## Energijska učinkovitost stavb

#### <u>← Nazaj</u>

Po Pravilniku o učinkoviti rabi energije v stavbah (Uradni list RS, št. 70/22 z dne 20. 5. 2022) in Pravilniku o spremembah Pravilnika o učinkoviti rabi energije v stavbah (Uradni list RS, št. 161/22 z dne 23. 12. 2022).

Investitor: Janez Novak

Mestna cesta 12, 1000 Ljubljana

Naziv projekta: **Testni Projekt** 

Izdelovalec elaborata: Franc Pavlin, udia, ZAPS 1122

Vodja projektiranja: Franc Pavlin, udia, ZAPS 1122

Številka elaborata: 2023-01 Datum elaborata: april 2023

## Podatki o projektu "Testni Projekt"

Analiza GF Izkaz GF Analiza SNES Izkaz sNES

Analiza ovoja cone "Cona1" Analiza cone "Cona1"

TSS "TC" TSS "Prezracevanje" TSS "Razsvetljava"

Naziv projekta Ulica, kraj Katastrska občina Parcele GK koordinate kraja

GKX GKY Testni Projekt Mestna cesta 12 Ljubljana 123/4

116215 469925

# Analiza Projekta "Testni Projekt"

### <u>← Nazaj</u>

| Bruto ogrevana<br>prostornina                    | $V_{e}$                 | 672,0 | m3              |
|--|-------------------------|-------|-----------------|
| stavbe<br>Površina<br>toplotnega ovoja<br>stavbe | $A_{ovoj}$              | 680,0 | m²              |
| Kondicionirana<br>površina stavbe                | $A_{use}$               | 160,0 | m²              |
| Transp. površina<br>v toplotnem ovoji<br>stavbe  |                         | 29,19 | m²              |
| Faktor oblike<br>stavbe                          | $f_0$                   | 1,012 | m <sup>-1</sup> |
| Razmerje<br>transp./celotne<br>površine ovoja    | z                       | 0,043 | -               |
| Spec. koef.<br>transm. topl.<br>izgub            | H' <sub>tr</sub>        | 0,212 | W/m²K           |
| $X_{H'tr} \times H'_{tr,do}$                     |                         | 0,326 | W/m²K           |
| X <sub>H'</sub>                                  | tr                      | 1,000 | W/m²K           |
| Potrebna toplota<br>za ogrevanje<br>stavbe       | $Q_{H,nd,an}$           | 4666  | kWh/an          |
| Potrebna toplota za hlajenje stavbo              |                         | 65    | kWh/an          |
| Potrebna toplota<br>za pripravo TSV              |                         | 1345  | kWh/an          |
| Potrebna energija<br>za vlaženje zraka           | a Q <sub>HU,nd,an</sub> | 0     | kWh/an          |
| Potrebna energija<br>za razvlaževanje<br>zraka   | ${f Q}_{\sf DHU,nd,an}$ | 0     | kWh/an          |
| Dovedena<br>energija za<br>razsvetljavo          | $E_L,del,an$            | 1238  | kWh/an          |
| Specifična<br>potrebna toplota<br>za ogrevanje   | Q' <sub>H,nd,an</sub>   | 29,2  | kWh/m²an        |

## Analiza netransparentne konstrukcije

Naziv: Fasadni Zid Tip: Zunanje stene

|            | d<br>[m] | λ<br>[W/mK] | ρ<br>[kg/m³] | c <sub>p</sub><br>[J/kg K] | μ<br>[-] | R<br>[m²K/W] | S <sub>d</sub><br>[m] |       |
|------------|----------|-------------|--------------|----------------------------|----------|--------------|-----------------------|-------|
| Zid        | 0,250    | 0,610       | 1400         | )                          | 920      | 6,0          | 0,410                 | 1,500 |
| EPS Grafit | 0,200    | 0,031       | 15           |                            | 1260     | 25,0         | 6,452                 | 5,000 |
| Fasada     | 0,010    | 0,700       | 1850         | )                          | 1050     | 15,0         | 0,014                 | 0,150 |

#### Prikaz temperature v konstrukciji

```
const ctx = document.getElementById('myChart'); var temp = [ "x": -0.050000, "y": 20.000000 ],
{"x": 0.000000, "y":19.612532}, {"x": 0.125000, "y":19.001768}, {"x": 0.250000, "y":18.391004},
{"x": 0.257692, "y":17.651419}, {"x": 0.265385, "y":16.911835}, {"x": 0.273077, "y":16.172250},
{"x": 0.280769, "y":15.432665}, {"x": 0.288462, "y":14.693080}, {"x": 0.296154, "y":13.953496},
{"x": 0.303846, "y":13.213911}, {"x": 0.311538, "y":12.474326}, {"x": 0.319231, "y":11.734741},
{"x": 0.326923, "y":10.995156}, {"x": 0.334615, "y":10.255572}, {"x": 0.342308, "y":9.515987},
{"x": 0.350000, "y":8.776402}, {"x": 0.357692, "y":8.036817}, {"x": 0.365385, "y":7.297233}, {"x":
0.373077, "y":6.557648}, {"x": 0.380769, "y":5.818063}, {"x": 0.388462, "y":5.078478}, {"x":
0.396154, "y":4.338893}, {"x": 0.403846, "y":3.599309}, {"x": 0.411538, "y":2.859724}, {"x":
0.419231, "y":2.120139}, {"x": 0.426923, "y":1.380554}, {"x": 0.434615, "y":0.640970}, {"x":
0.442308, "y":-0.098615}, {"x": 0.450000, "y":-0.838200}, {"x": 0.460000, "y":-0.880779}, {"x":
0.460000, "y":-0.880779}, {"x": 0.510000, "y":-1.000000} ]; new Chart(ctx, { "type": 'scatter',
"data": { "datasets": [ { "label": "Temperatura v konstrukciji", "data": temp, "fill": false, "borderColor":
"#fa4444", "lineTension":0.1, showLine: true } ] }, plugins: [{ beforeDraw: chart => { var ctx =
chart.ctx; var xAxis = chart.scales.x; var yAxis = chart.scales.y; ctx.fillStyle = "lightgray";
ctx.rect(xAxis.getPixelForValue(temp[1].x), yAxis.top, xAxis.getPixelForValue(temp[temp.length -
2].x) - xAxis.getPixelForValue(temp[1].x), yAxis.bottom-yAxis.top); ctx.fill(); temp.forEach((value,
index) => { if (index > 0 && index Prikaz tlaka in kondenzacije
```

|              | d    | λ      | R [m <sup>2</sup> K/W] | S <sub>d</sub> | Т    | p <sub>dei</sub> | p <sub>nas</sub> | g <sub>d</sub> | Ma     |
|--------------|------|--------|------------------------|----------------|------|------------------|------------------|----------------|--------|
|              | [cm] | [W/mK] |                        | [m]            | [°C] |                  | [Pa]             |                | [g/m²] |
| Prostor      |      |        |                        |                | 20   | 1028             | 2337             |                |        |
| Notr.        |      |        |                        |                | 19.6 | 1028             | 2281             |                |        |
| površina     |      |        |                        |                |      |                  |                  |                |        |
| Zid.1        | 12.5 | 0.61   | 0.205                  | 0.75           | 19   | 964.3            | 2196.4           |                |        |
| Zid.2        | 12.5 | 0.61   | 0.205                  | 0.75           | 18.4 | 900.3            | 2114.1           |                |        |
| EPS Grafit.1 | 0.8  | 0.031  | 0.248                  | 0.1923         | 17.7 | 883.9            | 2018.1           |                |        |
| EPS Grafit.2 | 0.8  | 0.031  | 0.248                  | 0.1923         | 16.9 | 867.5            | 1925.9           |                |        |
| EPS Grafit.3 | 0.8  | 0.031  | 0.248                  | 0.1923         | 16.2 | 851.1            | 1837.4           |                |        |
| EPS Grafit.4 | 0.8  | 0.031  | 0.248                  | 0.1923         | 15.4 | 834.6            | 1752.5           |                |        |
| EPS Grafit.5 | 0.8  | 0.031  | 0.248                  | 0.1923         | 14.7 | 818.2            | 1671             |                |        |
| EPS Grafit.6 | 0.8  | 0.031  | 0.248                  | 0.1923         | 14   | 801.8            | 1592.9           |                |        |
| EPS Grafit.7 | 0.8  | 0.031  | 0.248                  | 0.1923         | 13.2 | 785.4            | 1518             |                |        |
| EPS Grafit.8 | 0.8  | 0.031  | 0.248                  | 0.1923         | 12.5 | 769              | 1446.3           |                |        |
| EPS Grafit.9 | 0.8  | 0.031  | 0.248                  | 0.1923         | 11.7 | 752.6            | 1377.5           |                |        |
| EPS          | 0.8  | 0.031  | 0.248                  | 0.1923         | 11   | 736.2            | 1311.6           |                |        |
| Grafit.10    |      |        |                        |                |      |                  |                  |                |        |
| EPS          | 0.8  | 0.031  | 0.248                  | 0.1923         | 10.3 | 719.8            | 1248.5           |                | _      |
| Grafit.11    |      |        |                        |                |      |                  |                  |                |        |
|              |      |        |                        |                |      |                  |                  |                |        |
| 1            | I    |        |                        |                |      |                  | 1                |                |        |

|           | d    | λ      | R [m <sup>2</sup> K/W] | S <sub>d</sub> | П    | p <sub>dej</sub> | $p_{nas}$ | g <sub>c</sub> | M <sub>a</sub> |
|-----------|------|--------|------------------------|----------------|------|------------------|-----------|----------------|----------------|
|           | [cm] | [W/mK] |                        | [m]            | [°C] | [Pa]             | [Pa]      | [g/m² m]       | [g/m²]         |
| EPS       | 0.8  | 0.031  | 0.248                  | 0.1923         | 9.5  | 703.4            | 1188.1    |                |                |
| Grafit.12 |      |        |                        |                |      |                  |           |                |                |
| EPS       | 0.8  | 0.031  | 0.248                  | 0.1923         | 8.8  | 687              | 1130.2    |                |                |
| Grafit.13 |      |        |                        |                |      |                  |           |                |                |
| EPS       | 0.8  | 0.031  | 0.248                  | 0.1923         | 8    | 670.6            | 1074.9    |                |                |
| Grafit.14 |      |        |                        |                |      |                  |           |                |                |
| EPS       | 0.8  | 0.031  | 0.248                  | 0.1923         | 7.3  | 654.2            | 1022      |                |                |
| Grafit.15 |      |        |                        |                |      |                  |           |                |                |
| EPS       | 0.8  | 0.031  | 0.248                  | 0.1923         | 6.6  | 637.8            | 971.3     |                |                |
| Grafit.16 |      |        |                        |                |      |                  |           |                |                |
| EPS       | 0.8  | 0.031  | 0.248                  | 0.1923         | 5.8  | 621.3            | 922.9     |                |                |
| Grafit.17 |      |        |                        |                |      |                  |           |                |                |
| EPS       | 0.8  | 0.031  | 0.248                  | 0.1923         | 5.1  | 604.9            | 876.7     |                |                |
| Grafit.18 |      |        |                        |                |      |                  |           |                |                |
| EPS       | 0.8  | 0.031  | 0.248                  | 0.1923         | 4.3  | 588.5            | 832.4     |                |                |
| Grafit.19 |      |        |                        |                |      |                  |           |                |                |
| EPS       | 0.8  | 0.031  | 0.248                  | 0.1923         | 3.6  | 572.1            | 790.2     |                |                |
| Grafit.20 |      |        |                        |                |      |                  |           |                |                |
| EPS       | 0.8  | 0.031  | 0.248                  | 0.1923         | 2.9  | 555.7            | 749.9     |                |                |
| Grafit.21 |      |        |                        |                |      |                  |           |                |                |
| EPS       | 0.8  | 0.031  | 0.248                  | 0.1923         | 2.1  | 539.3            | 711.4     |                |                |
| Grafit.22 |      |        |                        |                |      |                  |           |                |                |
| EPS       | 0.8  | 0.031  | 0.248                  | 0.1923         | 1.4  | 522.9            | 674.6     |                |                |
| Grafit.23 |      |        |                        |                |      |                  |           |                |                |
| EPS       | 0.8  | 0.031  | 0.248                  | 0.1923         | 0.6  | 506.5            | 639.6     |                |                |
| Grafit.24 |      |        |                        |                |      |                  |           |                |                |
| EPS       | 0.8  | 0.031  | 0.248                  | 0.1923         | -0.1 | 490.1            | 605.6     |                |                |
| Grafit.25 |      |        |                        |                |      |                  |           |                |                |
| EPS       | 0.8  | 0.031  | 0.248                  | 0.1923         | -0.8 | 473.7            | 569.6     |                |                |
| Grafit.26 |      |        |                        |                |      |                  |           |                |                |
| Fasada    | 1    | 0.7    | 0.014                  | 0.15           | -0.9 | 460.9            | 567.6     |                |                |
| Zun.      |      |        |                        |                | -0.9 |                  |           |                |                |
| površina  |      |        |                        |                |      |                  |           |                |                |
| Okolica   |      |        |                        |                | -1   | 461              | 562       |                |                |

 $nasicenTlak = [ \{"x": -0.332500, "y": 2336.951144\}, \{"x": 0.000000, "y": 2281.485971\}, \{"x": 0.0000000, "y": 2281.485971\}, \{"x": 0.000000, "y": 2281.485971\}, \{"x": 0.000000, "y": 2281.485971\}, \{"x": 0.000000, "y": 2281.485971], ["x": 0.0000000, "y": 2281.485971], ["x": 0.0000000, "y": 2281.485971], ["x": 0.0000000, "y": 2281.485971], ["x": 0.00000000, "y": 2281.485971], ["x": 0.00000000, "y": 2281.485971], ["x": 0.0000000, "y": 2281.485971], ["x": 0.0000000, "y": 2281.485971], ["x": 0.000000, "y": 2281.485971], ["x": 0.000000, "y": 2$  $0.750000, "y": 2196.393459\}, \{"x": 1.500000, "y": 2114.090711\}, \{"x": 1.692308, "y": 2018.051830\}, \{"x": 2018.05180\}, \{"x": 2018.05180\}, \{"x": 2018.05180\}, \{"x": 2018.05180\}, \{"x": 2018.05180\}, \{"x":$  ${"x": 1.884615, "y":1925.854747}, {"x": 2.076923, "y":1837.368328}, {"x": 2.269231, "y":1837.368328}, {"y": 2.269231, "y": 2.26924, "y": 2.26924$ "y":1752.465063}, {"x": 2.461538, "y":1671.020984}, {"x": 2.653846, "y":1592.915602}, {"x": 2.846154, "y":1518.031831}, {"x": 3.038462, "y":1446.255919}, {"x": 3.230769, "y":1377.477383},  ${"x": 3.423077, "y":1311.588933}, {"x": 3.615385, "y":1248.486412}, {"x": 3.807692, "y":1248.486412}, {"x": 3.807692}, {"x": 3.80769}, {"x": 3.80769}, {"x": 3.8076}, {"x": 3.8076}, {"x": 3.8076}, {"x": 3.8076$ "y":1188.068722}, {"x": 4.000000, "y":1130.237764}, {"x": 4.192308, "y":1074.898369}, {"x": 4.384615, "y":1021.958233}, {"x": 4.576923, "y":971.327853}, {"x": 4.769231, "y":922.920467}, {"x": 4.961538, "y":876.651987}, {"x": 5.153846, "y":832.440942}, {"x": 5.346154, "y":790.208413}, {"x": 5.538462, "y":749.877974}, {"x": 5.730769, "y":711.375636}, {"x": 5.923077, "y":674.629784}, {"x": 6.115385, "y":639.571122}, {"x": 6.307692, "y":605.557910}, {"x": 6.500000, "y":569.636730}, {"x": 6.650000, "y":567.628902}, {"x": 6.650000,  $dejanskiTlak = [ {"x": 0, "y": 1028.258503273}, {"x": 6.65, "y": 460.87374857031} ];$  $\frac{1}{1} = \frac{1}{1} = \frac{1}$  $\{ "x": 0.750000, "y": 964.267741 \}, \ \{ "x": 1.500000, "y": 900.276980 \}, \ \{ "x": 1.692308, \}, \ \{ "x": 1.692308, \}, \ \{ "x": 1.692308, \}, \},$ "y":883.869092}, {"x": 1.884615, "y":867.461204}, {"x": 2.076923, "y":851.053317}, {"x": 2.269231, "y":834.645429}, {"x": 2.461538, "y":818.237541}, {"x": 2.653846, "y":801.829654}, {"x": 2.846154, "y":785.421766}, {"x": 3.038462, "y":769.013879}, {"x": 3.230769, "y":752.605991}, {"x": 3.423077, "y":736.198103}, {"x": 3.615385, "y":719.790216}, {"x": 3.807692, "y":703.382328}, {"x": 4.000000, "y":686.974440}, {"x": 4.192308, "y":670.566553}, {"x": 4.384615, "y":654.158665}, {"x": 4.576923, "y":637.750777}, {"x": 4.769231, "y":621.342890}, {"x": 4.961538, "y":604.935002}, {"x": 5.153846, "y":588.527114}, {"x": 5.346154, "y":572.119227}, {"x": 5.538462, "y":555.711339}, {"x": 5.730769, "y":539.303452},  $\{ "x": 5.923077, "y": 522.895564 \}, \ \{ "x": 6.115385, "y": 506.487676 \}, \ \{ "x": 6.307692, \ ( 10.101888 ), \ ( 10.10188$ "y":490.079789}, {"x": 6.500000, "y":473.671901}, {"x": 6.650000, "y":460.873749}, {"x": 6.650000, "y":460.873749}, ]; new Chart(ctx2, { "type": 'scatter', "data": { "datasets": [ {

```
"label":"Nasičen Tlak", "data": nasicenTlak, "fill":false, "borderColor":"rgb(75, 192, 192)", showLine: true }, { "label":"Dejanski Tlak", "data": dejanskiTlak, "showLine": true }, { "label":"Dejanski Tlak Tocke", "data": dejanskiTlakTocke, "borderColor":"rgb(75, 50, 20)", "showLine": true } ] }, "plugins": [{ beforeDraw: chart => { var ctx = chart.ctx; var xAxis = chart.scales.x; var yAxis = chart.scales.y; ctx.fillStyle = "lightgray"; ctx.rect(xAxis.getPixelForValue(nasicenTlak[1].x), yAxis.top, xAxis.getPixelForValue(nasicenTlak[nasicenTlak.length - 2].x) - xAxis.getPixelForValue(nasicenTlak[1].x), yAxis.bottom-yAxis.top); ctx.fill(); nasicenTlak.forEach((value, index) => { if (index > 0 && index < nasicenTlak.length - 1) { var x = xAxis.getPixelForValue(nasicenTlak[index].x); var yTop = yAxis.getPixelForValue(nasicenTlak[index].y); ctx.save(); ctx.strokeStyle = '#404040'; ctx.beginPath(); ctx.moveTo(x, yAxis.bottom); ctx.lineTo(x, yAxis.top); ctx.stroke(); ctx.restore(); } }); } }], "options": { "scales": { x: { type: "linear", position: "bottom", min: -0.10, max: 6.65 + 0.1 } }, "plugins": { zoom: { zoom: { wheel: { enabled: true, }, pinch: { enabled: true }, mode: 'x', }, pan: { enabled: true, mode: 'x', }, } } });
```

## Analiza netransparentne konstrukcije

Naziv: Temeljna plošča

Tip: Tla na terenu pri ploskovnem gretju

|         | d     | λ      | ρ       | Cp       | μ    | R                    | S <sub>d</sub> |        |
|---------|-------|--------|---------|----------|------|----------------------|----------------|--------|
|         | [m]   | [W/mK] | [kg/m³] | [J/kg K] | [-]  | [m <sup>2</sup> K/W] | [m]            |        |
| Les     | 0,010 | 0,210  | 800     |          | 2510 | 60,0                 | 0,048          | 0,600  |
| Estrih  | 0,050 | 0,930  | 1800    | )        | 960  | 15,0                 | 0,054          | 0,750  |
| EPS 100 | 0,080 | 0,039  | 15      |          | 1260 | 25,0                 | 2,051          | 2,000  |
| Beton   | 0,300 | 2,040  | 2400    | )        | 960  | 60,0                 | 0,147          | 18,000 |
| XPS     | 0,120 | 0,038  | 33      |          | 1500 | 120,0                | 3,158          | 14,400 |

#### Prikaz temperature v konstrukciji

```
const ctx = document.getElementById('myChart'); var temp = [ \{"x": -0.050000, "y": 20.000000\}, 
{"x": 0.000000, "y":20.000000}, {"x": 0.010000, "y":19.818103}, {"x": 0.060000, "y":19.612736},
{"x": 0.068889, "y":18.742118}, {"x": 0.077778, "y":17.871500}, {"x": 0.086667, "y":17.000882},
{"x": 0.095556, "y":16.130264}, {"x": 0.104444, "y":15.259646}, {"x": 0.113333, "y":14.389028},
{"x": 0.122222, "y":13.518410}, {"x": 0.131111, "y":12.647792}, {"x": 0.140000, "y":11.777174},
{"x": 0.440000, "y":11.215434}, {"x": 0.449231, "y":10.287538}, {"x": 0.458462, "y":9.359643},
{"x": 0.467692, "y":8.431747}, {"x": 0.476923, "y":7.503852}, {"x": 0.486154, "y":6.575957}, {"x":
0.495385, "y":5.648061}, {"x": 0.504615, "y":4.720166}, {"x": 0.513846, "y":3.792270}, {"x":
0.523077, "y":2.864375}, {"x": 0.532308, "y":1.936480}, {"x": 0.541538, "y":1.008584}, {"x":
0.550769, "y":0.080689}, {"x": 0.560000, "y":-0.847207}, {"x": 0.560000, "y":-0.847207}, {"x":
0.610000, "y":-1.000000} ]; new Chart(ctx, { "type": 'scatter', "data": { "datasets": [ {
"label":"Temperatura v konstrukciji", "data": temp, "fill":false, "borderColor": "#fa4444",
"lineTension":0.1, showLine: true } ] }, plugins: [{ beforeDraw: chart => { var ctx = chart.ctx; var
xAxis = chart.scales.x; var yAxis = chart.scales.y; ctx.fillStyle = "lightgray";
ctx.rect(xAxis.getPixelForValue(temp[1].x),\ yAxis.top,\ xAxis.getPixelForValue(temp[temp.length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-l
2].x) - xAxis.getPixelForValue(temp[1].x), yAxis.bottom-yAxis.top); ctx.fill(); temp.forEach((value,
index) => { if (index > 0 && index Prikaz tlaka in kondenzacije
```

|           | d    | λ      | R [m <sup>2</sup> K/W] | Sd     | T    | $p_{de}$ | p <sub>nas</sub> | g <sub>a</sub> | M <sub>a</sub>      |
|-----------|------|--------|------------------------|--------|------|----------|------------------|----------------|---------------------|
|           | [cm] | [W/mK] |                        | [m]    | [°C] |          | [Pa]             | [g/m² m]       | [g/m <sup>2</sup> ] |
| Prostor   |      |        |                        |        | 20   | 1028     | 2337             |                |                     |
| Notr.     |      |        |                        |        | 20   | 1028     | 2337             |                |                     |
| površina  |      |        |                        |        |      |          |                  |                |                     |
| Les       | 1    | 0.21   | 0.048                  | 0.6    | 19.8 | 1018.7   | 2310.8           |                |                     |
| Estrih    | 5    | 0.93   | 0.054                  | 0.75   | 19.6 | 1006.8   | 2281.5           |                |                     |
| EPS 100.1 | 0.9  | 0.039  |                        | 0.2222 | 18.7 | 1003.3   | 2161.1           |                |                     |
| EPS 100.2 | 0.9  | 0.039  | 0.228                  | 0.2222 | 17.9 | 999.8    | 2046.2           |                |                     |
| EPS 100.3 | 0.9  | 0.039  | 0.228                  | 0.2222 | 17   | 996.3    | 1936.8           |                |                     |
| EPS 100.4 | 0.9  | 0.039  | 0.228                  | 0.2222 | 16.1 | 992.7    | 1832.5           |                |                     |
| EPS 100.5 | 0.9  | 0.039  | 0.228                  | 0.2222 | 15.3 | 989.2    |                  |                |                     |
| EPS 100.6 | 0.9  | 0.039  |                        |        | 14.4 | 985.7    | 1638.5           |                |                     |
| EPS 100.7 | 0.9  | 0.039  |                        |        | 13.5 |          |                  |                |                     |
| EPS 100.8 | 0.9  | 0.039  | 0.228                  | 0.2222 | 12.6 | 978.6    | 1462.8           |                |                     |
| EPS 100.9 | 0.9  | 0.039  | 0.228                  | 0.2222 | 11.8 | 975.1    | 1381.3           |                |                     |
| Beton     | 30   | 2.04   |                        | 18     | 11.2 | 689.4    | 1330.9           |                |                     |
| XPS.1     | 0.9  | 0.038  |                        |        | 10.3 | 671.8    |                  |                |                     |
| XPS.2     | 0.9  | 0.038  | 0.243                  | 1.1077 | 9.4  | 654.3    | 1175.6           |                | •                   |
| XPS.3     | 0.9  | 0.038  | 0.243                  | 1.1077 | 8.4  | 636.7    | 1104.1           |                | _                   |

|          | d    | λ      | R [m <sup>2</sup> K/W] | S <sub>d</sub> | T    | $p_{dei}$ | p <sub>nas</sub> | ga                   | M <sub>a</sub>      |
|----------|------|--------|------------------------|----------------|------|-----------|------------------|----------------------|---------------------|
|          | [cm] | [W/mK] |                        | [m]            | [°C] | [Pa]      | [Pa]             | [g/m <sup>2</sup> m] | [g/m <sup>2</sup> ] |
| XPS.4    | 0.9  | 0.038  | 0.243                  | 1.1077         | 7.5  | 619.1     | 1036.5           |                      |                     |
| XPS.5    | 0.9  | 0.038  | 0.243                  | 1.1077         | 6.6  | 601.5     | 972.6            |                      |                     |
| XPS.6    | 0.9  | 0.038  | 0.243                  | 1.1077         | 5.6  | 583.9     | 912.1            |                      |                     |
| XPS.7    | 0.9  | 0.038  | 0.243                  | 1.1077         | 4.7  | 566.4     | 855              |                      |                     |
| XPS.8    | 0.9  | 0.038  | 0.243                  | 1.1077         | 3.8  | 548.8     | 801              |                      |                     |
| XPS.9    | 0.9  | 0.038  | 0.243                  | 1.1077         | 2.9  | 531.2     | 750.1            |                      |                     |
| XPS.10   | 0.9  | 0.038  | 0.243                  | 1.1077         | 1.9  | 513.6     | 702.1            |                      |                     |
| XPS.11   | 0.9  | 0.038  | 0.243                  | 1.1077         | 1    | 496       | 656.8            |                      |                     |
| XPS.12   | 0.9  | 0.038  | 0.243                  | 1.1077         | 0.1  | 478.5     | 614.1            |                      |                     |
| XPS.13   | 0.9  | 0.038  | 0.243                  | 1.1077         | -0.8 | 460.9     | 569.2            |                      |                     |
| Zun.     |      |        |                        |                | -0.8 | 461       | 569              | -                    |                     |
| površina |      |        |                        |                |      |           |                  |                      |                     |
| Okolica  |      |        |                        |                | -1   | 461       | 562              |                      |                     |

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## Analiza netransparentne konstrukcije

Naziv: Strop

Tip: Strop proti terenu

|                | d     | λ      | ρ       | Cp       | μ    | R                    | S <sub>d</sub> |       |
|----------------|-------|--------|---------|----------|------|----------------------|----------------|-------|
|                | [m]   | [W/mK] | [kg/m³] | [J/kg K] | [-]  | [m <sup>2</sup> K/W] | [m]            |       |
| Beton          | 0,150 | 2,040  | 2400    | 0        | 960  | 60,0                 | 0,074          | 9,000 |
| Steklena volna | 0,300 | 0,034  | 23      |          | 1030 | 1,0                  | 8,824          | 0,300 |

#### Prikaz temperature v konstrukciji

```
const ctx = document.getElementById('myChart'); var temp = [ "x": -0.050000, "y": 20.000000 ],
{"x": 0.000000, "y":19.767624}, {"x": 0.150000, "y":19.596758}, {"x": 0.158333, "y":19.027208},
{"x": 0.166667, "y":18.457658}, {"x": 0.175000, "y":17.888108}, {"x": 0.183333, "y":17.318558},
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0.500000, "y":-1.000000} ]; new Chart(ctx, { "type": 'scatter', "data": { "datasets": [ {
"label":"Temperatura v konstrukciji", "data": temp, "fill":false, "borderColor": "#fa4444",
"lineTension":0.1, showLine: true } ] }, plugins: [{ beforeDraw: chart => { var ctx = chart.ctx; var
xAxis = chart.scales.x; var yAxis = chart.scales.y; ctx.fillStyle = "lightgray";
ctx.rect(xAxis.getPixelForValue(temp[1].x), yAxis.top, xAxis.getPixelForValue(temp[temp.length -
2].x) - xAxis.getPixelForValue(temp[1].x), yAxis.bottom-yAxis.top); ctx.fill(); temp.forEach((value,
index) => { if (index > 0 && index Prikaz tlaka in kondenzacije
```

|          | d    | λ      | R [m <sup>2</sup> K/W] | S <sub>d</sub> | Т    | p <sub>de</sub> | p <sub>nas</sub> | g <sub>d</sub>       | $M_a$               |
|----------|------|--------|------------------------|----------------|------|-----------------|------------------|----------------------|---------------------|
|          | [cm] | [W/mK] |                        | [m]            | [°C] |                 |                  | [g/m <sup>2</sup> m] | [g/m <sup>2</sup> ] |
| Prostor  |      |        |                        |                | 20   |                 | 2337             |                      | -                   |
| Notr.    |      |        |                        |                | 19.8 | 1028            | 2304             |                      |                     |
| površina |      |        |                        |                |      |                 |                  |                      |                     |
| Beton    | 15   | 2.04   | 0.074                  |                | 19.6 |                 |                  |                      |                     |
| Steklena | 0.8  | 0.034  | 0.245                  | 0.0083         | 19   | 478.7           | 2199.9           |                      |                     |
| volna.1  |      |        |                        |                |      |                 |                  |                      |                     |
| Steklena | 0.8  | 0.034  | 0.245                  | 0.0083         | 18.5 | 478.2           | 2122.9           |                      |                     |
| volna.2  |      |        |                        |                |      |                 |                  |                      |                     |
| Steklena | 0.8  | 0.034  | 0.245                  | 0.0083         | 17.9 | 477.7           | 2048.4           |                      |                     |
| volna.3  |      |        |                        |                |      |                 |                  |                      |                     |
| Steklena | 0.8  | 0.034  | 0.245                  | 0.0083         | 17.3 | 477.1           | . 1976.1         |                      |                     |
| volna.4  |      |        |                        |                |      |                 |                  |                      |                     |
| Steklena | 0.8  | 0.034  | 0.245                  | 0.0083         | 16.7 | 476.6           | 1906.1           |                      |                     |
| volna.5  |      |        |                        |                |      |                 |                  |                      |                     |
| Steklena | 0.8  | 0.034  | 0.245                  | 0.0083         | 16.2 | 476.1           | . 1838.2         |                      |                     |
| volna.6  |      |        |                        |                |      |                 |                  |                      |                     |
|          |      |        |                        |                |      |                 |                  |                      |                     |

|                      |           |             | 2·····    |                       |           |                          |                          |                            |                          |
|----------------------|-----------|-------------|-----------|-----------------------|-----------|--------------------------|--------------------------|----------------------------|--------------------------|
|                      | d<br>[cm] | λ<br>[W/mK] | R [m²K/W] | Տ <sub>d</sub><br>[m] | T<br>[°C] | p <sub>dej</sub><br>[Pa] | p <sub>nas</sub><br>[Pa] | g <sub>c</sub><br>[g/m² m] | M <sub>a</sub><br>[g/m²] |
| Steklena<br>volna.7  | 0.8       | 0.034       | 0.245     | 0.0083                | 15.6      |                          | 1772.5                   |                            |                          |
| Steklena<br>volna.8  | 0.8       | 0.034       | 0.245     | 0.0083                | 15        | 475.1                    | 1708.8                   |                            |                          |
| Steklena<br>volna.9  | 0.8       | 0.034       | 0.245     | 0.0083                | 14.5      | 474.6                    | 1647.2                   |                            |                          |
| Steklena             | 0.8       | 0.034       | 0.245     | 0.0083                | 13.9      | 474.1                    | 1587.5                   |                            |                          |
| volna.10<br>Steklena | 0.8       | 0.034       | 0.245     | 0.0083                | 13.3      | 473.6                    | 1529.7                   |                            |                          |
| volna.11<br>Steklena | 0.8       | 0.034       | 0.245     | 0.0083                | 12.8      | 473.1                    | 1473.8                   |                            |                          |
| volna.12<br>Steklena | 0.8       | 0.034       | 0.245     | 0.0083                | 12.2      |                          |                          |                            |                          |
| volna.13             |           |             |           |                       |           |                          |                          |                            |                          |
| Steklena<br>volna.14 | 0.8       | 0.034       | 0.245     | 0.0083                | 11.6      |                          | 1367.3                   |                            |                          |
| Steklena<br>volna.15 | 0.8       | 0.034       | 0.245     | 0.0083                | 11.1      | 471.6                    | 1316.7                   |                            |                          |
| Steklena<br>volna.16 | 0.8       | 0.034       | 0.245     | 0.0083                | 10.5      | 471                      | 1267.7                   |                            |                          |
| Steklena             | 0.8       | 0.034       | 0.245     | 0.0083                | 9.9       | 470.5                    | 1220.3                   |                            |                          |
| volna.17<br>Steklena | 0.8       | 0.034       | 0.245     | 0.0083                | 9.3       | 470                      | 1174.5                   |                            |                          |
| volna.18<br>Steklena | 0.8       | 0.034       | 0.245     | 0.0083                | 8.8       | 469.5                    | 1130.2                   |                            |                          |
| volna.19<br>Steklena | 0.8       | 0.034       | 0.245     | 0.0083                | 8.2       | 469                      | 1087.3                   |                            |                          |
| volna.20<br>Steklena | 0.8       | 0.034       | 0.245     | 0.0083                | 7.6       |                          |                          |                            |                          |
| volna.21             |           |             |           |                       |           |                          |                          |                            |                          |
| Steklena<br>volna.22 | 0.8       | 0.034       | 0.245     | 0.0083                |           |                          |                          |                            |                          |
| Steklena<br>volna.23 | 0.8       | 0.034       | 0.245     | 0.0083                | 6.5       | 467.5                    | 967.3                    |                            |                          |
| Steklena<br>volna.24 | 0.8       | 0.034       | 0.245     | 0.0083                | 5.9       | 467                      | 929.9                    |                            |                          |
| Steklena<br>volna.25 | 0.8       | 0.034       | 0.245     | 0.0083                | 5.4       | 466.5                    | 893.9                    |                            |                          |
| Steklena             | 0.8       | 0.034       | 0.245     | 0.0083                | 4.8       | 466                      | 859.1                    |                            |                          |
| volna.26<br>Steklena | 0.8       | 0.034       | 0.245     | 0.0083                | 4.2       | 465.4                    | 825.5                    |                            |                          |
| volna.27<br>Steklena | 0.8       | 0.034       | 0.245     | 0.0083                | 3.6       | 464.9                    | 793                      |                            |                          |
| volna.28<br>Steklena | 0.8       | 0.034       | 0.245     | 0.0083                | 3.1       | 464.4                    | 761.7                    |                            |                          |
| volna.29<br>Steklena | 0.8       | 0.034       | 0.245     | 0.0083                | 2.5       | 463.9                    | 731.5                    |                            |                          |
| volna.30<br>Steklena | 0.8       | 0.034       | 0.245     | 0.0083                |           |                          |                          |                            |                          |
| volna.31             |           |             |           |                       |           |                          |                          |                            |                          |
| Steklena<br>volna.32 | 0.8       | 0.034       | 0.245     | 0.0083                |           |                          |                          |                            |                          |
| Steklena<br>volna.33 | 0.8       | 0.034       | 0.245     | 0.0083                | 0.8       | 462.4                    | 647                      |                            |                          |
| Steklena<br>volna.34 | 0.8       | 0.034       | 0.245     | 0.0083                | 0.2       | 461.9                    | 620.9                    |                            |                          |
| Steklena<br>volna.35 | 0.8       | 0.034       | 0.245     | 0.0083                | -0.3      | 461.4                    | 593.7                    |                            |                          |
| Steklena             | 0.8       | 0.034       | 0.245     | 0.0083                | -0.9      | 460.9                    | 566.4                    |                            |                          |
| volna.36<br>Zun.     |           |             |           |                       | -0.9      | 461                      | 566                      |                            |                          |
| površina<br>Okolica  |           |             |           |                       | -1        | 461                      | 562                      |                            |                          |

```
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Tocke", "data": dejanskiTlakTocke, "borderColor": "rgb(75, 50, 20)", "showLine": true } ] }, "plugins":
[{ beforeDraw: chart => { var ctx = chart.ctx; var xAxis = chart.scales.x; var yAxis = chart.scales.y;
ctx.fillStyle = "lightgray"; ctx.rect(xAxis.getPixelForValue(nasicenTlak[1].x), yAxis.top,
xAxis.getPixelForValue(nasicenTlak[nasicenTlak.length - 2].x) -
xAxis.getPixelForValue(nasicenTlak[1].x), yAxis.bottom-yAxis.top); ctx.fill();
nasicenTlak.forEach((value, index) => { if (index > 0 && index < nasicenTlak.length - 1) { var x = } }
xAxis.getPixelForValue(nasicenTlak[index].x); var yTop =
yAxis.getPixelForValue(nasicenTlak[index].y); ctx.save(); ctx.strokeStyle = '#404040';
ctx.beginPath(); ctx.moveTo(x, yAxis.bottom); ctx.lineTo(x, yAxis.top); ctx.stroke(); ctx.restore(); }
}); } }], "options": { "scales": { x: { type: "linear", position: "bottom", min: -0.10, max: 9.3 + 0.1 } },
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enabled: true, mode: 'x', }, } } });
```

# Ovoj cone "Ogrevana cona"

### <u>← Nazaj</u>

| Zaporedna št. kon<br>Št. enakih<br>Orientacija<br>Naklon<br>Toplotna prehodno<br>Površina<br>Faktor |  | °<br>W/m²K<br>m²   |   | Tp1<br>1<br>0<br>0,125<br>200,0<br>1,30   | Ts1<br>1<br>0<br>0,111<br>200,0<br>1,00  | V1<br>1<br>S<br>90<br>1,000<br>3,0<br>1,00  | 15,0  | 5,0   | O1<br>2<br>V<br>90<br>0,820<br>1,0<br>1,00  | 9<br>0,8<br>1   | 01<br>2<br>5<br>90<br>320<br>,0   |
|---|--|--|---|---|--|---|---|---|---|---|---|
|   | U×A×   | d <sub>f</sub> W/K   |   | 32,5  | 22,1   | 3,0   | 10,2  | 3,7   | 0,8   | 0   | ,8  |
| Faktor senčenja ol  | koliških ovir  | jan<br>feb<br>mar<br>apr<br>maj<br>jun<br>jul<br>avg<br>sep<br>okt<br>nov        | 1,000<br>1,000<br>1,000<br>1,000<br>1,000<br>1,000<br>1,000<br>1,000<br>1,000<br>1,000                | 1,000<br>1,000<br>1,000<br>1,000<br>1,000<br>1,000<br>1,000<br>1,000<br>1,000   | 1,000<br>1,000<br>1,000<br>1,000<br>1,000<br>1,000<br>1,000<br>1,000<br>1,000                | 1,000<br>0,993<br>0,964<br>0,945<br>0,953<br>0,984<br>1,000<br>1,000                    | 0 0,984<br>0 0,982<br>8 0,980<br>4 0,978<br>6 0,793<br>8 0,788<br>4 0,799<br>0 0,843<br>0 0,986   | 0,936<br>0,913<br>0,895<br>0,888<br>0,895<br>0,889<br>0,889<br>0,887<br>0,908<br>0,930<br>0,956 | 0,938<br>0,938<br>0,937<br>0,937<br>0,939<br>0,937<br>0,935<br>0,943<br>0,948           | 1,0<br>0,9<br>0,9<br>0,9<br>0,9<br>0,9<br>1,0<br>1,0                    | 000<br>000<br>000<br>994<br>978<br>971<br>974<br>988<br>000<br>000        |
| Mesečno sončno c<br>H <sub>sol,m</sub> (Wh/m²m)   | jan<br>feb<br>mar<br>apr<br>maj<br>jun<br>jul<br>avg<br>sep<br>okt<br>nov<br>dec | dec<br>št. dni<br>31<br>28<br>31<br>30<br>31<br>30<br>31<br>30<br>31<br>30<br>31 | 7967<br>11480<br>19654<br>30810<br>37200<br>42510<br>39370<br>32240<br>23610<br>16306<br>9720<br>7006 | 1,000<br>28427<br>48468<br>85529<br>121470<br>151714<br>158220<br>169539<br>146909<br>100620<br>59241<br>29490<br>21638 | 48468<br>85529<br>121470<br>151714<br>158220<br>169539<br>146909<br>100620<br>59241<br>29490 | 11480<br>19654<br>30810<br>4 37200<br>42510<br>39370<br>32240<br>23610<br>16300<br>9720 | 14446<br>22484<br>441664<br>58440<br>71333<br>69660<br>73129<br>66619<br>45420<br>628113<br>15960 | 5 43431<br>4 59752<br>4 72354<br>0 69870<br>1 65999<br>0 66774<br>9 74803<br>0 72000<br>7 56451 | 14446<br>22484<br>41664<br>58440<br>71331<br>69660<br>473129<br>66619<br>45420<br>28117 | 79<br>114<br>190<br>300<br>370<br>420<br>390<br>320<br>230<br>160<br>97 | 967<br>480<br>654<br>810<br>200<br>510<br>370<br>240<br>610<br>306<br>720 |
| Transmisijske<br>toplotne izgube Q<br>(kWh/m)   | ΔT<br>:r,m   | št. dni  | OGREVAN   | IJE   |  |   |   |   |   |   |   |
| jan   | 21   | 31 69  | 90,7  | 348,7   | 470,8  | 48,7  | 169,5   | 181,3   | 26,9  | 26,9  | 196<br>3,4  |
| feb   | 19   | 28 56  | 54,5 2  | 295,6   | 384,7  | 39,8  | 138,5   | 148,2   | 22,0  | 22,0  | 161   |
| mar   | 15   | 31 49  | 93,4 2  | 284,3   | 336,3  | 34,8  | 121,1   | 129,5   | 19,2  | 19,2  | 5,2<br>143  |
| apr   | 11   | 30 35  | 50,1 2  | 290,2   | 238,6  | 24,7  | 85,9  | 91,9  | 13,6  | 13,6  | 7,7<br>110<br>8,7   |
| maj   | 6  | 31 19  | 97,3 2  | 279,4   | 134,5  | 13,9  | 48,4  | 51,8  | 7,7   | 7,7   | 740<br>,8   |
| jun   | 3  | 30 9   | 5,5 2   | 258,6   | 65,1   | 6,7   | 23,4  | 25,1  | 3,7   | 3,7   | 481   |
| jul   | 1  | 31 3   | 2,9 2   | 259,0   | 22,4   | 2,3   | 8,1   | 8,6   | 1,3   | 1,3   | ,8<br>335<br>,9   |
| avg   | 1  | 31 3   | 2,9 2   | 259,0   | 22,4   | 2,3   | 8,1   | 8,6   | 1,3   | 1,3   | ,3<br>335<br>,9   |
| sep   | 5  | 30 15  | 59,2 2  | 266,5   | 108,5  | 11,2  | 39,1  | 41,8  | 6,2   | 6,2   | 638<br>,6   |

|                           | okt        | 10  | 31      | 328,9     | 230,7 | 224,2 | 23,2 | 80,7   | 86,3   | 12,8  | 12,8  | 999               |
|---------------------------|------------|-----|---------|-----------|-------|-------|------|--------|--------|-------|-------|-------------------|
|                           | nov        | 16  | 30      | 509,3     | 285,5 | 347,1 | 35,9 | 125,0  | 133,7  | 19,8  | 19,8  | ,7<br>147         |
|                           | dec        | 20  | 31      | 657,8     | 337,9 | 448,4 | 46,4 | 161,4  | 172,7  | 25,6  | 25,6  | 6,2<br>187<br>5,8 |
| Transmisij<br>toplotne iz | zgube      | ΔΤ  | št. dni | HLAJENJE  |       |       |      |        |        |       |       | Sku<br>paj        |
| Q <sub>tr,m</sub> (kWh    | /m)<br>jan | 27  | 31      | 888,1     | 348,7 | 605,3 | 62,7 | 217,9  | 233,1  | 34,6  | 34,6  | 242               |
|                           | feb        | 25  | 28      | 742,7     | 295,6 | 506,2 | 52,4 | 182,2  | 194,9  | 28,9  | 28,9  | 4,8<br>203        |
|                           | mar        | 21  | 31      | 690,7     | 284,3 | 470,8 | 48,7 | 169,5  | 181,3  | 26,9  | 26,9  | 1,9<br>189        |
|                           | apr        | 17  | 30      | 541,1     | 290,2 | 368,8 | 38,2 | 132,8  | 142,0  | 21,1  | 21,1  | 9,1<br>155        |
|                           | maj        | 12  | 31      | 394,7     | 279,4 | 269,0 | 27,9 | 96,9   | 103,6  | 15,4  | 15,4  | 5,2<br>120        |
|                           | jun        | 9   | 30      | 286,5     | 258,6 | 195,2 | 20,2 | 70,3   | 75,2   | 11,1  | 11,1  | 2,2<br>928        |
|                           | jul        | 7   | 31      | 230,2     | 259,0 | 156,9 | 16,2 | 56,5   | 60,4   | 9,0   | 9,0   | ,3<br>797         |
|                           | avg        | 7   | 31      | 230,2     | 259,0 | 156,9 | 16,2 | 56,5   | 60,4   | 9,0   | 9,0   | ,3<br>797<br>2    |
|                           | sep        | 11  | 30      | 350,1     | 266,5 | 238,6 | 24,7 | 85,9   | 91,9   | 13,6  | 13,6  | ,3<br>108<br>5,0  |
|                           | okt        | 16  | 31      | 526,3     | 230,7 | 358,7 | 37,1 | 129,1  | 138,1  | 20,5  | 20,5  | 146               |
|                           | nov        | 22  | 30      | 700,3     | 285,5 | 477,3 | 49,4 | 171,8  | 183,8  | 27,2  | 27,2  | 1,0<br>192<br>2,6 |
|                           | dec        | 26  | 31      | 855,2     | 337,9 | 582,9 | 60,4 | 209,8  | 224,5  | 33,3  | 33,3  | 233<br>7,2        |
| Dobitki so                |            |     | śt. dni | OGREVANJI | E     |       |      |        |        |       |       | Sku               |
| obsevanja                 | QS0I,III   | jan | 31      | 4,20      | 0,00  | 0,00  | 0,00 | 104,15 | 280,05 | 12,08 | 6,97  | paj<br>407        |
|                           |            | feb | 28      | 6,06      | 0,00  | 0,00  | 0,00 | 161,27 | 376,09 | 18,46 | 10,04 | ,4<br>571<br>,9   |
|                           |            | mar | 31      | 10,40     | 0,00  | 0,00  | 0,00 | 298,33 | 443,90 | 34,18 | 17,19 | ,9<br>804<br>,0   |
|                           |            | apr | 30      | 16,32     | 0,00  | 0,00  | 0,00 | 417,50 | 420,50 | 47,88 | 26,79 | 929               |
|                           |            | maj | 31      | 19,70     | 0,00  | 0,00  | 0,00 | 508,76 | 394,22 | 58,48 | 31,82 | ,0<br>101<br>3,0  |
|                           |            | jun | 30      | 22,52     | 0,00  | 0,00  | 0,00 | 402,45 | 365,77 | 57,24 | 36,13 | 884<br>,1         |
|                           |            | jul | 31      | 20,86     | 0,00  | 0,00  | 0,00 | 419,82 | 399,24 | 59,91 | 33,54 | 933               |
|                           |            | avg | 31      | 17,07     | 0,00  | 0,00  | 0,00 | 388,24 | 446,15 | 54,49 | 27,86 | ,4<br>933<br>,8   |
|                           |            | sep | 30      | 12,50     | 0,00  | 0,00  | 0,00 | 278,97 | 439,57 | 37,47 | 20,65 | ,6<br>789<br>,2   |
|                           |            | okt | 31      | 8,62      | 0,00  | 0,00  | 0,00 | 202,08 | 353,03 | 23,31 | 14,26 | ,2<br>601<br>,3   |
|                           |            | nov | 30      | 5,13      | 0,00  | 0,00  | 0,00 | 114,85 | 216,99 | 13,25 | 8,50  | ,5<br>358<br>,7   |
|                           |            | dec | 31      | 3,69      | 0,00  | 0,00  | 0,00 | 87,86  | 200,32 | 10,11 | 6,13  | ,,<br>308<br>,1   |

Dobitki sončnega št. dni obsevanja Qsol,m (kWh/m)

# Analiza sNES "Testni Projekt"

### <u>← Nazaj</u>

| Kazalniki energijsk                                    |                               | Količina (kWh/an) |
|--|-------------------------------|-------------------|
| Neutežena dovedena energija<br>za delovanje TSS        | E <sub>del,an</sub>           | 14290             |
| delovanje TSS  | E <sub>w,del,an</sub>         | 26124             |
| dovedene energije                                      | E <sub>Pren,an</sub>          | 14290             |
| Neobnovljiva primarna energija<br>dovedene energije    | •                             | 11834             |
| Skupna primarna energija                               | E <sub>Ptot.an</sub>          | 26124             |
|  |                               | Vrednost (%)      |
| Razmernik obnovljivih virov<br>energije ROVE           |                               | 55                |
| Minimalni zahtevani razmernik<br>ROVE <sub>min</sub>   |                               | 50                |
| Ustreza minimalni zahtevi                              |                               | DA                |
|  |                               | Vrednost (-)      |
| Korekcijski faktor razmernika<br>ROVE X <sub>ove</sub> |                               | 1                 |
| Kompenzacijski faktor                                  |                               | 1                 |
| razmernika ROVE Y <sub>ROVE</sub>                      |                               |                   |
| Korekcijski faktor dovoljene                           | <u> </u>                      | 1,0               |
| skupne primarne energije                               |                               | 1,0               |
| glede na vrsto stavbe X <sub>s</sub>                   |                               |                   |
| Korekcijski faktor dovoljene                           |                               | 1,0               |
| skupne primarne energije                               |                               |                   |
| glede na leto uveljavitve X <sub>p</sub>               |                               |                   |
| Kompenzacijski faktor potrebne                         |                               | 1,2               |
| toplote za ogrevanje Y <sub>H.nd</sub>                 |                               |                   |
|  |                               | Količina (kWh/an) |
| Specifična potrebna skupna                             | E' <sub>Ptot,an</sub>         | 163               |
| primarna energija                                      | rtot,an                       |                   |
|  | E' <sub>Ptot,kor,an</sub>     | 157               |
| primarna energija                                      | - rtot,kor,an                 | 137               |
| 5,   | E' <sub>Ptot,kor,an</sub>     | 75                |
| skupna primarna energija                               | I LOL, KUI, ali               |                   |
| Korigirana dovoljena specifična                        | E' <sub>Ptot.kor.dov.an</sub> | 75                |
| potrebna skupna primarna                               |                               |                   |
| energija   |                               |                   |
| Ustreza minimalni zahtevi                              |                               | NE                |
|  |                               |                   |
|  | h.                            | Vrednost (kg/an)  |
| Izpusti ogljikovega dioksida                           | M <sub>CO2.an</sub>           | 3314              |