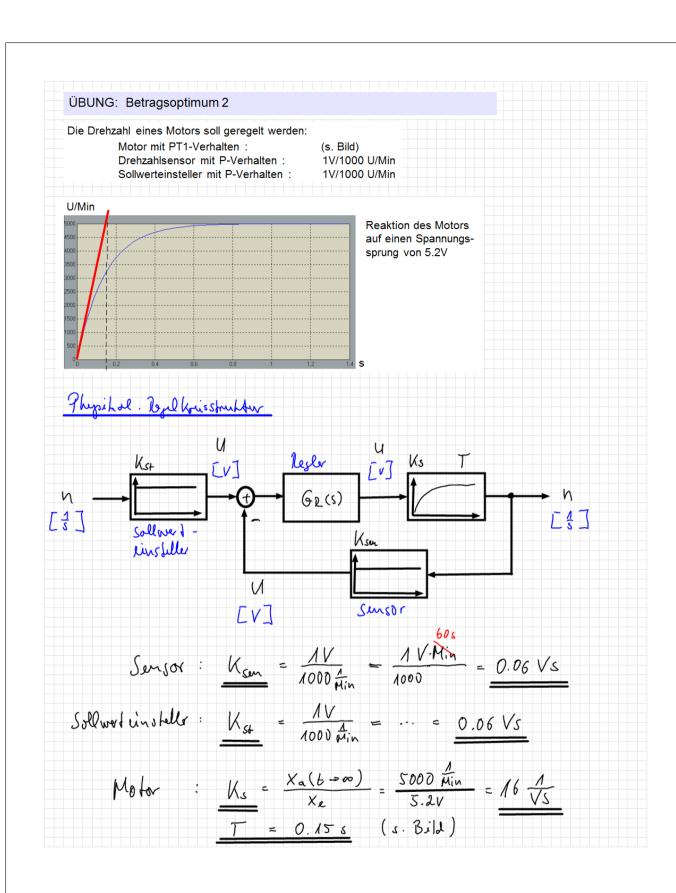


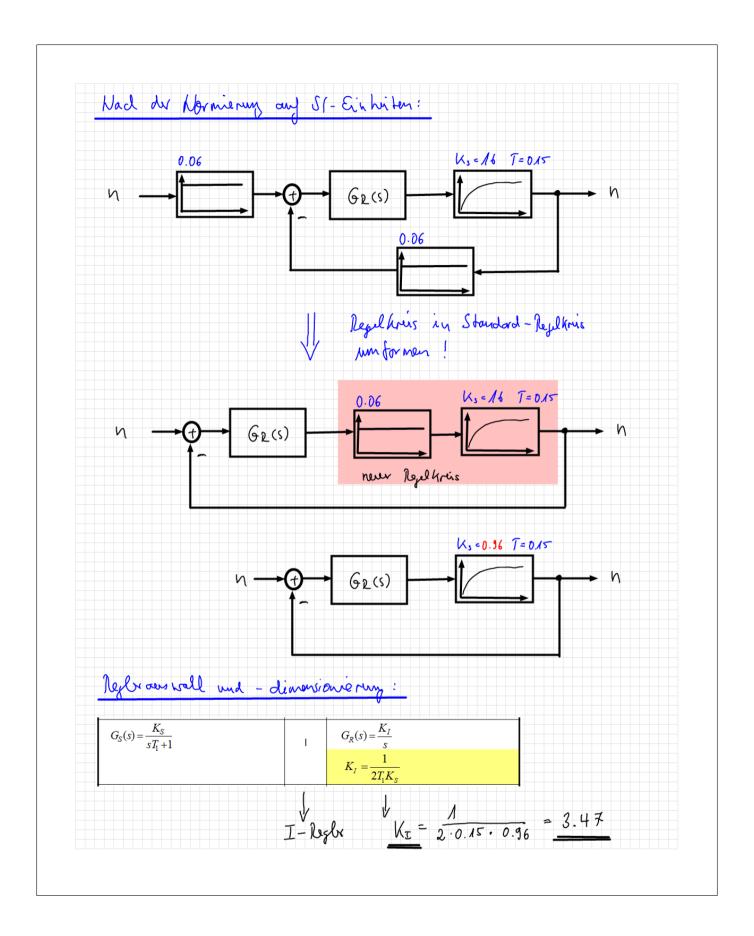
$$G(s) = \frac{G_{0}(s)}{A + G_{0}(s)} = \frac{\frac{5}{3(0.4s + A)}}{A + \frac{5}{3(0.4s + A)}}$$

$$= \frac{5}{3(0.4s + A)} + \frac{5}{3(0.4s + A)}$$

$$= \frac{5}{3(0.4s + A)} + \frac{5}{3(0.4s + A)}$$

$$= \frac{5}{3($$





ÜBUNG: Reglerentwurf mit dem symm. Optimum

Die lin. und normierten Differentialgleichungen des Ballons lauten:

$$\dot{\mathcal{G}} + \frac{1}{T_1} \mathcal{G} = q \tag{1}$$

$$T_2 \cdot \ddot{h} + \dot{h} = a \cdot \mathcal{G} \tag{2}$$

: Temperatur q : Wärmezufuhr

tur
$$T_1 = 250$$
ufuhr $T_2 = 25$

$$h$$
 : Höhe



$$S \Theta(s) + \frac{1}{T_A} \Theta(s) = Q(s)$$
 $\Longrightarrow \Theta(s) \cdot \left(S + \frac{1}{T_A}\right) = Q(s)$

$$\implies \bigcirc (s) \cdot \left(S + \frac{1}{7} \right) = Q(s)$$

$$s^2 T_2 H(s) + s H(s) = a \Theta(s) \implies H(s) \cdot (T_2 s^2 + s) = a \cdot \Theta(s)$$

Doraus erseben sid die Teilnibertragungsfunktionen:

$$G_{\Lambda}(S) = \frac{\Theta(S)}{Q(S)} = \frac{1}{S + \frac{d}{T_{\Lambda}}} = \frac{T_{\Lambda}}{ST_{\Lambda} + 1} (PT_{\Lambda})$$

$$G_{2}(s) = \frac{H(s)}{\Theta(s)} = \frac{\alpha}{s(sT_{2}+1)}$$

Die Gerant übstragungs funktion lantet dann:

$$G(s) = G_{s}(s) \cdot G_{s}(s) = \frac{H(s)}{Q(s)} =$$

$$= \frac{62.5}{5(2505+1)(255+1)}$$

Wegen Integral element
$$\Longrightarrow$$
 Symm. Optimum
$$G_2.5 - K_0 \cdot K_L$$

$$G_C(s) = \frac{5(2.5) + 1}{5(2.5) + 1} (2.5 + 1) - 1$$

$$- T_E$$

$$G_S(s) = \frac{K_0 K_0}{5(3T_1 + 1)(3T_2 + 1)} - T_E$$

$$G_S(s) = \frac{K_0 K_0}{5(3T_1 + 1)(3T_2 + 1)} - T_E$$

$$T_1 > T_2, T_2 - \sum_{i=1}^{n} I_i$$

$$F = T_1, T_0 - B^2 T_0, K_0 = \frac{1}{\beta K_1 T_0 K_0}$$

$$F = T_1 = 250 \quad (Vorhalbent, D - Andmi)$$

$$T_N = \int_0^2 T_E = 100 \quad (Nadsallent, I - Andmi)$$

$$M_0 = \frac{1}{\beta (K_0 \cdot K_0) \cdot T_E} = \frac{1}{2 \cdot (2.5 \cdot 1.5)} = \frac{320 \cdot 10^{-6}}{2 \cdot (2.5 \cdot 1.5)}$$

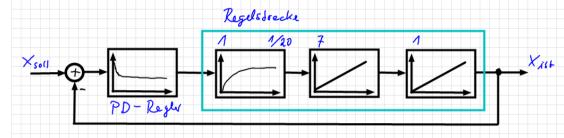
$$D = \frac{1}{\beta (K_0 \cdot K_0) \cdot T_0} = \frac{1}{2 \cdot (2.5 \cdot 1.5)} = \frac{320 \cdot 10^{-6}}{2 \cdot (2.5 \cdot 1.5)}$$

$$P_0 = \frac{1}{\beta (K_0 \cdot K_0) \cdot T_0} = \frac{1}{\beta (K_0 \cdot K_0) \cdot T_$$

Fortsetzung der Übung: "Balancieren eines Balls"

$$G_2(s) = \frac{X(s)}{\Phi(s)} = \frac{7}{s^2}$$
 a) Dimensionieren Sie den PD-Regler.

$$G_1(s) = \frac{\Phi(s)}{U(s)} = \frac{1}{\frac{1}{20}s + 1}$$



$$G_S = \frac{7}{S^2} \frac{1}{\left(\frac{1}{20}S + 1\right)}$$

$$k_s = 7$$

$$T_s = \frac{1}{2}$$

Regliamensionerung

$$T_{V} = 10 T_{S} \cdot \sqrt{27} = 10 \cdot \frac{1}{20} \cdot \sqrt{57} = 1.118$$

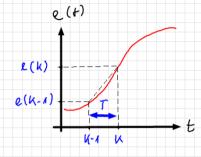
$$\frac{Ke}{K_{s} \cdot T_{v}^{2}} = \frac{\sqrt{57}}{7 \cdot 1.118^{2}} = 0.2556$$

$$G_{PD}(s) = K_2 \frac{s Tv + 1}{s \frac{Tv}{a} + 1} = \frac{0.286s + 0.256}{0.224s + 1}$$

I Simulation in Vorlessing

Quasikontinnierliche Payler

a) Diffrentiation



 $\frac{de(b)}{dt} \approx \frac{e(u) - e(h-1)}{T}$ $= \frac{1}{2} \int_{a}^{b} \frac{du}{dt} du dt$ $= \frac{1}{2} \int_{a}^{b} \frac{du}{dt} dt$ $= \frac{1}{2} \int_{a}^{b} \frac{du}{dt} dt$

b) Indegration
e(+)

 $\int_{0}^{kT} e(z) dz \approx T \cdot \sum_{i=0}^{k-1} e(i)$ gluidable Integration

Pekurcine Form du addition PID - leglers

$$M(h) - M(K-1) = K\rho \cdot e(h) + \frac{K\rho}{TN} \cdot T \sum_{k=0}^{M} e(k) + K\rho \cdot T_v \stackrel{A}{+} \cdot \left[e(h) - e(h-1) \right]$$

$$- K\rho \cdot e(h-1) - \frac{K\rho}{TN} \cdot T \sum_{k=0}^{M} e(k) - K\rho \cdot T_v \cdot \stackrel{A}{+} \cdot \left[e(h-1) - e(h-1) \right]$$

$$= K\rho \cdot \left[e(h) - e(h-1) \right] + \frac{K\rho}{TN} \cdot T \cdot e(h-1) + \frac{K\rho}{TN} \cdot T \cdot e(h-1) + \frac{K\rho}{TN} \cdot T \cdot \frac{A}{+} \cdot \left[e(h-1) + e(h-2) \right]$$

$$= e(h) \left[K\rho \left(1 + \frac{T\nu}{T} \right) \right] + e(h-1) \left[K\rho \left(-1 + \frac{T}{TN} - 2\frac{T\nu}{T} \right) \right]$$

$$+ e(h-2) \cdot K\rho \cdot \frac{T\nu}{TN}$$

$$= \frac{A}{4}$$