0° and 180°, which is precisely the range (principal values) of the arccosine function. Hence, there is no quadrant ambiguity to contend with here. If $90^{\circ} < i \le 180^{\circ}$, the angular momentum h points in a southerly direction. In that case, the orbit is retrograde, which means that the motion of the satellite around the earth is opposite to earth's rotation.

7. Calculate

$$\mathbf{N} = \hat{\mathbf{K}} \times \mathbf{h} = \begin{vmatrix} \hat{\mathbf{I}} & \hat{\mathbf{J}} & \hat{\mathbf{K}} \\ 0 & 0 & 1 \\ h_X & h_Y & h_Z \end{vmatrix}$$
(4.8)

This vector defines the node line.

- 8. Calculate the magnitude of N, $N = \sqrt{N \cdot N}$.
- Calculate the right ascension of the ascending node, Ω = cos⁻¹(N_X/N). This is the third orbital element. If $N_X > 0$, then Ω lies in either the first or fourth quadrant. If $N_X < 0$, then Ω lies in either the second or third quadrant. To place Ω in the proper quadrant, observe that the ascending node lies on the positive side of the vertical XZ plane ($0 \le \Omega < 180^{\circ}$) if $N_Y > 0$. On the other hand, the ascending node lies on the negative side of the XZ plane (180° $\leq \Omega < 360^{\circ}$) if $N_Y < 0$. Therefore, $N_Y > 0$ implies that $0 \le \Omega < 180^\circ$, whereas $N_Y < 0$ implies that $180^{\circ} \le \Omega < 360^{\circ}$. In summary,

$$\Omega = \begin{cases} \cos^{-1}\left(\frac{N_X}{N}\right) & (N_Y \ge 0) \\ 360^\circ - \cos^{-1}\left(\frac{N_X}{N}\right) & (N_Y < 0) \end{cases}$$
(4.9)

10. Calculate the eccentricity vector. Starting with Eq. (2.40),

$$\mathbf{e} = \frac{1}{\mu} \Big[\mathbf{v} \times \mathbf{h} - \mu \frac{\mathbf{r}}{r} \Big] = \frac{1}{\mu} \Big[\mathbf{v} \times (\mathbf{r} \times \mathbf{v}) - \mu \frac{\mathbf{r}}{r} \Big] = \frac{1}{\mu} \Bigg[\underbrace{\mathbf{r} v^2 - \mathbf{v} (\mathbf{r} \cdot \mathbf{v})}_{bac-cab \ rule} - \mu \frac{\mathbf{r}}{r} \Big]$$

so that

$$\mathbf{e} = \frac{1}{\mu} \left[\left(v^2 - \frac{\mu}{r} \right) \mathbf{r} - r v_r \mathbf{v} \right] \tag{4.10}$$

11. Calculate the eccentricity, $e = \sqrt{e \cdot e}$, which is the fourth orbital element. Substituting Eq. (4.10) leads to a form depending only on the scalars obtained thus far,

$$e = \sqrt{1 + \frac{h^2}{u^2} \left(v^2 - \frac{2\mu}{r}\right)}$$
 (4.11)

12. Calculate the argument of perigee

$$\omega = \cos^{-1}\left(\frac{\mathbf{N}}{N} \cdot \frac{\mathbf{e}}{e}\right)$$

This is the fifth orbital element. If N·e > 0, then ω lies in either the first or fourth quadrant. If N-e < 0, then ω lies in either the second or third quadrant. To place ω in the proper quadrant, observe that perigee lies above the equatorial plane (0° $\leq \omega < 180$ °) if e points up (in the positive Z direction) and that perigee lies below the plane (180° $\leq \omega < 360$ °) if e points down. Therefore, $e_Z \ge 0$ implies that $0^\circ < \omega < 180^\circ$, whereas $e_Z < 0$ implies that $180^\circ < \omega < 0$ 360°. To summarize,

$$\omega = \begin{cases} \cos^{-1}\left(\frac{\mathbf{N} \cdot \mathbf{e}}{Ne}\right) & (e_Z \ge 0) \\ 360^{\circ} - \cos^{-1}\left(\frac{\mathbf{N} \cdot \mathbf{e}}{Ne}\right) & (e_Z < 0) \end{cases}$$
(4.12)

13. Calculate the true anomaly,

$$\theta = \cos^{-1}\left(\frac{\mathbf{e}}{e} \cdot \frac{\mathbf{r}}{r}\right)$$

This is the sixth and final orbital element. If $e \cdot r > 0$, then θ lies in the first or fourth quadrant. If $\mathbf{e} \cdot \mathbf{r} < 0$, then θ lies in the second or third quadrant. To place θ in the proper quadrant, note that if the satellite is flying away from perigee $(\mathbf{r} \cdot \mathbf{v} \ge 0)$, then $0 \le \theta < 180^{\circ}$, whereas if the satellite is flying toward perigee ($\mathbf{r} \cdot \mathbf{v} < 0$), then $180^{\circ} \le \theta < 360^{\circ}$. Therefore, using the results

$$\theta = \begin{cases} \cos^{-1}\left(\frac{\mathbf{e}}{e} \cdot \frac{\mathbf{r}}{r}\right) & (\nu_r \ge 0) \\ 360^{\circ} - \cos^{-1}\left(\frac{\mathbf{e}}{e} \cdot \frac{\mathbf{r}}{r}\right) & (\nu_r < 0) \end{cases}$$
(4.13a)

Substituting Eq. (4.10) yields an alternative form of this expression,

$$\theta = \begin{cases} \cos^{-1} \left[\frac{1}{e} \left(\frac{h^2}{ur} - 1 \right) \right] & (v_r \ge 0) \\ 360^\circ - \cos^{-1} \left[\frac{1}{e} \left(\frac{h^2}{ur} - 1 \right) \right] & (v_r < 0) \end{cases}$$
(4.13b)

Example

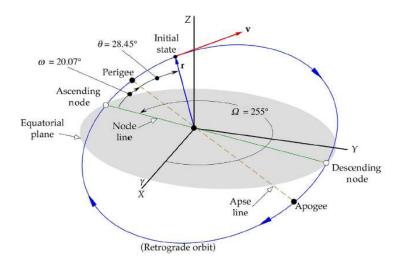
Given the state vector,

$$r = -6045\hat{I} - 3490\hat{J} + 2500\hat{K} (km)$$

 $v = -3.457\hat{I} + 6.618\hat{J} + 2.533\hat{K} (km/s)$

find the orbital elements h, i, Ω , e, ω , and θ using Algorithm 4.2.

Details Follow the above algorithm.



Coordinate Transformation

$$\hat{\mathbf{k}}$$

$$-\hat{i}\cdot\hat{j} = \hat{j}\cdot\hat{j} = \hat{k}\cdot\hat{k} = 1$$

$$\hat{i}\cdot\hat{j} = \hat{i}\cdot\hat{k} = \hat{j}\cdot\hat{k} = 0$$

$$- \hat{i}' \cdot \hat{i}' = \hat{j}' \cdot \hat{j}' = \hat{k}' \cdot \hat{k}' = |\hat{i}' \cdot \hat{k}' = |\hat{i}$$

$$- \hat{i}' = Q_{11}\hat{i} + Q_{12}\hat{j} + Q_{13}\hat{k}$$

$$\hat{j}' = Q_{11}\hat{i} + Q_{21}\hat{j} + Q_{23}\hat{k}$$

$$\hat{k}' = Q_{31}\hat{i} + Q_{32}\hat{j} + Q_{33}\hat{k}$$

$$- \hat{i} = Q_{11}\hat{i} + Q_{12}\hat{j} + Q_{13}\hat{k}'$$

$$\hat{j} = Q_{11}\hat{i} + Q_{21}\hat{j} + Q_{13}\hat{k}'$$

$$\hat{k} = Q_{31}\hat{i} + Q_{32}\hat{j} + Q_{33}\hat{k}'$$

$$- \hat{i} = Q_{11}\hat{i}' + Q_{21}\hat{j}' + Q_{31}\hat{k}'$$

$$\hat{j} = Q_{12}\hat{i}' + Q_{21}\hat{j}' + Q_{31}\hat{k}'$$

$$\hat{k} = Q_{13}\hat{i}' + Q_{23}\hat{j}' + Q_{33}\hat{k}'$$

$$- \hat{i} \cdot \hat{j} = 0 \Rightarrow Q_{i1}Q_{i1} + Q_{i1}Q_{i1} + Q_{31}Q_{32} = 0$$

$$\hat{i} \cdot \hat{k} = 0 \Rightarrow Q_{i1}Q_{i3} + Q_{i1}Q_{23} + Q_{31}Q_{33} = 0$$

$$\hat{j} \cdot \hat{k} = 0 \Rightarrow Q_{i2}Q_{i3} + Q_{i2}Q_{23} + Q_{31}Q_{33} = 0$$

$$[\mathbf{Q}] = \begin{bmatrix} Q_{11} & Q_{12} & Q_{13} \\ Q_{21} & Q_{22} & Q_{23} \\ Q_{31} & Q_{32} & Q_{33} \end{bmatrix} = \begin{bmatrix} \hat{\mathbf{i}}' \cdot \hat{\mathbf{i}} & \hat{\mathbf{i}}' \cdot \hat{\mathbf{j}} & \hat{\mathbf{i}}' \cdot \hat{\mathbf{k}} \\ \hat{\mathbf{j}}' \cdot \hat{\mathbf{i}} & \hat{\mathbf{j}}' \cdot \hat{\mathbf{j}} & \hat{\mathbf{j}}' \cdot \hat{\mathbf{k}} \end{bmatrix}$$

$$(Direction Logine Matrix)$$

$$[\mathbf{Q}]^T = \begin{bmatrix} Q_{11} & Q_{21} & Q_{31} \\ Q_{12} & Q_{22} & Q_{32} \\ Q_{13} & Q_{23} & Q_{33} \end{bmatrix} = \begin{bmatrix} \hat{\mathbf{i}} \cdot \hat{\mathbf{i}}' & \hat{\mathbf{i}} \cdot \hat{\mathbf{j}}' & \hat{\mathbf{i}} \cdot \hat{\mathbf{k}}' \\ \hat{\mathbf{j}} \cdot \hat{\mathbf{i}}' & \hat{\mathbf{j}} \cdot \hat{\mathbf{j}}' & \hat{\mathbf{j}} \cdot \hat{\mathbf{k}}' \\ \hat{\mathbf{k}} \cdot \hat{\mathbf{i}}' & \hat{\mathbf{k}} \cdot \hat{\mathbf{j}}' & \hat{\mathbf{k}} \cdot \hat{\mathbf{k}}' \end{bmatrix}$$

$$\begin{aligned} \left[\mathbf{Q}\right]^{T}\left[\mathbf{Q}\right] &= \begin{bmatrix} Q_{11} & Q_{21} & Q_{31} \\ Q_{12} & Q_{22} & Q_{32} \\ Q_{13} & Q_{23} & Q_{33} \end{bmatrix} \begin{bmatrix} Q_{11} & Q_{12} & Q_{13} \\ Q_{21} & Q_{22} & Q_{23} \\ Q_{31} & Q_{32} & Q_{33} \end{bmatrix} \\ &= \begin{bmatrix} Q_{11}^{2} + Q_{21}^{2} + Q_{31}^{2} & Q_{11}Q_{12} + Q_{21}Q_{22} + Q_{31}Q_{32} & Q_{11}Q_{13} + Q_{21}Q_{23} + Q_{31}Q_{33} \\ Q_{12}Q_{11} + Q_{22}Q_{21} + Q_{32}Q_{31} & Q_{12}^{2} + Q_{22}^{2} + Q_{31}^{2} & Q_{12}Q_{13} + Q_{22}Q_{23} + Q_{32}Q_{33} \\ Q_{13}Q_{11} + Q_{23}Q_{21} + Q_{33}Q_{31} & Q_{13}Q_{12} + Q_{23}Q_{22} + Q_{33}Q_{32} & Q_{13}^{2} + Q_{23}^{2} + Q_{23}^{2} + Q_{33}^{2} \end{bmatrix} \end{aligned}$$

- Q is an orthogonal matrix.