

AE 330 Rocket Propulsion

Multi-stage Rockets

Kowsik Bodi

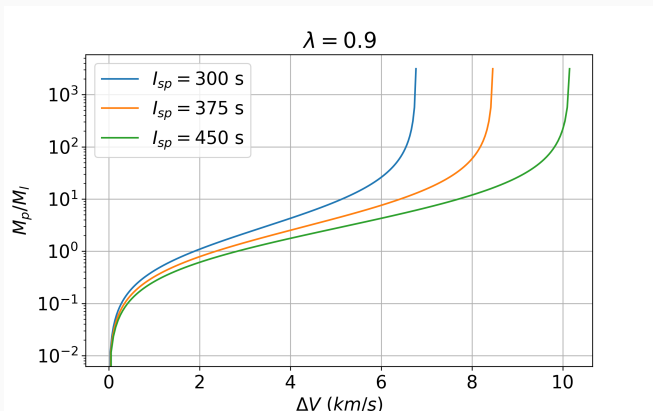
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Single-Stage Rocket

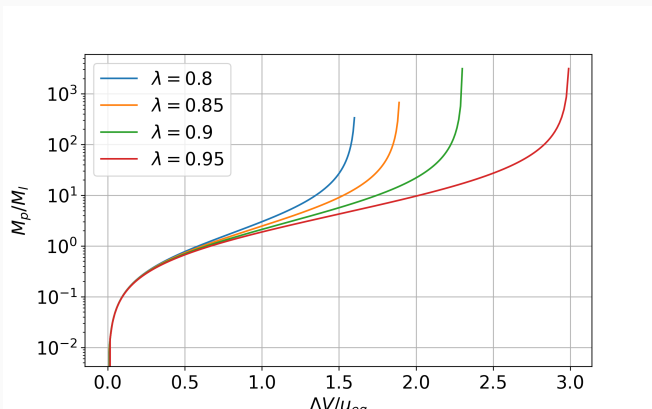
Rocket Equation: ΔV

$$\Delta V = u_{eq} \ln \left(\frac{M_o}{M_f} \right) \equiv u_{eq} \ln (\text{MR}) \quad \text{or} \quad \text{MR} = \exp \left(\frac{\Delta V}{u_{eq}} \right)$$



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Continuous Ejection

Eject inert mass along with propellant

$$\lambda = \frac{M_p}{M_p + M_i} \implies \dot{m} = \dot{m}_p + \dot{m}_i = \frac{\dot{m}_p}{\lambda}$$
$$M \frac{dv}{dt} = \dot{m}_p u_{eq} = (\dot{m}_p + \dot{m}_i) \lambda u_{eq} = -\frac{dM}{dt} \lambda u_{eq}$$

$$\Delta V_\infty = \lambda u_{eq} \ln \left(\frac{M_o}{M_l} \right)$$

For the masses considered for the earlier Vikas engine

$M_i = 1$ ton, $M_p = 22$ tons, $M_i = 2.45$ tons

$$\Delta V_\infty = \lambda u_{eq} \ln \left(\frac{M_o}{M_l} \right) = 8,572 \text{ m/s}$$



Launch mass to Payload mass ratio

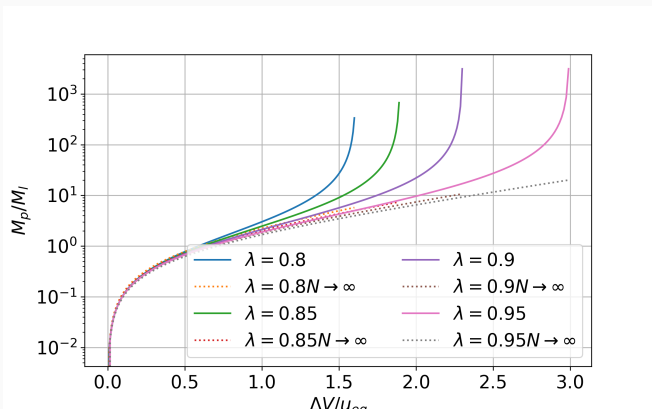
$$MR_{\infty} \equiv \frac{M_o}{M_l} = \exp \left(\frac{\Delta V}{\lambda u_{eq}} \right)$$
$$1 + \frac{M_p + M_i}{M_l} \equiv 1 + \frac{M_p}{\lambda M_l} = MR_{\infty}$$

$$\frac{M_p}{M_l} = \lambda \left(\exp \left(\frac{\Delta V}{\lambda u_{eq}} \right) - 1 \right)$$
$$\frac{M_i}{M_l} = (1 - \lambda) \left(\exp \left(\frac{\Delta V}{\lambda u_{eq}} \right) - 1 \right)$$



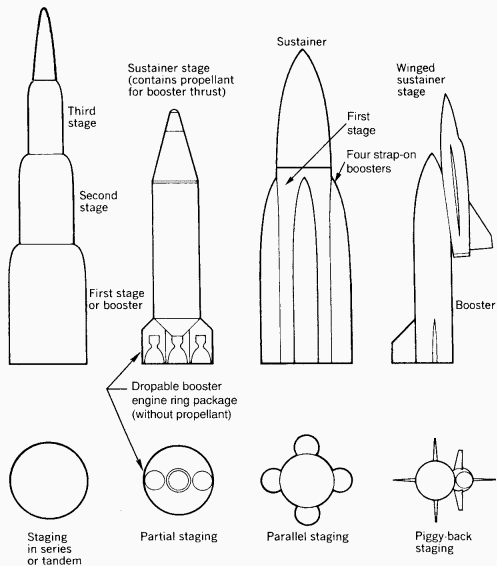
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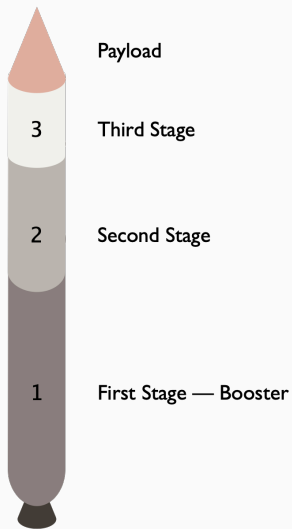


Multistage Rocket

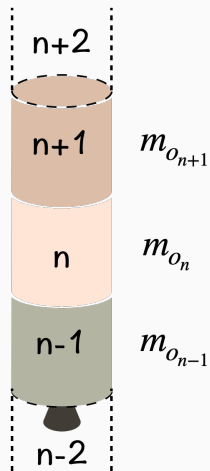
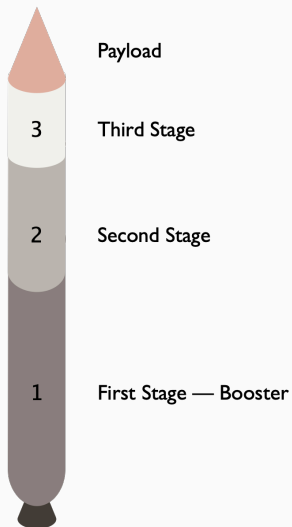
Launch Vehicle Staging



Multistage Rocket



Multistage Rocket



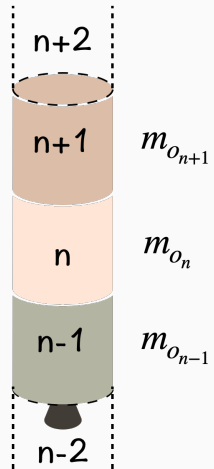
Multistage Rocket

	Mass
Propellant	m_{p_n}
Inert	m_{i_n}
Stage	m_{o_n}

Stage Mass: $m_{o_n} = m_{p_n} + m_{i_n}$

Structural Factor: $\epsilon_n = \frac{m_{f_n}}{m_{o_n}} \equiv \frac{m_{i_n}}{m_{i_n} + m_{p_n}}$

Propellant Fraction: $\lambda_n = \frac{m_{p_n}}{m_{i_n} + m_{p_n}} \equiv 1 - \epsilon_n$



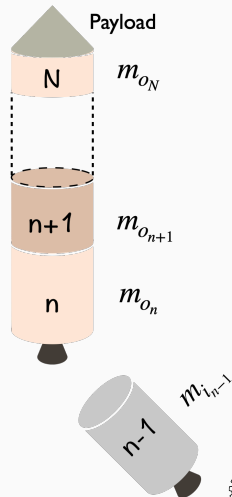
For n^{th} —stage

$$\text{Total Mass: } M_{o_n} = \sum_{j=n}^N m_{o_j}$$

$$\text{Payload Mass: } M_{l_n} \equiv M_{o_{n+1}} = \sum_{j=n+1}^N m_{o_j}$$

$$\text{Stage Payload Factor: } \beta_n = \frac{M_{l_n}}{M_{o_n}}$$

$$\text{Final Mass: } M_{f_n} = m_{i_n} + M_{l_n}$$



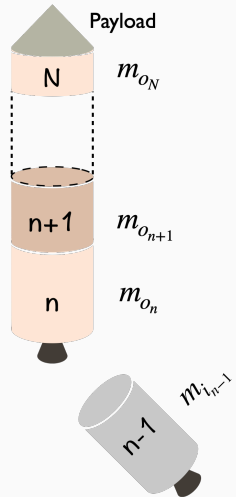
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$$\begin{aligned}\Delta V_n &= u_{eq_n} \ln \left(\frac{M_{o_n}}{M_{f_n}} \right) \\ &= -u_{eq_n} \ln (\epsilon_n + (1 - \epsilon_n) \beta_n)\end{aligned}$$



Total ΔV

$$\Delta V_n = u_{eq_n} \ln \left(\frac{M_{o_n}}{M_{f_n}} \right) = -u_{eq_n} \ln (\epsilon_n + (1 - \epsilon_n) \beta_n)$$

$$\begin{aligned} \Delta V &= \sum_{n=1}^N \Delta V_n \\ &= - \sum_{n=1}^N u_{eq_n} \ln (\epsilon_n + (1 - \epsilon_n) \beta_n) \end{aligned}$$

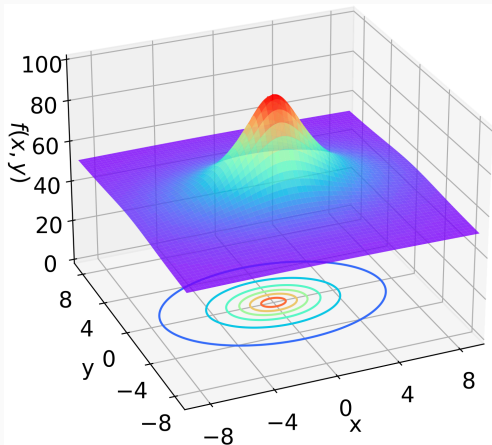
For a given M_l and $M_p = \sum_{n=1}^N m_{p_n}$ (and hence, $M_o \equiv M_{o_1}$):

For a given M_l/M_o , when is ΔV maximum?



Optimisation with Constraints

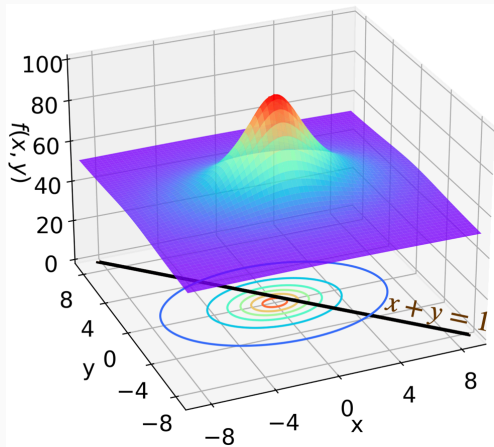
Function in 2D-space



$$f(x, y) = 50 + \frac{10}{0.2 + \left(\frac{x}{6}\right)^2 + \left(\frac{y}{4}\right)^2} \quad (\text{max. at origin})$$



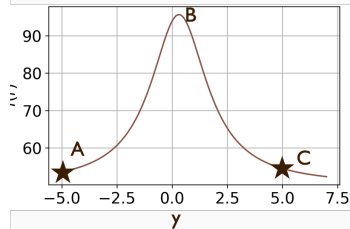
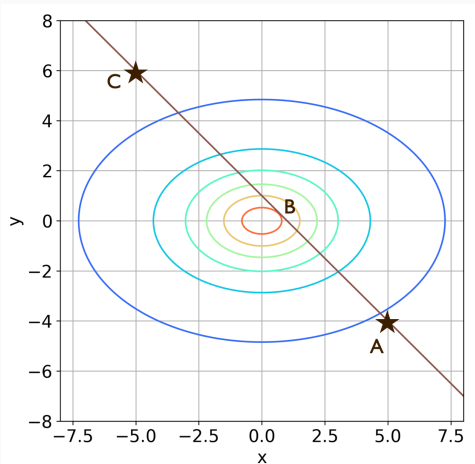
Along a straight line: $x + y = 1$



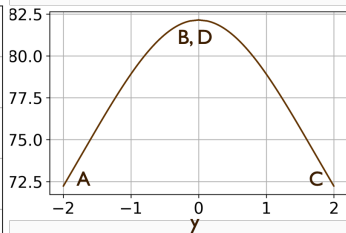
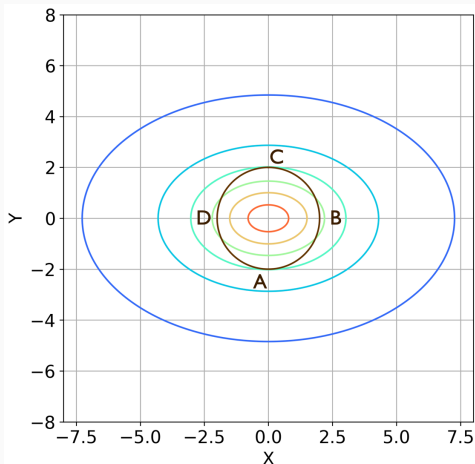
$$f(x, y) = 50 + \frac{10}{0.2 + \left(\frac{x}{6}\right)^2 + \left(\frac{y}{4}\right)^2}$$



Along a straight line: $x + y = 1$



Along a circle: $x^2 + y^2 = 4$



Maximum/Minimum along a curve

- We considered two curves (straight line and circle)
- We can find the peak location by plotting the function along the curve
- If s is the coordinate along the curve or interest, we can verify that $\partial f / \partial s = 0$ at the maximum/minimum location
- Can be tedious for more number of variables \rightarrow higher dimensions



Maximum/Minimum along a curve

These curves restrict the domain of interest

So, we call them **constraint functions** or **constraints**

Our constraint functions were:

$$g_l(x, y) = x + y - 1$$

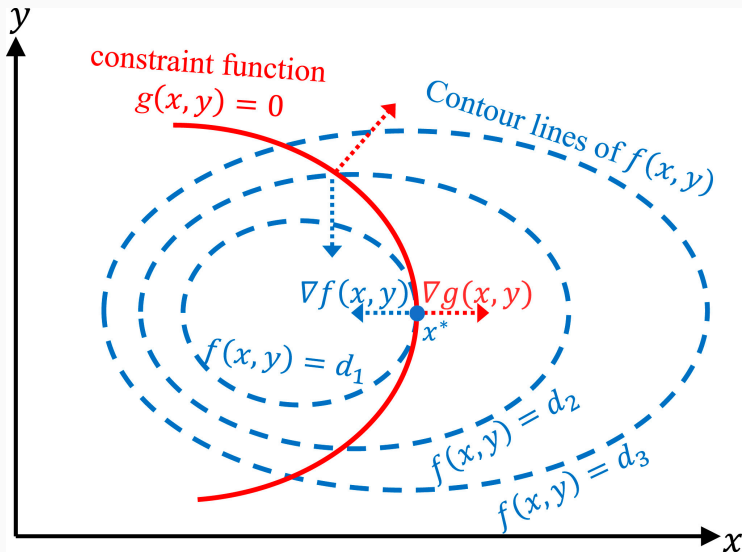
$$g_c(x, y) = x^2 + y^2 - 4$$

The constraints were $g_l(x, y) = 0$ and $g_c(x, y) = 0$

The function that is to be minimised is called the **objective function** or **merit function**. We denote it by $f(x, y)$



At a constrained maxima/minima



At a constrained maxima/minima

$$\begin{aligned}\nabla f(x, y) \propto \nabla g(x, y) &\implies \nabla f(x, y) = \alpha \nabla g(x, y) \\ \nabla \{f(x, y) - \alpha g(x, y)\} &= 0\end{aligned}$$

So, we can minimise $f - \alpha g$ instead of $f(x, y)$

α is called **Lagrange Multiplier**



Optimum mass distribution

Staging

Our **objective function** was

$$\begin{aligned} f(u_{eq_n}, \epsilon_n, \beta_n) &\equiv \Delta V = \sum_{n=1}^N \Delta V_n \\ &= - \sum_{n=1}^N u_{eq_n} \ln(\epsilon_n + (1 - \epsilon_n) \beta_n) \end{aligned}$$

Our **constraint function** is the vehicle payload fraction:

$$\begin{aligned} \frac{M_l}{M_o} &= \frac{M_{l_1}}{M_o} \frac{M_{l_2}}{M_{o_3}} \cdots \frac{M_l}{M_{o_N}} \equiv \prod_{n=1}^N \beta_n \\ g(\beta_n) &= \ln \frac{M_l}{M_o} = \sum_{n=1}^N \ln \beta_n \end{aligned}$$



Function to be minimised

$$f - \alpha g = - \sum_{n=1}^N u_{eqn} \ln (\epsilon_n + (1 - \epsilon_n) \beta_n) - \alpha \sum_{n=1}^N \ln \beta_n$$

f and g depend on β_n

$$\begin{aligned} \frac{\partial}{\partial \beta_n} (f - \alpha g) &= 0 \\ -u_{eqn} \frac{1 - \epsilon_n}{\epsilon_n + (1 - \epsilon_n) \beta_n} &= \frac{\alpha}{\beta_n} \implies \beta_n = - \frac{\alpha}{(\alpha + u_{eqn})} \frac{\epsilon_n}{(1 - \epsilon_n)} \end{aligned}$$



Optimum mass distribution

Our constraint is now

$$\frac{M_l}{M_o} = \prod_{n=1}^N \beta_n = \prod_{n=1}^N \frac{-\alpha}{(\alpha + u_{eqn})} \frac{\epsilon_n}{(1 - \epsilon_n)}$$

Once we select the rocket engines for different stages, we know (u_{eqn}, ϵ_n)

The only unknown now is α , which can be found from the above constraint.

$$\begin{aligned} \Delta V &= - \sum_{n=1}^N u_{eqn} \ln (\epsilon_n + (1 - \epsilon_n) \beta_n) \\ &= \sum_{n=1}^N u_{eqn} \ln \left(\frac{u_{eqn} + \alpha}{u_{eqn} \epsilon_n} \right) \end{aligned}$$



Simplification: Use the same engine in all stages

Same engine $\implies u_{eq_n} = u_{eq}$ and $\epsilon_n = \epsilon$

$$\beta_n = -\frac{\alpha}{(\alpha + u_{eq_n})} \frac{\epsilon_n}{(1 - \epsilon_n)}$$
$$\implies \beta_n \equiv \beta = -\frac{\alpha}{(\alpha + u_{eq})} \frac{\epsilon}{(1 - \epsilon)}$$

Our constraint is

$$\frac{M_l}{M_o} = \prod_{n=1}^N \beta_n = \beta^N \implies \beta = \left(\frac{M_l}{M_o} \right)^{1/N}$$



ΔV and Payload Fraction

$$\beta_{opt} = \left(\frac{M_l}{M_o} \right)^{1/N}$$

$$\Delta V = - \sum_{n=1}^N u_{eqn} \ln (\epsilon_n + (1 - \epsilon_n) \beta_n)$$

$$\implies \Delta V_{opt} = -N u_{eq} \ln \left(\epsilon + (1 - \epsilon) \left(\frac{M_l}{M_o} \right)^{1/N} \right)$$

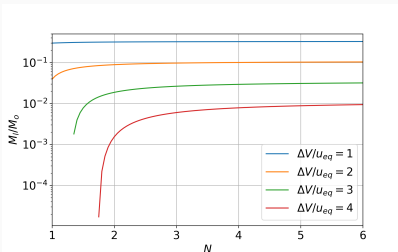
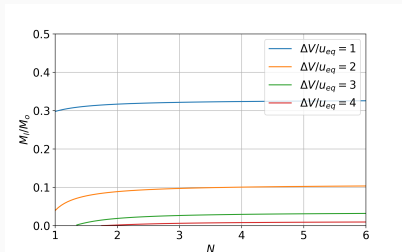
We can express the payload fraction as

$$\frac{M_l}{M_o} = \left(\frac{w^{-1/N} - \epsilon}{1 - \epsilon} \right)^N$$

where $w = \exp (\Delta V / u_{eq})$



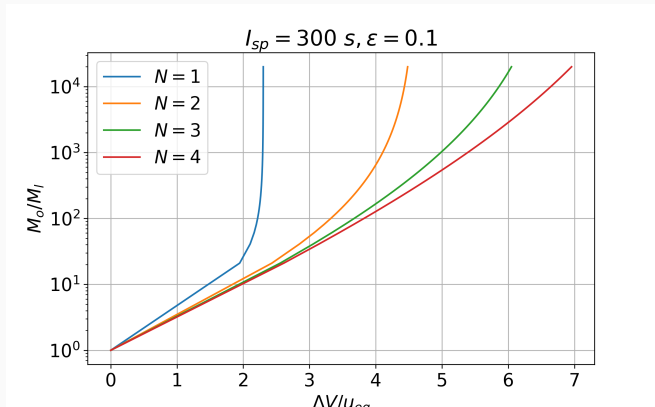
Payload Fraction vs ΔV



No particular advantage beyond 4 stages for most missions (near Earth)



Payload Fraction vs ΔV



Optimum no:of stages depends on ΔV

