Fitted ALE scheme for Two-Phase Navier–Stokes Flow

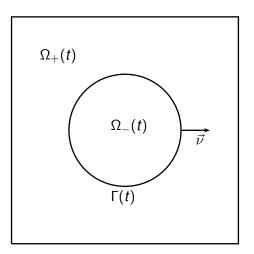
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Problem setting

Domain Ω in the 2-dimensional case.



Governing equations

Bulk equations

$$\rho (\vec{u}_t + (\vec{u} \cdot \nabla) \vec{u}) - \nabla \cdot \underline{\underline{\sigma}} = \vec{f} = \rho \vec{f}_1 + \vec{f}_2 \quad \text{in } \Omega_{\pm}(t),$$

$$\nabla \cdot \vec{u} = 0 \quad \text{in } \Omega_{\pm}(t),$$

where

$$\underline{\underline{\sigma}} = \mu \left(\nabla \vec{u} + (\nabla \vec{u})^T \right) - \rho \underline{\underline{id}} = 2 \mu \underline{\underline{D}} (\vec{u}) - \rho \underline{\underline{id}}.$$

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Interface equations

$$[\vec{u}]_{-}^{+} = \vec{0}$$
 on $\Gamma(t)$,
 $[\underline{\sigma}\vec{v}]_{-}^{+} = -\gamma \varkappa \vec{v}$ on $\Gamma(t)$,
 $\vec{\mathcal{V}} \cdot \vec{v} = \vec{u} \cdot \vec{v}$ on $\Gamma(t)$.

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▶ To close the system, we prescribe the initial data $\Gamma(0) = \Gamma_0$ and some boundary condition for \vec{u} on $\partial\Omega$.



Interface treatment

▶ $\Gamma(t)$ is a sufficiently smooth evolving hypersurface without boundary that is parameterized by $\vec{x}(\cdot,t): \Upsilon \to \mathbb{R}^d$, therefore

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It holds that

$$\Delta_{\mathbf{s}} \, \mathbf{id} = \varkappa \, \vec{\nu} \quad \text{on } \Gamma(t)$$
,

where $\Delta_s = \nabla_s$. ∇_s is the Laplace-Beltrami operator on $\Gamma(t)$ with ∇_s . and ∇_s denoting surface divergence and surface gradient on $\Gamma(t)$.



Stokes weak formulation

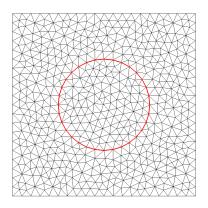
Using the function spaces

$$\begin{split} \mathbb{U} &:= [H^1_0(\Omega)]^d \,, \qquad \mathbb{P} := L^2(\Omega) \qquad \text{and} \\ \widehat{\mathbb{P}} &:= \left\{ \eta \in \mathbb{P} : \int_\Omega \eta \; \mathrm{d}\mathcal{L}^d = 0 \right\}, \end{split}$$

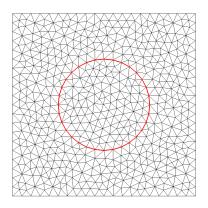
the Stokes weak formulation is

$$\begin{split} &2\left(\mu\,\underline{\underline{\mathcal{D}}}(\vec{u}),\underline{\underline{\mathcal{D}}}(\vec{\xi})\right) - \left(p,\nabla\,.\,\vec{\xi}\right) - \gamma\,\left\langle\varkappa\,\vec{\nu},\vec{\xi}\right\rangle_{\Gamma(t)} = \left(\vec{f},\vec{\xi}\right) \quad\forall\,\vec{\xi}\in\mathbb{U}\,,\\ &(\nabla\,.\,\vec{u},\varphi) = 0 \quad\forall\,\varphi\in\widehat{\mathbb{P}}\,,\\ &\left\langle\vec{\mathcal{V}} - \vec{u},\chi\,\vec{\nu}\right\rangle_{\Gamma(t)} = 0 \quad\forall\,\chi\in H^1(\Gamma(t))\,,\\ &\left\langle\varkappa\,\vec{\nu},\vec{\eta}\right\rangle_{\Gamma(t)} + \left\langle\nabla_s\,\mathrm{id},\nabla_s\,\vec{\eta}\right\rangle_{\Gamma(t)} = 0 \quad\forall\,\vec{\eta}\in[H^1(\Gamma(t))]^d\,. \end{split}$$

Fitted approach

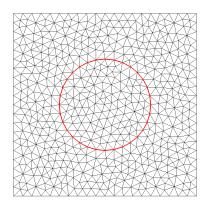


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- Cons: possible bulk mesh distortion and difficult bulk mesh adaptation.

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- Let $(\mathbb{U}^m, \mathbb{P}^m)$ be an LBB-stable pair of velocity/pressure finite element spaces in the bulk, e.g. P2-P0 (only in 2d) or P2-P1, with \mathbb{P}^m possibly extended by an additional basis function.

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- ► Then our finite element approximation is based directly on the discretization of the weak formulation.

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- Pressure jumps at the interface are captured accurately for standard pressure finite element spaces without the need for XFEM extensions.
- ► The surface mesh quality is maintained and for the semidiscrete scheme an equidistribution property can be shown in 2d.

Solution method

Find $(\vec{U}^{m+1}, P^{m+1}, \kappa^{m+1}, \delta \vec{X}^{m+1})$ such that

$$\begin{pmatrix} \vec{B}_{\Omega} & \vec{C}_{\Omega} & -\gamma \, \vec{N}_{\Gamma,\Omega} & 0 \\ \vec{C}_{\Omega}^T & 0 & 0 & 0 \\ \vec{N}_{\Gamma,\Omega}^T & 0 & 0 & -\frac{1}{\tau_m} \, \vec{N}_{\Gamma}^T \\ 0 & 0 & \vec{N}_{\Gamma} & \vec{A}_{\Gamma} \end{pmatrix} \begin{pmatrix} \vec{U}^{m+1} \\ P^{m+1} \\ \kappa^{m+1} \\ \delta \vec{X}^{m+1} \end{pmatrix} = \begin{pmatrix} \vec{c} \\ 0 \\ 0 \\ -\vec{A}_{\Gamma} \, \vec{X}^m \end{pmatrix} \,,$$

where $\vec{X}^{m+1} = \vec{X}^m + \delta \vec{X}^{m+1}$.

Schur complement approach

Let

$$\Xi_\Gamma := \begin{pmatrix} 0 & -\frac{1}{\tau_m} \vec{N}_\Gamma^T \\ \vec{N}_\Gamma & \vec{A}_\Gamma \end{pmatrix} \,.$$

Therefore

$$\begin{pmatrix} \vec{B}_{\Omega} + \gamma \left(\vec{N}_{\Gamma,\Omega} \ 0 \right) \Xi_{\Gamma}^{-1} \begin{pmatrix} \vec{N}_{\Gamma,\Omega}^{T} \\ 0 \end{pmatrix} & \vec{C}_{\Omega} \\ \vec{C}_{\Omega}^{T} & 0 \end{pmatrix} \begin{pmatrix} \vec{U}^{m+1} \\ P^{m+1} \end{pmatrix} =$$

$$\begin{pmatrix} \vec{c} - \gamma \left(\vec{N}_{\Gamma,\Omega} \ 0 \right) \Xi_{\Gamma}^{-1} \begin{pmatrix} 0 \\ \vec{A}_{\Gamma} \vec{X}^{m} \end{pmatrix} \end{pmatrix}$$

and

$$\begin{pmatrix} \kappa^{m+1} \\ \delta \vec{X}^{m+1} \end{pmatrix} = \Xi_{\Gamma}^{-1} \begin{pmatrix} -\vec{N}_{\Gamma,\Omega}^T \vec{U}^{m+1} \\ -\vec{A}_{\Gamma} \vec{X}^m \end{pmatrix}.$$

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As preconditioner we use the matrix

$$\mathcal{P} = egin{pmatrix} ec{\mathcal{B}}_\Omega & ec{\mathcal{C}}_\Omega \ 0 & -M_\Omega \end{pmatrix} \,.$$



Mesh smoothing and remeshing

▶ Smoothing: find a displacement $\vec{\psi} \in [H^1(\Omega)]^d$ such that

$$\nabla \cdot \underline{\underline{S}} = \vec{0} \qquad \text{in } \Omega^m_{\pm},$$

$$\vec{\psi} = \delta \vec{X} \qquad \text{on } \Gamma^m,$$

$$\vec{\psi} \cdot \vec{\mathbf{n}} = \mathbf{0} \qquad \text{on } \partial \Omega,$$

where $\underline{\underline{S}} = 2 \, \underline{\underline{D}}(\vec{\psi}) + (\nabla \, .\vec{\psi}) \, \underline{\underline{id}}$ is the stress tensor and where $\underline{\vec{n}}$ is the outer unit normal to Ω on $\partial \Omega$.

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Remeshing: perform remeshing when

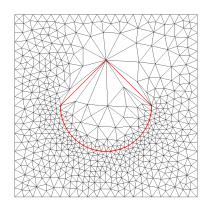
$$\frac{\max_{o \in \mathcal{T}^{m+1}}(\mathcal{H}^d(o))}{\min_{o \in \mathcal{T}^{m+1}}(\mathcal{H}^d(o))} \ge C_r,$$

where $C_r \ge 1$ is a fixed constant.



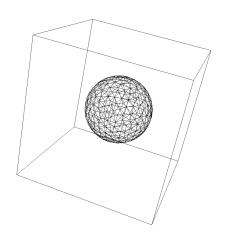
Equidistribution property experiment

$$\rho_{\pm} = 0, \quad \mu_{\pm} = 1, \quad \gamma = 1$$



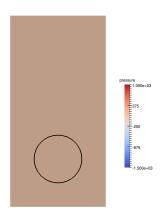
Shear flow experiment

$$ho_{\pm}=0\,,\quad \mu_{\pm}=1\,,\quad \gamma=3\,,\quad ec{g}(ec{x})=x_{3}ec{e}_{1}\quad ext{on }\partial\Omega$$



Rising bubble experiment

$$\rho_{+} = 10^{3} \,, \rho_{-} = 10^{2} \,, \mu_{+} = 10 \,, \mu_{-} = 1 \,, \gamma = 24.5 \,, \vec{f} = -0.98 \vec{e}_{2}$$



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- In order to reduce the computational cost of the interpolation, bulk elements are sorted and traversed following a continuous path; barycentric coordinates are used to locate the interpolation points in the previous bulk mesh.
- On the other hand, to improve the accuracy, the interpolation should be performed only after a remeshing.

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- This prescribed flow needs to be accounted for in the approximation of the momentum equation; in practice, it adds a convective-type term to the momentum balance.
- ► The movement of the bulk mesh is incorporated in the finite element approximation therefore it avoids the repeated interpolation onto the bulk mesh.

Outlook

- ► Test other solvers/preconditioners to solve the algebraic linear system more efficiently.
- Include surface active agents (surfactants) to the model.
- Use adaptive meshes to increase the accuracy of the scheme.
- Test higher order spaces to approximate the displacement of the interface.

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