

Aircraft Structural Analysis

Master Course in Aerospace Engineering

Extra material II — Levy's approximate solution for rectangular plates (for comparison with FEM)

Reference material

Rectangular Plates - Approximate Solutions, Chapter 5
Levy's solution for simply supported rectangular plates
(sections 5.4, 5.5)

of the reference book: Ansel C. Ugural, "Stresses in Plates and Shells", 2nd ed., McGraw-Hill

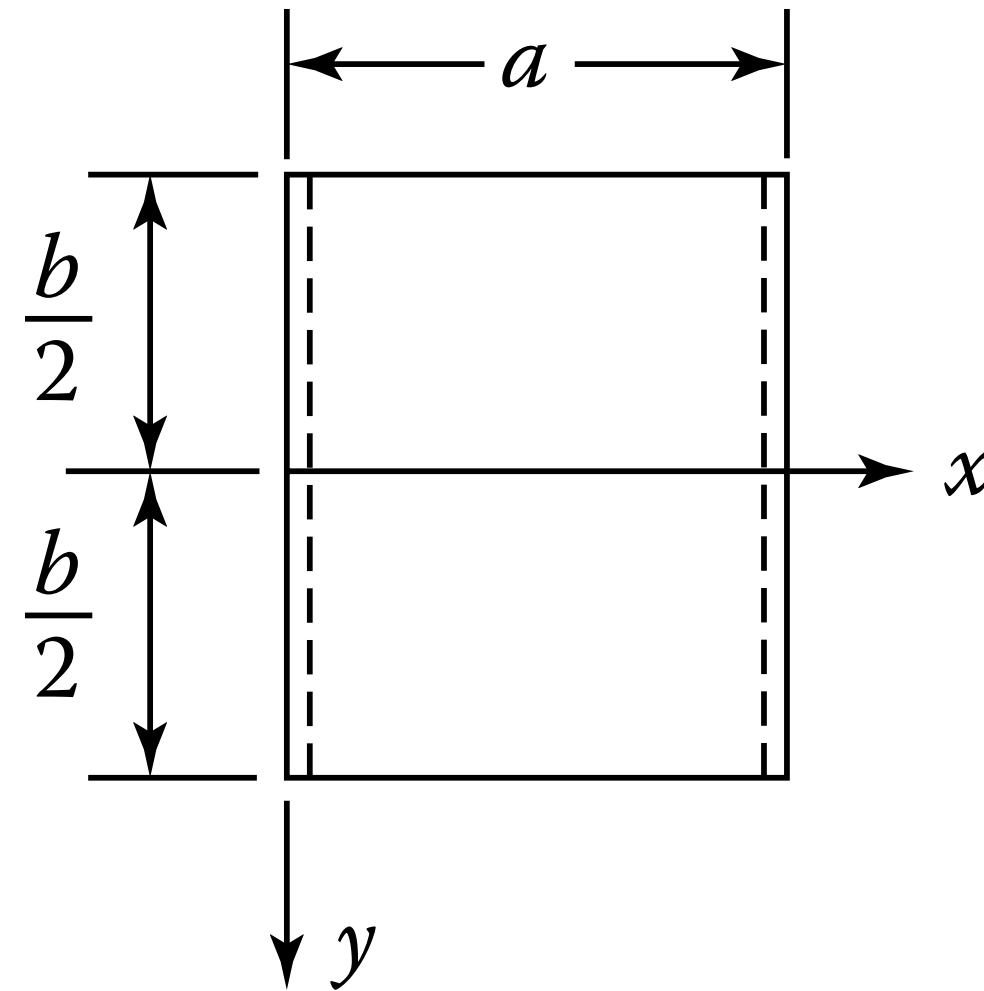
The motivation...

- to find a solution for the **out-of-plane displacements (deflections)**, in an approximate way
- to write the approximate solution for deflections as a **single Fourier series**
- to **increase the convergence rate** of the solution, for bending moments (and stresses)
- to avoid using (directly) the fourth-order differential equation for displacements

$$w(x,y) = ???$$

The idea...

- the solution for the deflection will come from the **superposition** of two individual problems
- rectangular plates with **particular boundary conditions** on two opposite sides (simply supported, $x=0, x=a$) and **arbitrary boundary conditions** on the other edges ($y=\pm b/2$)

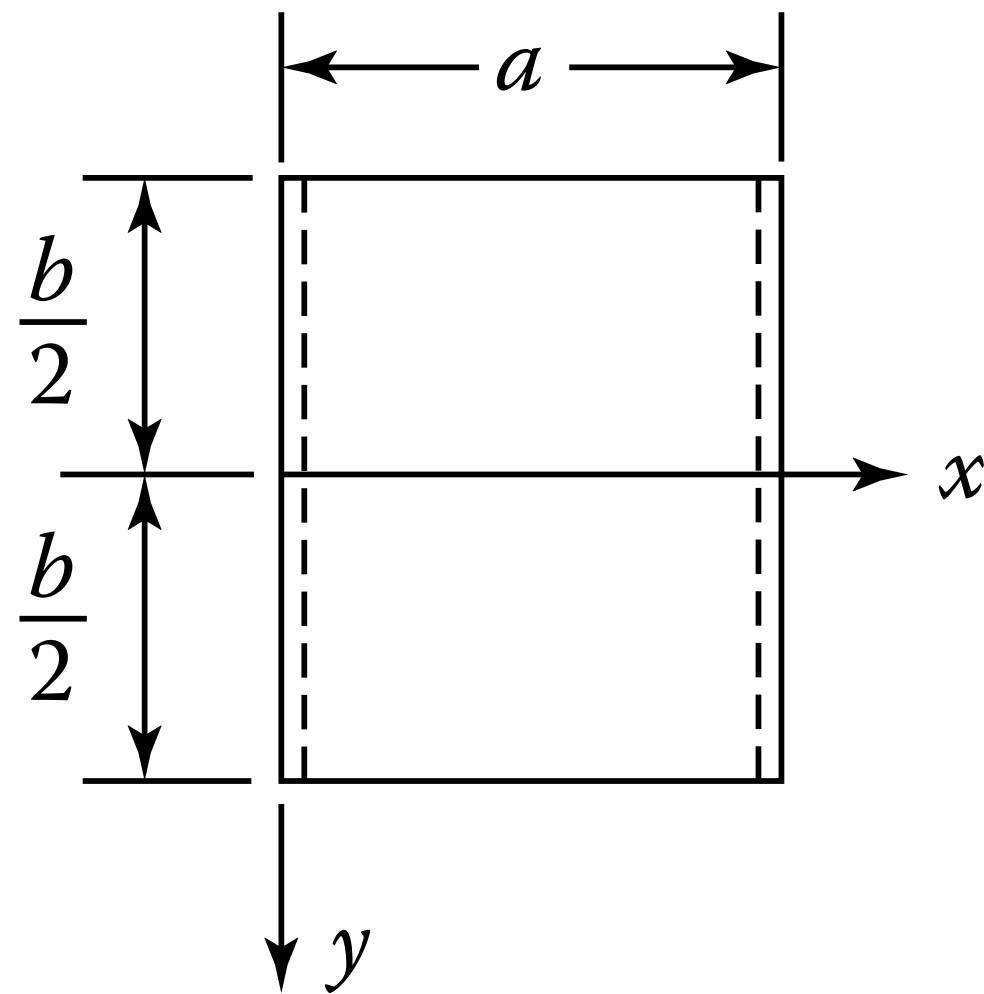


$$\begin{cases} w = 0 \Big|_{x=0, x=a} \\ \frac{\partial^2 w}{\partial x^2} = 0 \Big|_{x=0, x=a} \end{cases}$$

The idea...

- the solution for the deflection will come from the superposition of two individual problems

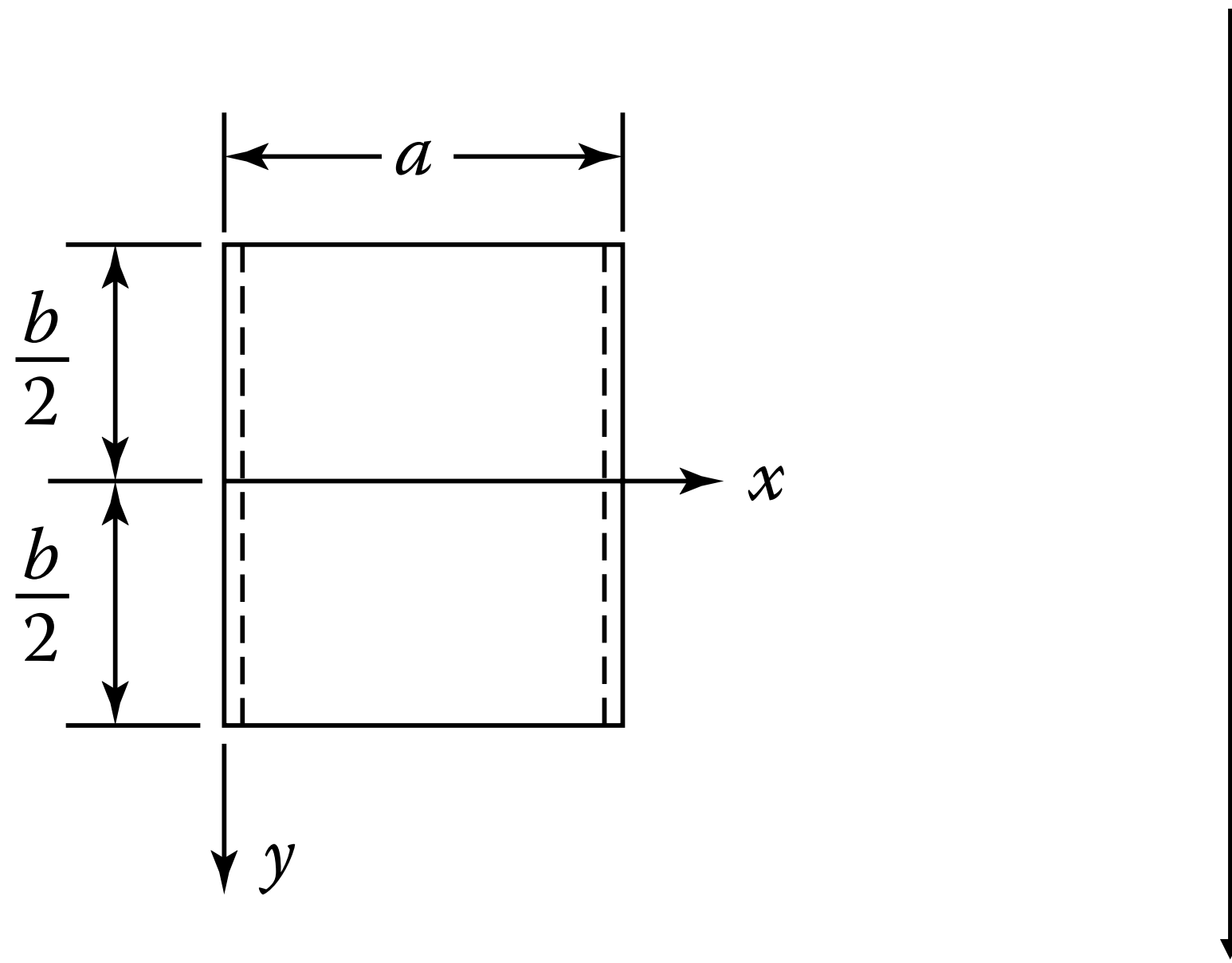
$$w(x,y) = w_h(x,y) + w_p(x,y)$$



The idea...

- the solution for the deflection will come from the superposition of two individual problems

$$w(x,y) = w_h(x,y) + w_p(x,y)$$



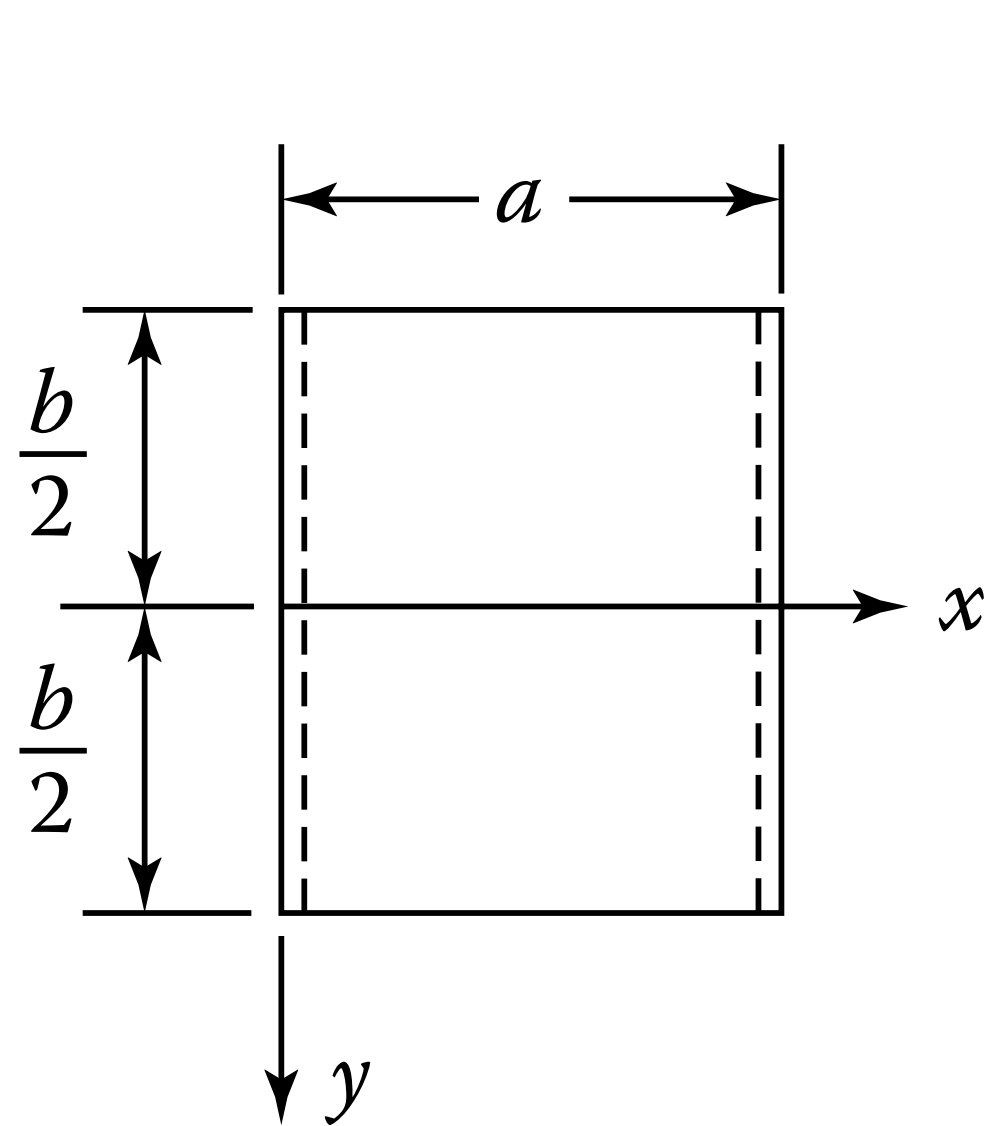
a **homogeneous solution** that depends only on the **geometry** and **boundary conditions** of the plate

$$p(x,y) = 0 \rightarrow \nabla^4 w_h(x,y) = 0$$

The idea...

- the solution for the deflection will come from the superposition of two individual problems

$$w(x,y) = w_h(x,y) + w_p(x,y)$$



a **particular solution** that depends only on the **loading**

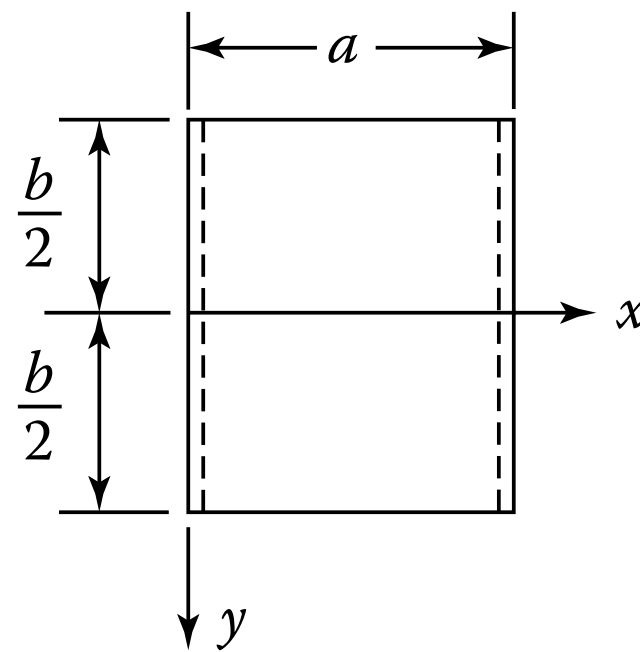
$$\nabla^4 w_p(x,y) = \frac{p(x,y)}{D}$$

a **homogeneous solution** that depends only on the **geometry** and **boundary conditions** of the plate

$$p(x,y) = 0 \rightarrow \nabla^4 w_h(x,y) = 0$$

A proposal for the homogeneous solution...

here it is, a (single) Fourier series, separating the variables...



$$f_m(y) = ???$$

$$w_h(x, y) = \sum_{m=1}^{\infty} f_m(y) \sin \frac{m\pi}{a} x \longrightarrow \nabla^4 w_h(x, y) = 0$$

$$\nabla^4 w(x, y) = \frac{\partial^4 w}{\partial x^4} + 2 \frac{\partial^4 w}{\partial x^2 \partial y^2} + \frac{\partial^4 w}{\partial y^4} = \frac{p}{D}$$

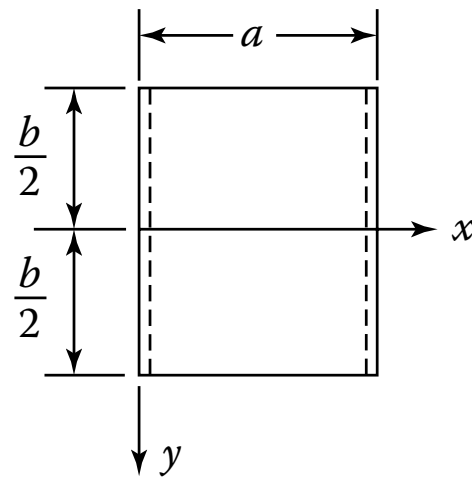
$$\nabla^4 w_h(x, y) = \frac{\partial^4 w_h}{\partial x^4} + 2 \frac{\partial^4 w_h}{\partial x^2 \partial y^2} + \frac{\partial^4 w_h}{\partial y^4} = 0$$

$$\left[\left(\frac{m\pi}{a} \right)^4 f_m(y) - 2 \left(\frac{m\pi}{a} \right)^2 \frac{d^2 f_m(y)}{dy^2} + \frac{d^4 f_m(y)}{dy^4} \right] \sin \frac{m\pi x}{a} = 0$$

$$\frac{d^4 f_m(y)}{dy^4} - 2 \left(\frac{m\pi}{a} \right)^2 \frac{d^2 f_m(y)}{dy^2} + \left(\frac{m\pi}{a} \right)^4 f_m(y) = 0$$

$$m = 1, 2, 3, \dots$$

Here comes the homogeneous part of the deflection...

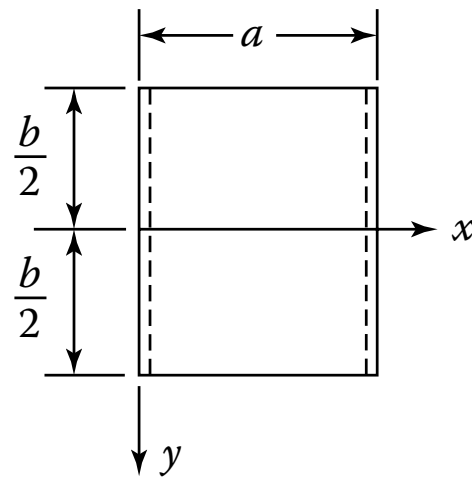


$$w_h(x, y) = \sum_{m=1}^{\infty} f_m(y) \sin \frac{m\pi}{a} x \quad \longrightarrow \quad \nabla^4 w_h(x, y) = 0$$

$$f_m(y) = A_m \sinh \frac{m\pi y}{a} + B_m \cosh \frac{m\pi y}{a} + \frac{m\pi y}{a} \left(C_m \sinh \frac{m\pi y}{a} + D_m \cosh \frac{m\pi y}{a} \right)$$

$$w_h = \sum_{m=1}^{\infty} \left[A_m \sinh \frac{m\pi y}{a} + B_m \cosh \frac{m\pi y}{a} + \frac{m\pi y}{a} \left(C_m \sinh \frac{m\pi y}{a} + D_m \cosh \frac{m\pi y}{a} \right) \right] \sin \frac{m\pi}{a} x$$

Here comes the homogeneous part of the deflection...



$$w(x, y) = w_h(x, y) + w_p(x, y)$$

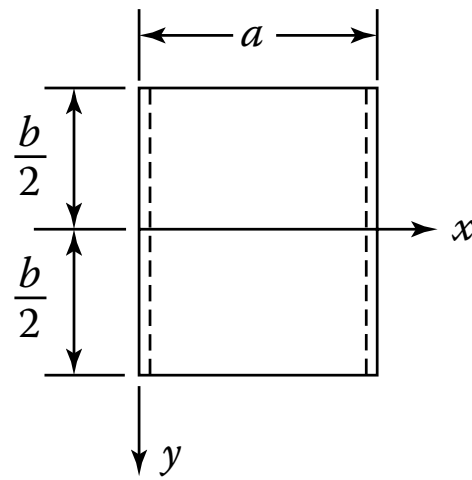
$$w_h(x, y) = \sum_{m=1}^{\infty} f_m(y) \sin \frac{m\pi}{a} x \quad \longrightarrow \quad \nabla^4 w_h(x, y) = 0$$

$$f_m(y) = A_m \sinh \frac{m\pi y}{a} + B_m \cosh \frac{m\pi y}{a} + \frac{m\pi y}{a} \left(C_m \sinh \frac{m\pi y}{a} + D_m \cosh \frac{m\pi y}{a} \right)$$

$$w_h = \sum_{m=1}^{\infty} \left[A_m \sinh \frac{m\pi y}{a} + B_m \cosh \frac{m\pi y}{a} + \frac{m\pi y}{a} \left(C_m \sinh \frac{m\pi y}{a} + D_m \cosh \frac{m\pi y}{a} \right) \right] \sin \frac{m\pi}{a} x$$

these constants will now come from the boundary conditions on $y = \pm b/2$

Now for the particular solution for the deflection...



$$w(x, y) = w_h(x, y) + w_p(x, y) \qquad w_h(x, y) = \sum_{m=1}^{\infty} f_m(y) \sin \frac{m\pi}{a} x$$

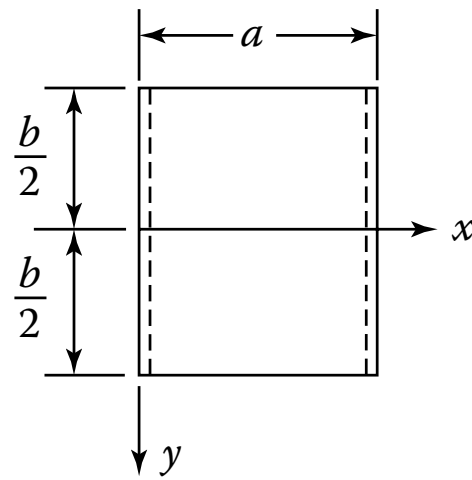
- the same idea, with a single Fourier series also for the term $w_p(x, y)$

$$w_p(x, y) = \sum_{m=1}^{\infty} g_m(y) \sin \frac{m\pi}{a} x$$

- and doing exactly the same, for the general loading term...

$$p(x, y) = \sum_{m=1}^{\infty} p_m(y) \sin \frac{m\pi}{a} x \qquad p_m(y) = \frac{2}{a} \int_0^a p(x, y) \sin \frac{m\pi}{a} x \, dx$$

Next, we put everything together into the differential equation...



$$w_p(x, y) = \sum_{m=1}^{\infty} g_m(y) \sin \frac{m\pi}{a} x \quad \longrightarrow \quad \nabla^4 w_p(x, y) = \frac{p(x, y)}{D}$$

$$p(x, y) = \sum_{m=1}^{\infty} p_m(y) \sin \frac{m\pi}{a} x$$

$$\frac{d^4 g_m(y)}{dy^4} - 2 \left(\frac{m\pi}{a} \right)^2 \frac{d^2 g_m(y)}{dy^2} + \left(\frac{m\pi}{a} \right)^4 g_m(y) = \frac{p_m(y)}{D}$$

$$g_m(y) = \frac{1}{D\pi^4} \frac{a^4}{m^4} p_m(y)$$

$$D = \frac{Et^3}{12(1-\nu^2)}$$

The complete solution for the deflection will finally come as

$$w(x, y) = w_h(x, y) + w_p(x, y)$$

$$w(x, y) = \sum_{m=1}^{\infty} \left[\frac{p_m a^4}{\pi^4 D m^4} + A_m \sinh \frac{m\pi y}{a} + B_m \cosh \frac{m\pi y}{a} + \frac{m\pi y}{a} \left(C_m \sinh \frac{m\pi y}{a} + D_m \cosh \frac{m\pi y}{a} \right) \right] \sin \frac{m\pi}{a} x$$

where the constants are calculated from the boundary conditions on $y = \pm b/2$

$$D = \frac{Et^3}{12(1 - \nu^2)}$$

Summary chart (Levy method)

- represent the external load by a Fourier series:
$$p(x, y) = \sum_{m=1}^{\infty} p_m(y) \sin \frac{m\pi}{a} x$$
- calculate the loading coefficients:
$$p_m(y) = \frac{2}{a} \int_0^a p(x, y) \sin \frac{m\pi}{a} x dx$$
- represent the homogeneous solution as a Fourier series:
$$w_h(x, y) = \sum_{m=1}^{\infty} f_m(y) \sin \frac{m\pi}{a} x$$

- calculate the coefficients for the homogeneous part of the deflection:

$$f_m(y) = A_m \sinh \frac{m\pi y}{a} + B_m \cosh \frac{m\pi y}{a} + \frac{m\pi y}{a} \left(C_m \sinh \frac{m\pi y}{a} + D_m \cosh \frac{m\pi y}{a} \right)$$

- represent the particular solution as a Fourier series:

$$w_p(x, y) = \sum_{m=1}^{\infty} g_m(y) \sin \frac{m\pi}{a} x \quad g_m(y) = \frac{1}{D\pi^4} \frac{a^4}{m^4} p_m(y)$$

- calculate the total deflection:
$$w(x, y) = w_h(x, y) + w_p(x, y) \quad D = \frac{Et^3}{12(1-\nu^2)}$$

Summary chart (moments, stresses, general)

$$M_x = -\frac{Et^3}{12(1-\nu^2)} \left(\frac{\partial^2 w}{\partial x^2} + \nu \frac{\partial^2 w}{\partial y^2} \right) = -D \left(\frac{\partial^2 w}{\partial x^2} + \nu \frac{\partial^2 w}{\partial y^2} \right)$$

$$\sigma_{xx} = -\frac{E}{1-\nu^2} z \left(\kappa_x + \nu \kappa_y \right) = -\frac{E}{1-\nu^2} z \left(\frac{\partial^2 w}{\partial x^2} + \nu \frac{\partial^2 w}{\partial y^2} \right)$$

$$M_y = -\frac{Et^3}{12(1-\nu^2)} \left(\frac{\partial^2 w}{\partial y^2} + \nu \frac{\partial^2 w}{\partial x^2} \right) = -D \left(\frac{\partial^2 w}{\partial y^2} + \nu \frac{\partial^2 w}{\partial x^2} \right)$$

$$\sigma_{yy} = -\frac{E}{1-\nu^2} z \left(\kappa_y + \nu \kappa_x \right) = -\frac{E}{1-\nu^2} z \left(\frac{\partial^2 w}{\partial y^2} + \nu \frac{\partial^2 w}{\partial x^2} \right)$$

$$M_{xy} = -\frac{Et^3}{12(1-\nu^2)} (1-\nu) \frac{\partial^2 w}{\partial x \partial y} = -D(1-\nu) \frac{\partial^2 w}{\partial x \partial y}$$

$$\tau_{xy} = -\frac{E}{1-\nu^2} z \kappa_{xy} = -\frac{E}{1+\nu} z \frac{\partial^2 w}{\partial x \partial y}$$

$$\sigma_{xx} = \frac{12M_x}{t^3} z \quad \Rightarrow \quad \sigma_{xx}|_{\max/\min} = \pm \frac{6M_x}{t^2}$$

$$\sigma_{yy} = \frac{12M_y}{t^3} z \quad \Rightarrow \quad \sigma_{yy}|_{\max/\min} = \pm \frac{6M_y}{t^2}$$

$$\tau_{xy} = \frac{12M_{xy}}{t^3} z \quad \Rightarrow \quad \tau_{xy}|_{\max/\min} = \pm \frac{6M_{xy}}{t^2}$$

$$D = \frac{Et^3}{12(1-\nu^2)}$$

End!