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Degradation of acetamiprid in UV/H₂O₂ and UV/persulfate systems: A comparative study



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HIGHLIGHTS

- UV/PS process was much more effective than the UV/H2O2 process in degrading ACE.
- The TOC removal rate achieved 50% and 26.6% for the UV/PS and UV/H₂O₂, respectively.
- The degradation was greatly inhibited in secondary effluent of wastewater treatment facility.
- Second-order rate constants of ACE with 'OH and SO₄. were derived.

ARTICLE INFO

Keywords: Sulfate radical Hydroxyl radical Second order rate constant Secondary effluent Advanced oxidation

ABSTRACT

Acetamiprid (ACE) was degraded by using ultraviolet (UV) irradiation and UV based advanced oxidation processes (AOPs) including UV/hydrogen peroxide (UV/H₂O₂) and UV/potassium persulfate (UV/PS). Among them, UV/PS process exhibited the best performance for the elimination of ACE and reduction of total organic carbon (TOC). The degradation kinetics was comprehensively compared in terms of dose of oxidants, solution pH, and water matrix species. A linear relationship was tentatively developed between the [Oxidant]/[ACE] ratio and the pseudo-first-order kinetic rate constant (k). The degradation was significantly inhibited at basic conditions no matter for UV/H₂O₂ process or UV/PS process. The effects induced by the water matrix species including inorganic anions and natural organic matter (NOM) were also non-negligible. For UV/PS process, both SO₄ $^-$ and HO $^-$ contributed to the ACE degradation, whereas only HO $^-$ participated in the degradation in the UV/H₂O₂ process. The corresponding second-order rate constants of ACE with HO $^-$ and SO₄ $^-$ were determined to be 7.59 \times 10⁸ and 3.68 \times 10⁸ M $^-$ 1 s $^-$ 1, respectively. Due to the different active radical species, different degradation products were detected through the HPLC-MS analysis. This work would be meaningful for the remediation of ACE from water by AOPs.

1. Introduction

Acetamiprid (ACE), chemically known as N-[(6-chloro-3-pyridyl) methyl]-N'- cyano-N-methyl-acetamidine, is a typical neonicotinoid insecticide. According to its relatively low acute and chronic mammalian toxicity, ACE exhibits broader applications than conventional insecticides which have caused severe environmental pollution and pesticide-resistance issues [1]. As a consequence, ACE has been intensively detected in different environmental media, such as soil and vegetables [2–4]. The maximum residue limit (MRL) for ACE in vegetables and fruits is strictly regulated ($< 5 \, \mu g \, g^{-1}$ in Japan and $< 3 \, \mu g \, g^{-1}$ in United States, respectively) [5,6]. However, with high water solubility (4250 mg L⁻¹), ACE can be readily washed out from the soil and invade the aquatic environment. Noteworthily, due to its bio-refractory and

recalcitrant nature, ACE cannot be effectively removed by conventional biological wastewater treatment processes [7]. It has been detected in the secondary effluents at concentrations ranging from 50 ng L^{-1} [8] to $16 \,\mu\text{g L}^{-1}$ [9]. The presence of ACE in the environment can pose potential risks to human health and aquatic systems. For example, the European Food Safety Authority (EFSA) recently delivered a Scientific Opinion claiming that chronic exposure to ACE could affect neural development and function in humans [10]. Recently, some other adverse effects on human health were associated with the chronic exposure to ACE, including memory loss and finger tremors [11]. In addition to human beings, ACE would pose negative effects on other species such as aquatic and soil microorganisms, as well as beneficial insects [12]. Therefore, it is very desirable to develop effective methods to remove the residual ACE in water [13].

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Biodegradation is recognized as an economically competitive method for the elimination of organic pollutants from environmental media. For instance, Yang et al. [14] successfully isolated an ACE-degradable strain D-2 from a wastewater treatment pool located in an ACE-manufacturing factory. However, the degradation process was extremely time-consuming (~72 h) and therefore significantly limited its application. Moreover, the metabolism of ACE by pure strain was regulated by specific functional genes, which possessed high selectivity towards target organic compounds. Consequently, the ACE was hardly to be completely mineralized to the end products, i.e. CO2 and H2O [15]. On the other hand, the chemical methods especially advanced oxidation processes (AOPs) could remarkably reduce the reaction time and more easily achieve the mineralization [16.17]. Through generation of strong oxidative radical species (hydroxyl radical, sulfate radical, and etc.), various organic pollutants could be completely decomposed within several hours [18]. For instance, Cao et al. [19] reported the photocatalytic degradation of ACE by using the Ag doped TiO2 nanoparticles. The half-live of the degradation process was no longer than 20 min. Moreover, the degradation rate could be further enhanced significantly by adding the electron acceptors (H₂O₂, KBrO₃, K₂S₂O₈) [20]. Carra et al. [21] investigated the degradation of ACE in an UVC-LED enhanced photo-Fenton process. The ACE at a concentration of $100\,\mu g\,L^{-1}$ in synthetic secondary effluent could be removed within 20 min by adding (1 + 1 + 1) mg L⁻¹ Fe²⁺ (sequential iron dosage) and 12 mg L⁻¹ H₂O₂. They also compared the performance of various photo-Fenton processes (UV/TiO2, UV/H2O2, and UV/persulfate (UV/PS)) for the abatement of ACE from water [22]. Among them, the UV/H₂O₂ and UV/PS processes exhibited great potential for the removal of ACE from deionized water and synthetic secondary treated wastewater. However, some important points need to be further elucidated. For example, the degradation behavior of ACE by the AOPs is not comparatively investigated. The underlying degradation mechanism especially in the UV/PS process has yet been clearly revealed. The effective degradation of ACE in natural waters deserves to be further investigated.

To fulfill the abovementioned gaps, the ACE degradation by UV/ H_2O_2 and UV/PS processes was particularly focused in this study. The influences of environmental conditions (solution pH, inorganic anions, natural organic materials (NOM)) on the degradation processes were systematically investigated. Specifically, the degradation behaviors in natural waters (river water, lake water, and treated wastewater) were tentatively studied for the first time. Moreover, the degrees of mineralization and degradation products were detected, respectively. Finally, the contributions of the reactive oxidative species were distinguished.

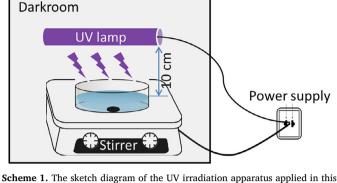
2. Materials and methods

2.1. Materials

High purity ACE (99%) was obtained from Jiangsu Changqing Agrochemical Co. Ltd., China. The basic information of ACE was listed in Table 1. Reagent-grade hydrogen peroxide (35 wt%), potassium persulfate (99.9%) were purchased from Aladdin, China. All the other reagents used in this study were obtained from Sinopharm, China or Aladdin, China and used without further purification. Solutions used in

 Table 1

 The basic information of the insecticide acetamiprid.



Scheme 1. The sketch diagram of the UV irradiation apparatus applied in this study.

the experiments were prepared with deionized water from a water purification system (EPED-S2).

The river water, lake water, and secondary effluent (SE) of wastewater were collected from Yangtze river (YR), Taihu lake (TL), and wastewater treatment facility located in a local insecticide factory, respectively. The fresh water samples were filtered with qualitative filter paper (Whatman, GE) upon arrival and stored under 4°C in a refrigerator.

2.2. Experimental procedure

As given in Scheme 1, the degradation experiments were conducted in an air-conditioned darkroom (~25 °C). A glass dish served as the reactor was placed under a Philips UV lamp (851 mm in length, 55 W, emission at 253.7 nm). The distance between the lamps and the liquid level was approximately 10 cm. The thickness of the ACE solution (50 mL) was around 1 cm to ensure the radiation intensity in the mixture. Due to the low power of the lamp and the distance between lamp and solution, the temperature of reaction mixture was not significantly changed during irradiation process. Therefore, no cooling system was applied in this study and the water loss through evaporation was negligible. The ACE solution was magnetically agitated (~50 rpm) to maintain the homogeneity throughout the reaction. The solution pH was adjusted by using 0.1 M H₂SO₄ or NaOH. Water samples were collected at regular time intervals and quenched with equal volume of methanol immediately to stop the reactions. Each experiment was conducted for at least 2 times and the average and standard deviations were reported. The effects of inorganic anions and organic matter on the degradation process were also investigated respectively.

For the radical-quenching studies, excess methanol and *tert*-butanol were added into the solution prior to the oxidants. According to the distinct reaction rate constants, the *tert*-butanol could consume HO-prior to the organic pollutants while methanol could scavenge HO- and SO_4 effectively [23,24].

For the determination of degradation products, the treated ACE solution was concentrated with a solid phase extraction cartridge (WAT106202, Waters Oasis). The HLB cartridge was pre-activated prior to the use with 5 mL methanol and 5 mL Milli-Q water, respectively. The final extracted sample was obtained by eluting with 4 mL methanol

Molecule	MW (g mol ⁻¹)	Structure	p <i>K</i> a	Water solubility $(mg L^{-1})$	Logk _{ow}	Henry's law constant (atm m ³ mol ⁻¹)	Vapor pressure (mm Hg)
C ₁₀ H ₁₁ ClN ₄	222.676	CI N N N C N	0.7	4250	0.8	6.9×10^{-8}	4.4×10^{-5}

 $(2 \text{ mL} \times \text{twice}).$

2.3. Kinetic analysis

The degradation of organic compounds by AOPs usually follows the pseudo-first-order kinetics (especially for the initial period) [25–29]. The derived apparent rate constant (k) could indicate the rate of the whole reaction to some extent. Therefore, the pseudo-first-order kinetic model shown in Eq. (1) was adopted to mimic the degradation kinetics in this study.

$$\ln\left(\frac{C_t}{C_0}\right) = -kt \tag{1}$$

where C_0 is initial concentration of ACE, C_t is concentration of ACE at time t, k is the apparent pseudo-first order constant. By plotting $\ln (C_t/C_0)$ versus t, k can be graphically calculated.

2.4. Determination of the second-order rate constants

Competition kinetic approaches were applied to determine the second-order rate constants of HO \cdot and SO₄ $\dot{}$ with ACE, using *para*-chlorobenzoic acid (pCBA) and *meta*-toluic acid (mTA) as competitors [24,30]. Experiments were conducted in phosphate buffer (PB) at pH 7. Concentrations of ACE and competitors were 90 μ M and 100 μ M, respectively. The concentrations of H₂O₂ and PS were 12 mM and 2 mM, respectively. Noting that, although SO₄ $\dot{}$ can react with OH $^-$ to generate HO \cdot in UV/PS system, the reaction could be neglected at pH 7 [31]. Detailed information for competition kinetic methods was shown in Supporting Information Text S1.

2.5. Analytical methods

The concentration of ACE was measured using a high performance liquid chromatograph (HPLC, FL 2200) equipped with a C 18 column. Aliquots of 20 μL were injected manually through an injection loop. Column temperature was held at 25 °C, mobile phase was consisted of acetonitrile (35%) and water (65%), and the flow rate was 0.8 mL min $^{-1}$. Acetamiprid was monitored at 248 nm (ACE absorption maximum) with the retention time being 8.1 min. The UV spectrum of ACE solution was recorded with a Cary 50 spectrophotometer (VARIAN). TOC of the water samples were determined by a Shimadzu TOC VCSH analyzer with an ASI-V auto sampler. COD_{Cr} and total salinity of the real waters were measured according to the standard method [32]. Inorganic anions were detected by using an ion chromatography (Thermo ICS 900). pH value was determined with a pH meter (Leici).

The Agilent 1200 series HPLC coupled with an Agilent G6410B triple quadrupole (QQQ) mass spectrometer (Agilent Technologies, USA) was adopted for the detection of degradation products. The detailed operation conditions of the HPLC-MS were given in Supporting Information Text S2.

3. Results and discussion

3.1. Degradation of ACE in deionized water

Fig. 1 shows the overall degradation performance of ACE by UV, UV/H_2O_2 and UV/PS processes. Due to the refractory property, the ACE could not be decomposed effectively with only chemical oxidants (H_2O_2 or PS). Accordingly, no more than 15% of the degradation rate was observed within 60 min. On the other hand, near 30% ACE was reduced with the direct UV irradiation. This reduction was probably attributed to the direct photolysis of organic compounds [33]. The direct photolysis was highly dependent on the decadic molar absorption coefficient of the compound at a certain wavelength [34]. The results meant that

ACE could absorb the photons in UV radiation with wavelength at 254 nm, agreeing well with the UV spectrum of ACE solution which showed a remarkable absorption peak at 220-260 nm (Fig. S1). Kim and Tanaka [35] investigated the degradation of over 30 kinds of pharmaceutical and personal care products (PPCPs) with UVC irradiaclassified tion and them into easily-degrading **PPCPs** slowly-degrading $(k \ge 2.6 \times 10^{-3} \,\mathrm{s}^{-1})$ and **PPCPs** $(k < 6.4 \times 10^{-4} \,\mathrm{s}^{-1})$. In this case, the k of ACE during the UV treatment was around $8.3 \times 10^{-5} \, \text{s}^{-1}$, belonging to the slowly-degrading PPCP.

With the UV radiation, the chemical oxidants such as H_2O_2 and PS can be transferred into powerful free radicals through the following reactions [36,37].

$$H_2O_2 + h\nu \rightarrow 2HO$$
 (2)

$$S_2O_8^{2-} + hv \rightarrow 2SO_4^{\cdot -}$$
 (3)

As a result, the UV based AOPs (UV/PS and UV/H2O2) possessed significantly enhanced degradation performance (Fig. 1). Over 60% of ACE was removed from the aqueous solution within 60 min by the UV/ H₂O₂ process. Meanwhile, almost complete degradation was achieved by the UV/PS process. The remarkably accelerated degradation processes revealed that there should be a synergistic effect between UV radiation and chemical oxidants. Moreover, the higher k value clearly indicated that the UV/PS process was much more effective than the UV/H₂O₂ process in degrading ACE (Fig. S2). It was also the case for the degradation of antiepileptic drug carbamazepine and azo dye [22,38,39]. This was probably due to that PS was more photosensitive than H₂O₂ [40], resulting a higher radical production yield in the UV/ PS process [41]. However, it was not the case for the degradation of antipyrine [42]. The degradation rate of antipyrine followed the order of UV/H₂O₂ > UV/PS. The probable reason was that the reactivity (second-order rate constant) of organic compounds with different radical species was different [27].

To verify this hypothesis and identify the contributions of HO \cdot and SO $_4$ $\dot{}^-$ in the degradation process, the corresponding second-order rate constants were determined by competition kinetics. The derived second-order rate constants of ACE with HO \cdot and SO $_4$ $\dot{}^-$ were calculated to be 7.59 \times 10 8 and 3.68 \times 10 8 M $^{-1}$ s $^{-1}$, respectively (Fig. S3). Therefore, the distinct reactivity of ACE with different radical species could probably be ruled out because of the comparable second-order rate constant.

3.2. Effect of oxidant dosage

Fig. 2 depicts the degradation profiles of ACE in UV/H₂O₂ and UV/ PS processes with different oxidant dosage (expressed in terms of [Oxidant]/[ACE] ratio). Generally, the degradation rate would be proportional to the amount of radicals at the low concentrations of chemical oxidants. However, the excess oxidants would inhibit the degradation process due to the self-scavenging effect [29,36]. In this case, the degradation rate constant increased with the [H₂O₂]/[ACE] ratio, indicating the concentration of H2O2 was below the inhibition point [38]. On the other hand, the rate constant was nearly unchanged when the [PS]/[ACE] ratio is higher than 20. Moreover, the degradation rate constants exhibited a linear relationship with the oxidant $k = 0.00081 \times ([H_2O_2]/[ACE]) + 0.00352$ $(UV/H_2O_2:$ $([H_2O_2]/[ACE] < 30)$ and $k = 0.00019 \times ([H_2O_2]/[ACE]) + 0.0314$ $([H_2O_2]/[ACE] > 60); UV/PS: k = 0.0049 \times ([PS]/[ACE]) - 0.028,$ ([PS]/[ACE] < 20)) [42,43]. As shown in Fig. 2C, the slope was significantly reduced when the [H₂O₂]/[ACE] ratio was higher than 60, meaning the increase rate of k reduced. Similarly, the slope was absolutely near 0 when the [PS]/[ACE] ratio was higher than 20. This was probably due to the self-scavenging effect. Similar phenomenon was also reported in previous study [44].

Noting that, the ACE could not be efficiently removed in the UV/

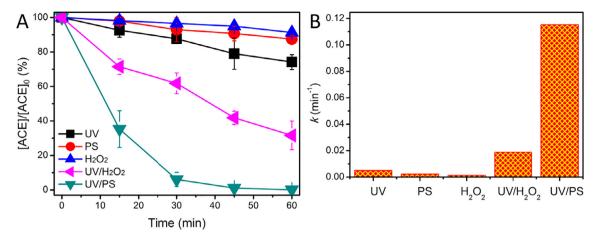


Fig. 1. The overall degradation performance of ACE in UV, PS, H_2O_2 , UV/PS, and UV/H_2O_2 systems (A), and the corresponding pseudo-first-order kinetic rate constant (B). ([ACE] = 90 μ M, $[H_2O_2] = [K_2S_2O_8] = 1.5 \,\text{mM}$, pH = 7, $T = 25\,^{\circ}\text{C}$).

 H_2O_2 system unless the $[H_2O_2]/[ACE]$ was higher than 65. Therefore, we conducted the following experiments with the $[H_2O_2]/[ACE]$ was 130 ($[H_2O_2] = 11.8$ mM, [ACE] = 90 µM).

3.3. Effect of solution pH

Fig. 3 presents the degradation of ACE at different pH values. The results clearly indicated that both of the processes were highly dependent on the solution pH. As well known, the solution pH played two important roles during the degradation process. Firstly, the active oxidation species in the solution was greatly influenced by the solution pH [45]. Secondly, the organic compounds would be transferred into

different forms according to their specific pKa(s) under varied solution pHs, leading to the distinct reactivity towards radical species [46]. For this study, the pKa of ACE was 0.7, far below the studied pH values. The difference of degradation rate brought by the different dissociated forms of ACE could be therefore excluded. Besides, the reduction of ACE resulted from the hydrolysis at different pH values could be ignored because the hydrolysis process is rather time-consuming (took for several days) [7].

For the UV/ H_2O_2 process, the degradation was significantly inhibited under basic conditions. This was probably due to the reduction of oxidation power of HO· because the redox potential $E_{\rm HO·,H2O}$ decreased from 2.62 to 2.15 V with pH increasing from 3 to 11 (derived

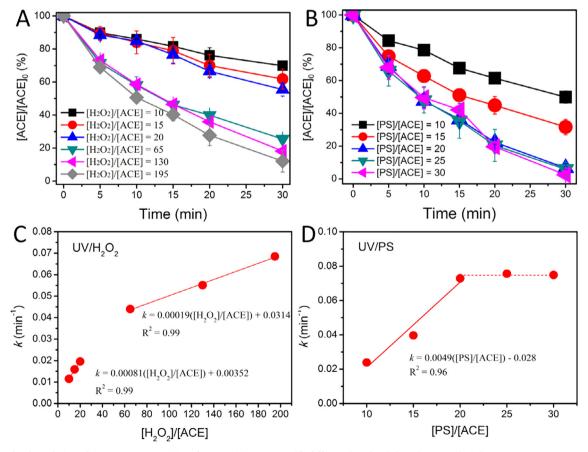


Fig. 2. The degradation of ACE in UV/H_2O_2 (A) and UV/PS (B) systems with different [Oxidant]/[ACE] ratios. ([ACE] = $90 \, \mu M$, pH = 7, $T = 25 \, ^{\circ}C$).

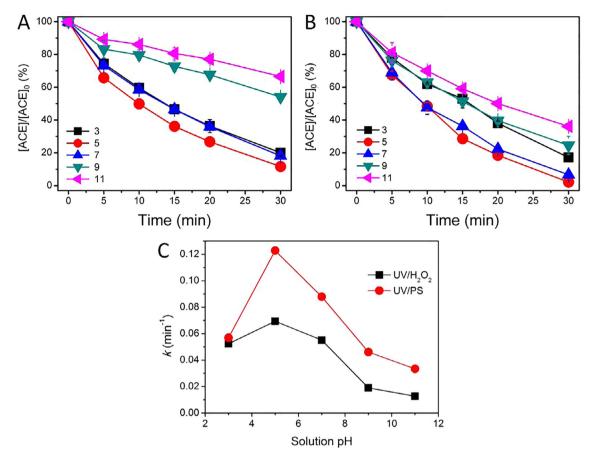


Fig. 3. The degradation of ACE in UV/H_2O_2 (A) and UV/PS (B) systems at different solution pHs. ([ACE] = 90 μ M, $[H_2O_2]$ = 11.8 mM, $[K_2S_2O_8]$ = 1.5 mM, T = 25 °C).

from Nernst equation) [27]. In addition, the reaction between OH⁻ and HO· would be enhanced at basic conditions through Eq. (4) [30]. The generated O· was less reactive with a redox potential of only 1.78 V. Noticeably, when the pH came to 11, the predominant form of H₂O₂ would be the hydroperoxide anion HO_2^- [47], which possessed a much higher UV₂₅₄ absorption coefficient than H₂O₂ [48]. The much higher UV₂₅₄ absorption coefficient of HO₂⁻ might significantly depress the decomposition of H₂O₂ to HO· under UV irradiation. Moreover, the $\mathrm{HO_2}^-$ exhibited a much higher reaction rate constant with $\mathrm{HO}\cdot$ (Eq. $k = 7.5 \times 10^9 \,\mathrm{M}^{-1} \,\mathrm{s}^{-1}$ [49]) than $(k = 2.7 \times 10^7 \,\mathrm{M}^{-1} \,\mathrm{s}^{-1}$ [30]), making it a strong scavenger towards HO. Therefore, the reduction of the redox potential of HO. and the scavenging effects of OH⁻/HO₂⁻ both accounted for the lower ACE degradation rate at higher pH value.

$$OH^{-} + HO^{\cdot} \rightarrow H_{2}O + O^{\cdot -}$$
 (4)

$$HO_2^- + HO^- \to OH^- + HO_2^-$$
 (5)

$$OH^{-} + SO_{4}^{-} \rightarrow HO^{-} + SO_{4}^{2} - pH = 11$$
 (6)

For the UV/PS process, a similar inhibition phenomenon was observed for the high pH conditions. This was because the HO· was massively generated through the reaction between SO_4 . and OH^- (Eq. (6)) at high pH condition [24]. The generated HO· possessed slow rate constant (as demonstrated in Fig. 1). On the other hand, the SO_4 was the predominant radical species under the acidic condition [26].

Overall, the acidic and neutral conditions were favorable for the ACE degradation in UV based AOPs. This was also in consistent with a previous work that reported the photolysis of ACE was favorable in acidic ($k=0.0119\,\mathrm{min}^{-1}$ at pH = 4) and neutral conditions whilst depressed in basic condition ($k=0.0061\,\mathrm{min}^{-1}$ at pH = 9) [28].

3.4. Effect of aqueous matrix species

The inorganic anions and natural organic matters (NOM) ubiquitously occurred in natural water bodies usually participate in the degradation process during the field applications of the UV based AOPs and bring positive/negative effects on the removal performance. Therefore, chloride (Cl $^-$), bicarbonate (HCO $_3^-$), nitrate (NO $_3^-$), and humic acid (HA) were selected in this case to investigate their potential effects on the ACE degradation by UV/H $_2$ O $_2$ and UV/PS processes.

It was reported that Cl $^-$ could scavenge active radicals (HO \cdot and SO $_4$ $^-$) to form less reactive species (ClOH $^-$, Cl \cdot and Cl $_2$ $^-$) through Eqs. (7–10), leading to a decreased degradation efficiency [23,30]. Consequently, as shown in Fig. 4, the degradation process was clearly depressed in the both processes. Similarly, Zhang et al. [27] indicated that the presence of Cl $^-$ reduced the degradation of azathioprine in both UV/H $_2$ O $_2$ and UV/PS systems. Compared with UV/PS process, the negative effect of Cl $^-$ on UV/H $_2$ O $_2$ process was much more insignificant. This was probably attributed to that the few ClOH $^-$ could rapidly revert back to Cl $^-$ and HO \cdot under neutral condition (Eq. (11)) [23]. Moreover, the ratio of [Cl $^-$]/[Oxidant] was relatively low in UV/H $_2$ O $_2$ system compared with that in UV/PS system, which also might be the plausible reason for the weak inhibition.

 HCO_3^- could also react with $HO \cdot$ and $SO_4^{\cdot -}$ to produce $CO_3^{\cdot -}$, a less reactive species (Eqs. (12) and (13)). Thus, the inhibition of the degradation process was usually expected in the presence of HCO_3^- . However, quite interestingly, this was not the case in the present study. As shown in Fig. 4, HCO_3^- in the concentration of 5–15 mM brought negative effect on UV/PS process, whilst slightly promoted the ACE degradation by UV/H_2O_2 process. Liu et al. [44] also reported that the HCO_3^- promoted the degradation of oxytetracycline by UV/H_2O_2 and

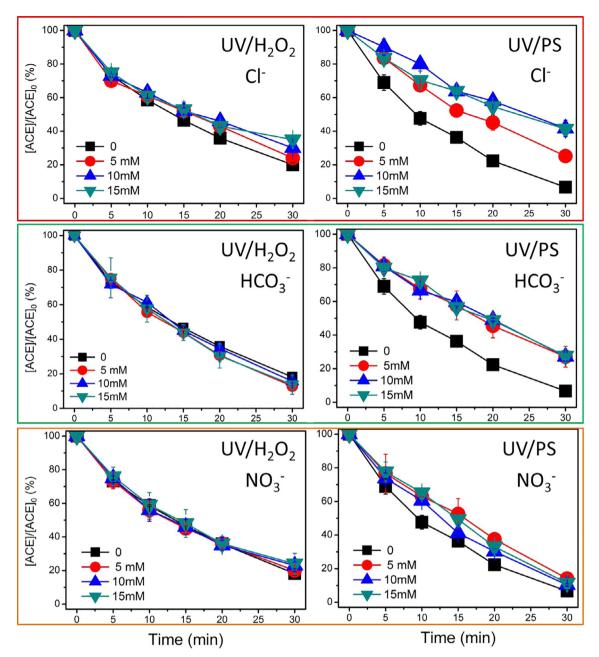


Fig. 4. Effects of Cl^- , HCO_3^- , and NO_3^- on the degradation of ACE in UV/H_2O_2 and UV/PS systems. ([ACE] = 90 μ M, [H₂O₂] = 11.8 mM, [K₂S₂O₈] = 1.5 mM, pH = 7, T = 25 °C).

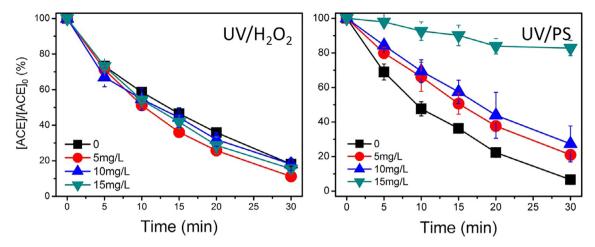
UV/PS processes. The adverse effects were probably dependent on the concentration of HCO_3^- . In contrast, NO_3^- did not give rise to an obvious positive/negative effects on the degradation processes. This was probably due to its slow reaction rates with radical species (Eq. (14)).

HA generally plays two important roles in the UV based AOPs, radical scavenger and UV absorption agent [50]. It was reported that the second-order rate constant of Suwannee River Humic Acid (SRHA) with SO_4 $\dot{}$ was 2.35 \times 10 7 M^{-1} s $^{-1}$ [51], which was much lower than that with HO $\dot{}$. Therefore, SRHA played a lower scavenging effect in UV/PS process than UV/H₂O₂ process. On the other hand, HA could also lead to a photosensitization process involving reactive oxygen species by absorbing UV radiation and enhance the degradation process. As shown in Fig. 5, the dose of HA clearly brought negative effects on the ACE degradation by UV/PS process. The similar phenomenon was well documented in previous works [25,50]. Noticeably, the degradation

rate was significantly reduced to < 20% in the UV/PS process when the dose of HA was $15\,\mathrm{mg}\,L^{-1}$, probably indicating its low efficiency in treating NOM-rich wastewater. On the contrary, the degradation process was slightly improved in the UV/H₂O₂ system with the low dose of HA (5 mg L^{-1}). Tan et al. [42] found that the low level of HA (2.5 mg L^{-1}) was beneficial (catalytic effect) while high level of HA was inhibitory (scavenging effect) for the degradation process. In this case, the dosage of HA (5–15 mg L^{-1}) was relatively low when comparing with that of H₂O₂. However, this dosage was higher in the UV/PS system because the concentration of $K_2S_2O_8$ was only 1.5 mM. This result clearly suggested that the effect of HA was also dependent on its concentration. In other words, the negative effects of HA could be crippled by increasing the dosage of chemical oxidants.

$$Cl^- + HO \rightarrow ClOH^- - k = 4.3 \times 10^9 M^{-1} s^{-1}$$
 (7)

$$ClOH^{-} + H^{+} \rightarrow Cl^{-} + H_{2}O \quad k = 3.0 \times 10^{10} \quad M^{-1}s^{-1}$$
 (8)



 $\textbf{Fig. 5.} \ \ \text{Effect of HA on the degradation of ACE in UV/H}_2O_2 \ \ \text{and UV/PS systems.} \ \ ([ACE] = 90 \ \mu\text{M}, \ [H}_2O_2] = 11.8 \ \text{mM}, \ [K}_2S_2O_8] = 1.5 \ \text{mM}, \ pH = 7, \ T = 25 \ \text{°C}).$

(12)

$$ClOH' + Cl^{-} \rightarrow Cl_{2}'^{-} + OH^{-} \quad k = 1.0 \times 10^{5} \ M^{-1} \ s^{-1}$$
 (9)

$$Cl^- + SO_4^{--} \rightarrow Cl^- + SO_4^{2-} \quad k = 3.1 \times 10^8 \, M^{-1} \, s^{-1}$$
 (10)

$$ClOH^{-} \rightarrow Cl^{-} + HO^{-} \quad k = 6.0 \times 10^{9} \, M^{-1} s^{-1}$$
 (11)

$$HCO_3^- + HO \rightarrow CO_3^{--} + H_2 O \quad k = 8.5 \times 10^6 M^{-1} s^{-1}$$

$$HCO_3^- + SO_4^- \rightarrow CO_3^- + HSO_4^- \quad k = 9.1 \times 10^6 M^{-1} s^{-1}$$
 (13)

$$NO_3^- + SO_4^- \rightarrow NO_3^+ + SO_4^{2-}$$
 $k = 5 \times 10^4 M^{-1} s^{-1}$ (14)

3.5. Identification of radical species

The active radical species in the UV base AOPs were identified by using methanol and tert-butanol as radical scavengers. According to their distinct reactivity towards HO and SO4 $^-$, their respective contributions to the ACE degradation were distinguished [23,24]. Specifically, the decrease of the degradation rate after adding tert-butanol was attributed to the contribution of HO \cdot . Similarly, the decrease observed after adding methanol was attributed to the total contributions of HO \cdot and SO4 $^-$.

As depicted in Fig. 6, only HO \cdot contributed for the ACE degradation by UV/H₂O₂ process while both HO \cdot and SO₄ $\dot{}$ contributed in UV/PS process. The occurrence of HO \cdot in the UV/PS process was reasonable because the reaction between SO₄ $\dot{}$ and H₂O (Eq. (15)). Moreover, the main reactive radical species was HO \cdot while SO₄ $\dot{}$ played a minor role during the degradation process in the UV/PS process. Similarly, the HO \cdot made a non-negligible contribution during the degradation of β -

lactam antibiotics in the UV/PS system [26].

$$SO_4^{-} + H_2O \rightarrow HO^{-} + SO_4^{-2} + H^{+} \quad k < 60 \ M^{-1} \, s^{-1} \ (pH = 7)$$
 (15)

3.6. TOC variation

The degree of mineralization during the ACE degradation process was respectively assessed and the results were given in Fig. 7. The complete mineralization usually takes a much longer time compared with the partly decomposition of organic compounds due to the generation of recalcitrant intermediates [50]. As shown, though the ACE could be completely removed within 1 h, the TOC removal rate was even lower than 40%. After 2 h's treatment, the TOC removal rate achieved 50% for the UV/PS process, while it was only 26.6% for the UV/H₂O₂ process. The results clearly revealed that a large part of ACE was transformed into intermediates rather than completely mineralized. Similarly, up to 50% of TOC was removed within 6 h though the ACE diminished in the first minute of the Fenton process [7]. The poor TOC reduction was extensively reported in the degradation processes of other organic compounds by UV based AOPs [26].

In addition, a remarkable difference between the two processes in terms of the TOC removal was also presented. The UV/PS process exhibited a much higher TOC removal efficiency than the UV/ H_2O_2 process, which was in well agreement with the ACE elimination profiles (Fig. 1). Similar results had been reported in previous studies [27,52]. Considering the lower second-order rate constant between SO_4 and ACE and the minor contribution of SO_4 , the higher TOC removal rate

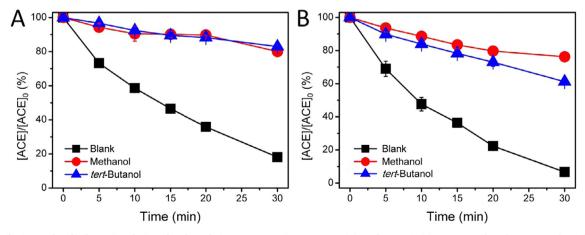


Fig. 6. Contributions of radical species during the degradation processes in UV/H_2O_2 (A) and UV/PS (B) systems. ([ACE] = 90 μ M, $[H_2O_2]$ = 11.8 mM, $[K_2S_2O_8]$ = 1.5 mM, [Methanol] = [tert-Butanol] = 1 M, pH = 7, T = 25 °C).

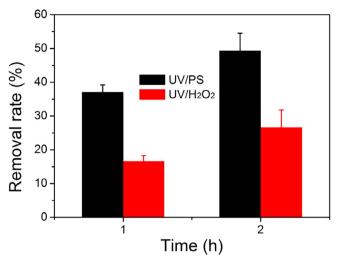


Fig. 7. The variations of TOC during the degradation process. ([ACE] = 90 μ M, [H_2O_2] = 11.8 mM, [$K_2S_2O_8$] = 1.5 mM, pH = 7, T = 25 °C).

was probably attributed to the more generated HO \cdot in UV/PS than in UV/H₂O₂ process.

3.7. Degradation products

Due to the distinct reaction mechanisms between free radicals and organic compounds [53], different products might be generated by UV/ H_2O_2 and UV/PS processes [27,42]. The degradation product was directly related with the degree of mineralization (TOC removal efficiency) and toxicity of effluent. As shown in Fig. 7, the TOC removal efficiency was lower than 40% within 1 h while the ACE was absent, indicating the ACE was partly transformed into intermediates other than completely mineralized. Therefore, the ultimate degradation products were analyzed through HPLC-MS.

As shown in the HPLC spectra (Fig. 8), several peaks were clearly

Table 2The characteristics of the real waters.

Item	YR	TL	SE
$COD_{Cr} (mg L^{-1})$	< 5 ^a	< 5 ^a	429 ± 12.7
$TOC (mg L^{-1})$	1.644	3.315	139.4
TIC $(mg L^{-1})$	26.3	31.58	304.7
Salinity (g/L)	0.53	0.95	9.75
$Cl^{-} (mg L^{-1})$	19.35	20.47	16.8
$NO_3^- (mg L^{-1})$	1.63	0.15	1.58
pH	7.30	6.98	8.07

^a The values are under the limitations of detection according to the standard detection method.

observed, indicating that the ACE was transformed into several intermediates. This was well agreed with the preceding TOC results. In addition, more products were identified in the UV/PS process, which was not strange because both HO \cdot and SO₄. presented in UV/PS process while only HO \cdot was detected in UV/H₂O₂ process (Fig. 7). The HO-non-selectively attacked the organic compounds mainly through hydrogen abstraction or electrophilic addition mechanism [48]. On the other hand, SO₄. was more likely to do that through the electron transfer reactions [30].

For the identification of the degradation intermediates, the mass spectra was recorded and given in Fig. 8C. The protonated ACE molecular possessed a charge-to-mass ratio (m/z) of 223.2. It was documented that the hydroxylated product (M-OH) was usually detected in the $HO \cdot$ and $SO_4 \cdot^-$ induced degradation processes [27]. For example, the hydroxylated ACE (with m/z 239.0) was found in a previous study which investigated the degradation of ACE with Fenton process [54,55]. As in this case, the molecular ion peak with an m/z of 238.9 was detected, which was therefore assigned to the hydroxylated ACE (+16 Da). In addition, the intermediate with an m/z of 209.0 was also identified in the both oxidation processes. According to the previous study, the demethylation reaction usually occurred in the free radical induced oxidation process [27]. Therefore, this intermediate could be assigned to the demethylated derivative (-14 Da) [54,56].

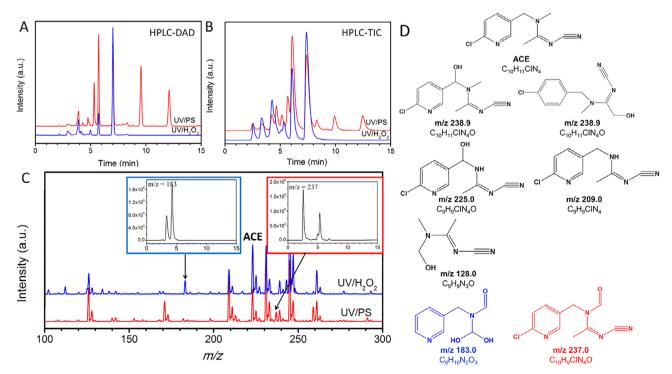


Fig. 8. HPLC (A: diode array detector (DAD) chromatogram, B: total ion chromatogram (TIC)), corresponding mass spectra (C), and proposed structure (D) of the ACE degradation products in UV/H_2O_2 and UV/PS systems. Inset of C shows the extracted ion chromatograms (EIC) of m/z 171, 183, and 259, respectively.

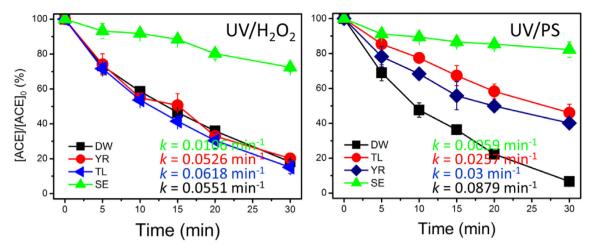


Fig. 9. Degradation of ACE by UV/H_2O_2 and UV/PS systems in different water matrices. ([ACE] = $90\,\mu\text{M}$, $[H_2O_2] = 11.8\,\text{mM}$, $[K_2S_2O_8] = 1.5\,\text{mM}$, pH = 7, $T = 25\,^{\circ}\text{C}$).

Noticeably, we also found some unique peaks in different oxidation processes. For example, the molecular ion peaks at m/z 171 (-52 Da), 237 (+14 Da), and 259 (+36 Da) were only observed in UV/PS process while absent in UV/H₂O₂ process. Among them, the structure of the product with m/z of 237 was proposed based on the previous study [54]. However, the structures of the other two products were still obscure and need to be further characterized in the future. Similarly, the molecular ion peak at m/z 183 (-40 Da) was only observed in the UV/H₂O₂ process. Sirtori et al. [54] proposed a non-chlorinated molecular ion ($C_8H_{10}N_2O_3$, m/z 183) during the degradation of ACE by Fenton process based on the four fragment ions (155, 137, 109, 68). According to the previously documented structures of the byproducts of ACE, the possible structures of the degradation intermediates detected in this study were proposed (Fig. 8D). Nevertheless, more evidences were needed to confirm the proposed structures.

3.8. Degradation of ACE in real waters

The feasibility of the UV based AOPs in degrading ACE from real waters (TL, YR, and SE) was evaluated in this study. The characteristics of the collected real waters were presented in Table 2.

Due to the occurrence of high level NOM and salinity, the degradation process was significantly inhibited in SE by both UV/H2O2 and UV/PS processes (Fig. 9). The degradation rate constants decreased from $0.0551\,\text{min}^{-1}$ and $0.0879\,\text{min}^{-1}$ to $0.0106\,\text{min}^{-1}$ and 0.0059 min⁻¹, respectively. Noticeably, the UV/H₂O₂ process performed better stability than UV/PS, agreeing well with the results shown in Figs. 4 and 5. Moreover, probably ascribed to the extremely high concentration of TOC, the promotion effect brought by the HA in UV/H₂O₂ process (Fig. 5) disappeared. Large amounts of NOM would scavenge the reactive radical species and compete for the UV radiation, remarkably inhibiting the generation of radical species. The concentrations of inorganic anions were comparable among the three types of real waters. According to the preceding discussion, the relatively low concentrations (< < 5 mM) of Cl⁻ and NO₃⁻ in the real waters would not produce significant negative effects on the degradation process. Therefore, it was concluded that the NOM occurred in the real water played a vital role in the ACE degradation by UV based AOPs. Xiao et al. [50] compared the degradation of iodoacids from river water, treated water, and SE by UV/H2O2 and UV/PS processes, respectively. Similarly, they found the worst degradation rate in the SE no matter for the UV/H₂O₂ or UV/PS process. This result suggests that a pretreatment for the removal of NOM was necessary for the application of UV based AOPs in some real waters such as SE.

In addition, the degradation process was moderately decreased in

TL and YR water compared with in DW for the UV/PS process. Probably due to the relatively low concentration of TOC, the degradation rate constant was higher in YR than in TL. On the other hand, the degradation of ACE in TL and YR was comparable with that in DW for the UV/H_2O_2 process. This was well agreed with the results in Fig. 5.

4. Conclusions

This paper evaluated the ACE degradation by UV/H_2O_2 and UV/PSprocesses. The combination of UV and chemical oxidants (H₂O₂ or PS) significantly improved the degradation of ACE. Specifically, UV/PS process showed better degradation performance than UV/H2O2 at the same dosage of PS and H₂O₂ probably due to the higher radical yield in UV/PS process. Moreover, the degradation process was highly dependent on the solution pH. Inorganic anions ubiquitously existed in natural waters exhibited negative effects on the degradation process due to the scavenging effect except NO₃⁻. Humic acid significantly inhibited the degradation process due to the scavenging effect and competition of radiation. Only HO· contributed to the degradation process by UV/ H₂O₂ while both HO⋅ and SO₄. were responsible for the degradation of ACE in UV/PS process. The corresponding second-order rate constants of ACE with HO \cdot and SO₄ $^{\cdot}$ were determined to be 7.59 \times 10⁸ and $3.68 \times 10^8 \, \text{M}^{-1} \, \text{s}^{-1}$, respectively. Different degradation products were detected in the two processes. Eventually, the degradation process was inhibited to some extent in real waters, especially in the secondary effluent of wastewater.

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Appendix A. Supplementary data

Supplementary data associated with this article can be found, in the online version, at http://dx.doi.org/10.1016/j.cej.2018.06.107.

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