# Robust Control of Nonlinear Systems

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SMART LAB TECHNICAL SEMINAR
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# Robust Control of Nonlinear Systems

Weekly Plan

#### Week 1 (today)

- Nonlinear Systems
- Robust Control
- Sliding Mode Control (Theoretical)

#### Week 2

- Example problem control formulation with implementation notes (Applied)
- Introduction to and MATLAB/SIMULINK implementation

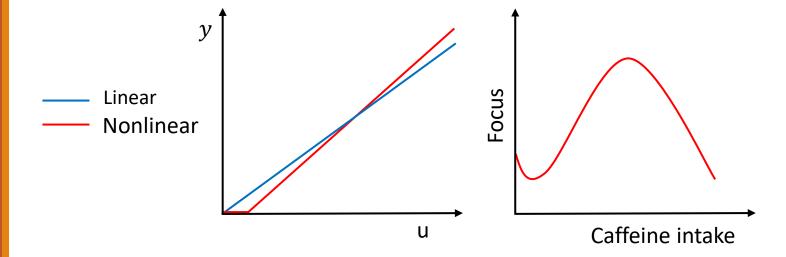
Week 1

## Linear vs. Nonlinear Systems

Linear systems follow the Superposition principle and are Homogeneous.

$$F(u_1) = y_1 F(u_2) = y_2 F(u_1 + u_2) = y_1 + y_2$$

$$F(u) = y$$
$$F(au) = ay$$

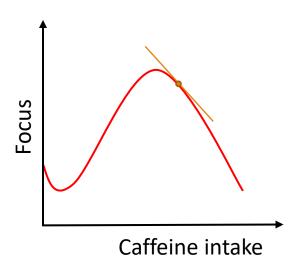


Nonlinear Systems <u>do not</u> follow the Superposition principle nor are homogeneous.

Most systems in real life are nonlinear!

### Control Strategies

#### **Linear Control of Linearized Nonlinear Systems**



Nonlinear Systems maybe **linearized** around operating points to apply linear control methods.

#### However,

- Inefficient control input
- Performance not as good as it could be
- Fixed control law cannot accommodate system if system state goes outside the operating region

#### **Nonlinear Control of Nonlinear Systems**

**Nonlinear Control Methods:** 

- Feedback Linearization
- Backstepping Control
- Sliding Mode Control

Nonlinear Control Analysis tools:

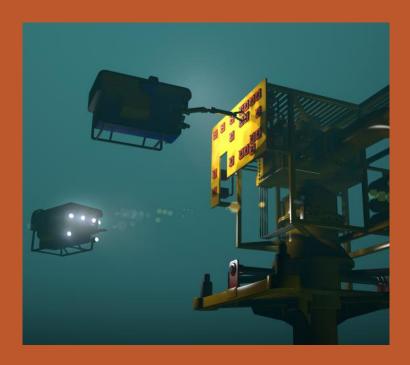
- Lyapunov methods
- Limit Cycles
- Describing Functions

However, each one has its own advantages and disadvantages.

Nonlinear Control Theory still an active field of research!

# Uncertainty and unmodeled dynamics in Nonlinear Systems

Importance of controller robustness



#### Examples:

UUV underwater pipeline inspection

<u>Imperfect plant data</u> - each plant is slightly different because of the tolerances associated with individual components.

<u>Time varying plants</u> - The dynamics of some plants vary over time. A fixed control model may not accurately depict the plant at all times.

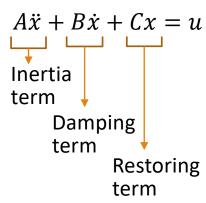
<u>Modelling error</u> - Mechanical and electrical systems are inherently complex to model. Even a simple system requires complex differential equations to describe its behavior.

<u>External disturbance</u> – changing environmental conditions change operating conditions; a fixed controller may not be able to reject disturbance effects

# Nonlinear Systems with uncertainty and unmodeled dynamics

Activity

2<sup>nd</sup> order differential equation model:



#### **Activity (4 min)**

What nonlinear systems do you deal with in your research?
List some unmodeled dynamics and uncertainties involved with your method

- you do not need equations
- think about what affects as inertia, damping, restoring force in your systems

## Robust Control Theory

An approach to controller design that explicitly deals with plant uncertainty.

Designed to function properly provided that <u>uncertain parameters</u> or <u>disturbances</u> are found within some (typically compact) set.

Aim to achieve robust performance and/or stability in the presence of bounded modelling errors.

#### Example control methods:

- High gain feedback
- H-infinity loop shaping
- Loop transfer recovery (LTR) for Linear quadratic Gaussian (LQG) control
- Sliding Mode Control

Developed by <u>Vadim Utkin</u> (Russian control theorist; currently a professor at Ohio State University)

- Deals explicitly with uncertainty in its approach to controller design
- Tend to be able to cope with small differences between the true system and the nominal model used for design

A nonlinear control method that alters the dynamics of a nonlinear system by application of a discontinuous control signal (or more rigorously, a set-valued control signal) that forces the system to "slide" along a cross-section of the system's normal behavior.

The sliding-mode control scheme involves

- 1. Selection of a hypersurface or a manifold (i.e., the sliding surface) such that the system trajectory exhibits desirable behavior when confined to this manifold.
- 2. Finding feedback gains so that the system trajectory intersects and stays on the manifold.

Consider the n<sup>th</sup> order scalar nonlinear system:

$$x^{n} = f(x, \dot{x}, ..., x^{n-1}, t) + b(x, \dot{x}, ..., x^{n-1}, t)u$$
  
 $\underline{x} > 0$ 

Trajectory tracking error:

$$\tilde{x}(t) = x(t) - x_d(t)$$

Goal: 
$$\tilde{x}(t) \rightarrow 0$$

In real systems, f and b are never exactly known. Modelling errors exist.

Modeling inaccuracies can be classified into two major kinds:

- structured (or parametric) uncertainties
- unstructured uncertainties (or unmodeled dynamics)

But under operating conditions we can estimate upper and lower bounds on these parametric uncertainties.

$$|\hat{f}(\underline{x},t) - f(\underline{x},t)| \le F(\underline{x},t)$$
  $|\hat{b}(\underline{x},t) - b(\underline{x},t)| \le B(\underline{x},t)$  (Estimate) (actual) (bound)

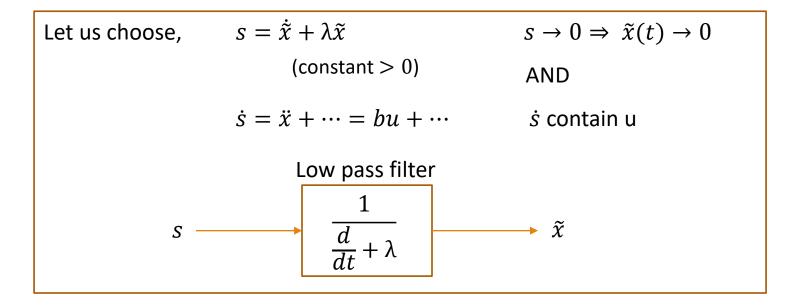
$$\ddot{x} = f(\underline{x}, t) + b(\underline{x}, t)u$$
  
$$\tilde{x}(t) = x(t) - x_d(t)$$

Step 1: Create intermediate variable s  $\dot{s}$  contains u  $s \to 0 \Rightarrow \tilde{x}(t) \to 0$ 

Step 1: "Replace" the n<sup>th</sup> order problem with an equivalent 1<sup>st</sup> order problem.

Create intermediate variable s, such that  $s \Rightarrow \begin{cases} s \text{ contains} \\ s \to 0 \Rightarrow \tilde{x} \end{cases}$ 

Consider, for n=2: 
$$\ddot{x} = f + bu$$
  
We could pick  $s = \dot{x}$   $\dot{s}$  contains  $u$   
or,  $s = \dot{x} - \dot{x}_d = \dot{\tilde{x}}$   $but s \not\rightarrow 0 \not\Rightarrow \tilde{x}(t) \not\rightarrow 0$   
or,  $s = \tilde{x}$   $but s \rightarrow 0 \Rightarrow \tilde{x}(t) \rightarrow 0$   
 $\dot{s}$  does not contain  $u$ 



$$\ddot{x} = f(\underline{x}, t) + b(\underline{x}, t)u$$
  
$$\tilde{x}(t) = x(t) - x_d(t)$$

Step 1: Create intermediate variable s  $\dot{s}$  contains u  $s \to 0 \Rightarrow \tilde{x}(t) \to 0$ 

For the general case,

$$s = \left(\frac{d}{dt} + \lambda\right)^{n-1} \tilde{\chi}$$

(n-1)<sup>th</sup> order stable linear filter

$$\tilde{x} \longrightarrow \frac{1}{(\frac{d}{dt} + \lambda)^{n-1}}$$

$$\dot{s}$$
 contain  $\frac{d}{dt}x^{(n-1)}=x^{(n)}$ , and therefore, u

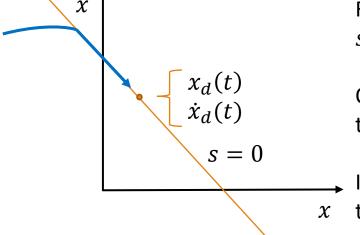
$$s \to 0 \Rightarrow \tilde{x}(t) \to 0$$

Geometrically (visually) what does it look like?

Considering the 2<sup>nd</sup> order system,

$$s = \dot{\tilde{x}} + \lambda \tilde{x}$$
  
$$s \to 0 \Rightarrow \tilde{x}(t) \to 0$$

For the general n-th order case, s = 0 looks like a <u>hyperplane</u>.



Once on this surface in finite time, the state remains there.

It slides along the surface x towards  $\underline{x}_d(t)$ .

$$\ddot{x} = f(\underline{x}, t) + b(\underline{x}, t)u$$
  
$$\tilde{x}(t) = x(t) - x_d(t)$$

Step 1: Create intermediate variable s  $\dot{s}$  contains u  $s \to 0 \Rightarrow \tilde{x}(t) \to 0$ 

What if, as  $t \to \infty$ , we can only guarantee  $|s| \le \varphi$ ? (constant)

For n=2, 
$$s = \dot{\tilde{x}} + \lambda \tilde{x}$$
 
$$s(t) \xrightarrow{s(t)} \frac{1}{(\frac{d}{dt} + \lambda)^{n-1}} \tilde{x}(t)$$
 
$$|s(t)| \leq \varphi$$
 After transient

$$\tilde{x}(t) = (\text{effect of I.C.}) + \int_0^t e^{-\lambda(t-\tau)} s(r) dr$$

$$\to 0 \qquad \text{Upper bound}$$

$$\Rightarrow 1 \int_0^t 1 \le \int_0^1 |\dots| \le \varphi \int_0^1 e^{-\lambda(t-\tau)} dr \le \frac{\varphi}{\lambda}$$
For n=n,
$$\text{n-1 filters}$$

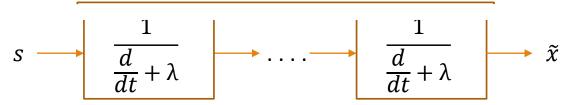
$$s \qquad \frac{1}{\frac{d}{dt} + \lambda} \qquad \tilde{x} \le \frac{\varphi}{\lambda^{n-1}}$$

## Activity

Recall, we design hyperplane as,

$$s = \left(\frac{d}{dt} + \lambda\right)^{n-1} \tilde{x}$$





For n=2, it was

$$s = \dot{\tilde{x}} + \lambda \tilde{x}$$

#### **Activity (3 min)**

Derive s for (n=3)  $3^{rd}$  order system in terms of  $\tilde{x}$  and  $\lambda$ 

#### **Answer**

For n=2, it was 
$$s = \dot{\tilde{x}} + \lambda \tilde{x}$$
 For n=3, 
$$s = \left(\frac{d}{dt} + \lambda\right) \left(\dot{\tilde{x}} + \lambda \tilde{x}\right)$$
$$= \ddot{\tilde{x}} + 2\lambda \dot{\tilde{x}} + \lambda^2 \tilde{x}$$

# Example Problem:

$$\ddot{x} = f(\underline{x}, t) + b(\underline{x}, t)u$$
  
$$\tilde{x}(t) = x(t) - x_d(t)$$

Step 1: Create intermediate variable s  $\dot{s}$  contains u  $s \to 0 \Rightarrow \tilde{x}(t) \to 0$ 

Consider a 2<sup>nd</sup> order scalar system:

$$\ddot{x} + a(t) \, \dot{x}^2 \cos 3x = u$$

with  $1 \le a(t) \le 2$ 

We can choose,

$$\hat{f} = -1.5 \, \dot{x}^2 \cos 3x$$
 So that, 
$$F = 0.5 \, \dot{x}^2 |\cos 3x|$$

Design 
$$s = \dot{\tilde{x}} + \lambda \tilde{x}$$
 
$$\dot{s} = \ddot{\tilde{x}} + \lambda \dot{\tilde{x}}$$
 
$$= \ddot{x} - \ddot{x}_d + \lambda \dot{\tilde{x}}$$
 
$$= f + bu - \ddot{x}_d + \lambda \dot{\tilde{x}}$$

We choose a control law that makes  $\dot{s}=0$ , if we knew exactly the dynamics of f, i.e.  $\hat{f}=f$ ,  $\hat{u}=-\hat{f}+\ddot{x}_d-\lambda\dot{\tilde{x}}$ 

Therefore, plugging in 
$$\mathbf{u} = \hat{u}$$
, We get,  $\dot{s} = f - \hat{f}$ 

### Sliding Condition

$$\ddot{x} = f(\underline{x}, t) + b(\underline{x}, t)u$$
  
$$\tilde{x}(t) = x(t) - x_d(t)$$

Step 1: Create intermediate variable s  $\dot{s}$  contains u  $s \to 0 \Rightarrow \tilde{x}(t) \to 0$ 

Step 2: Determine rate of convergence based on the Sliding Condition

We know the system converges to s=0, But how do we ensure that it happens within a finite time?

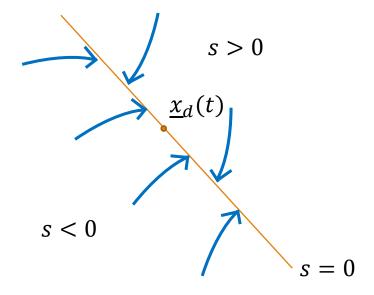
We choose control input u, such that

$$\frac{d}{dt}s^2 \le 0$$

More precisely,

$$\frac{1}{2}\frac{d}{dt}s^2 \le -\eta|s|$$

i.e. we want s to decrease to its absolute value at the rate described by



$$\dot{s}\dot{s} \leq -\eta s'$$
If we solved for time, t
We get,  $t \leq \frac{|s(t=0)|}{\eta}$ 

Therefore, s = 0 is reached in a finite time!

# Continuing the previous example:

$$\ddot{x} = f(\underline{x}, t) + b(\underline{x}, t)u$$
  
$$\tilde{x}(t) = x(t) - x_d(t)$$

Step 1: Create intermediate variable s

Step 2: Determine rate of convergence based on the Sliding Condition

Step 3: Determine Control Law

#### Example problem formulation so far:

$$\ddot{x} + a(t) \ \dot{x}^2 \cos 3x = u$$
with  $1 \le a(t) \le 2$ 

We had  $\hat{f} = -1.5 \, \dot{x}^2 \cos 3x$ 

So that,  $F = 0.5 \dot{x}^2 |\cos 3x|$ 

Design,  $s = \dot{\tilde{x}} + \lambda \tilde{x}$  $\dot{s} = \ddot{\tilde{x}} + \lambda \dot{\tilde{x}}$ 

We chose,  $\hat{u} = -\hat{f} + \ddot{x}_d - \lambda \dot{\tilde{x}}$ 

To get,  $\dot{s} = f - \hat{f}$ 

We previously got, For

$$\dot{s} = f - \hat{f}$$

$$\hat{u} = -\hat{f} + \ddot{x}_d - \lambda \dot{\tilde{x}}$$

Following the Sliding Condition,

$$\frac{1}{2}\frac{d}{dt}s^2 = s\dot{s} = s(f - \hat{f})$$

Does not say much about the rate of convergence of s.

We could modify u such that the rate is accounted for:

Trying,  $u = \hat{u} - k \operatorname{sgn}(s)$ 

Following the Sliding Condition,

$$\frac{1}{2}\frac{d}{dt}s^2 = s\dot{s} = s(f - \hat{f}) - k\operatorname{sgn}(s) \le -\eta|s|$$

For this condition to hold,

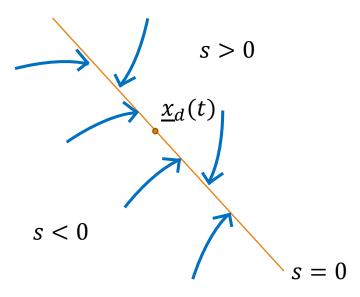
$$k = F + \eta$$

So the new control law would be,

$$u = \hat{u} - k \operatorname{sgn}(s)$$
  
=  $(1.5 \dot{x}^2 \cos 3x + \ddot{x}_d - \lambda \dot{\tilde{x}}) - (0.5 \dot{x}^2 |\cos 3x| + \eta) \operatorname{sgn}(\dot{\tilde{x}} + \lambda \tilde{x})$ 

# SMC switching control law:

Switching control law:  $u = \hat{u} - (F + \eta) \operatorname{sgn}(s)$ 



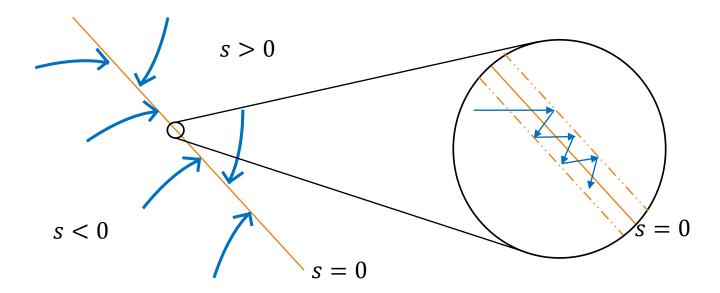
As desired state  $\underline{x}_d$  changes , the hyperplane s shifts on the n-dimensional space.

The controller forces the system to go to s = 0.

# SMC switching control law:

Disadvantage: Control chattering

Switching control law:  $u = \hat{u} - (F + \eta) \operatorname{sgn}(s)$ 



Bigger F (uncertainty bounds) means bigger discontinuity in the control signal due to the *sgn* term.

Chattering occurs at full range  $k=(F+\eta)$ . The overshooting occurs due to system sampling, computation time.

(Maybe okay for certain systems/applications utilizing PWM, but without it, s does not tend to zero, but remains close to it.)

# Sliding Mode Control Theory Summary

Consider the nth order scalar nonlinear system:

$$x^{n} = f(x, \dot{x}, ..., x^{n-1}, t) + b(x, \dot{x}, ..., x^{n-1}, t)u$$

$$|\hat{f}(\underline{x},t) - f(\underline{x},t)| \le F(\underline{x},t)$$
  $|\hat{b}(\underline{x},t) - b(\underline{x},t)| \le B(\underline{x},t)$ 

Trajectory tracking error:

$$\tilde{x}(t) = x(t) - x_d(t)$$

$$\tilde{x}(t) \rightarrow 0$$

Create intermediate variable s, such that  $s \Rightarrow \begin{cases} \dot{s} \text{ contains } u \\ s \to 0 \Rightarrow \tilde{x} \to 0 \end{cases}$ Step 1:

$$s = \left(\frac{d}{dt} + \lambda\right)^{n-1} \tilde{x}$$

$$s \Rightarrow \begin{cases} s \text{ contains } u \\ s \to 0 \Rightarrow \tilde{x} \to 0 \end{cases}$$

Determine rate of convergence based on the Sliding Condition Step 2:

$$\frac{1}{2}\frac{d}{dt}s^2 \le -\eta|s|$$

<u>Step 3:</u> Determine switching control Law

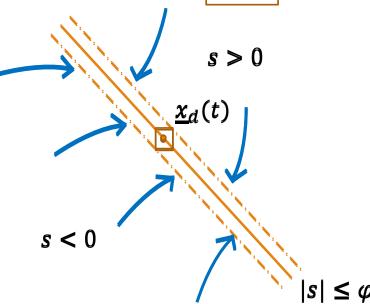
$$u = \hat{u} - k \operatorname{sgn}(s)$$

where,

$$\mathbf{k} = (F + \mathbf{\eta})$$

### Conclusion

Switching control law:  $u = \hat{u} - (F + \eta) \operatorname{sgn}(s)$ 



Chattering occurs within bounds  $\varphi$ .

The control law must be modified to "<u>smoothen</u>" the control signal for implementation.

#### Therefore, Week 2:

- Example problem control formulation with implementation notes (Applied)
- Introduction to and MATLAB/SIMULINK implementation

# Thank you

#### **Control design activity:**

Consider a 2<sup>nd</sup> order scalar system:

$$\ddot{x} + \dot{x}\cos 3a(t)x = u$$

with 
$$1 \le a(t) \le 2$$

Good luck!!

# Robust Control of Nonlinear Systems

Tamzidul Mina

Week 2

#### Introduction to SIMULINK

Simple example – building blocks on SIMULINK

Example problem controller design

Example problem SIMULINK implementation

Example problem <u>chatter free</u> controller improvement

Example problem SIMULINK implementation

Design and implement your own controller!

### Brief Introduction to Simulink

Simulink® is a block diagram environment for multi-domain simulation and Model-Based Design.

#### It supports:

- system-level design
- simulation
- automatic code generation
- continuous test and verification of embedded systems.

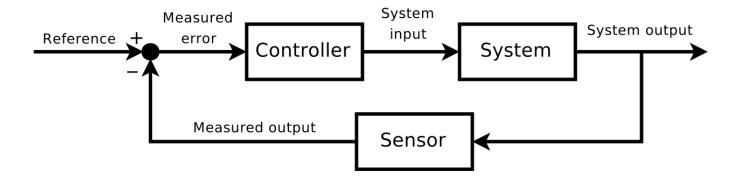
#### Simulink provides:

- customizable block libraries
- solvers for modeling and simulating dynamic systems.

It is integrated with MATLAB®, enabling you to incorporate MATLAB algorithms into models and export simulation results to MATLAB for further analysis.

## SIMULINK – Getting Started

Create your first block



Lets start your MATLAB and dive right in!

Open MATLAB, type Simulink in the command window and hit enter

#### Tasks:

SIMULINK overview

## SIMULINK – Getting Started

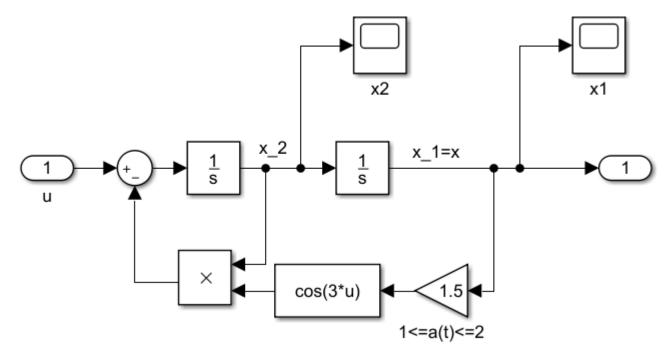
Create your first block

#### **Create the following plant model as a block:**

$$\ddot{x} + \dot{x}\cos 3a(t)x = u \qquad \text{with } 1 \le a(t) \le 2$$

Trajectory tracking error:

$$\tilde{x}(t) = x(t) - x_d(t)$$
 Goal:  $\tilde{x}(t) \to 0$ 



Start with a 'subsystem' block to create this.

### Example Problem:

$$\ddot{x} = f(\underline{x}, t) + b(\underline{x}, t)u$$
  
$$\tilde{x}(t) = x(t) - x_d(t)$$

Step 1: Create intermediate variable s

Step 2: Determine rate of convergence based on the Sliding Condition, n

Step 3: Determine Control Law

Consider a 2<sup>nd</sup> order scalar system:

$$\ddot{x} + a(t) \, \dot{x}^2 \cos 3x = u$$

with 
$$1 \le a(t) \le 2$$

Write this as:

$$\ddot{x} = -a(t) \, \dot{x}^2 \cos 3x + u$$

So that.

We can choose, 
$$\hat{f} = -1.5 \, \dot{x}^2 \cos 3x$$
  
So that,  $F = 0.5 \, \dot{x}^2 |\cos 3x|$ 

Design of sliding manifold:

$$s = \dot{\tilde{x}} + \lambda \tilde{x}$$

$$\dot{s} = \ddot{\tilde{x}} + \lambda \dot{\tilde{x}} = \ddot{x} - \ddot{x}_d + \lambda \dot{\tilde{x}}$$

$$= f + bu - \ddot{x}_d + \lambda \dot{\tilde{x}}$$

We choose a control law that makes  $\dot{s} = 0$ , if we knew exactly the dynamics of f, i.e.  $\hat{f} = f$ ,

$$\hat{u} = -\hat{f} + \ddot{x}_d - \lambda \dot{\tilde{x}}$$

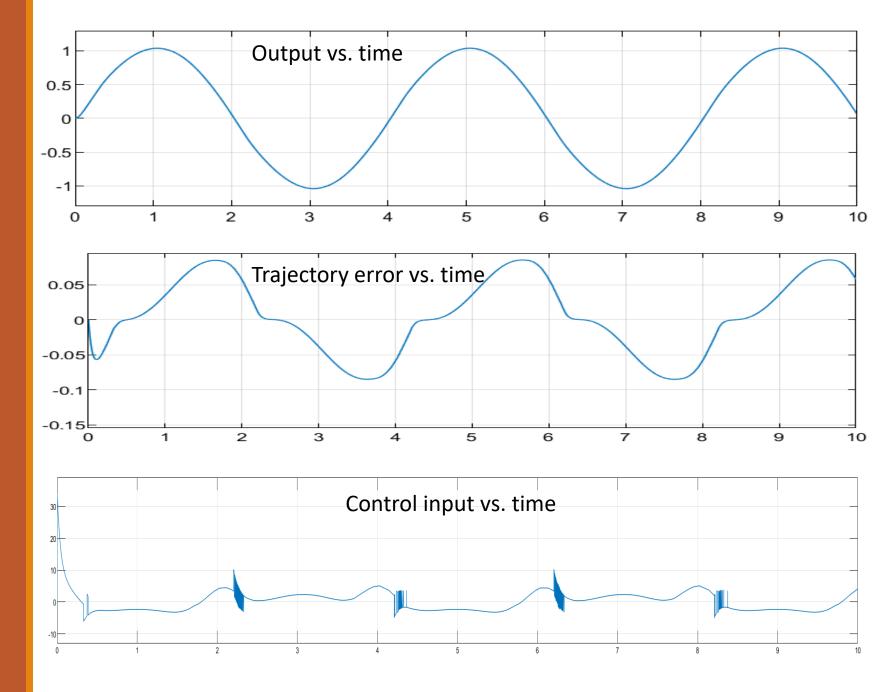
$$u = \hat{u} - k \operatorname{sgn}(s)$$

$$= (1.5 \dot{x}^2 \cos 3x + \ddot{x}_d - \lambda \dot{\tilde{x}}) - (0.5 \dot{x}^2 |\cos 3x| + \eta) \operatorname{sgn}(\dot{\tilde{x}} + \lambda \tilde{x})$$

Download file: SlidingMode sign.mdl

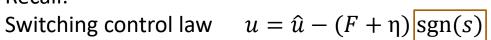
From https://github.com/tmina01/robust-control

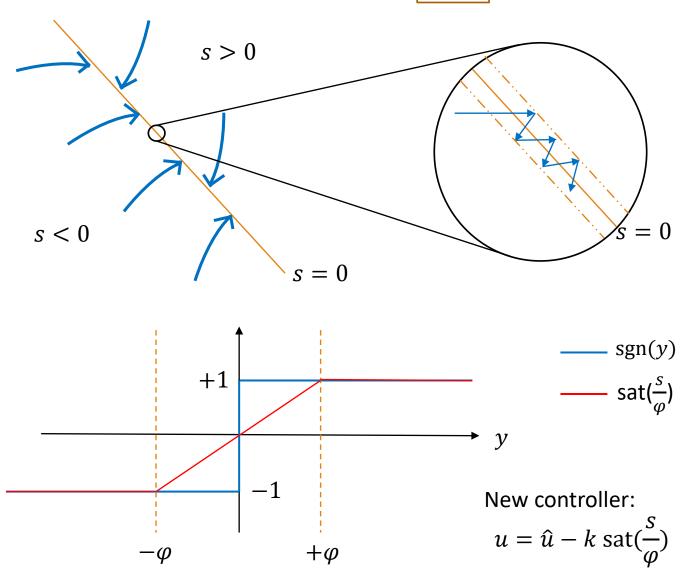
### Results



# Control chatter smoothing

Recall:

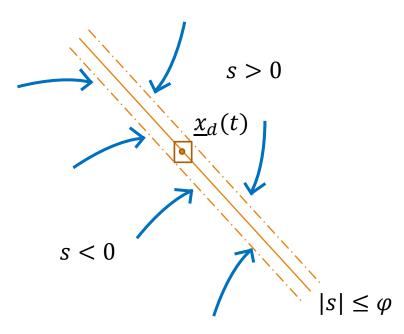




# Control chatter smoothing

How do we design  $\varphi$ ?

Inside the  $|s| \le \varphi$  region:



Step 2: Outside the  $\varphi$  region, i.e.  $|s| \ge \varphi$ ; since k(x, t), the Sliding Condition becomes:

$$\frac{1}{2}\frac{d}{dt}s^2 \le (\dot{\varphi} - \eta)|s|$$

i.e. if  $\varphi$  is decreasing, the system must converge to within the boundary layer faster than the rate  $\varphi$  is shrinking.

Step 3: Determine switching control Law:  $u=\hat{u}-k \ \mathrm{sat}(\frac{s}{\varphi})$  where,  $k=(F+\eta-\dot{\varphi})$   $\dot{\varphi}=k_d-\lambda\varphi$ 

# Chatter free control of example problem:

$$\ddot{x} = f(\underline{x}, t) + b(\underline{x}, t)u$$
  
$$\tilde{x}(t) = x(t) - x_d(t)$$

Step 1: Create intermediate variable s

Step 2: Determine rate of convergence based on the Sliding Condition, n

Step 3: Determine Control Law

Consider a 2<sup>nd</sup> order scalar system:

$$\ddot{x} + a(t) \, \dot{x}^2 \cos 3x = u$$

with 
$$1 \le a(t) \le 2$$

Write this as:

$$\ddot{x} = -a(t) \ \dot{x}^2 \cos 3x + u$$

So that,

We can choose, 
$$\hat{f} = -1.5 \, \dot{x}^2 \cos 3x$$
  
So that,  $F = 0.5 \, \dot{x}^2 |\cos 3x|$ 

Design of sliding manifold:

$$s = \dot{\tilde{x}} + \lambda \tilde{x}$$

$$\dot{s} = \ddot{\tilde{x}} + \lambda \dot{\tilde{x}} = \ddot{x} - \ddot{x}_d + \lambda \dot{\tilde{x}}$$

$$= f + bu - \ddot{x}_d + \lambda \dot{\tilde{x}}$$

We choose a control law that makes  $\dot{s} = 0$ , if we knew exactly the dynamics of f, i.e.  $\hat{f} = f$ ,

$$\hat{u} = -\hat{f} + \ddot{x}_d - \lambda \dot{\tilde{x}}$$

$$u = \hat{u} - k \operatorname{sat}(\frac{s}{\varphi})$$

$$= (1.5 \dot{x}^2 \cos 3x + \ddot{x}_d - \lambda \dot{\tilde{x}}) - (0.5 \dot{x}^2 | \cos 3x | + \eta - \dot{\varphi}) \operatorname{sat}(\frac{s}{\varphi})$$

Download file: SlidingMode sat.mdl

from https://github.com/tmina01/robust-control

# Controller performance observations

#### Tasks:

- How does the two controller designs compare?
- Change a(t) for both controllers and observe changes
  - In what range for a(t) does the controller prove to be robust?
  - Find the value of a(t) for which the controller starts to fail.
- Change  $\lambda$  and  $\eta$  and observe controller performance.

# Design a controller for the following system

#### **Control design activity:**

Consider a 2<sup>nd</sup> order scalar system:

$$\ddot{x} + \dot{x}\cos 3a(t)x = u$$

with 
$$1 \le a(t) \le 2$$

Good luck!!

### Example Problem:

$$\ddot{x} = f(\underline{x}, t) + b(\underline{x}, t)u$$
  

$$\tilde{x}(t) = x(t) - x_d(t)$$

Step 1: Create intermediate variable s

Step 2: Determine rate of convergence based on the Sliding Condition, η

Step 3: Determine Control Law

Consider a 2<sup>nd</sup> order scalar system:

$$\ddot{x} + \dot{x}\cos 3a(t)x = u$$

with 
$$1 \le a(t) \le 2$$

Write this as:

$$\ddot{x} = -\dot{x}\cos 3a(t)x + u$$

So that,

We can choose, 
$$\hat{f} = -\dot{x}\cos 3(1.5)x$$
  
So that,  $F = \dot{x}\cos 3(0.5)x$ 

Design of sliding manifold:

$$s = \dot{\tilde{x}} + \lambda \tilde{x}$$

$$\dot{s} = \ddot{\tilde{x}} + \lambda \dot{\tilde{x}} = \ddot{x} - \ddot{x}_d + \lambda \dot{\tilde{x}}$$

$$= f + bu - \ddot{x}_d + \lambda \dot{\tilde{x}}$$

We choose a control law that makes  $\dot{s} = 0$ , if we knew exactly the dynamics of f, i.e.  $\hat{f} = f$ ,

$$\hat{u} = -\hat{f} + \ddot{x}_d - \lambda \dot{\tilde{x}}$$

$$u = \hat{u} - k \operatorname{sgn}(s)$$
  
=  $(\dot{x} \cos 3(1.5)x + \ddot{x}_d - \lambda \dot{\tilde{x}}) - (\dot{x} \cos 3(0.5)x + \eta) \operatorname{sgn}(\dot{\tilde{x}} + \lambda \tilde{x})$ 

# Chatter free control of example problem:

$$\ddot{x} = f(\underline{x}, t) + b(\underline{x}, t)u$$
  
$$\tilde{x}(t) = x(t) - x_d(t)$$

Step 1: Create intermediate variable s

Step 2: Determine rate of convergence based on the Sliding Condition, n

Step 3: Determine Control Law

Consider a 2<sup>nd</sup> order scalar system:

$$\ddot{x} + \dot{x}\cos 3a(t)x = u$$

with 
$$1 \le a(t) \le 2$$

Write this as:

$$\ddot{x} = -\dot{x}\cos 3a(t)x + u$$

So that,

We can choose, 
$$\hat{f} = -\dot{x}\cos 3(1.5)x$$
  
So that,  $F = \dot{x}\cos 3(0.5)x$ 

Design of sliding manifold:

$$\begin{split} s &= \dot{\tilde{x}} + \lambda \tilde{x} \\ \dot{s} &= \ddot{\tilde{x}} + \lambda \dot{\tilde{x}} = \ddot{x} - \ddot{x}_d + \lambda \dot{\tilde{x}} \\ &= f + bu - \ddot{x}_d + \lambda \dot{\tilde{x}} \end{split}$$

We choose a control law that makes  $\dot{s} = 0$ , if we knew exactly the dynamics of f, i.e.  $\hat{f} = f$ ,

$$\hat{u} = -\hat{f} + \ddot{x}_d - \lambda \dot{\tilde{x}}$$

$$u = \hat{u} - k \operatorname{sat}(\frac{s}{\varphi})$$

$$= (\dot{x} \cos 3(1.5)x + \ddot{x} - \lambda \dot{x})$$

$$= \left(\dot{x}\cos 3(1.5)x + \ddot{x}_d - \lambda \dot{\tilde{x}}\right) - \left(\dot{x}\cos 3(0.5)x + \eta - \dot{\varphi}\right) \operatorname{sat}(\frac{3}{\varphi})$$