

Fault diagnosis technology of wind turbines pitch sensor offset based on the multi-Innovation Kalman filter

Dinghui Wu · Yiyang Li · Zhicheng Ji

Abstract This paper presents a fault diagnosis method for detecting pitch sensor offset fault according to the mechanical structure characteristics of wind turbine. The method establishes corresponding relation between the change of pitch angle and the minute displacement which produced by the force acting on tower of wind turbine. It is based on the change of displacement to diagnosis whether the fault occurs. With regard to the large noise of sensors, we adopt the multi-innovation Kalman filter to enhance the estimation accuracy and convergence speed. The simulation results show that the multi-innovation Kalman filter based method can diagnose the fault effectively and is better than the common Kalman filter.

Keywords Wind turbine · Kalman filter · fault diagnosis · multi-innovation

1 Introduction

Wind energy is playing a more and more important role in world power production. Since most wind farms are located in desert or sea areas where the natural environment is harsh [1], wind turbines often have faults. Modern wind turbines often adopt fault tolerant control methods to maintain normal operation, and fault diagnosis is the premise and necessary condition [2]. The variable pitch system is an important part of wind turbines, the pitch fault will affect the generated power when the wind velocity is above the rated one, when the wind velocity is below the rated one, the pitch fault has a little impact on the generated power.

There have been many fault diagnosis methods for wind turbines. Watson et al. has studied the rotor fault based on the wavelet analysis, the analysis involves monitoring the power output and processing the data to obtain the magnitude of particular frequency components [3]. This method can extract the characteristic of fault, however, the wavelet analysis must be calculated off-line, which limits the widespread applications. Guo et al. has studied the current feedback sensor fault, speed sensor fault and constant gain output fault of wind turbine control system [4]. The neural networks are trained to analyze fault conditions by selecting the appropriate eigenvalue and training samples. But the neural networks algorithm relies on a large number of training samples, which is not available in remote areas. Some faults do not change system structures, but will affect the system parameters, we can set up the linear model of the turbines, and the fault information can be reflected on the parameters' change. So, the system identification technology can be adopted to fault detection and diagnosis [5–7].

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When the wind velocity is above the rated one, the control objective is to maintain constant generated power [8], the objective is realized by adjusting the angle of three pitches. The pitch angle sensor is an important part of the closed-loop pitch system, if an offset fault happens to pitch angle sensors, the whole pitch system will become unstable. Under the effective wind velocity, there will be a thrust acting on the rotor, the thrust makes the tower sway back and forth [9], which results in a tiny displacement. The value of thrust depends on the thrust coefficient, and the thrust coefficient relies on the pitch angle and tip-speed ratio, therefore, the pitch angle will influence the thrust. A corresponding relationship can be formed between the pitch angle and the tiny displacement, but the pitch sensor fault will break the relationship. As a consequence, the fault can be detected by monitoring the relationship.

The above method involves a lot of data processing, the Kalman filter based on the multi-innovation method is utilized to filter the value obtained from the pitch angle sensor and tower displacement sensor. The multi-innovation algorithm extends the scalar value [10–12], and uses not only the current data but the past data as well, which significantly improves the accuracy of the estimate and the convergence speed [13]. The tower displacement calculated from pitch angle and the displacement from sensor should be equal when the pitch angle sensor is normal. When there is a deviation between two displacements, we can detect a fault.

The rest of this paper is organized as follows. Section 2 gives the wind turbine model for simulation, and presents the fault model for analysis. Section 3 gives the fault diagnosis and data processing procedure using the multi-innovation Kalman filter. Section 4 contains a simulation result. Finally, concluding remarks are given in Section 5.

2 The wind turbine model

2.1 Aerodynamic Model

The wind energy captured from the three blades is transformed to the rotational motion of the rotor, the rotor speed is $\omega_r(t)$. The captured wind energy is dependent on the effective wind speed $v_r(t)$, the air density ρ and the rotor swept area A and the power coefficient $C_p(\lambda(t), \beta(t))$. The power coefficient relies on tip-speed ratio $\lambda(t)$ and pitch angle $\beta(t)$. The aerodynamic torque $T_a(t)$ applied to the rotor by blade can be obtained from tip-speed ratio $\lambda(t)$ and blade radius r [14], as illustrated below

$$\lambda(t) = \frac{r\omega_r(t)}{v_r(t)}, \quad (1)$$

$$T_a(t) = \frac{1}{2\omega_r(t)} \rho A v_r^3 C_p(\lambda(t), \beta(t)). \quad (2)$$

2.2 Tower Model

The wind acting on each blade results in a thrust on the rotor, which can be calculated as [15]

$$F_t(t) = \frac{1}{2} \rho A v_r^2 C_t(\lambda(t), \beta(t)). \quad (3)$$

The thrust coefficient $C_t(\lambda(t), \beta(t))$ is dependent on $\lambda(t)$ and $\beta(t)$.

The resulting tower force $F_{th}(t)$ on the tower at hub height h depends on the azimuth angle of rotor, which is the synthesis of three thrusts [9]

$$F_{th}(t) = \sum_{i=1}^3 F_{th,i}(t), \quad (4)$$

$$F_{th,i}(t) = F_{t,i}(t) \left(1 + \frac{r_t}{h} \cos(\Psi_i(t))\right), \quad (5)$$

where $F_{t,i}$ is the thrust from blade i , r_i is the distance from the hub to the point where the thrust acts on the blade. The relationship between $\Psi_1(t)$, $\Psi_2(t)$, $\Psi_3(t)$ and the location of the blades

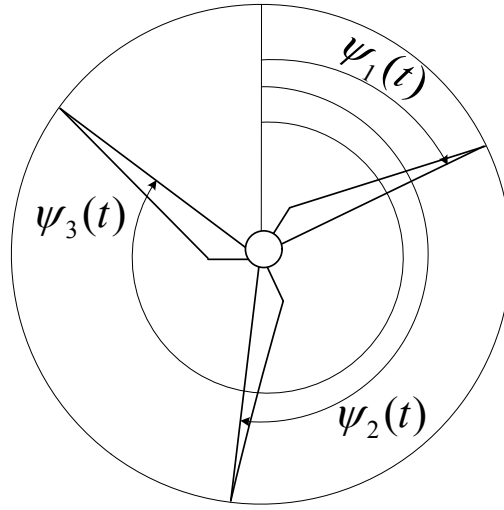


Fig. 1 Position of blades

are illustrated in Fig. 1. From (4) and (5), it is shown that the location of the blades affects the tower force components, which is different from the aerodynamic torque.

Under the tower force, the tower will produce a tiny displacement $x_t(t)$. Due to the fact that $x_t(t)$ is the only measured variable in the tower model, the movement of the tower can be described as a linear displacement of the nacelle. An illustration of this model is given in Fig. 2, using a spring-damper terminology the tower model is given as

$$M_t \ddot{x}_t(t) = F_{th}(t) - B_t \dot{x}_t(t) - K_t x_t(t), \quad (6)$$

where M_t is the top mass of the tower, B_t is the tower damping coefficient, K_t is the tower torsion coefficient.

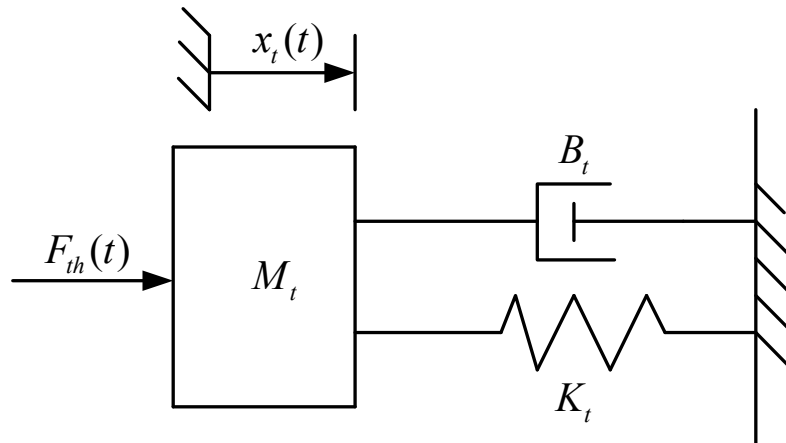


Fig. 2 Tower model

2.3 Pitch Model

The pitch actuator is modeled as a second order system [16],

$$\frac{\beta(s)}{\beta_{ref}(s)} = \frac{\omega_n^2}{s^2 + 2\zeta\omega_n s + \omega_n^2}, \quad (7)$$

$$\ddot{\beta}(t) = 2\zeta\omega_n\dot{\beta}(t) - \omega_n^2\beta(t) + \omega_n^2\beta_{ref}(t), \quad (8)$$

$$\beta_m(t) = \beta(t) + v_\beta(t), \quad (9)$$

where $\beta_{ref}(t)$ is the reference to the pitch angle, ω_n is the natural frequency of the pitch actuator model, ζ is the damping ratio of the pitch actuator model, $\beta_m(t)$ is the value returned from the pitch angle sensor and v_β is the measurement noise.

When an offset pitch angle fault happens, the model of the actuator is

$$\begin{aligned} \ddot{\beta}(t) = & -2\zeta\omega_n\dot{\beta}(t) - \omega_n^2(\beta(t) + \beta_{bias}(t)) \\ & + \omega_n^2\beta_{ref}(t), \end{aligned} \quad (10)$$

$$\beta_m(t) = \beta(t) + \beta_{bias}(t) + v_\beta(t). \quad (11)$$

where $\beta_{bias}(t)$ is the offset added to the pitch angle sensor output.

3 Fault Diagnosis Algorithm

3.1 Structure of the Diagnosis System

A fault diagnosis structure is designed for the pitch system, which is illustrated in Fig.3.

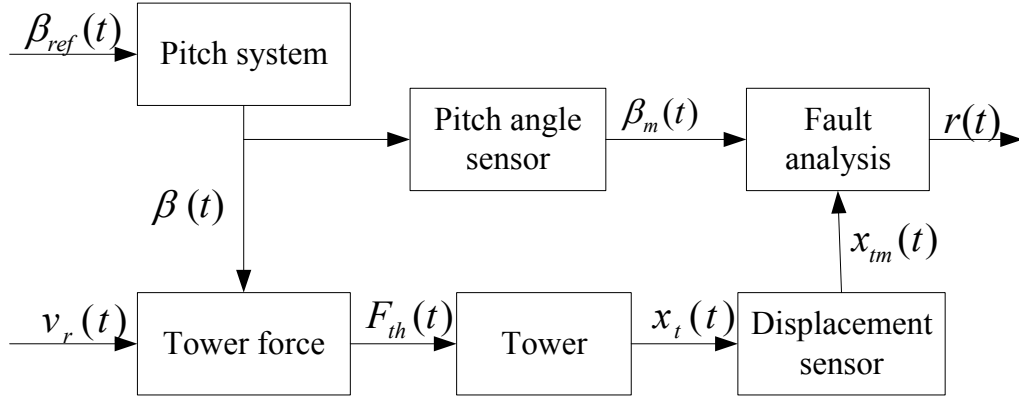


Fig. 3 Structure of the diagnosis system

From (3), the thrust $F_t(t)$ on blade is related to the thrust coefficient C_t , and the coefficient C_t is related to $\lambda(t)$ and $\beta(t)$. The tower force $F_{th}(t)$ can be deduced from (4) and (5). Using (6), we can obtain the tiny displacement $x_t(t)$ from the tower force $F_{th}(t)$. An offset in pitch angle will result in a small change in thrust coefficient, and the tower force will change correspondingly. As a result, by monitoring the variation of displacement, the fault can be detected.

To maintain a constant wind power output, the closed-loop pitch system works continuously to obtain the pitch angle objective β_0 . If there is a constant offset output $-\theta$ adding to the pitch angle sensor, the sensor output will become $\beta_m = \beta_0 - \theta$. For the pitch control system, the value from measurement does not match the control objective, so under the action of the pitch actuator, the pitch is adjusted to force the sensor output back to the objective, that is $\beta'_m = \beta_m + \theta = \beta_0$. Due to the offset in the sensor output, the real pitch angle is $\beta = \beta'_m + \theta = \beta_0 + \theta$. Therefore, we draw the conclusion that the measured displacement x_{tm} is different from the calculated

displacement obtained from β_0 . The fault severity can be concluded by comparing the measured and calculated displacement.

As the wind turbines work in a harsh condition, the value returned from the sensor is polluted by noise and the displacement caused by the sensor offset fault is rather small, it is possible for the displacement information to be submerged by the noise. It is necessary to filter the sensor output, the Kalman filter based on the multi-innovation technology is an efficient way to obtain the optimal state estimation, and to realize the accurate judgement of the sensor offset fault.

3.2 Kalman Filter Based on Multi-Innovation

The Kalman filter is a recursive method which estimate the optimal system states [17]. The Kalman filter consists of two steps: a prediction step and an update step. In the prediction step, the estimate of the state at the current time is produced from the previous time. The predicted step combines the priori prediction with the current observation information to refine the state estimate.

The innovation is defined as the useful information which can improve parameters or states estimation accuracy [?]. For the linear discrete system of the wind turbine, the conventional Kalman filter can be written as the following five equations,

$$\hat{x}_{k|k-1} = A_{k-1}\hat{x}_{k-1}, \quad (12)$$

$$P_{k|k-1} = A_{k-1}P_{k-1}A_{k-1}^T + \Gamma_{k-1}Q_{k-1}\Gamma_{k-1}^T, \quad (13)$$

$$\hat{x}_k = \hat{x}_{k|k-1} + K_k[z_k - C_k\hat{x}_{k|k-1}], \quad (14)$$

$$P_k = [I - K_kC_k]P_{k|k-1}, \quad (15)$$

$$K_k = P_{k|k-1}C_k^T[C_kP_{k|k-1}C_k^T + R_k]^{-1}, \quad (16)$$

where $x_{k|k-1}$ is posteriori state estimate at time k given observations up to and including time k , $P_{k|k-1}$ is the posteriori error covariance matrix, A_{k-1} is the state transition matrix which is applied to the previous state \hat{x}_{k-1} , K_k is the optimal Kalman gain, \hat{x}_k is the updated state estimate, P_k is the updated estimate covariance matrix, C_k and Q_k is the noise covariance matrix.

The single innovation for the conventional Kalman filter is defined as

$$c(k) = z_k - C_k\hat{x}_{k|k-1}. \quad (17)$$

Then we extend the single innovation to a multi-innovation vector,

$$\begin{aligned} E(p, k) &= \begin{bmatrix} e(k) \\ e(k-1) \\ \vdots \\ e(k-p+1) \end{bmatrix} \\ &= \begin{bmatrix} z_k - C_k\hat{x}_{k|k-1} \\ z_{k-1} - C_{k-1}\hat{x}_{k-1|k-2} \\ \vdots \\ z_{k-p+1} - C_{k-p+1}\hat{x}_{k-p+1|k-p} \end{bmatrix}, \end{aligned} \quad (18)$$

where p is the innovation length. Then the updated state estimate is changed to

$$\begin{aligned} \hat{x}_k &= A_{k-1}\hat{x}_{k-1} + [K_k, K_{k-1}, K_{k-2}, \dots, K_{k-p}]E(p, k) \\ &= A_{k-1}\hat{x}_{k-1} + \sum_{i=1}^p K_i(k)e(k-i+1). \end{aligned} \quad (19)$$

Here we choose $K_i(k) = K(k-i+1)$.

3.3 Design of the State and Observation Equation

The measurement of displacement $x_{tm}(k)$ is processed by the multi-innovation Kalman filter to obtain the optimal state estimate, which is polluted by noise. Under the random tower force, the wind turbine is not moving uniformly from the equilibrium position. In order to get the discretization expression of the displacement and its derivative, the sampling period $T_0 = 0.01s$ is taken, it is assumed that within a sampling period of displacement generated by the wind turbine tower, it moves uniformly. $x_{tm}(k)$ is the displacement measured at time kT_0 , by applying the kinematics formulas, the motion of tower can be obtained as

$$x_{tm}(k+1) = x_{tm}(k) + \dot{x}_{tm}(k)T_0, \quad (20)$$

$$\dot{x}_{tm}(k+1) = \dot{x}_{tm}(k). \quad (21)$$

The displacement and velocity of tower is chosen as the state parameters, then the system states at time kT_0 is

$$x(k) = \begin{bmatrix} x_{tm}(k) \\ \dot{x}_{tm}(k) \end{bmatrix}. \quad (22)$$

Then the state space model is

$$\begin{bmatrix} x_{tm}(k+1) \\ \dot{x}_{tm}(k+1) \end{bmatrix} = \begin{bmatrix} 1 & T_0 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} x_{tm}(k) \\ \dot{x}_{tm}(k) \end{bmatrix} + w(k). \quad (23)$$

The observation equation is

$$z(k) = [1 \ 0] \begin{bmatrix} x_{tm}(k) \\ \dot{x}_{tm}(k) \end{bmatrix} + v(k). \quad (24)$$

The pitch sensor output β_m is polluted by noise, the method utilized to process displacement can be applied here. The pitch angle changed in a single period is the uniform motion, and the similar states can be established as

$$\begin{bmatrix} x_{tm}(k+1) \\ \dot{x}_{tm}(k+1) \\ \beta_m(k+1) \\ \dot{\beta}_m(k+1) \end{bmatrix} = \begin{bmatrix} 1 & T_0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & T_0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} x_{tm}(k) \\ \dot{x}_{tm}(k) \\ \beta_m(k) \\ \dot{\beta}_m(k) \end{bmatrix} + w(k), \quad (25)$$

$$z(k) = \begin{bmatrix} x_{tm}(k) \\ \beta_m(k) \end{bmatrix} \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix} \begin{bmatrix} x_{tm}(k) \\ \dot{x}_{tm}(k) \\ \beta_m(k) \\ \dot{\beta}_m(k) \end{bmatrix} + v(k). \quad (26)$$

The state space model is

$$x(k+1) = Ax(k) + w(k), \quad (27)$$

$$z(k) = Cx(k) + v(k), \quad (28)$$

where the parameter matrixes are $A = \begin{bmatrix} 1 & T_0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & T_0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$, $C = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \end{bmatrix}$.

The procedure for the multi-innovation Kalman filter is described as follows: the optimal state estimate $\hat{x}(k)$ and state covariance matrix $P(k)$ is known at step k , we compute the optimal Kalman gain $K(k)$, innovation $e(k)$, then choose the appropriate innovation length p , the innovation vector is extended to innovation the matrix $E(p, k)$ and the optimal state estimate $\hat{x}(k+1)$ at step $k+1$ can be calculated. In this section, the fault diagnosis for the pitch angle sensor offset fault is simulated. Fig. 4 is the original observation of the tower displacement, Fig. 5 is the displacement curve of the Kalman filter, and Fig. 6 is the displacement curve of the

multi-innovation Kalman filter. It is shown from the comparison that both the conventional and the multi-innovation Kalman filter can remove the influence of noise, and the multi-innovation method is more accurate.

The innovation length p introduced by the multi-innovation Kalman filter not only can improve the estimation accuracy, but also can improve the convergence speed. But a large innovation length p involves a large amount of matrix computation. It is illustrated in Fig. 7 that the innovation length $p = 8$ is an appropriate one.

This algorithm can be used to detect the severity of the fault. The tested wind velocity is 25m/s, in 40s – 100s, the fault happens, a offset -3° is added to the pitch angle sensor output. It is shown in Fig. 8 that, the displacement of tower changes significantly.

In Fig. reffig:fault5, the offset is changed to -5° , in 20s – 140s, the wind velocity accelerates every ten seconds. As the Fig. 9 depicted, the tower displacement is related to the wind velocity. In Fig. 10, the wind velocity is 25m/s, the offset added to pitch angle output increases every ten seconds. The result shows that the displacement changes corresponding to the offset.

The relationship between the wind velocity, the pitch angle sensor offset and the tower displacement is shown in Fig. 11.

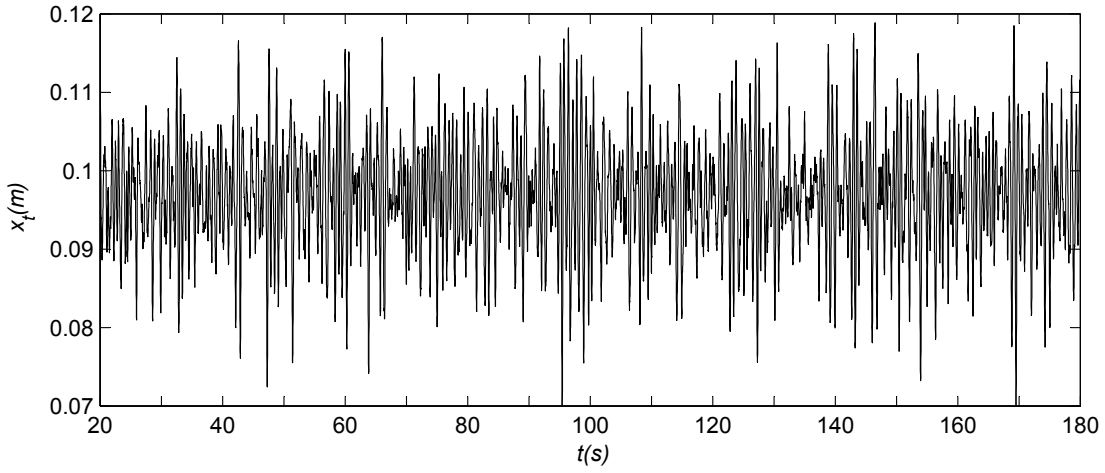


Fig. 4 Observation of displacement

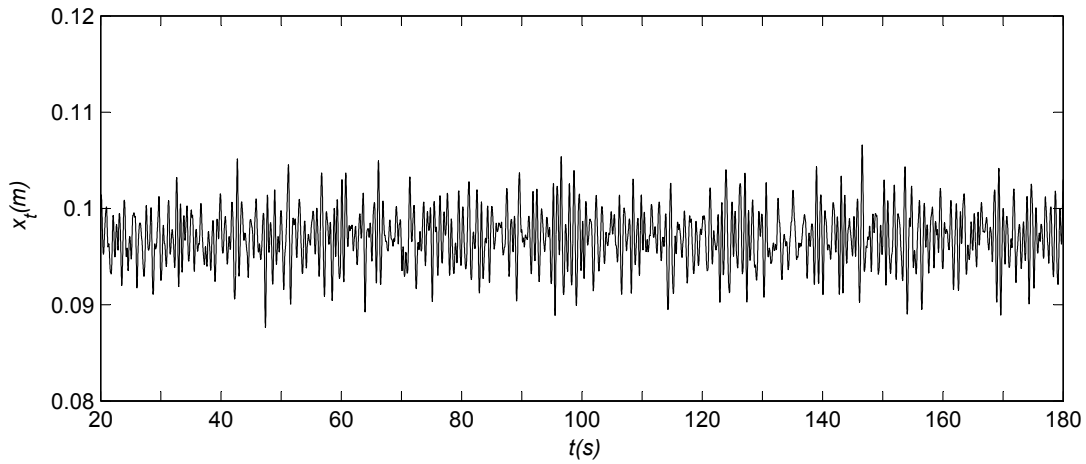


Fig. 5 Displacement curve of Kalman filter

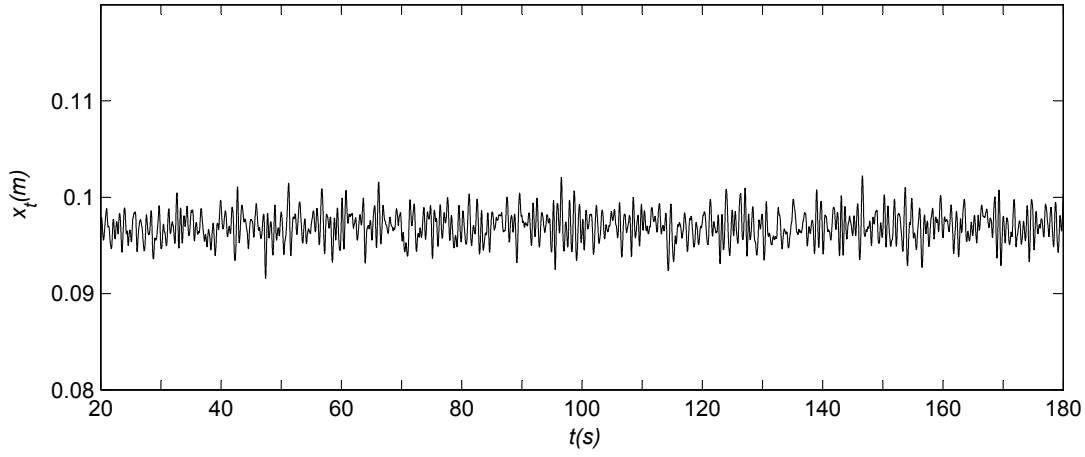


Fig. 6 Displacement curve of the multi-innovation Kalman filter

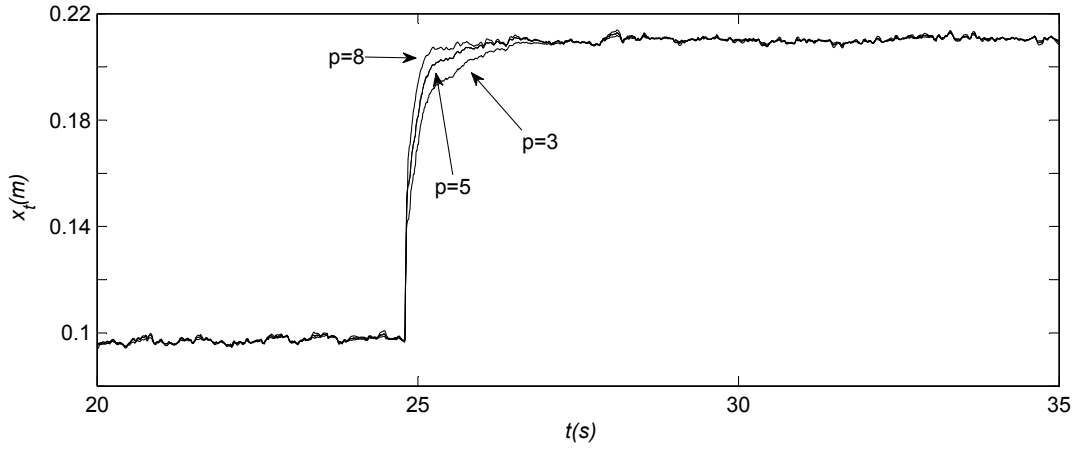


Fig. 7 Displacement of the different innovation length

4 Conclusion

In this paper, the pitch angle sensor offset fault is considered, and a relationship between the sensor offset and the tiny displacement of tower is established for fault diagnosis. To obtain more accurate displacement states, the conventional Kalman filter is extended to the multi-innovation Kalman filter. The multi-innovation algorithm shows faster convergence. It is shown in Fig. 11 that the sensor offset value can be estimated from the wind velocity and the displacement deviation.

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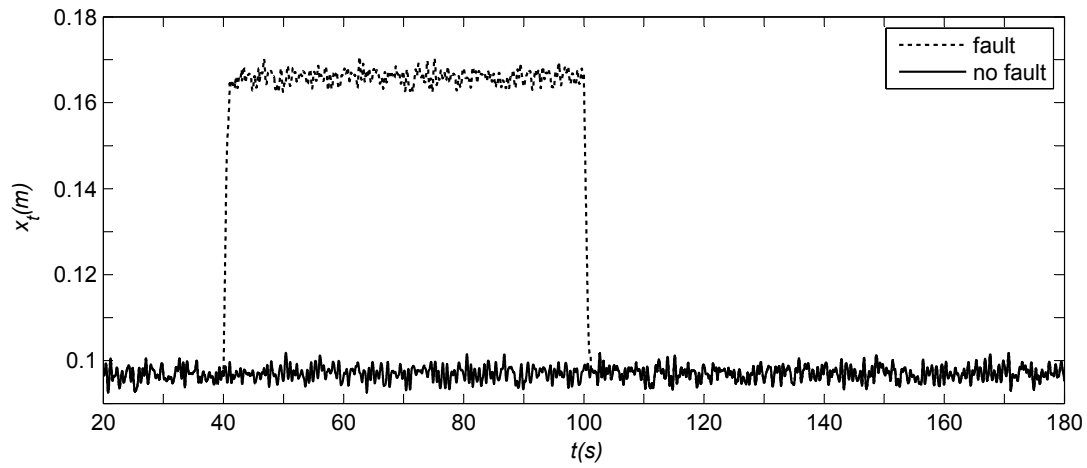


Fig. 8 Displacement of the fault and fault-free

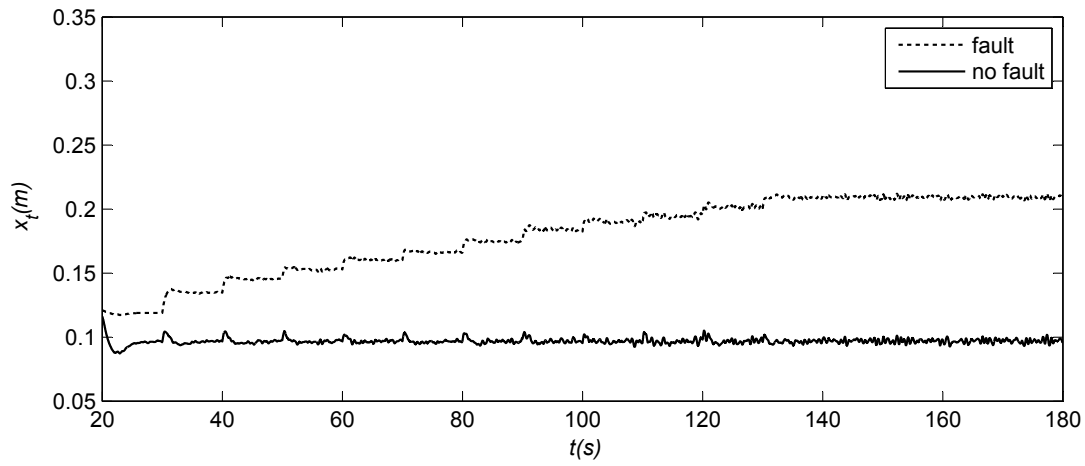


Fig. 9 Displacement of the different wind velocities

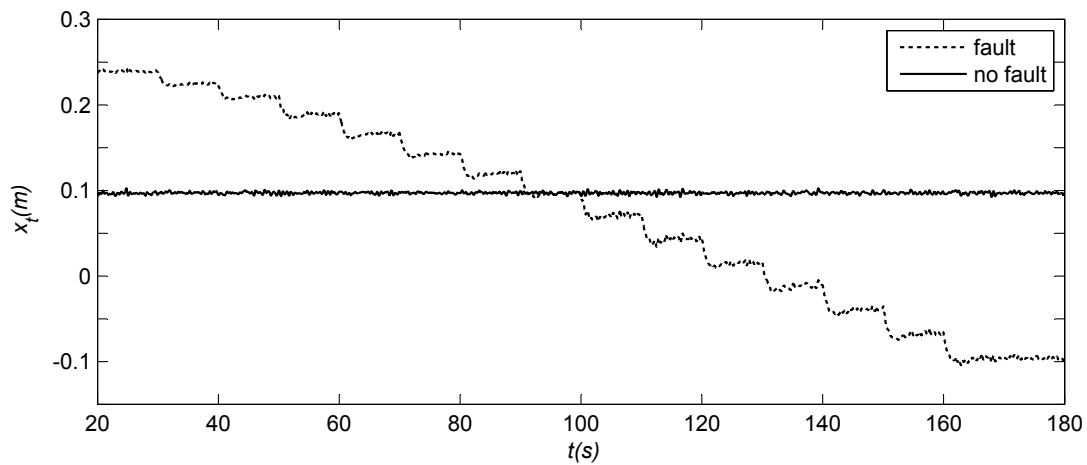


Fig. 10 Displacement of the different pitch angles

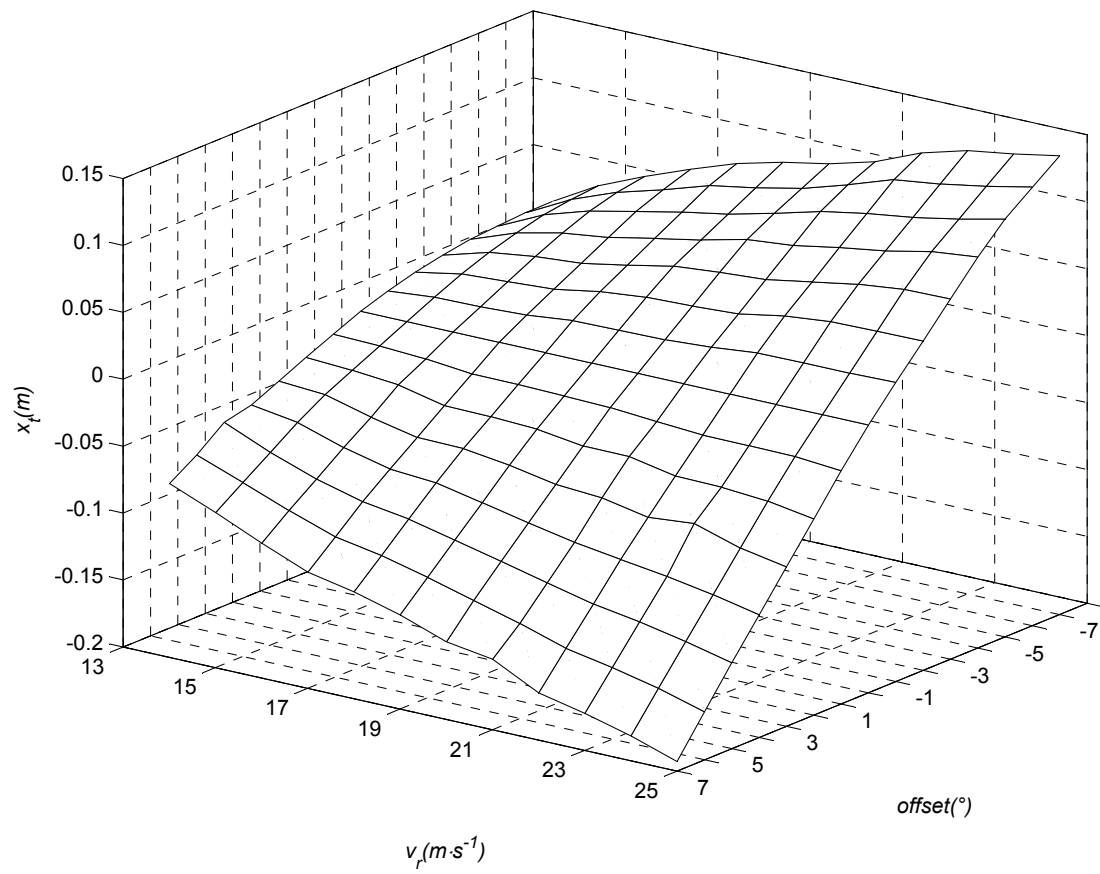


Fig. 11 Wind velocity-pitch angle-displacement

References

1. Fu, Z.X.: Status and prospects on condition monitoring technologies of offshore wind turbine. *J. Control Autom. Electr. Syst.* **36**(1), 121-129, (2012)
2. Li, S.B., Sauter, D., Aubrun, C.: Stability guaranteed active fault-tolerant control of networked control systems. *J. Control Sci. Eng.* **2008**(5), 22-31 (2008)
3. Watson, S.J., Xiang, B.J., Yang, W., Tavaner, P.J., Crabtree, C.J.: Condition monitoring of the power output of wind turbine generators using wavelets. *IEEE Trans. Energy Convers.* **25**(3), 715-721 (2010)
4. Guolian, H., Pan, J., Zhen, W.T.: Research on fault diagnosis of wind turbine control system based on Artificial Neural Network. *Proceedings of 8th world congress on intelligent control and automation (WCICA2010)*, July 6-9, 2010, Jinan, China, pp. 4875-4879
5. Yao, J., Wang, J.H.: Recursive identification of parameters in the minimum variance control. *Proceedings of 10th world congress on intelligent control and automation (WCICA2012)*, July 6-8, 2012, Beijing, China, 2870-2877
6. Wang, C., Tang, T.: Several gradient-based iterative estimation algorithms for a class of nonlinear systems using the filtering technique. *Nonlinear Dyn.* **77**(3), 769-780 (2014)
7. Ji, Y., Liu, X.M., et al.: Ji Y, Liu XM, Ding F. New criteria for the robust impulsive synchronization of uncertain chaotic delayed nonlinear systems. *Nonlinear Dyn.* 2015. doi: 10.1007/s11071-014-1640-6
8. Munteanu, I., Bratcu, A.I., Cutululis, N.A.: Optimal control of wind energy systems: towards a global approach. Springer, (2008)
9. Esbensen, T., Sloth, C.: Fault Diagnosis and Fault-Tolerant Control of Wind Turbines. Aalborg University, (2009)
10. Ding, F.: Several multi-innovation identification methods. *Digit. Signal Process.* **20**(4), 1027-1039 (2010)
11. Ding, F., Liu, X.P., Liu, G.: Multi-innovation least squares identification for system modeling. *IEEE Trans. Syst. Man. Cybern. B. Cybern.* **40**(3), 767-778 (2010)
12. Han, L.L., Ding, F.: Multi-innovation stochastic gradient algorithms for multi-input multi-output systems. *Digit. Signal Process.* **19**(4), 545-554 (2009)
13. Ding, F., Chen, T.: Performance analysis of multi-innovation gradient type identification methods. *Automatica.* **43**(1), 1-14 (2007)
14. Mohammadpour, J., Scherer, C.W.: Control of linear parameter varying systems with applications. Springer, (2012)
15. Bianchi, F.D., Battista, H.D., Mantz, R.J.: Wind Turbine Control Systems: Principle, Modeling and Gain Scheduling Design, Springer, (2007)
16. Odgaard, P.F., Johnson, K.E.: Wind turbine fault detection and fault tolerant control-an enhanced benchmark challenge. *Proceedings of American Control Conference (ACC)*, June 17-19, 2013, Washington, America, 4447-4452.
17. Kolouri, S., Azimi-Sadjadi M.R., Ziemann A.: Acoustic tomography of the atmosphere using unscented Kalman filter. *IEEE Trans. Geosci. Remote Sens.* **52**(4), 2159-2171 (2014)
18. Ding, F.: System Identification – New Theory and Methods. Science Press, Beijing (2013)