

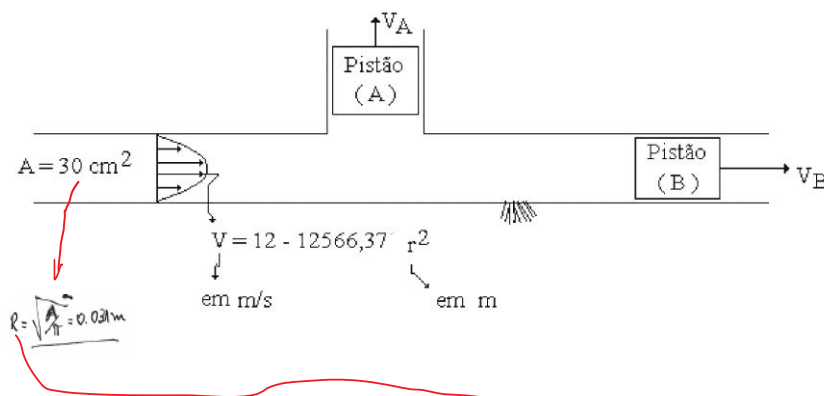
PARTE PRÁTICA (12 valores)

Nº:..... Nome:.....

Exercício 1 (3 val)

No circuito hidráulico representado na figura, em que o fluido é um óleo com uma densidade de 0,9, existe uma fuga. Determine o custo horário dessa fuga, admitindo que o preço do óleo é 5 €/litro.

In the hydraulic system schematically represented in the figure, the fluid is an oil with 0.9 of density., there is a leak. Determine the hourly cost of that leak, knowing that the oil price is 5 €/liter.



$$V_A = 2.5 \text{ m/s}$$

$$A_A = 40 \text{ cm}^2$$

$$V_B = 2.5 \text{ m/s}$$

$$A_B = 30 \text{ cm}^2$$

$$\dot{m}_1 = \dot{m}_A + \dot{m}_B + \dot{m}_F$$

$$\dot{m}_F = \dot{m}_1 - \dot{m}_A - \dot{m}_B$$

$$\dot{m}_F = 16.2 - 9 - 6.75$$

$$\boxed{\dot{m}_F = 0.45 \text{ kg/s}}$$

↳ Custo horário C_h

$$C_h = \dot{m}_F \times 3600 \text{ s/h} \times 0.5 \text{ €/l} \times \frac{1}{0.9} \frac{\text{l}}{\text{kg}}$$

$$\boxed{C_h = 900 \text{ €/h}}$$

Resposta

$$\dot{m}_1 = \rho \cdot 2\pi \int_0^{R_f} (V \cdot n^2) \cdot n \, dn$$

$$= \rho \cdot 2\pi \int_0^{R_f} (12 - 12566.37 n^2) \cdot n \, dn$$

$$= 900 \cdot 2\pi \cdot \left[\frac{12 n^2}{2} - \frac{12566.37 n^4}{4} \right]_0^{0.031}$$

$$\boxed{\dot{m}_1 = 16.2 \text{ kg/s}}$$

$$\dot{m}_A = \rho \cdot V_A \cdot A_A = 900 \cdot 2.5 \cdot 40 \cdot 10^{-4}$$

$$\boxed{\dot{m}_A = 9 \text{ kg/s}}$$

$$\dot{m}_B = \rho \cdot V_B \cdot A_B = 900 \cdot 2.5 \cdot 30 \cdot 10^{-4}$$

$$\boxed{\dot{m}_B = 6.75 \text{ kg/s}}$$

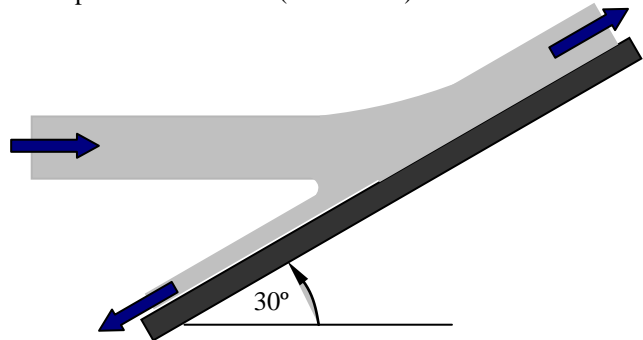
Exercício 2 (3 val)

Um jacto de água sai de uma mangueira com 2 cm de diâmetro e incide sobre uma placa plana (ver figura) mantendo a configuração geométrica inicial. O caudal debitado pela mangueira é de 30 litros por minuto. Admitindo ausência de forças de atrito, determine:

- a) A fração do caudal de água que se escoar para cada uma das direções (1.5 valores)
b) A força (módulo e direção) necessária para manter a placa estacionária. (1.5 valores)

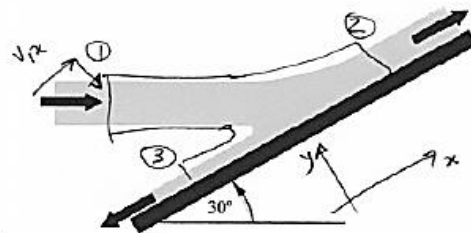
A 2 cm in diameter water jet exits a tube and hits a flat plate maintaining the original geometric configuration (see Figure). The flow rate delivered by the hose is 30 litres per minute. Assuming no friction forces, determine:

- a) The water fraction flowing into each of the directions
b) The required force (modulus and direction) for maintaining the plate stationary.



i)

$$\begin{cases} m_1 = m_2 + m_3 \\ m_2 = x \cdot m_1 \\ m_3 = (1-x) \cdot m_1 \end{cases}$$



x é a percentagem de m_1 que vai para ②

$$\sum F_x = 0 = \Delta \rho \frac{dm}{dt} x = 0 \text{ porque não há atrito}$$

$$0 = -m_1 v_{1x} + m_2 v_{2x} + m_3 v_{3x}$$

$$= -m_1 v_1 \cos 30^\circ + x m_1 v_1 - (1-x) m_1 v_1$$

$$0 = m_1 v_1 (-\cos 30^\circ + x - 1 + x) \Rightarrow 2x - 1 - \cos 30^\circ = 0$$

$$x = \frac{1.866}{2} = 0.93$$

93% → 1

7% → 3

$F_x = 0$ (já vimos na alínea anterior)

$$F_y = \Delta \rho \frac{dm}{dt} y = +m_1 v_{1y} + m_2 \cdot 0 + m_3 \cdot 0 = 0.5 \times 1.59 \sin 30^\circ = 0.397 \text{ N}$$

$$\begin{cases} F_x = 0 \\ F_y = 0.397 \end{cases} \Rightarrow \vec{F} = \sqrt{F_x^2 + F_y^2} = 0.397 \text{ N}$$

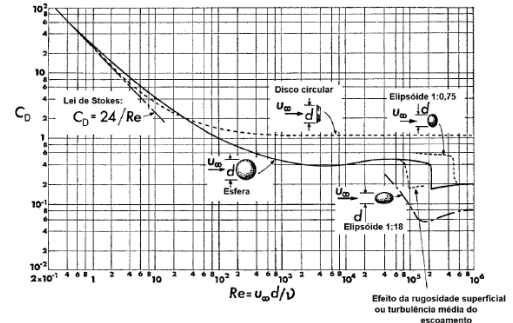
perpendicular à placa
e no sentido + segundo
o ref. estabelecido

Exercício 3 (3 val)

Considere que está a desenvolver um protótipo de um balão, com forma esférica, para ser lançado na atmosfera. O modelo do balão tem um diâmetro de 3 cm que se encontra mergulhado em água ($\mu_{\text{água}} = 0.001003 \text{ kg.m}^{-1}.\text{s}^{-1}$). A velocidade do modelo durante o ensaio é 2 m.s^{-1} .

a) Calcule o coeficiente de arrasto para este balão. (1.0 val)

b) Sabendo que o diâmetro pretendido para o protótipo do balão é 2 m, calcule a velocidade do protótipo e a força de arrasto exercida pelo ar sobre o protótipo nessas condições de utilização. Considere $\rho_{\text{ar}} = 1.205 \text{ kg.m}^{-3}$ e $\mu_{\text{ar}} = 1.80 \times 10^{-5} \text{ kg.m}^{-1}.\text{s}^{-1}$. (2.0 val)



A balloon prototype is under development, with a spherical shape, to be launched to the atmosphere. A balloon model has 3 cm of diameter and is tested in water ($\mu_{\text{water}} = 0.001003 \text{ kg.m}^{-1}.\text{s}^{-1}$). The model velocity is 2 m.s^{-1} .

a) Determine the drag coefficient for this ballon. (1 val)

b) Knowing that the desired diameter to the ballon prototype is 2 m, determine the expected prototype's velocity and respective dragforce. Consider $\rho_{\text{ar}} = 1.205 \text{ kg.m}^{-3}$ e $\mu_{\text{ar}} = 1.80 \times 10^{-5} \text{ kg.m}^{-1}.\text{s}^{-1}$. (2.0 val)

Problema do balão (exame 20150109)

$$a) C_{\text{drag}} = f(Re) \text{ então } Re_m = \frac{\rho N \cdot D}{\mu} = \frac{10^3 \times 2 \times 3 \times 10^{-2}}{1 \times 10^{-3}} \approx 6 \times 10^4 \quad (15\%)$$

Pelo diagrama $C_d \approx 0,5$ (15%) (5,98 \times 10^4)
(regime turbulento)

$$b) Re_p = Re_m \quad (20\%) \quad \rho \frac{N_p D_p}{\mu_p} = Re_m \text{ ou } N_p = Re_m \frac{\mu_p}{D_p} = 0,45 \text{ m.s}^{-1} \quad (20\%)$$

Sabendo que $C_{dp} = C_{dm}$ (10%) então

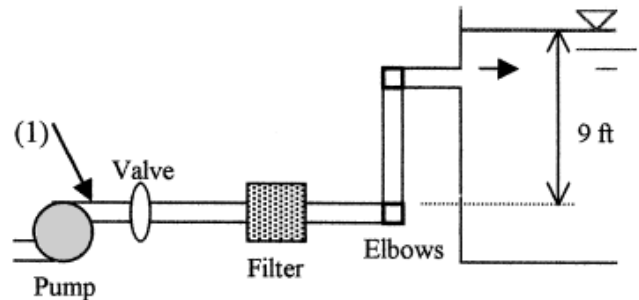
$$F_{\text{drag}} = \frac{1}{2} C_d \rho A N^2 = \frac{1}{2} \times 0,5 \times 1,205 \times \pi \times \frac{2^2}{4} \times (0,45)^2 = 9,162 \text{ N} \quad (10\%)$$

Exercício 4 (3 val)

A bomba de água da figura mantém uma pressão de 45 kPa no ponto 1. Nesta tubagem existe um filtro, uma válvula meia aberta ($k=2.8$) e dois cotovelos regulares aparafusados. A tubagem de aço comercial de 4 in de diâmetro tem 80 ft de comprimento.

- Se o caudal for de $0.4 \text{ ft}^3/\text{s}$, qual o coeficiente de perda de carga localizada do filtro?
- Se a válvula estiver totalmente aberta (assuma $k_{\text{válvula}}=0$) e $k_{\text{filtro}}=7$, qual é o caudal resultante?

The water pump in Figure maintains a pressure of 45 kPa at point 1. There is a filter, a half-open disk valve, and two regular screwed elbows. There are 80 ft of 4-inch diameter commercial steel pipe. a) If the flow rate is $0.4 \text{ ft}^3/\text{s}$, what is the loss coefficient of the filter? b) If the disk valve is wide open (assume $k=0$) and $K_{\text{filter}} = 7$, what is the resulting flow rate?



Solution: For water, take $\rho = 1.94 \text{ slug/ft}^3$ and $\mu = 2.09\text{E-}5 \text{ slug/ft}\cdot\text{s}$. The energy equation is written from point 1 to the surface of the tank:

$$\frac{p_1}{\rho g} + \frac{V_1^2}{2g} + z_1 = \frac{p_2}{\rho g} + \frac{V_2^2}{2g} + z_2 + h_f + K_{\text{valve}} + K_{\text{filter}} + 2K_{\text{elbow}} + K_{\text{exit}} \quad (30\%)$$

(a) From the flow rate, $V_1 = Q/A = (0.4 \text{ ft}^3/\text{s})/[(\pi/4)(4/12 \text{ ft})^2] = 4.58 \text{ ft/s}$. Look up minor losses and enter into the energy equation:

$$\begin{aligned} \frac{(6.5)(144) \text{ lbf/ft}^2}{62.4 \text{ lbf/ft}^3} + \frac{(4.58 \text{ ft/s})^2}{2(32.2 \text{ ft/s}^2)} + 0 \\ = 0 + 0 + 9 \text{ ft} + \frac{(4.58)^2}{2(32.2)} \left[f \frac{80 \text{ ft}}{(4/12 \text{ ft})} + 2.8 + K_{\text{filter}} + 2(0.64) + 1 \right] \end{aligned}$$

We can solve for K_{filter} if we evaluate f . Compute $\text{Re}_D = (1.94)(4.58)(4/12)/(2.09\text{E-}5) = 1.42 \times 10^5$ 141,700. For commercial steel, $\epsilon/D = 0.00015 \text{ ft}/0.333 \text{ ft} = 0.00045$. From the Moody chart, $f \approx 0.0193$, and $fL/D = 4.62$. The energy equation above becomes:

$$15.0 \text{ ft} + 0.326 \text{ ft} = 9 \text{ ft} + 0.326(4.62 + 2.8 + K_{\text{filter}} + 1.28 + 1) \text{ ft}, \quad (20\%)$$

$$\text{Solve } K_{\text{filter}} \approx 9.7 \quad \text{Ans. (a)}$$

(b) If $K_{\text{filter}} = 7.0$ and V is unknown, we must iterate for the velocity and flow rate. The energy equation becomes, with the disk valve wide open ($K_{\text{valve}} \approx 0$):

$$15.0 \text{ ft} + \frac{V^2}{2(32.2)} = 9 \text{ ft} + \frac{V^2}{2(32.2)} \left(f \frac{80}{1/3} + 0 + 7.0 + 1.28 + 1 \right) \quad (20\%)$$

Iterate to find $f \approx 0.0189$, $\text{Re}_D = 169,000$, $V = 5.49 \text{ ft/s}$, $Q = AV = 0.48 \text{ ft}^3/\text{s}$ Ans. (b) (10%)