Dimensional reduced modelling of the heart

A model for the blood flow

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Introduction

- The model accounts for the pressure gradient and the function of the valves.
- 3D model not required to describe the heart: lumped 0D model is simpler and faster to implement.
- Numerical solution with appropriate integrator of ODEs for 14 compartments, to model behavior of pressure, volume, and flow rate.

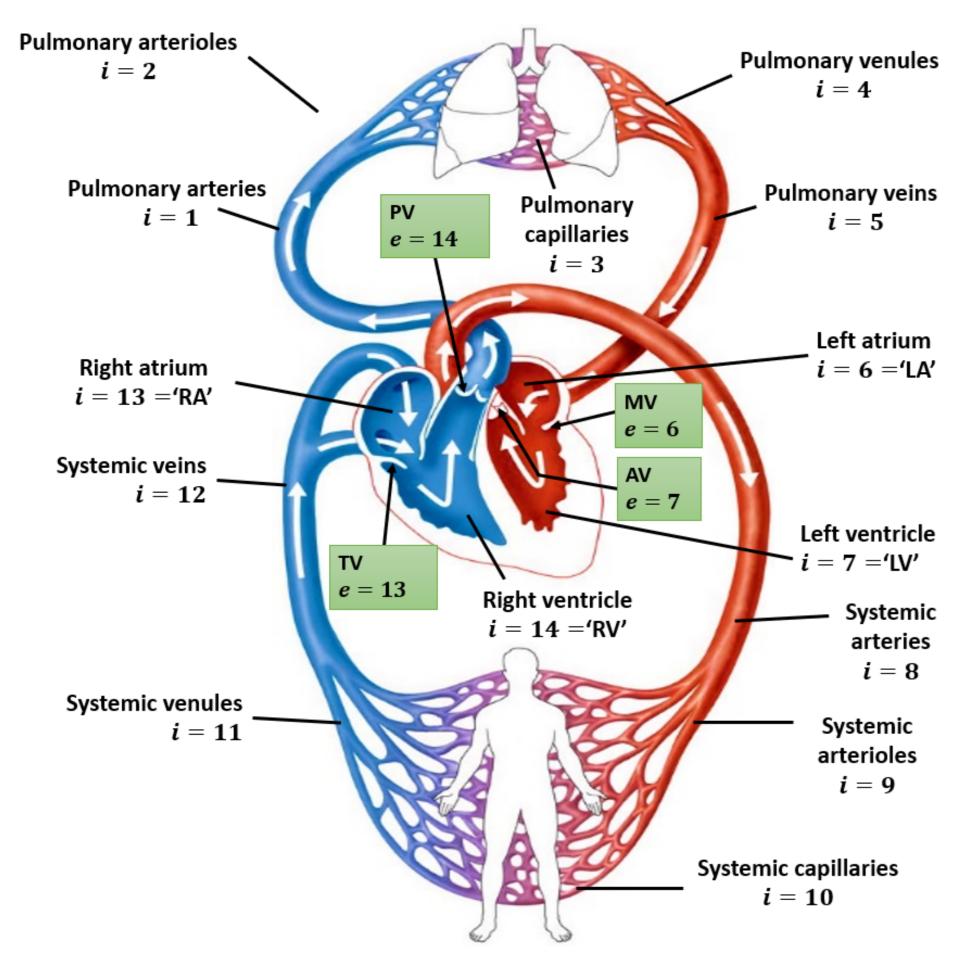


Figure 1: Schema of human cardiovascular system: heart, pulmonary and systemic circulation⁽⁵⁾. In increasing order of edges e, the valves are the mitral valve, aortic valve, tricuspid valve, and pulmonary valve.

Main Objectives

- 1. Formulation of mathematical model
- 2. Efficient and stable MATLAB simulation
- 3. Graphical User Interface to allow variation of parameters

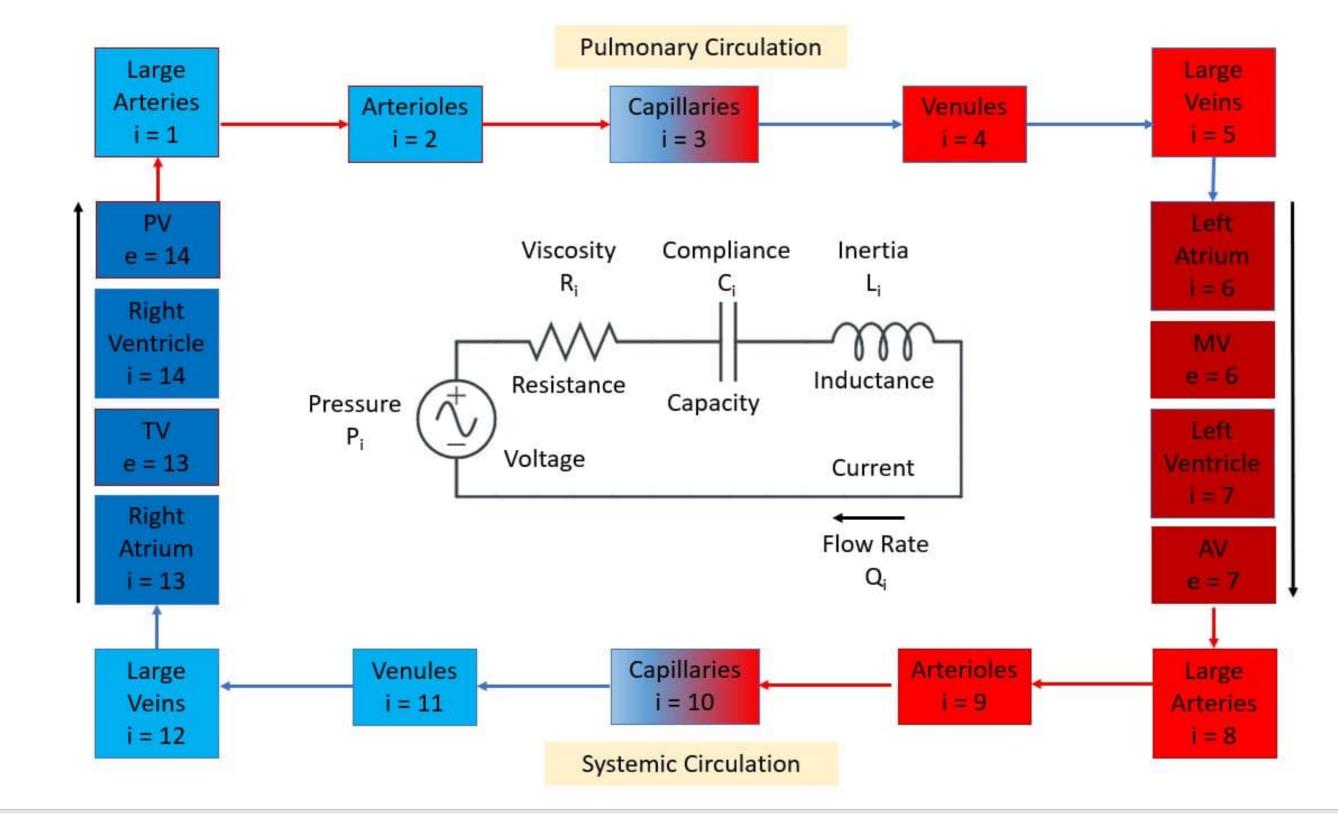


Figure 2: Comparison between model parameters and electrical circuits

Mathematical Section

- Index $i \in \{1, ..., 14\}$ represents the compartments, while $e \in \{1, ..., 14\}$ the edges (input/output) of respective compartment.
- $V_i(t)$ represents the volume of compartment i, $P_i(t)$ the pressure, and $Q_e(t)$ the flow rate at edge e.
- Opening coefficient for the valve in edges $e \in \{6, 7, 13, 14\}$ inside the heart, denoted by $O_e(t)$.

Each volume and flow rate follow an Ordinary differential equation:

 $\dot{V}_i(t) = Q_{in}(t) - Q_{out}(t)$ for each compartment i and its adjacent edges (1) $L_e \dot{Q}_e(t) = P_i(t) - P_{i+1}(t) - R_e Q_e(t) - B_e Q_e(t) |Q_e(t)|$ for each edge e adjacent to the heart (2) $L_e \dot{Q}_e(t) = P_i(t) - P_{i+1}(t) - R_e Q_e(t)$ for edges e not connected to any heart chamber (3)

Where L_e is the inertia and R_e , the viscosity at edge e. The turbulence produced by the heart valves is denoted by B_e . Observe that the turbulence term introduces a point of non-differentiability in our model.

Pressure follows an algebraic equation:

 $[1 - 0.0005(Q_{e-1}(t) - Q_e(t))] P_i(t) = E_i(t)(V_i(t) - V_{0,i})$ for each heart chamber i and edges (4) $C_i P_i(t) = V_i(t) - V_{0,i}$ for each compartment i outside heart (5)

Where C_i is the compliance, $V_{0,i}$ the dead volume and $E_i(t)$ the elasticity function of compartment i. The opening coefficients follow an Ordinary differential equation:

 $C_{d,e}\dot{O}_e(t) = 0.5\left[1 + \tanh\left(C_{v,e}(P_i(t) - P_{i+1}(t))\right)\right] - O_e(t)$ for each heart valve in edge e (6)

Lastly, a post-processing for the valve edges takes place:

 $Q_e(t) = O_e(t)Q_e(t)$ for each heart valve in edge e (7)

Method

- System solved using Runge-Kutta-Fehlberg 4(5) method: lower computational cost
- When flow is zero, non differentiability of ODE: classical RK4 plus approximation of solution as an alternative to Fehlberg's adaptive stepsize computation
- Coexistence of adaptive stepsize with root detection: RK method applied only when the ODE is differentiable

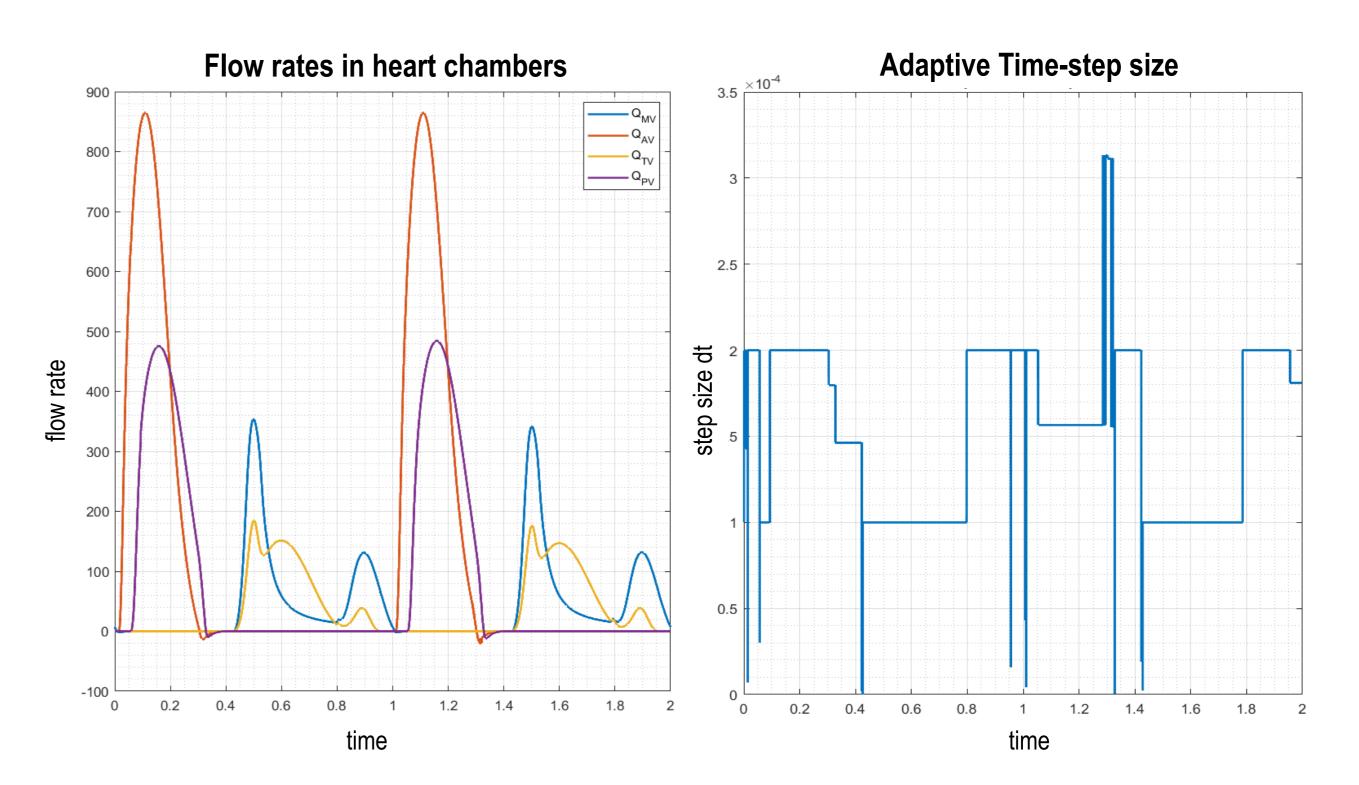


Figure 3: Left: Flow rate in heart cavities. Right: Variation of step size along time.

Results

- Variation of heart rate and elasticity affects the other parameters
- Solved the problem of the computation at points with no differentiability.

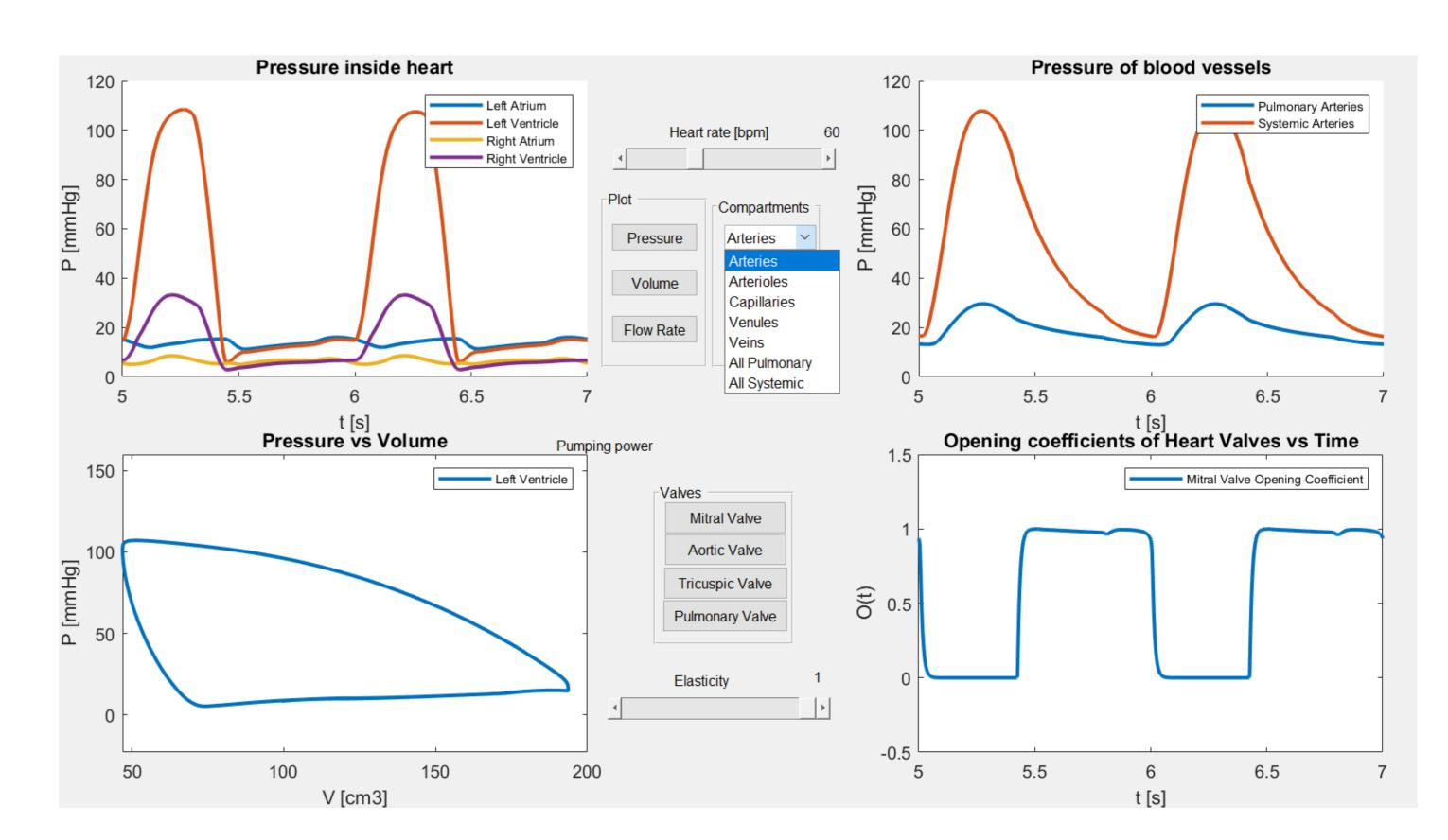


Figure 4: Preliminary Graphical User Interface to show the dependence of Pressure, Volume and Flux on Time, Heart Rate and Elasticity

Forthcoming Research

- Numerical solver: more efficient and accurate
- GUI: variation of heartbeat and elasticity
- Valves: more accurate equations
- Present research on website of partner institution:
- High Performance Computing Center Stuttgart (HRLS)

References and Acknowledgements

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