

Q.1 (a) Derive the expressions for the burnout velocity and altitude for a single stage rocket undergoing vertical rectilinear motion under constant sea level gravity and no atmosphere assumptions, starting from the simplified equations applicable for this case, as given below. (2)

$$m(t) \frac{dV(t)}{dt} = -\dot{m} g_0 I_{sp} - m(t) g_0(t)$$

Here,  $m_0$  is lift-off mass,  $m_p$  is total propellant mass having specific impulse  $I_{sp}$ , which is being consumed at the constant burn rate of  $\beta$ . Using the above relations, answer the following additional questions.

$$\frac{dV}{dt} = -\frac{\dot{m}}{m} g_0 I_{sp} - g_0; \quad V(t) = g_0 I_{sp} \ln \frac{m_0}{m(t)} - g_0 t; \quad V_b = g_0 I_{sp} \ln \frac{m_0}{m_b} - g_0 t_b$$

$$V_b = g_0 I_{sp} \ln \frac{m_0}{m_0 - m_p} - g_0 t_b; \quad m_p \rightarrow \text{Total Propellant Mass}; \quad m(t) = m_0 - \beta t;$$

$$t_b = \frac{m_p}{\beta}; \quad V_b(t) = g_0 I_{sp} \ln \frac{m_0}{(m_0 - m_p)} - g_0 \left( \frac{m_p}{\beta} \right)$$

$$h(t) = \int V(t) dt = \int \left( g_0 I_{sp} \ln \frac{m_0}{m(t)} - g_0 t \right) dt; \quad h(t) = g_0 I_{sp} \int \ln \frac{m_0}{m_0 - \beta t} dt - \frac{1}{2} g_0 t^2;$$

$$h(t) = \frac{m_0 g_0 I_{sp}}{\beta} \left[ \left( 1 - \frac{\beta}{m_0} t \right) \ln \left( 1 - \frac{\beta}{m_0} t \right) - \left( 1 - \frac{\beta}{m_0} t \right) \right] - \frac{1}{2} g_0 t^2 + C; \quad h = h_0 \text{ at } t = 0$$

$$C = h_0 + 1; \quad h_b = \frac{m_0 g_0 I_{sp}}{\beta} [(1 - \Lambda) \ln(1 - \Lambda) + \Lambda] - \frac{1}{2} g_0 \left( \frac{m_p}{\beta} \right)^2 + h_0; \quad t_b = \frac{m_p}{\beta}; \quad \Lambda = \frac{m_p}{m_0}$$

(b) Calculate the burnout velocity and altitude reached by the above rocket with  $m_0$  of 10,000 kg,  $m_p$  of 7,500 kg,  $I_{sp}$  of 200 seconds and  $\beta$  of 250 kg/s. Assume  $g_0 = 9.81 \text{ m/sec}^2$ . (2)

$$V_b(t) = 9.81 \times 200 \times \ln \frac{10000}{2500} - 9.81 \times \frac{7500}{250} = 2425.6 \text{ m/s}$$

$$\Lambda = 0.75, \quad h_b = \frac{10000 \times 9.81 \times 200}{250} [0.25 \times \ln 0.25 + 0.75] - \frac{1}{2} \times 9.81 \times 900 = 27246.4 \text{ m}$$

(c) If it is known that peak drag acceleration occurs at the end of the burnout, determine the value of the average drag acceleration applicable for this trajectory, using standard triangular approximation. ( $S_r = 0.1 \text{ m}^2$ ,  $C_{D0} = 0.8$ , Air Density as per the table below). (1)

$$\rho = 0.041 - \frac{0.041 - 0.018}{25 - 30} (25 - 27.246) = 0.030 \text{ kg/m}^3$$

$$Q = 0.5 \times 0.03 \times (2425.6)^2 = 90219.3 \text{ N/m}^2; \quad D = 90219.3 \times 0.8 \times 0.1 = 7217.5 \text{ N}$$

$$a_{DPeak} = \frac{7217.5}{2500} = 2.887 \text{ m/s}^2; \quad a_{DAvg} = 1.443 \text{ m/s}^2$$

Q.2 Obtain the relation between time (t) and inclination ( $\theta$ ) for a constant specific thrust gravity turn trajectory ( $T/m = n_0 g_0$ ), for the case when ' $n_0$ ' is 1. (Hint: Use following basic relations, as applicable.). (1)

$$\dot{\theta} = \frac{g_0 \sin^2 \theta}{k \left\{ \tan\left(\frac{\theta}{2}\right) \right\}^{n_0}}; \quad k = V_0 \sin(\theta_0) \left| \cot\left(\frac{\theta_0}{2}\right) \right|^{n_0}$$

$$\frac{d\theta}{dt} = \frac{g_0 \sin \theta}{V} \rightarrow \int dt = \int \frac{V d\theta}{g_0 \sin \theta} \rightarrow t = \int \frac{k \tan\left(\frac{\theta}{2}\right)}{g_0 \sin^2 \theta} d\theta = \frac{k}{4g_0} \int \frac{\sec^2\left(\frac{\theta}{2}\right) d\theta}{\sin\left(\frac{\theta}{2}\right) \cos\left(\frac{\theta}{2}\right)}$$

$$t = \frac{k}{4g_0} \int \left[ \frac{2}{\sin \theta} d\theta + \sec^2\left(\frac{\theta}{2}\right) \tan\left(\frac{\theta}{2}\right) d\theta \right] = \frac{k}{4g_0} \left[ 2 \ln \tan\left(\frac{\theta}{2}\right) + \sec^2\left(\frac{\theta}{2}\right) \right]$$

Q.3 (a) Derive the expressions for the burnout velocity ( $V_b$ ) and burnout mass fraction ( $m_b/m_0$ ), in respect of constant specific thrust ( $T/m = n_0 g_0$ , neglecting drag effect) gravity turn trajectory, using the following equations of motion. (2)

$$\dot{V} = -\frac{\dot{m} g_0 I_{sp}}{m} - g_0 \cos \theta; \quad \dot{\theta} = \frac{g_0 \sin \theta}{V};$$

Where, all the quantities have their standard meaning. (V is the velocity along the vehicle axis and thrust direction,  $g_0$  is sea level gravitational acceleration, and  $\theta$  is the angle measured from local vertical). Answer part (b) using results obtained in part (a).

$$\dot{V} = -\frac{\dot{m} g_0 I_{sp}}{m(t)} - \tilde{g} \cos \theta = -\tilde{g} \cos \theta + n_0 \tilde{g}; \quad \dot{\theta} = \frac{\tilde{g} \sin \theta}{V};$$

$$\frac{\dot{V}}{\dot{\theta}} = \frac{dV}{d\theta} = V(-\cot \theta + n_0 \operatorname{cosec} \theta); \quad \int \frac{dV}{V} = -\int \frac{\cos \theta}{\sin \theta} d\theta + n_0 \int \frac{1}{\sin \theta} d\theta$$

$$\int \frac{dV}{V} = -\int \frac{d(\sin \theta)}{\sin \theta} + n_0 \int \frac{1}{2} \frac{\sec^2 \theta/2}{\tan \theta/2} d\theta; \quad \ln V = \ln \operatorname{cosec} \theta + n_0 \ln |\tan(\theta/2)| + C$$

$$V = k \frac{|\tan(\theta/2)|^{n_0}}{\sin \theta}; \quad k = V_0 \frac{\sin(\theta_0)}{|\tan(\theta_0/2)|^{n_0}}; \quad V_b = V_0 \frac{\sin \theta_0 |\tan(\theta_b/2)|^{n_0}}{\sin \theta_b |\tan(\theta_0/2)|^{n_0}}$$

$$\frac{T}{m} = -\frac{\dot{m} g_0 I_{sp}}{m} = n_0 g_0 \rightarrow \frac{dm}{m} = -\frac{n_0}{I_{sp}} dt \rightarrow \ln m = -\frac{n_0}{I_{sp}} t + C; \quad \frac{m_0}{m} = e^{\frac{n_0}{I_{sp}}(t-t_0)} \rightarrow t_b = \frac{I_{sp}}{n_0} \ln \left( \frac{m_0}{m_0 - m_p} \right)$$

(b) A single stage rocket is directly launched into a gravity turn trajectory (constant specific thrust) in vacuum with  $n_0$  of 1.1 &  $\theta_0$  of  $0.15^\circ$ . If at the end of trajectory lasting for 250 s, the inclination from vertical is  $90^\circ$ , determine the initial velocity at the start of the gravity turn (Hint: Use time expression given below). Also, what is the final velocity achieved, and the value of the propellant mass fraction ( $\Lambda = m_p/m_0$ ) needed to complete the mission, assuming constant sea level gravity and flat earth ( $g_0 = 9.81 \text{ m/s}^2$ ,  $I_{sp} = 275 \text{ s}$ )? (2)

$$250 = \frac{V_0 \times 0.0026}{2 \times 9.81 \times (0.0013)^{1.1}} \left[ \frac{1}{2.1} + \frac{1}{0.1} - \frac{(0.0013)^{2.1}}{2.1} - \frac{(0.0013)^{0.1}}{0.1} \right] = 0.198 V_0 \times 5.331$$

$$V_0 = \frac{250}{0.198 \times 5.331} = 236.8 \text{ m/s}; \quad V_b = k = 236.8 \times \frac{0.0026}{|0.0013|^{1.1}} = 9206 \text{ m/s}; \quad \theta_b = 90^\circ$$

$$250 = \frac{275}{1.1} \times \ln \left( \frac{m_0}{m_0 - m_p} \right) \rightarrow \frac{m_0}{m_0 - m_p} = 2.718; \quad 1 - \frac{m_p}{m_0} = 0.368 \rightarrow \frac{m_p}{m_0} = 0.632$$