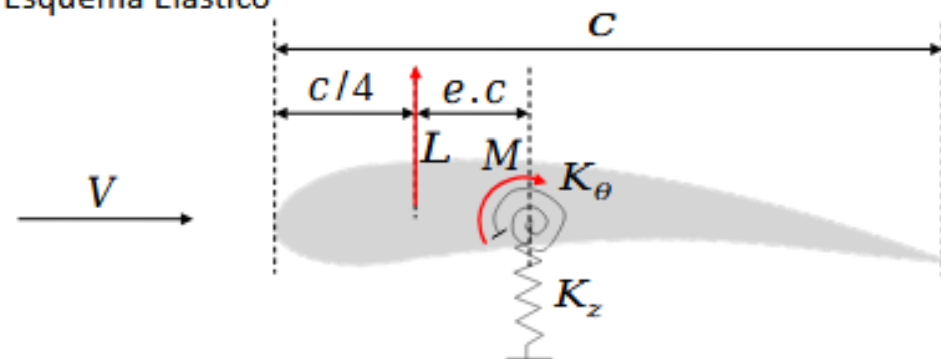


# Quinta Aula de Aeroelasticidade

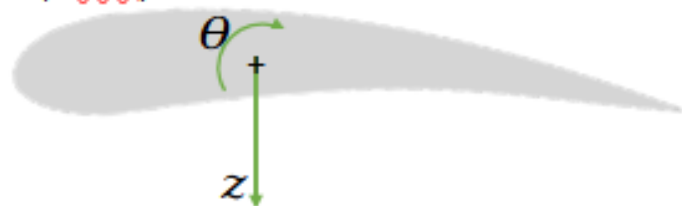
# Roteiro

- 1) Modelo Aeroelástico do Túnel de Vento desenvolvido pelo Prof Juan
- 2) Programa binário modificado
- 3) Análise do arquivo f06
- 4) Representação gráfica do amortecimento e da frequência
- 5) Perguntas Comuns sobre o trabalho

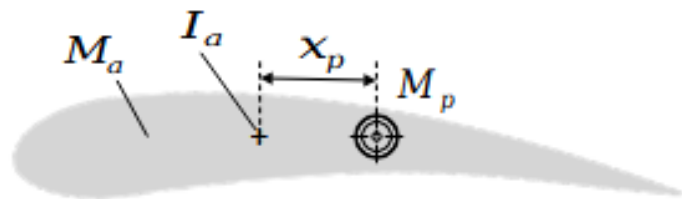
### Esquema Elástico



### Grados de libertad (2 DoF)



### Esquema de inercia



### 1.- Ecuación de Lagrange

$$\frac{d}{dt} \left( \frac{\partial T}{\partial \dot{q}_i} \right) + \frac{\partial U}{\partial q_i} = Q_i$$

### 2.- Energía Potencial Elástica

$$U = \frac{1}{2} K_\theta \theta^2 + \frac{1}{2} K_z Z^2$$

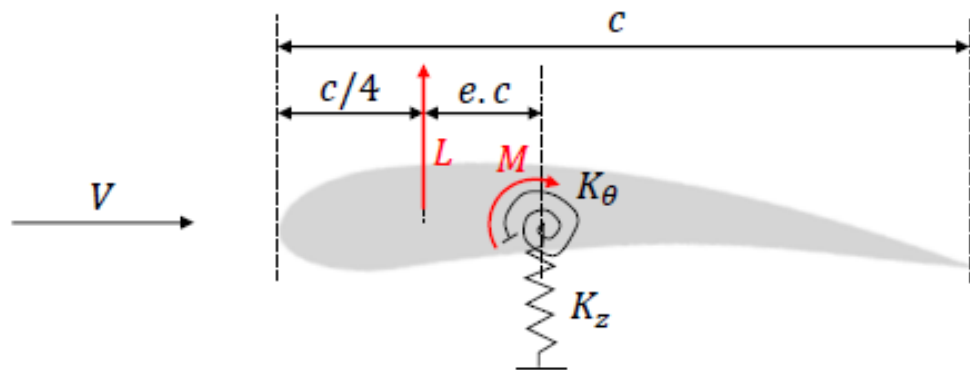
### 3.- Energía Cinética

$$T = \frac{1}{2} M_a \dot{Z}^2 + \frac{1}{2} I_a \dot{\theta}^2 + \frac{1}{2} M_p (\dot{Z} + x_p \dot{\theta})^2$$

### 3.- Fuerzas Generalizadas

$$Q_z = -\frac{1}{2} \rho V^2 c a_1 s \left( \theta + \frac{\dot{z}}{V} \right)$$

$$Q_\theta = \frac{1}{2} \rho V^2 c^2 s \left( a_1 e \left( \theta + \frac{\dot{z}}{V} \right) + M_\theta \frac{\partial c}{4 V} \right)$$



Amortiguamiento  
Aerodinámico

Rigidez  
Aerodinámica

$$\begin{bmatrix} M_z & M_{z\theta} \\ M_{z\theta} & M_\theta \end{bmatrix} \begin{Bmatrix} \ddot{z} \\ \ddot{\theta} \end{Bmatrix} + \frac{1}{2} \rho V \begin{bmatrix} ca_1 s & 0 \\ -c^2 s e a_1 & -\frac{c^3 s M_{\dot{\theta}}}{4} \end{bmatrix} \begin{Bmatrix} \dot{z} \\ \dot{\theta} \end{Bmatrix} + \left( \frac{1}{2} \rho V^2 \begin{bmatrix} 0 & ca_1 s \\ 0 & -c^2 s e a_1 \end{bmatrix} + \begin{bmatrix} K_z & 0 \\ 0 & K_\theta \end{bmatrix} \right) \begin{Bmatrix} z \\ \theta \end{Bmatrix} = 0$$

$$\mathbf{A}\ddot{\mathbf{q}} + \rho V \mathbf{B}\dot{\mathbf{q}} + (\rho V^2 \mathbf{C} + \mathbf{E})\mathbf{q} = 0$$

$$\begin{bmatrix} M_z & M_{z\theta} \\ M_{z\theta} & M_\theta \end{bmatrix} \begin{Bmatrix} \ddot{z} \\ \ddot{\theta} \end{Bmatrix} + \frac{1}{2} \rho V \begin{bmatrix} ca_1 s & 0 \\ -c^2 s e a_1 & -\frac{c^3 s M_{\dot{\theta}}}{4} \end{bmatrix} \begin{Bmatrix} \dot{z} \\ \dot{\theta} \end{Bmatrix} + \left( \frac{1}{2} \rho V^2 \begin{bmatrix} 0 & ca_1 s \\ 0 & -c^2 s e a_1 \end{bmatrix} + \begin{bmatrix} K_z & 0 \\ 0 & K_\theta \end{bmatrix} \right) \begin{Bmatrix} z \\ \theta \end{Bmatrix} = 0$$



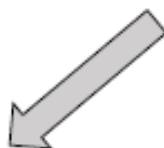
$$\mathbf{A} \ddot{\mathbf{q}} + \rho V \mathbf{B} \dot{\mathbf{q}} + (\rho V^2 \mathbf{C} + \mathbf{E}) \mathbf{q} = 0$$

+

$$\mathbf{I} \dot{\mathbf{q}} - \mathbf{I} \dot{\mathbf{q}} = 0$$



$$\begin{bmatrix} \mathbf{I} & 0 \\ 0 & \mathbf{A} \end{bmatrix} \begin{Bmatrix} \dot{\mathbf{q}} \\ \ddot{\mathbf{q}} \end{Bmatrix} - \begin{bmatrix} 0 & \mathbf{I} \\ -(\rho V^2 \mathbf{C} + \mathbf{E}) & -(\rho V \mathbf{B}) \end{bmatrix} \begin{Bmatrix} \mathbf{q} \\ \dot{\mathbf{q}} \end{Bmatrix} = 0$$



$$\begin{Bmatrix} \dot{\mathbf{q}} \\ \ddot{\mathbf{q}} \end{Bmatrix} - \begin{bmatrix} 0 & \mathbf{I} \\ -\mathbf{A}^{-1}(\rho V^2 \mathbf{C} + \mathbf{E}) & -\mathbf{A}^{-1}(\rho V \mathbf{B}) \end{bmatrix} \begin{Bmatrix} \mathbf{q} \\ \dot{\mathbf{q}} \end{Bmatrix} = 0$$



$$(\mathbf{I} \lambda - \mathbf{Q}) \{q_0\} = 0$$

$$\begin{Bmatrix} \mathbf{q} \\ \dot{\mathbf{q}} \end{Bmatrix} = \{q_0\} e^{\lambda t} \quad \begin{Bmatrix} \dot{\mathbf{q}} \\ \ddot{\mathbf{q}} \end{Bmatrix} = \lambda \{q_0\} e^{\lambda t}$$

$$\lambda_i = -\xi_i \omega_i \pm i \omega_i \sqrt{1 - \xi_i^2}$$

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aula5\_aeroelasticidade.ppt

binario\_TeoricoPractico\_General.asv

binario\_TeoricoPractico\_General.m

ClaseAeroelasticidadTeoricoPractico.pptx

binario\_TeoricoPractico\_General.m (Script)

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a1	5.7300
A_p	1.2000
a_w	1.8191
b	0.1000
c	0.2000
C	[1.0696,0;0.0267,0.0071]
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e	-0.1250
f	1470.0000 0.0 0.0 16001

Editor - C:\02 universidade de aveiro\

aeroelasticidade\aulas aerolasticidade ppt\05 aeroelasticidade 5\binario\_TeoricoPractico\_General.m

kmethord.m

flutterconico.m

binario\_K\_Method.m

binario\_pK\_Method.m

convertf06.m

binario\_TeoricoPractico\_General.m

```

1 % Programa_Binario
2 % Matrices Aeroelásticas para o Modelo Binário,
3 % Calcula a solução dos autovalores em velocidades desejadas e
4 % obtém os gráficos de frequência e amortecimento (V_omega) e V_g
5
6 clear; clf; close all;
7
8 %% Dados do problema
9
10 %%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%
11 % DATOS MODIFICABLES
12
13 % Datos de rigidez kz=470.9
14 K_z = 470.9; %[N/m]
15 K_theta = 0.46; %[Nm]
16
17 % Datos de masas

```

Command Window

New to MATLAB? See resources for [Getting Started.](#)

>> binario\_TeoricoPractico\_General

>> binario\_TeoricoPractico\_General

>> binario\_TeoricoPractico\_General

>> binario\_TeoricoPractico\_General

>> binario\_TeoricoPractico\_General

>> binario\_TeoricoPractico\_General

Zoom: 110%

UTF-8

CRLF

script

Ln 20 Col 10

# Influência da Rigidez

	Túnel de Vento	Aumento de $K_z$	Aumento de $K_q$	Aumento de ambos
$K_z$	470,9	1000	470,9	1000
$K_q$	0,46	0,46	2	2
$V_f$				



































# Influência da Massa $M_p$

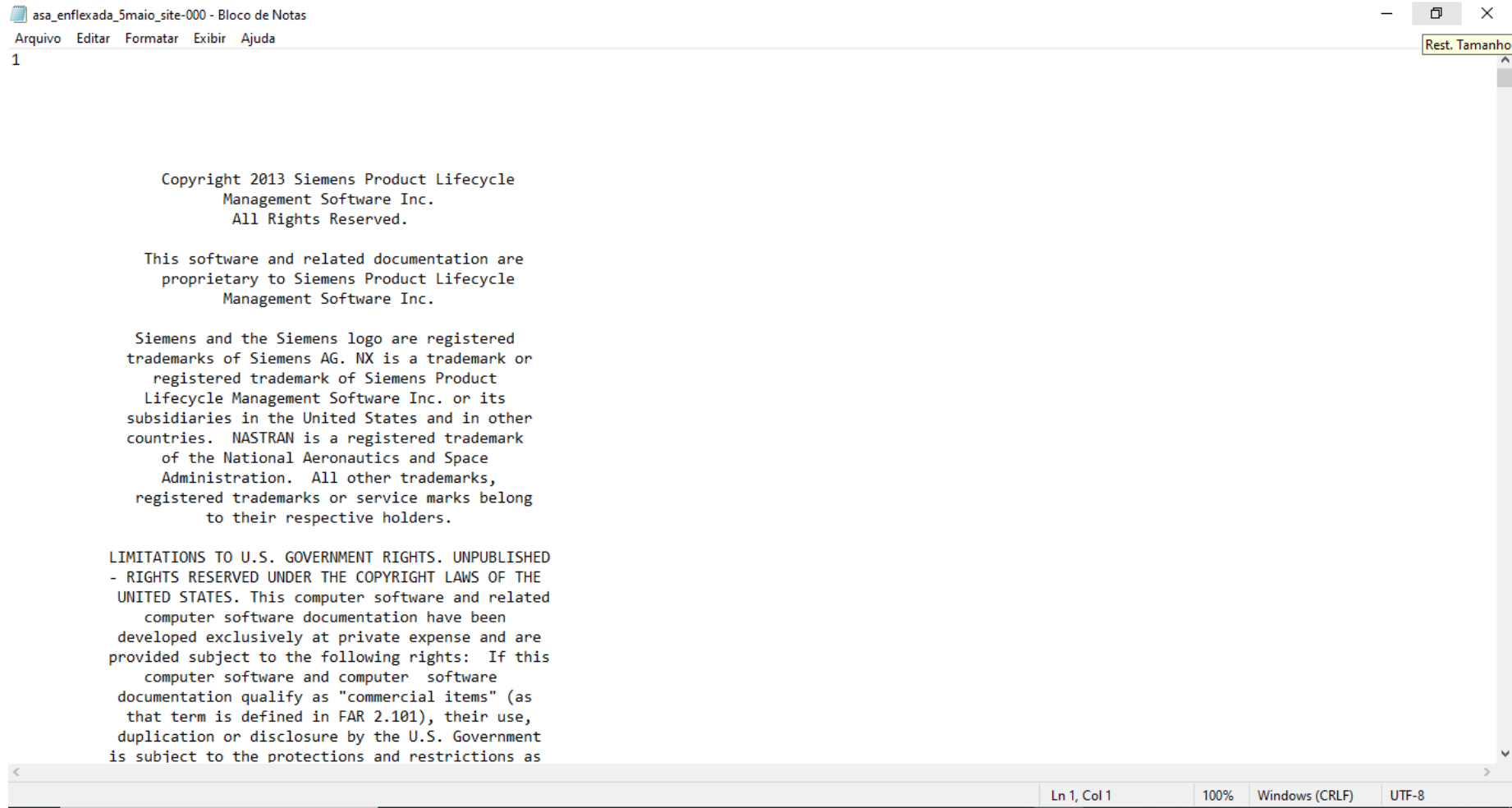
	Túnel de Vento	Aumento da Massa	Sem Massa	$V_f$ (m/s)
$M_p$	0,1 kg	0,5 kg	0	-
e1	-	0	0	
e2	-	-0,0875	-0,0875	
e3	-0,125	-0,125	-0,125	

# Roteiro

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 asa_enflexada_5maio_site-000	05/05/2024 20:18	Arquivo DAT	11 KB	
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# arquivo \*.f06



asa\_enflexada\_5maio\_site-000 - Bloco de Notas

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Rest. Tamanho

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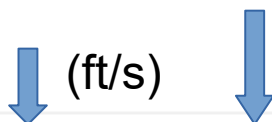
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## FLUTTER SUMMARY

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 POINT = 1 MACH NUMBER = 0.8000 DENSITY RATIO = 3.1060E-01 METHOD = PK

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0.0022	4.5202206E+02	1.0020000E+04	-2.2226544E-02	3.5279970E+00	-2.4634856E-01	2.2167059E+01
0.0022	4.5159683E+02	1.0030000E+04	-2.2291552E-02	3.5348432E+00	-2.4754854E-01	2.2210075E+01
0.0022	4.5116611E+02	1.0040000E+04	-2.2357265E-02	3.5417457E+00	-2.4876308E-01	2.2253445E+01
0.0022	4.5072986E+02	1.0050000E+04	-2.2423686E-02	3.5487049E+00	-2.4999239E-01	2.2297171E+01
0.0022	4.5028793E+02	1.0060000E+04	-2.2490844E-02	3.5557220E+00	-2.5123692E-01	2.2341261E+01
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0.0022	4.4938705E+02	1.0080000E+04	-2.2627437E-02	3.5699329E+00	-2.5377294E-01	2.2430552E+01
0.0022	4.4892789E+02	1.0090000E+04	-2.2696916E-02	3.5771296E+00	-2.5506532E-01	2.2475769E+01
0.0022	4.4846280E+02	1.0100000E+04	-2.2767214E-02	3.5843885E+00	-2.5637451E-01	2.2521378E+01
0.0022	4.4799179E+02	1.0110000E+04	-2.2838347E-02	3.5917096E+00	-2.5770080E-01	2.2567377E+01
0.0022	4.4751471E+02	1.0120000E+04	-2.2910345E-02	3.5990953E+00	-2.5904480E-01	2.2613783E+01
0.0022	4.4703146E+02	1.0130000E+04	-2.2983231E-02	3.6065459E+00	-2.6040685E-01	2.2660597E+01
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0.0022	4.4451999E+02	1.0180000E+04	-2.3361921E-02	3.6448240E+00	-2.6750693E-01	2.2901106E+01
0.0023	4.4399811E+02	1.0190000E+04	-2.3440711E-02	3.6526933E+00	-2.6898861E-01	2.2950550E+01
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0.0023	4.4293365E+02	1.0210000E+04	-2.3601618E-02	3.6686575E+00	-2.7201873E-01	2.3050856E+01
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0.0023	4.3956866E+02	1.0270000E+04	-2.4113595E-02	3.7184663E+00	-2.8169277E-01	2.3363813E+01
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(ft/s)

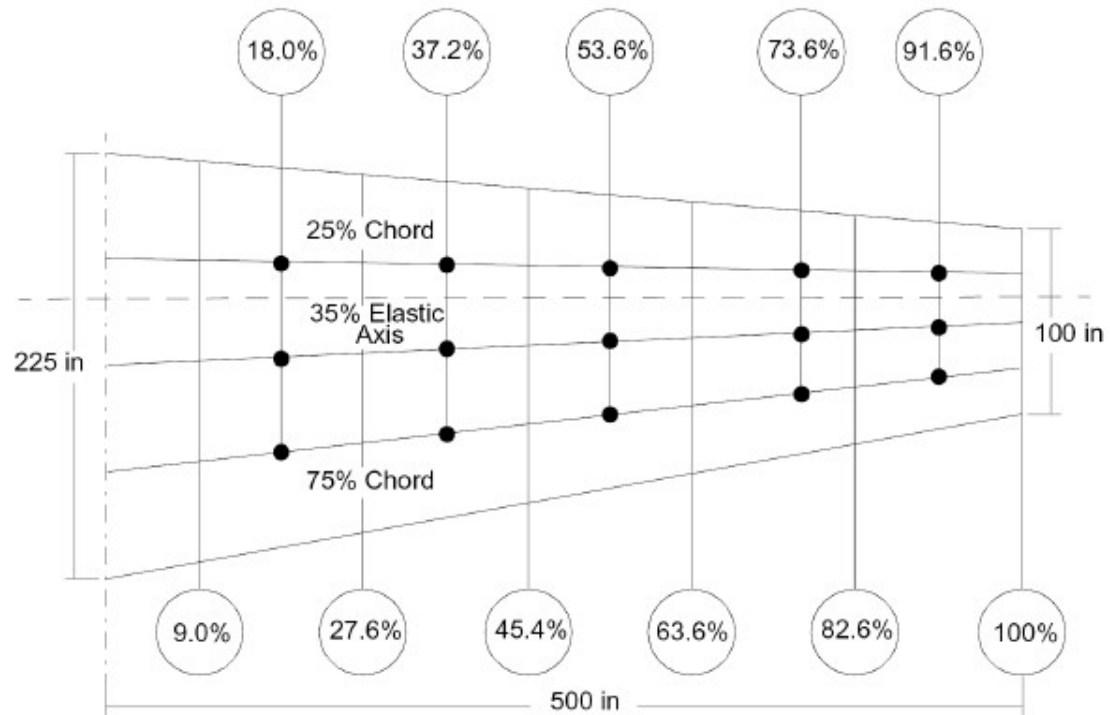
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0.0036	2.7486902E+02	1.0740000E+04	-8.7167864E-04	6.2186856E+00	-1.7029617E-02	3.9073154E+01
0.0036	2.7622272E+02	1.0750000E+04	-5.4046640E-04	6.1939712E+00	-1.0516901E-02	3.8917870E+01
0.0036	2.7761093E+02	1.0760000E+04	-1.8360102E-04	6.1687312E+00	-3.5581219E-03	3.8759281E+01
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0.0035	2.8854739E+02	1.0830000E+04	3.3996431E-03	5.9735351E+00	6.3799113E-02	3.7532829E+01
0.0034	2.9033374E+02	1.0840000E+04	4.1531012E-03	5.9422631E+00	7.7530801E-02	3.7336342E+01
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0.0031	3.2277014E+02	1.0960000E+04	4.9707040E-02	5.4042740E+00	8.4392750E-01	3.3956055E+01
0.0031	3.2644827E+02	1.0970000E+04	6.9910102E-02	5.3482585E+00	1.1746330E+00	3.3604099E+01
0.0030	3.2920123E+02	1.0980000E+04	9.3164891E-02	5.3083677E+00	1.5536857E+00	3.3353458E+01
0.0030	3.3114365E+02	1.0990000E+04	1.1560261E-01	5.2820363E+00	1.9183105E+00	3.3188015E+01
0.0030	3.3260214E+02	1.1000000E+04	1.3610810E-01	5.2636595E+00	2.2507207E+00	3.3072548E+01
0.0030	3.3378342E+02	1.1010000E+04	1.5478502E-01	5.2497993E+00	2.5528278E+00	3.2985462E+01
0.0030	3.3479688E+02	1.1020000E+04	1.7194355E-01	5.2386613E+00	2.8298023E+00	3.2915482E+01
0.0030	3.3570212E+02	1.1030000E+04	1.8786402E-01	5.2292757E+00	3.0862780E+00	3.2856510E+01
0.0030	3.3653372E+02	1.1040000E+04	2.0276792E-01	5.2210827E+00	3.3259039E+00	3.2805031E+01
0.0030	3.3731299E+02	1.1050000E+04	2.1682374E-01	5.2137399E+00	3.5514531E+00	3.2758896E+01

Flutter

# Roteiro

- 1) Modelo Aeroelástico do Túnel de Vento desenvolvido pelo Prof Juan
- 2) Programa binário modificado
- 3) Análise do arquivo f06
- 4) Representação gráfica do amortecimento e da frequência
- 5) Perguntas Comuns sobre o trabalho

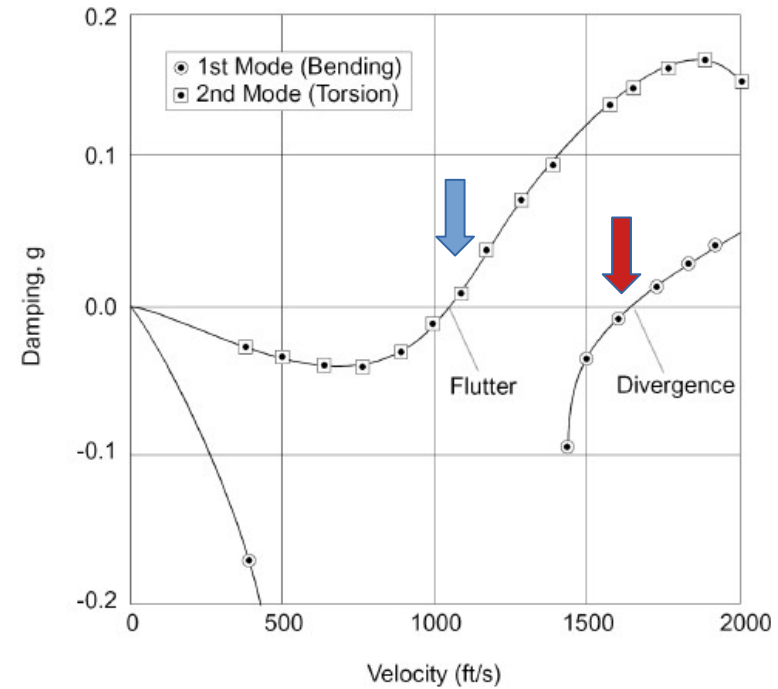
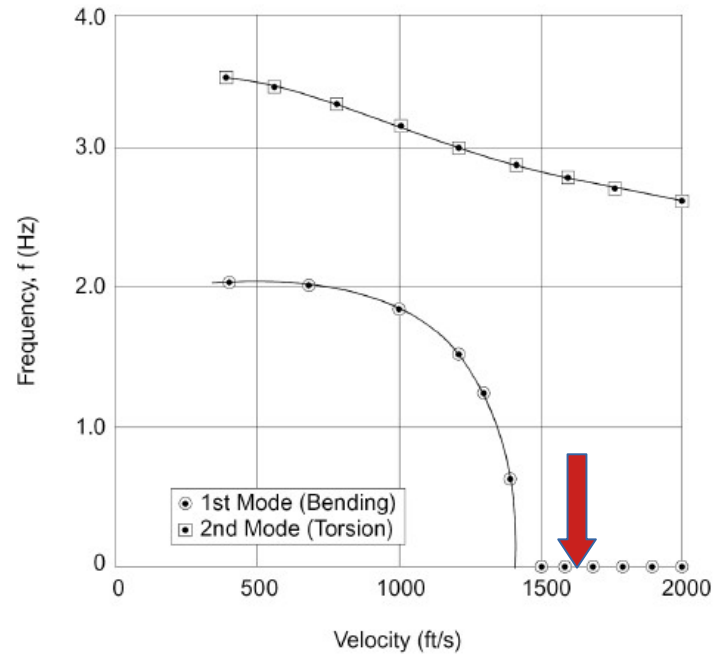
## Asa Exemplo - AH 145B



**Figure 7-3. BAH Wing Planform and Aerodynamic Strip Idealization**

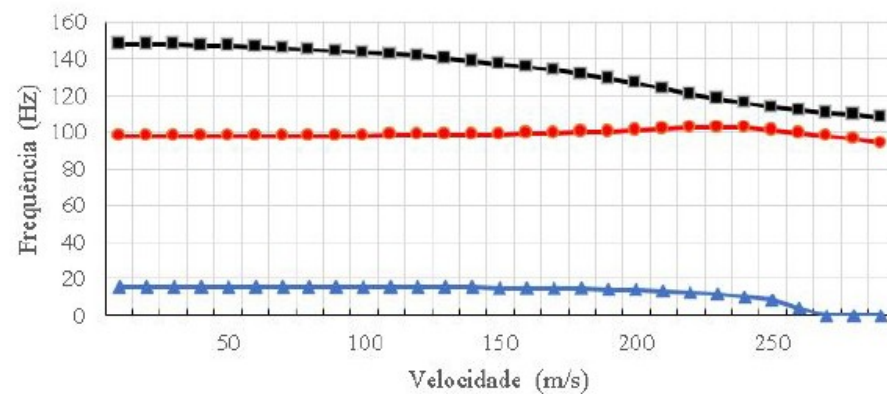


## Asa Exemplo - AH 145B

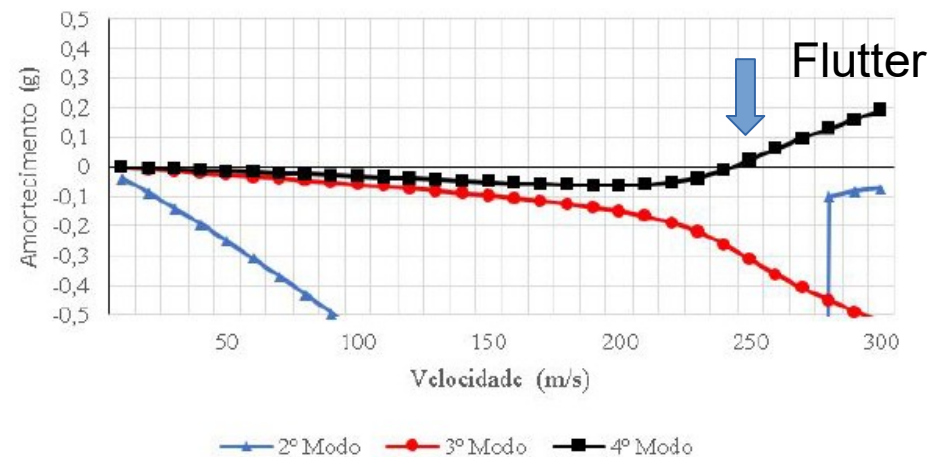


# Exemplo de um UAV

Frequência x Velocidade - Malha 2



Amortecimento x Velocidade - Malha 2

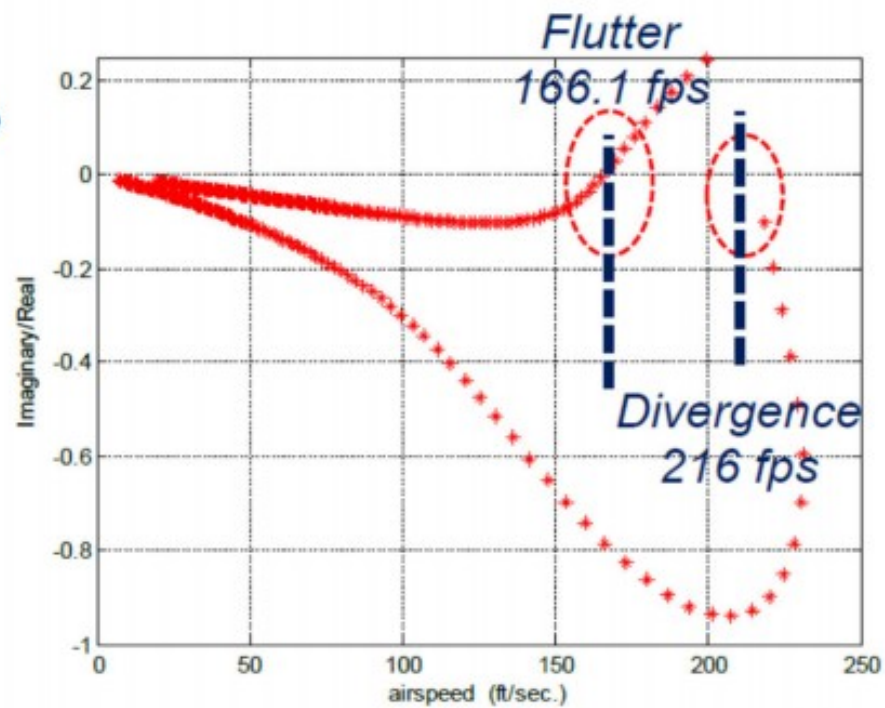
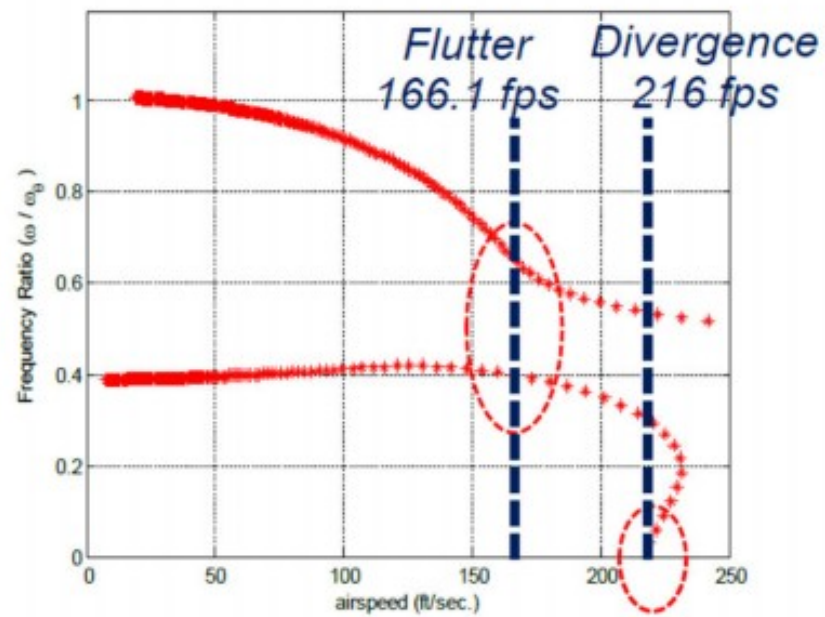


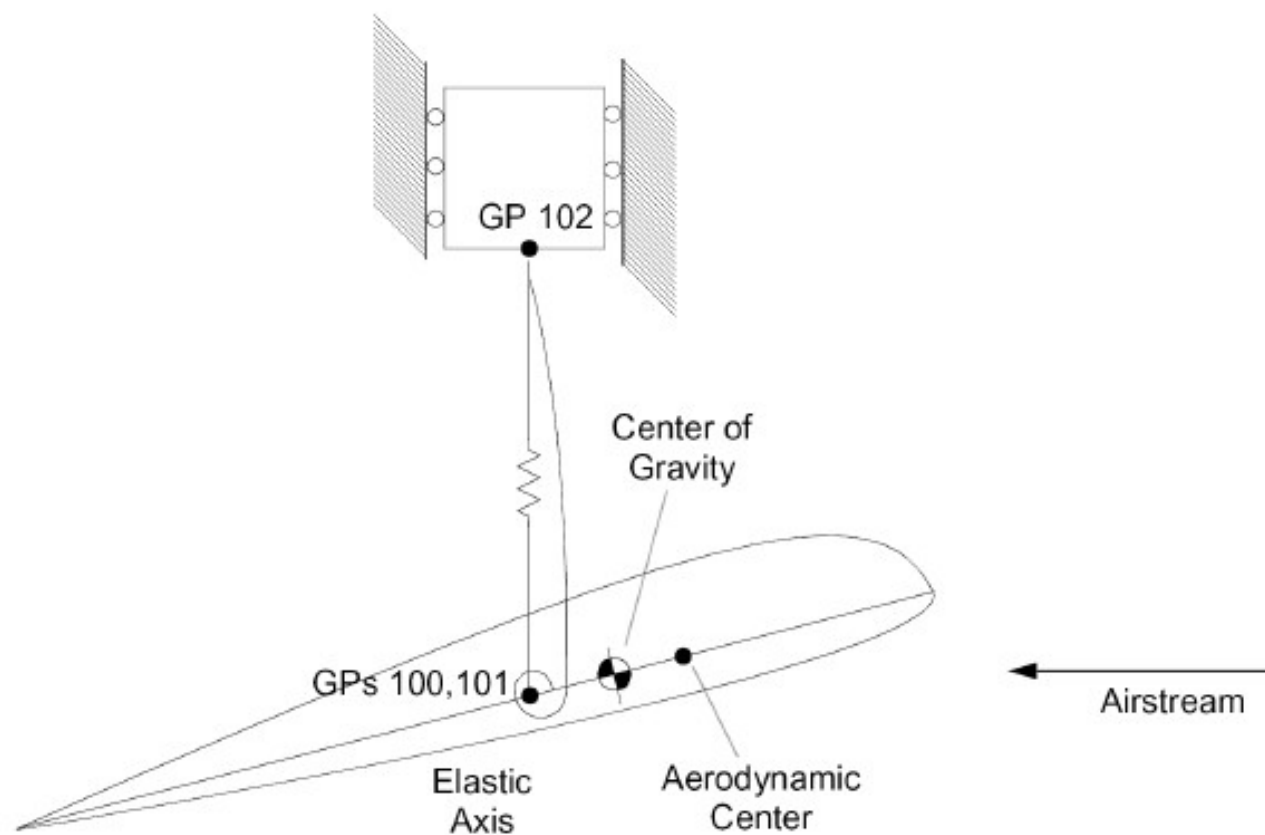
# Roteiro

- 1) Modelo Aeroelástico do Túnel de Vento desenvolvido pelo Prof Juan
- 2) Programa binário modificado
- 3) Análise do arquivo f06
- 4) Representação gráfica do amortecimento e da frequência
- 5) Perguntas Comuns sobre o trabalho

# Perguntas Comuns

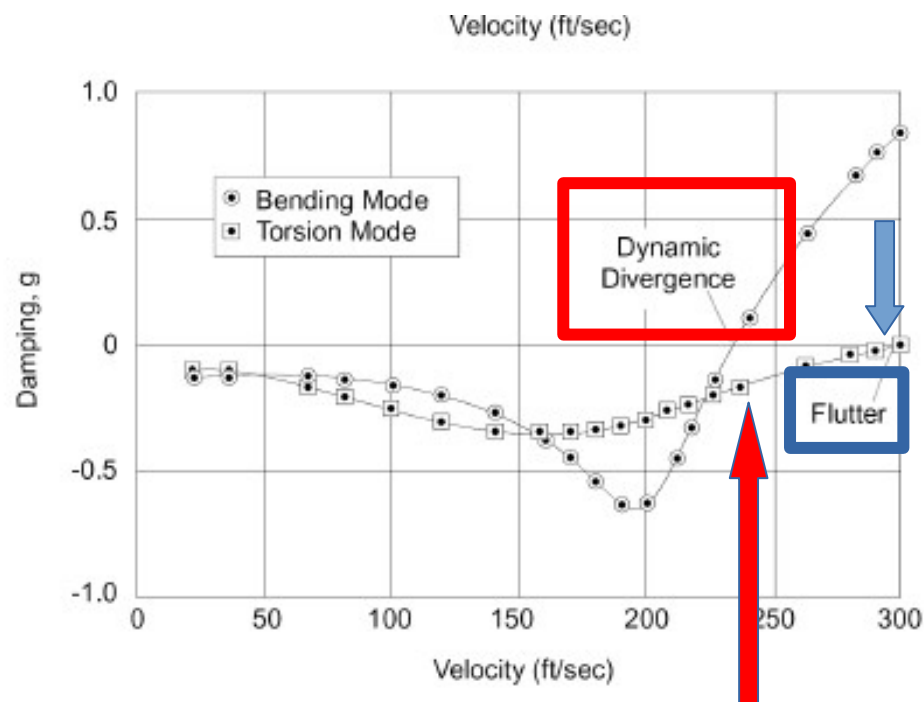
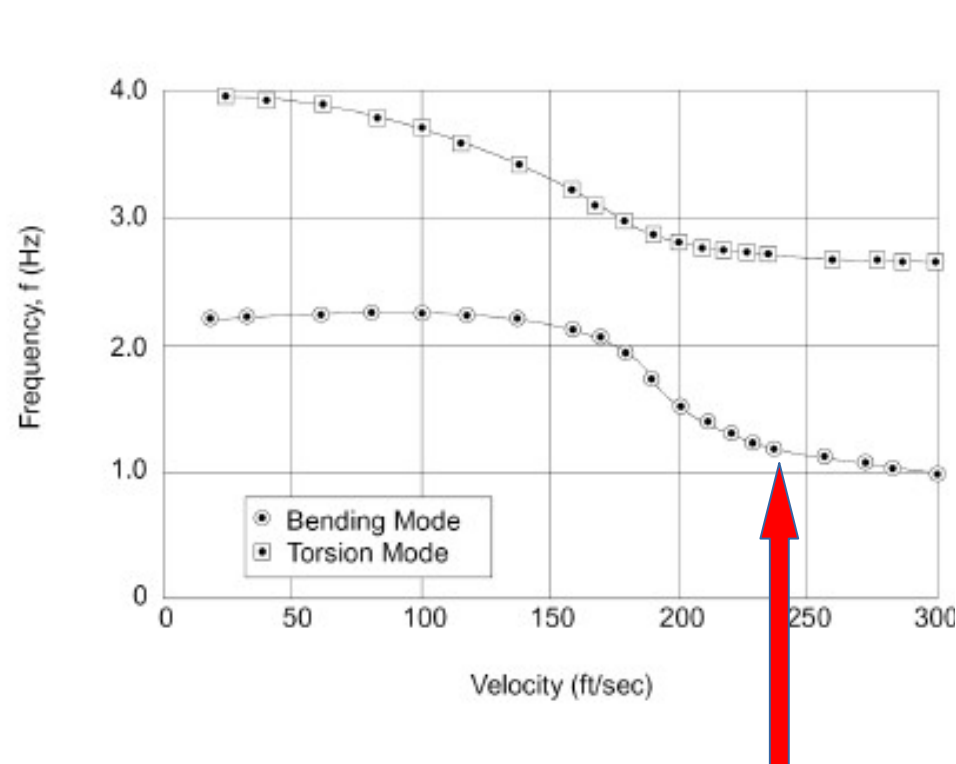
- 1) Como identificar a divergência?
- 2) Qual é o modo que ocorre o flutter? O de torção ou o de flexão?

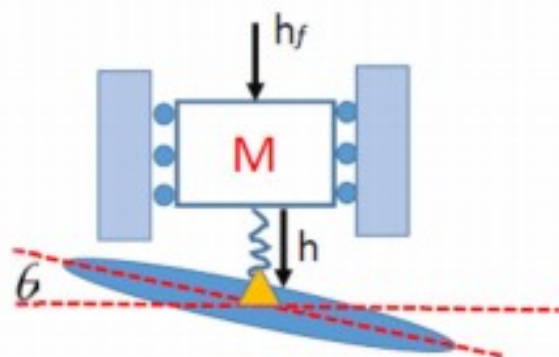




**Figure 7-1. Three Degree of Freedom Airfoil and Fuselage**

and unrestrained systems is a subject for further study. From Figure 7-2 and the printed Flutter Summary for Point 2, the “dynamic divergence” speed (i.e., the speed at which the oscillatory instability finds its origin in a tendency to static divergence) and frequency are 232.0 ft/s and 1.177 Hz, respectively. From Figure 7-2 and the Flutter Summary for Point 3, the flutter speed and frequency are 283.1 ft/s and 2.692 Hz, respectively. These results are only slightly different from



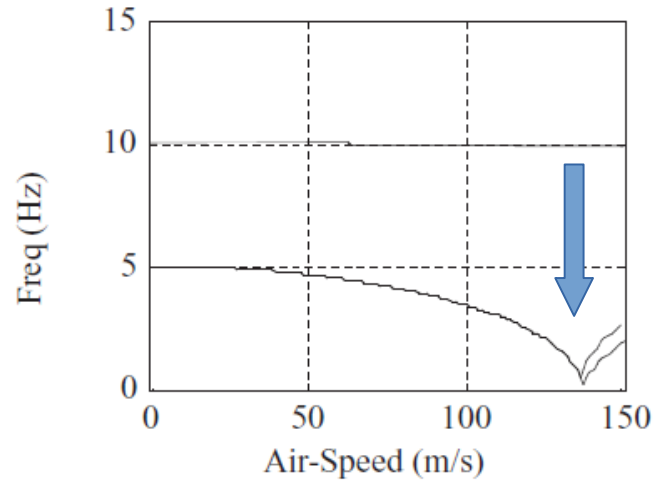


*Figure 4.4.18 – Body-freedom model with fuselage mass plunge degree of freedom.*

Figure 4.4.19 shows two figures that compare frequency merging results with and without pitch freedom. The figure on the right shows that flutter, through frequency merging, will not happen if pitch freedom is included. Instead, static divergence is the system mode of instability. Rodden<sup>243</sup> calls this phenomenon “dynamic divergence.” It is an instability that involves the entire vehicle and is a function of the system frequencies and relative masses. On the other hand, it is also an aperiodic instability, like classical fully restrained divergence, so the adjective “dynamic” is superfluous. A better term might be “vehicle divergence.” We will see this type of instability when we consider joined wing body-freedom flutter.

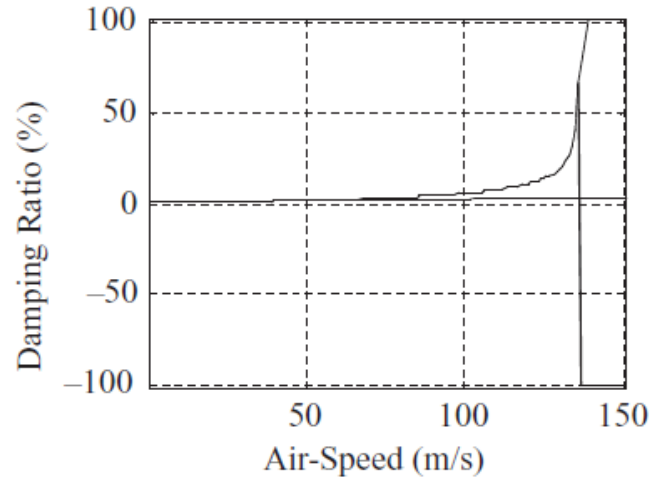


# ANÁLISE WRIGHT E COOPER

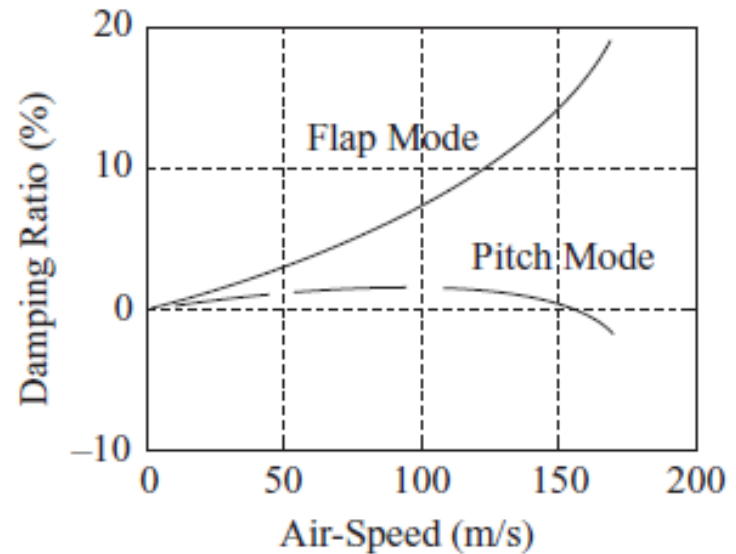
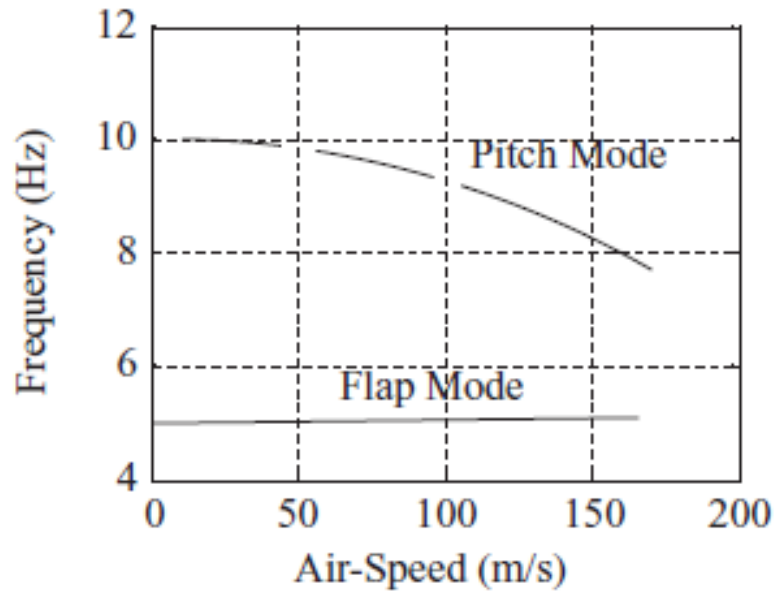


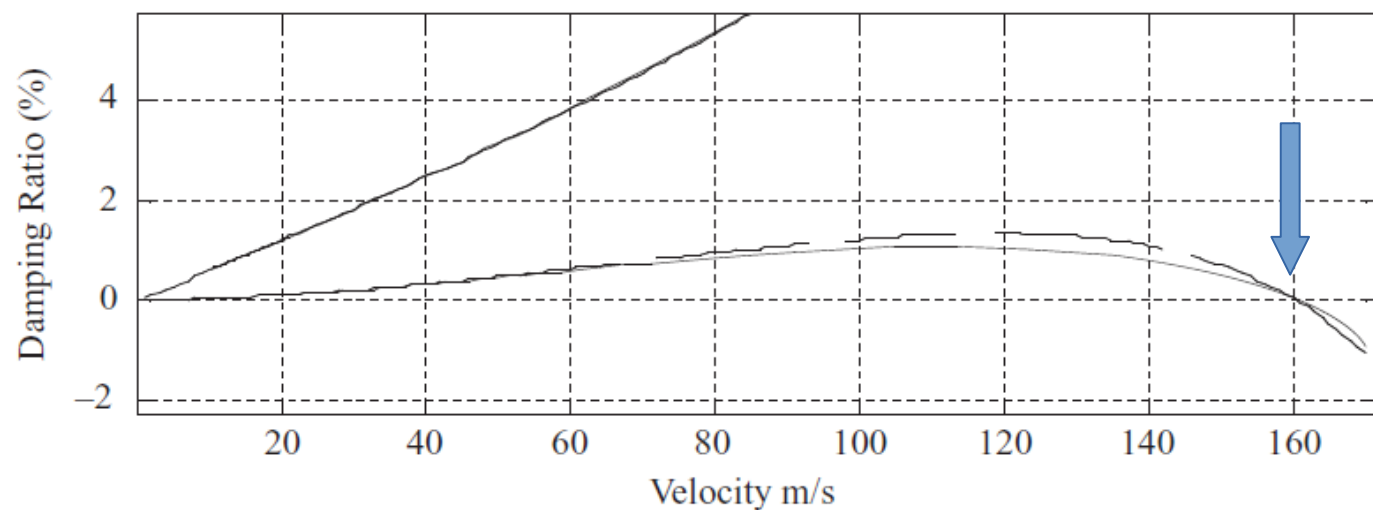
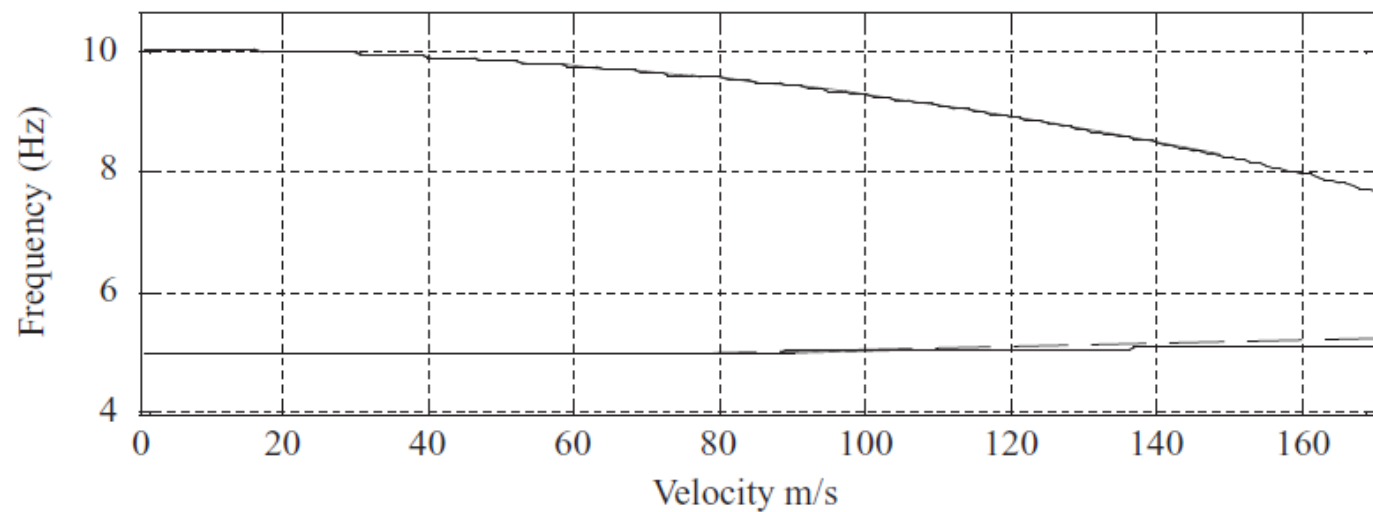
divERGÊNCIA

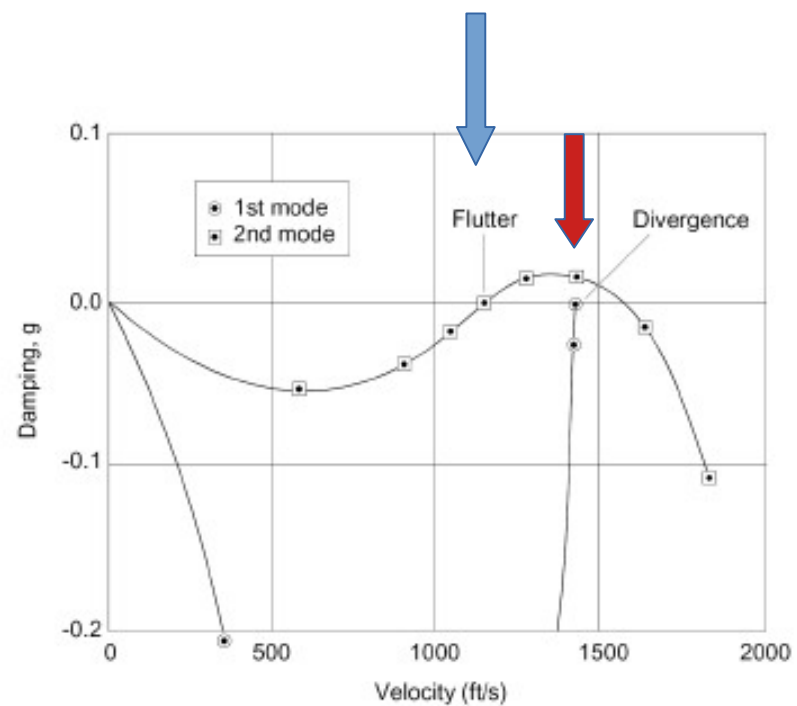
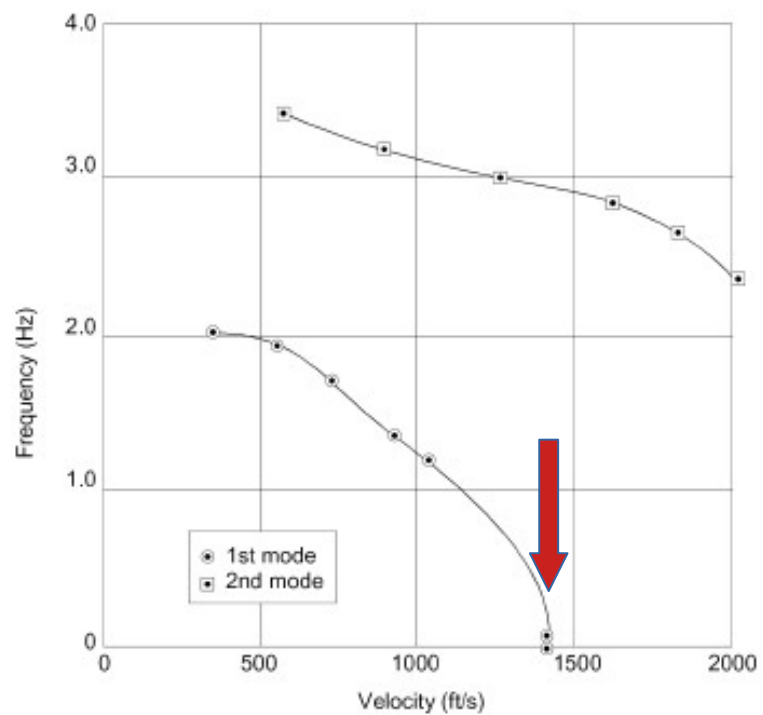
FREQUÊNCIA ZERO  
=> PARTE IMAGINÁRIA VAI A  
ZERO



# Modos do Flutter







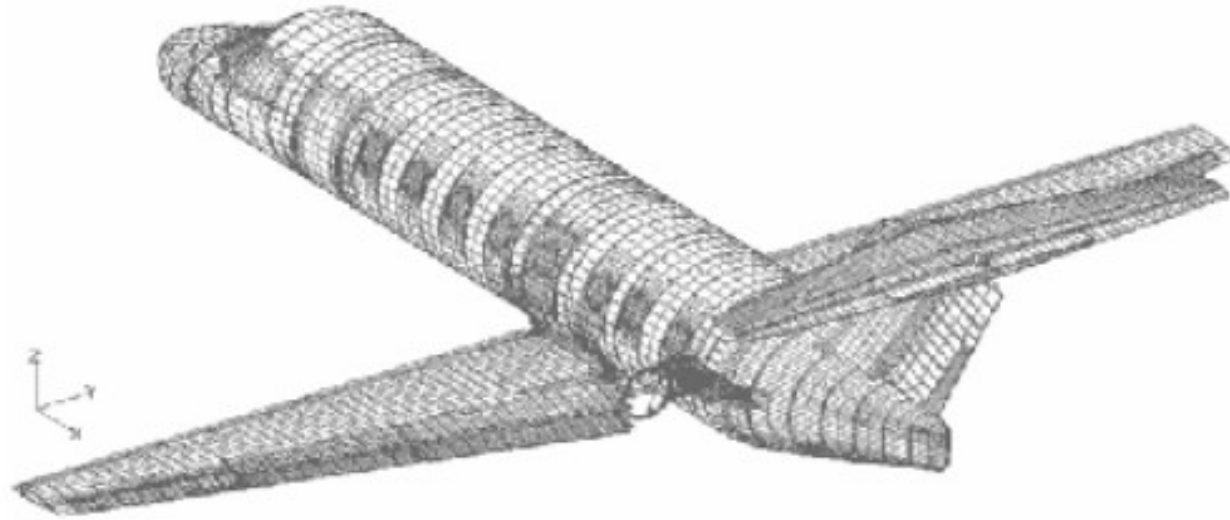
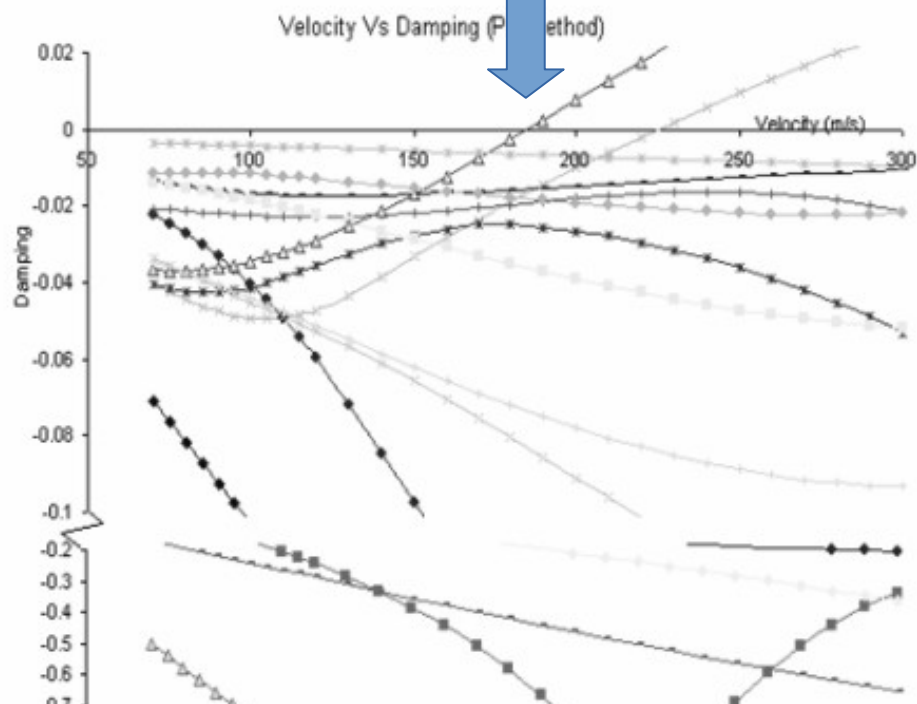
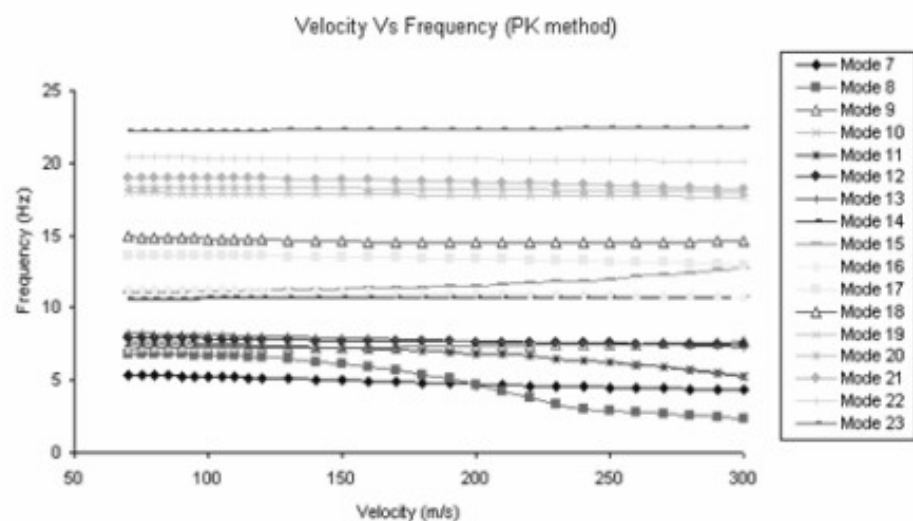


Fig.1 FE model of the aircraft

VITTALA N.G. V., PANKAJ A.C. e SWARNALATHA R. DYNAMIC AND AEROELASTIC ANALYSIS OF A TRANSPORT AIRCRAFT. Proceedings of the International Conference on Aerospace Science and Technology 26 - 28 June 2008, Bangalore, India.



**Table 3 Flutter Results of the Aircraft**

Configuration	Method	Mode No	Flutter Velocity (Vf) (m/s)	Flutter frequency (Hz)	Flutter Margins (%)
1	PK	18	179.59	14.3359	27.76
	KE	18	179.68	14.3378	27.83