

Q1 Thrust = 1061800 N = 1061.8 kN

takeoff mass = 540,000 kg

$V_a = 110 \text{ m/s}$, $\rho = 1.16 \text{ kg/m}^3$, $S = 858 \text{ m}^2$

$C_D = 0.02 + 0.042 C_L^2$

fan diameter = 2.95 m

$f = 0.01$, $V_{\text{core}} = V_{\text{bypass}}$ (exhaust jets).

number of engines = 4.

we have Thrust = 4x Lift = $Mg_0 = 540,000 \text{ kg} \times 9.81 \text{ m/s}^2$

$\therefore \text{Lift} = 5297400 \text{ N}$

From drag polar equation we have $C_{D_0} = 0.02$.

\therefore parasite drag $D_0 = C_{D_0} \cdot q \cdot S = C_{D_0} \cdot \frac{1}{2} \rho V_\infty^2 S$

$= \frac{1}{2} \times 0.02 \times 1.16 \times 110 \times 110 \times 858 = 120428.88 \text{ N}$
 $D_0 = 120.428 \text{ kN}$

$\therefore \text{Thrust} = \dot{m}(V_e - V_a)$

co-efficient of lift $C_L = \frac{L}{qS} = \frac{5297400}{\frac{1}{2} \rho V_\infty^2 \cdot S} = 0.879 = C_L$

\therefore substitute in drag polar.

$C_D = 0.02 + 0.042 \times (0.879)^2 = 0.0524 = C_D$

$\therefore \text{Drag} = C_D \cdot q \cdot S = C_D \times \frac{1}{2} \rho V_\infty^2 \times S = 315523.6656 \text{ N}$
 $= 315.523 \text{ kN}$

$\therefore \dot{m}_{\text{fan}} = \text{Area of fan} \times \rho V_\infty$

$= \pi \times \frac{(2.95)^2}{4} \times \rho \times V_\infty = 872.136 \text{ kg/s}$

$\therefore \text{Thrust} = 4 \times \dot{m} \times \left(\left(1 + \frac{f}{\pi} \right) V_e - V_a \right)$

$= 4 \times 872.136 \left((1 + 0.01) V_e - V_a \right) = 1061800$

$\therefore V_e = \left[\frac{1061800}{4 \times 872.136} + V_a \right] \frac{1}{1.01} = 410.265 \text{ m/s}$

$V_{\text{exhaust}} = 410.265 \text{ m/s}$

Now, $r = \frac{V_a}{V_e} = \frac{110}{410.265} = 0.268119$

$\therefore \eta_p = \frac{2r}{1+r} = 0.4227 = 42.27\%$

$\therefore \eta_{Th} = \frac{1-r^2}{E} \quad E = \frac{2fQ_R}{V_e^2} = \frac{2 \times 0.01 \times 42 \times 10^6}{(410.265)^2}$

$\therefore \eta_{Th} = \frac{1-(0.268)^2}{4.99} = 0.186$
 $= 18.6\%$

$\therefore \eta_{Overall} = \eta_{Th} \cdot \eta_p = 0.4227 \times 0.186 = 0.078$
 $= 7.8\%$

→ at $T = 40^\circ\text{C} = 313\text{ K}$.

hence we get from standard atmospheric tables

$p =$

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we should $p = 1.16\text{ kg/m}^3 \quad \therefore p = \rho R T$

$p = 1.16 \times 287.1 \times 313 = 104240.268\text{ Pascals}$

Because of temperature there will be change in density pressure, speed of sound. corresponding to it the mass flow rate through the engine fan. Then the thrust will get affected as it depends on mass flow rate. Because of this, exhaust velocity jet will change. Hence parameter E will change, Hence η_{Th} & $\eta_{Overall}$ will change & η_p .

η_p due to v . exhaust changing

η_{Th} due to " & E

η_{ove} " " "