

$$\omega_p = 0,2\pi, \omega_s = 0,4\pi \quad A = 60\text{dB} \rightarrow \text{Blackman} \quad 8A. Q1$$

$$\Delta\omega = \omega_s - \omega_p = 0,2\pi$$

$$\frac{11\pi}{M} = \Delta\omega \Rightarrow \frac{11\pi}{M} = 0,2\pi \rightarrow M = 55$$

$$\alpha = \frac{M-1}{2} = \frac{54}{2} = 27$$

$$\text{cut-off frequency} = \omega_c = \frac{\omega_p + \omega_s}{2} = \frac{0,6\pi}{2} = 0,3\pi$$

$$R_p = 0,25$$

$$\int R_p = 9004$$

$$A_s = 71\text{dB}$$

چون پنجره در یک فیلتر ضرب شده یک تضعیف ایجاد می کند، چون بکس $A = 74\text{dB}$ است، A فیلتر ما به سمت -74dB می رود.

چون باندها $\Delta\omega = 0,2\pi$ و $\omega_c = 0,3\pi$ چون بالایی آن پنجره متفاوت است پس می توان است متفاوت شود. چون باندها کوچکتر می شود، پس راندها بیشتر می گذارد.

$$\omega_p = 0,2\pi, \omega_s = 0,4\pi \rightarrow \Delta\omega = \omega_s - \omega_p = 0,2\pi \quad 8B. Q1$$

$$A = 60\text{dB} \rightarrow M = \frac{60-71,95}{2,285\Delta\omega} + 1 = 37,25 \rightarrow M = 38 \rightarrow \text{FIR-GLP Type I}$$

$$\beta = 0,1102(A_s - 8,7) = 0,1102(60 - 8,7) = 5,65326$$

چون FIR-GLP Type I شده فیلتر خوبی است.
 A_s درست آمده (واقعاً) 60dB است که خواسته مسئله را بر آورده کرده است.

$$\text{Rectangular} \quad \frac{1,8\pi}{M} = 0,2\pi \rightarrow M = 9$$

$$A_s = 18\text{dB} \rightarrow \text{peak approximate error}$$

$$R_p = 2 \rightarrow \text{بیل خیلی زیاد}$$

چون $A_s = 18\text{dB}$ است، بعضی از صداها می که انتظار نداریم در خروجی ظاهر می شود.

$$\omega_p = 0,2\pi, \omega_s = 0,4\pi$$

$$T_d = 2$$

$$R_p = 1 \text{ dB}, A_s = 20 \text{ dB}$$

$$\Omega_p = \frac{2}{T} \tan\left(\frac{\omega_p}{2}\right) = \tan\left(\frac{0,2\pi}{2}\right) = \tan(0,1\pi) = 0,32491$$

$$\Omega_s = \frac{2}{T} \tan\left(\frac{\omega_s}{2}\right) = \tan(0,2\pi) = 0,72654$$

$$\text{Butterworth: } |H_c(j\Omega)|^2 = \frac{1}{1 + \left(\frac{\Omega}{\Omega_c}\right)^{2N}} \rightarrow \boxed{N=4}$$

$$N = \frac{\log\left[\left(10^{\frac{R_p}{10}} - 1\right) / \left(10^{\frac{A_s}{10}} - 1\right)\right]}{2 \log_{10}\left(\frac{\Omega_p}{\Omega_s}\right)}$$

$$H(s) = \frac{\Omega_c^N}{\prod_{\text{LHP Poles}} (s - p_k)}$$

$$\left\{ \begin{aligned} \Omega_c &= \frac{\Omega_p}{\sqrt[2N]{10^{\frac{R_p}{10}} - 1}} = \frac{0,32491}{\sqrt[8]{10^{0,1} - 1}} = 0,38469 \\ \Omega_c &= \frac{\Omega_s}{\sqrt[2N]{10^{\frac{A_s}{10}} - 1}} = \frac{0,72654}{\sqrt[8]{10^2 - 1}} = 0,40907 \end{aligned} \right.$$

$$H_a(s) = \frac{0,0219}{(s^2 + 0,7108s + 0,1480)(s^2 + 0,2944s + 0,1480)}$$

$$H(z) = H_a\left(\frac{2}{T} \cdot \frac{1 - z^{-1}}{1 + z^{-1}}\right) = H_a\left(\frac{1 - z^{-1}}{1 + z^{-1}}\right)$$

$$\rightarrow H(z) = \frac{0,0082(1 + z^{-1})^4}{(1 - 0,9167z^{-1} + 0,2352z^{-2})(1 - 1,1814z^{-1} + 0,5918z^{-2})}$$

$$\omega_n = \frac{2}{\pi} \tan^{-1} \left(\frac{\Omega_c \cdot 2}{2} \right) = \frac{2}{\pi} \tan^{-1}(\Omega_c)$$

: B. Q2

$$\text{poles} = \Omega_c e^{j \frac{\pi}{2N} (2k+N-1)}$$

$$N = \frac{\log \left[(10^{\frac{R_p}{10}} - 1) / (10^{\frac{A_s}{10}} - 1) \right]}{2 \log \left(\frac{\Omega_p}{\Omega_s} \right)} = 3.8 \rightarrow 4$$

$$\Omega_c = \frac{\Omega_p}{2 \sqrt[2N]{10^{\frac{R_p}{10}} - 1}} = 0.3847$$

$$\omega_n = \frac{2}{\pi} \tan^{-1}(0.3847) = 0.2338$$

$$H(z) = \frac{0.0081684 (z+1)^4}{(z^2 - 0.9167z + 0.2352)(z^2 - 1.181z + 0.5918)}$$

Chebyshev: chebyshev-I filter have equiripple response in the passband, while chebyshev-II filter have equiripple response in the stopband. Butterworth filters have monotonic response in both bands.

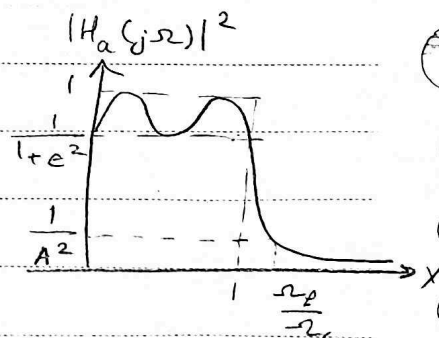
: C. Q2

→ chebyshev filters provide lower order than butterworth filters for the same specifications.

$$\text{chebyshev-I: } |H_a(j\Omega)|^2 = \frac{1}{1 + \epsilon^2 T_N^2 \left(\frac{\Omega}{\Omega_c} \right)}$$

Passband ripple factor
order of filter

$$T_N(x) = \begin{cases} \cos(N \cos^{-1}(x)) & , 0 \leq x \leq 1 \\ \cosh(\cosh^{-1}(x)) & , 1 < x < \infty \end{cases} \quad x = \frac{\Omega}{\Omega_c}$$



$$\epsilon = \sqrt{10^{R_p/10} - 1}, \quad A = 10^{A_s/20}$$

$$\Omega_c = \Omega_p, \quad \Omega_r = \frac{\Omega_s}{\Omega_p}$$

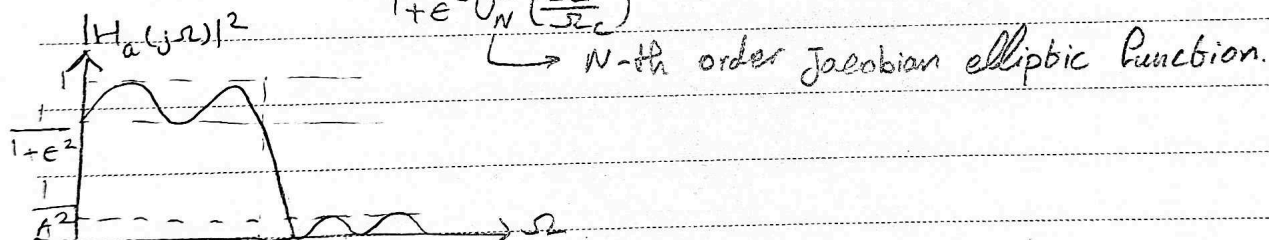
$$g = \sqrt{(A^2 - 1)/2}, \quad N = \left\lceil \frac{\log[g + \sqrt{g^2 - 1}]}{\log[\Omega_r + \sqrt{\Omega_r^2 - 1}]} \right\rceil$$

+ A Chebyshev-II filter is related to the Chebyshev-I filter through a simple transformation. It has monotone passband and an equiripple stopband which implies that this filter has both poles and zeros in the s-plane. Therefore the group delay characteristics are better (and the phase response more linear) in the passband than Chebyshev-I.

$$|H_a(j\Omega)|^2 = \frac{1}{1 + [e^2 T_N^2(\frac{\Omega}{\Omega_c})]^{-1}}$$

+ Elliptic low pass filters exhibit equiripple behavior in the passband as well as in the stopband. They are similar in magnitude response characteristics to the FIR equiripple filters. Therefore elliptic filters are optimum filters in that they achieve the minimum order N for the given specifications (or alternately, achieve the sharpest transition band for the given order N). These filters are very difficult to analyze and to design.

$$|H_a(j\Omega)|^2 = \frac{1}{1 + e^2 U_N^2(\frac{\Omega}{\Omega_c})}$$



→ Elliptic filters provide optimal performance in the magnitude-squared response but have highly nonlinear phase response in the passband (which is undesirable).

Butterworth filters, have maximally flat magnitude response and require a higher-order N (more poles) to achieve the same stopband specification. They exhibit a fairly linear phase response in their passband. The Chebyshev filters have phase characteristics that lie somewhere in between. In practical applications, we do consider Butterworth as well as Chebyshev filters, in addition

PAPCO to elliptic filters. The choice depends on both the filter order and phase characteristics.
 → Controls distortion influence processing speed and implementation complexity

for the 1st signal pairs linear convolution and circular convolution are the same because $\rightarrow L = 4 + 4 = 8$

$$P = 8 + 4 = 12$$

$$\Delta = L + P - 1 = 19$$

$$\Delta < N = 21$$

but for the 2nd signal pairs $\rightarrow L = 7 + 5 = 12$

$$P = 11 + 5 = 16$$

$$\Delta = 12 + 16 - 1 = 27$$

$$\Delta > N = 21$$

$$\Delta - N = 27 - 21 = 6 \rightarrow \text{6 زائد فواصل}$$

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