Energijska učinkovitost stavb

<u>← Nazaj</u>

Po Pravilniku o učinkoviti rabi energije v stavbah (Uradni list RS, št. 70/22 z dne 20. 5. 2022) in Pravilniku o spremembah Pravilnika o učinkoviti rabi energije v stavbah (Uradni list RS, št. 161/22 z dne 23. 12. 2022).

Investitor: Janez Novak

Mestna cesta 12, 1000 Ljubljana

Naziv projekta: **Testni Projekt**

Izdelovalec elaborata: Franc Pavlin, udia, ZAPS 1122

Vodja projektiranja: Franc Pavlin, udia, ZAPS 1122

Številka elaborata: 2023-01 Datum elaborata: april 2023

Podatki o projektu "Testni Projekt"

Analiza GF Izkaz GF Analiza SNES Izkaz sNES

Analiza ovoja cone "Cona1" Analiza cone "Cona1"

TSS "TC" TSS "Prezracevanje" TSS "Razsvetljava"

Naziv projekta Ulica, kraj Katastrska občina Parcele GK koordinate kraja

GKX GKY Testni Projekt Mestna cesta 12 Ljubljana 123/4

116215 469925

Analiza Projekta "Testni Projekt"

<u>← Nazaj</u>

Bruto ogrevana prostornina stavbe	V _e	672,0	m3
Površina toplotnega ovoja stavbe	A_{ovoj}	680,0	m²
Kondicionirana površina stavbe	A_{use}	160,0	m²
Transp. površina v toplotnem ovoji stavbe		29,19	m²
Faktor oblike stavbe	f_0	1,012	m ⁻¹
Razmerje transp./celotne površine ovoja	z	0,043	-
Spec. koef. transm. topl. izgub	H' _{tr}	0,212	W/m²K
$X_{H'tr} \times H'_{tr,do}$		0,326	W/m²K
X _{H'}	tr	1,000	W/m²K
Potrebna toplota za ogrevanje stavbe	$Q_{H,nd,an}$	5114	kWh/an
Potrebna toplota za hlajenje stavbe		57	kWh/an
Potrebna toplota za pripravo TSV		1345	kWh/an
Potrebna energija za vlaženje zraka		0	kWh/an
Potrebna energija za razvlaževanje zraka		0	kWh/an
Dovedena energija za razsvetljavo	$E_{L,del,an}$	1238	kWh/an
Specifična potrebna toplota za ogrevanje	Q' _{H,nd,an}	32,0	kWh/m²an

Analiza netransparentne konstrukcije

Naziv: Fasadni Zid Tip: Zunanje stene

	d [m]	λ [W/mK]	ρ [kg/m³]	c _p [J/kg K]	μ [-]	R [m²K/W]	S _d [m]	
Zid	0,250	0,610	1400)	920	6,0	0,410	1,500
EPS Grafit	0,200	0,031	15		1260	25,0	6,452	5,000
Fasada	0,010	0,700	1850)	1050	15,0	0,014	0,150

Prikaz temperature v konstrukciji

```
const ctx = document.getElementById('myChart'); var temp = [ "x": -0.050000, "y": 20.000000 ],
{"x": 0.000000, "y":19.612532}, {"x": 0.125000, "y":19.001768}, {"x": 0.250000, "y":18.391004},
{"x": 0.257692, "y":17.651419}, {"x": 0.265385, "y":16.911835}, {"x": 0.273077, "y":16.172250},
{"x": 0.280769, "y":15.432665}, {"x": 0.288462, "y":14.693080}, {"x": 0.296154, "y":13.953496},
{"x": 0.303846, "y":13.213911}, {"x": 0.311538, "y":12.474326}, {"x": 0.319231, "y":11.734741},
{"x": 0.326923, "y":10.995156}, {"x": 0.334615, "y":10.255572}, {"x": 0.342308, "y":9.515987},
{"x": 0.350000, "y":8.776402}, {"x": 0.357692, "y":8.036817}, {"x": 0.365385, "y":7.297233}, {"x":
0.373077, "y":6.557648}, {"x": 0.380769, "y":5.818063}, {"x": 0.388462, "y":5.078478}, {"x":
0.396154, "y":4.338893}, {"x": 0.403846, "y":3.599309}, {"x": 0.411538, "y":2.859724}, {"x":
0.419231, "y":2.120139}, {"x": 0.426923, "y":1.380554}, {"x": 0.434615, "y":0.640970}, {"x":
0.442308, "y":-0.098615}, {"x": 0.450000, "y":-0.838200}, {"x": 0.460000, "y":-0.880779}, {"x":
0.460000, "y":-0.880779}, {"x": 0.510000, "y":-1.000000} ]; new Chart(ctx, { "type": 'scatter',
"data": { "datasets": [ { "label": "Temperatura v konstrukciji", "data": temp, "fill": false, "borderColor":
"#fa4444", "lineTension":0.1, showLine: true } ] }, plugins: [{ beforeDraw: chart => { var ctx =
chart.ctx; var xAxis = chart.scales.x; var yAxis = chart.scales.y; ctx.fillStyle = "lightgray";
ctx.rect(xAxis.getPixelForValue(temp[1].x), yAxis.top, xAxis.getPixelForValue(temp[temp.length -
2].x) - xAxis.getPixelForValue(temp[1].x), yAxis.bottom-yAxis.top); ctx.fill(); temp.forEach((value,
index) => { if (index > 0 && index Prikaz tlaka in kondenzacije
```

	d	λ	R [m ² K/W]	S _d	Т	p _{dei}	p _{nas}	g _d	Ma
	[cm]	[W/mK]		[m]	[°C]		[Pa]		[g/m²]
Prostor					20	1028	2337		
Notr.					19.6	1028	2281		
površina									
Zid.1	12.5	0.61	0.205	0.75	19	964.3	2196.4		
Zid.2	12.5	0.61	0.205	0.75	18.4	900.3	2114.1		
EPS Grafit.1	0.8	0.031	0.248	0.1923	17.7	883.9	2018.1		
EPS Grafit.2	0.8	0.031	0.248	0.1923	16.9	867.5	1925.9		
EPS Grafit.3	0.8	0.031	0.248	0.1923	16.2	851.1	1837.4		
EPS Grafit.4	0.8	0.031	0.248	0.1923	15.4	834.6	1752.5		
EPS Grafit.5	0.8	0.031	0.248	0.1923	14.7	818.2	1671		
EPS Grafit.6	0.8	0.031	0.248	0.1923	14	801.8	1592.9		
EPS Grafit.7	0.8	0.031	0.248	0.1923	13.2	785.4	1518		
EPS Grafit.8	0.8	0.031	0.248	0.1923	12.5	769	1446.3		
EPS Grafit.9	0.8	0.031	0.248	0.1923	11.7	752.6	1377.5		
EPS	0.8	0.031	0.248	0.1923	11	736.2	1311.6		
Grafit.10									
EPS	0.8	0.031	0.248	0.1923	10.3	719.8	1248.5		_
Grafit.11									
1	I						1		

	d	λ	R [m ² K/W]	S _d	П	p _{dej}	p_{nas}	g _c	M _a
	[cm]	[W/mK]		[m]	[°C]	[Pa]	[Pa]	[g/m² m]	[g/m²]
EPS	0.8	0.031	0.248	0.1923	9.5	703.4	1188.1		
Grafit.12									
EPS	0.8	0.031	0.248	0.1923	8.8	687	1130.2		
Grafit.13									
EPS	0.8	0.031	0.248	0.1923	8	670.6	1074.9		
Grafit.14									
EPS	0.8	0.031	0.248	0.1923	7.3	654.2	1022		
Grafit.15									
EPS	0.8	0.031	0.248	0.1923	6.6	637.8	971.3		
Grafit.16									
EPS	0.8	0.031	0.248	0.1923	5.8	621.3	922.9		
Grafit.17									
EPS	0.8	0.031	0.248	0.1923	5.1	604.9	876.7		
Grafit.18									
EPS	0.8	0.031	0.248	0.1923	4.3	588.5	832.4		
Grafit.19									
EPS	0.8	0.031	0.248	0.1923	3.6	572.1	790.2		
Grafit.20									
EPS	0.8	0.031	0.248	0.1923	2.9	555.7	749.9		
Grafit.21									
EPS	0.8	0.031	0.248	0.1923	2.1	539.3	711.4		
Grafit.22									
EPS	0.8	0.031	0.248	0.1923	1.4	522.9	674.6		
Grafit.23									
EPS	0.8	0.031	0.248	0.1923	0.6	506.5	639.6		
Grafit.24									
EPS	0.8	0.031	0.248	0.1923	-0.1	490.1	605.6		
Grafit.25									
EPS	0.8	0.031	0.248	0.1923	-0.8	473.7	569.6		
Grafit.26									
Fasada	1	0.7	0.014	0.15	-0.9	460.9	567.6		
Zun.					-0.9				
površina									
Okolica					-1	461	562		

 $nasicenTlak = [\{"x": -0.332500, "y": 2336.951144\}, \{"x": 0.000000, "y": 2281.485971\}, \{"x": 0.0000000, "y": 2281.485971\}, \{"x": 0.000000, "y": 2281.485971\}, \{"x": 0.000000, "y": 2281.485971\}, \{"x": 0.000000, "y": 2281.485971], ["x": 0.0000000, "y": 2281.485971], ["x": 0.0000000, "y": 2281.485971], ["x": 0.0000000, "y": 2281.485971], ["x": 0.00000000, "y": 2281.485971], ["x": 0.00000000, "y": 2281.485971], ["x": 0.0000000, "y": 2281.485971], ["x": 0.0000000, "y": 2281.485971], ["x": 0.000000, "y": 2281.485971], ["x": 0.000000, "y": 2$ $0.750000, "y": 2196.393459\}, \{"x": 1.500000, "y": 2114.090711\}, \{"x": 1.692308, "y": 2018.051830\}, \{"x": 2018.05180\}, \{"x": 2018.05180\}, \{"x": 2018.05180\}, \{"x": 2018.05180\}, \{"x": 2018.05180\}, \{"x":$ ${"x": 1.884615, "y":1925.854747}, {"x": 2.076923, "y":1837.368328}, {"x": 2.269231, "y":1837.368328}, {"y": 2.269231, "y": 2.26924, "y": 2.26924$ "y":1752.465063}, {"x": 2.461538, "y":1671.020984}, {"x": 2.653846, "y":1592.915602}, {"x": 2.846154, "y":1518.031831}, {"x": 3.038462, "y":1446.255919}, {"x": 3.230769, "y":1377.477383}, ${"x": 3.423077, "y":1311.588933}, {"x": 3.615385, "y":1248.486412}, {"x": 3.807692, "y":1248.486412}, {"x": 3.807692}, {"x": 3.80769}, {"x": 3.80769}, {"x": 3.8076}, {"x": 3.8076}, {"x": 3.8076}, {"x": 3.8076$ "y":1188.068722}, {"x": 4.000000, "y":1130.237764}, {"x": 4.192308, "y":1074.898369}, {"x": 4.384615, "y":1021.958233}, {"x": 4.576923, "y":971.327853}, {"x": 4.769231, "y":922.920467}, {"x": 4.961538, "y":876.651987}, {"x": 5.153846, "y":832.440942}, {"x": 5.346154, "y":790.208413}, {"x": 5.538462, "y":749.877974}, {"x": 5.730769, "y":711.375636}, {"x": 5.923077, "y":674.629784}, {"x": 6.115385, "y":639.571122}, {"x": 6.307692, "y":605.557910}, {"x": 6.500000, "y":569.636730}, {"x": 6.650000, "y":567.628902}, {"x": 6.650000, $dejanskiTlak = [{"x": 0, "y": 1028.258503273}, {"x": 6.65, "y": 460.87374857031}];$ $\frac{1}{1} = \frac{1}{1} = \frac{1}$ $\{ "x": 0.750000, "y": 964.267741 \}, \ \{ "x": 1.500000, "y": 900.276980 \}, \ \{ "x": 1.692308, \}, \ \{ "x": 1.692308, \}, \ \{ "x": 1.692308, \}, \},$ "y":883.869092}, {"x": 1.884615, "y":867.461204}, {"x": 2.076923, "y":851.053317}, {"x": 2.269231, "y":834.645429}, {"x": 2.461538, "y":818.237541}, {"x": 2.653846, "y":801.829654}, {"x": 2.846154, "y":785.421766}, {"x": 3.038462, "y":769.013879}, {"x": 3.230769, "y":752.605991}, {"x": 3.423077, "y":736.198103}, {"x": 3.615385, "y":719.790216}, {"x": 3.807692, "y":703.382328}, {"x": 4.000000, "y":686.974440}, {"x": 4.192308, "y":670.566553}, {"x": 4.384615, "y":654.158665}, {"x": 4.576923, "y":637.750777}, {"x": 4.769231, "y":621.342890}, {"x": 4.961538, "y":604.935002}, {"x": 5.153846, "y":588.527114}, {"x": 5.346154, "y":572.119227}, {"x": 5.538462, "y":555.711339}, {"x": 5.730769, "y":539.303452}, $\{ "x": 5.923077, "y": 522.895564 \}, \ \{ "x": 6.115385, "y": 506.487676 \}, \ \{ "x": 6.307692, \ (10.101888), \ (10.10188$ "y":490.079789}, {"x": 6.500000, "y":473.671901}, {"x": 6.650000, "y":460.873749}, {"x": 6.650000, "y":460.873749},]; new Chart(ctx2, { "type": 'scatter', "data": { "datasets": [{

```
"label":"Nasičen Tlak", "data": nasicenTlak, "fill":false, "borderColor":"rgb(75, 192, 192)", showLine: true }, { "label":"Dejanski Tlak", "data": dejanskiTlak, "showLine": true }, { "label":"Dejanski Tlak Tocke", "data": dejanskiTlakTocke, "borderColor":"rgb(75, 50, 20)", "showLine": true } ] }, "plugins": [{ beforeDraw: chart => { var ctx = chart.ctx; var xAxis = chart.scales.x; var yAxis = chart.scales.y; ctx.fillStyle = "lightgray"; ctx.rect(xAxis.getPixelForValue(nasicenTlak[1].x), yAxis.top, xAxis.getPixelForValue(nasicenTlak[nasicenTlak.length - 2].x) - xAxis.getPixelForValue(nasicenTlak[1].x), yAxis.bottom-yAxis.top); ctx.fill(); nasicenTlak.forEach((value, index) => { if (index > 0 && index < nasicenTlak.length - 1) { var x = xAxis.getPixelForValue(nasicenTlak[index].x); var yTop = yAxis.getPixelForValue(nasicenTlak[index].y); ctx.save(); ctx.strokeStyle = '#404040'; ctx.beginPath(); ctx.moveTo(x, yAxis.bottom); ctx.lineTo(x, yAxis.top); ctx.stroke(); ctx.restore(); } }); } }], "options": { "scales": { x: { type: "linear", position: "bottom", min: -0.10, max: 6.65 + 0.1 } }, "plugins": { zoom: { zoom: { wheel: { enabled: true, }, pinch: { enabled: true }, mode: 'x', }, pan: { enabled: true, mode: 'x', }, } } });
```

Analiza netransparentne konstrukcije

Naziv: Temeljna plošča

Tip: Tla na terenu pri ploskovnem gretju

	d	λ	ρ	Cp	μ	R	S _d	
	[m]	[W/mK]	[kg/m³]	[J/kg K]	[-]	[m ² K/W]	[m]	
Les	0,010	0,210	800		2510	60,0	0,048	0,600
Estrih	0,050	0,930	1800)	960	15,0	0,054	0,750
EPS 100	0,080	0,039	15		1260	25,0	2,051	2,000
Beton	0,300	2,040	2400)	960	60,0	0,147	18,000
XPS	0,120	0,038	33		1500	120,0	3,158	14,400

Prikaz temperature v konstrukciji

```
const ctx = document.getElementById('myChart'); var temp = [ \{"x": -0.050000, "y": 20.000000\}, 
{"x": 0.000000, "y":20.000000}, {"x": 0.010000, "y":19.818103}, {"x": 0.060000, "y":19.612736},
{"x": 0.068889, "y":18.742118}, {"x": 0.077778, "y":17.871500}, {"x": 0.086667, "y":17.000882},
{"x": 0.095556, "y":16.130264}, {"x": 0.104444, "y":15.259646}, {"x": 0.113333, "y":14.389028},
{"x": 0.122222, "y":13.518410}, {"x": 0.131111, "y":12.647792}, {"x": 0.140000, "y":11.777174},
{"x": 0.440000, "y":11.215434}, {"x": 0.449231, "y":10.287538}, {"x": 0.458462, "y":9.359643},
{"x": 0.467692, "y":8.431747}, {"x": 0.476923, "y":7.503852}, {"x": 0.486154, "y":6.575957}, {"x":
0.495385, "y":5.648061}, {"x": 0.504615, "y":4.720166}, {"x": 0.513846, "y":3.792270}, {"x":
0.523077, "y":2.864375}, {"x": 0.532308, "y":1.936480}, {"x": 0.541538, "y":1.008584}, {"x":
0.550769, "y":0.080689}, {"x": 0.560000, "y":-0.847207}, {"x": 0.560000, "y":-0.847207}, {"x":
0.610000, "y":-1.000000} ]; new Chart(ctx, { "type": 'scatter', "data": { "datasets": [ {
"label":"Temperatura v konstrukciji", "data": temp, "fill":false, "borderColor": "#fa4444",
"lineTension":0.1, showLine: true } ] }, plugins: [{ beforeDraw: chart => { var ctx = chart.ctx; var
xAxis = chart.scales.x; var yAxis = chart.scales.y; ctx.fillStyle = "lightgray";
ctx.rect(xAxis.getPixelForValue(temp[1].x),\ yAxis.top,\ xAxis.getPixelForValue(temp[temp.length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-length-l
2].x) - xAxis.getPixelForValue(temp[1].x), yAxis.bottom-yAxis.top); ctx.fill(); temp.forEach((value,
index) => { if (index > 0 && index Prikaz tlaka in kondenzacije
```

	d	λ	R [m ² K/W]	Sd	T	p_{de}	p _{nas}	g _o	M _a
	[cm]	[W/mK]		[m]	[°C]		[Pa]	[g/m² m]	[g/m ²]
Prostor					20	1028	2337		
Notr.					20	1028	2337		
površina									
Les	1	0.21	0.048	0.6	19.8	1018.7	2310.8		
Estrih	5	0.93	0.054	0.75	19.6	1006.8	2281.5		
EPS 100.1	0.9	0.039		0.2222	18.7	1003.3	2161.1		
EPS 100.2	0.9	0.039	0.228	0.2222	17.9	999.8	2046.2		
EPS 100.3	0.9	0.039	0.228	0.2222	17	996.3	1936.8		
EPS 100.4	0.9	0.039	0.228	0.2222	16.1	992.7	1832.5		
EPS 100.5	0.9	0.039	0.228	0.2222	15.3	989.2			
EPS 100.6	0.9	0.039			14.4	985.7	1638.5		
EPS 100.7	0.9	0.039			13.5				
EPS 100.8	0.9	0.039	0.228	0.2222	12.6	978.6	1462.8		
EPS 100.9	0.9	0.039	0.228	0.2222	11.8	975.1	1381.3		
Beton	30	2.04		18	11.2	689.4	1330.9		
XPS.1	0.9	0.038			10.3	671.8			
XPS.2	0.9	0.038	0.243	1.1077	9.4	654.3	1175.6		•
XPS.3	0.9	0.038	0.243	1.1077	8.4	636.7	1104.1		_

	d	λ	R [m ² K/W]	S _d	T	p_{dei}	p _{nas}	ga	M _a
	[cm]	[W/mK]		[m]	[°C]	[Pa]	[Pa]	[g/m ² m]	[g/m ²]
XPS.4	0.9	0.038	0.243	1.1077	7.5	619.1	1036.5		
XPS.5	0.9	0.038	0.243	1.1077	6.6	601.5	972.6		
XPS.6	0.9	0.038	0.243	1.1077	5.6	583.9	912.1		
XPS.7	0.9	0.038	0.243	1.1077	4.7	566.4	855		
XPS.8	0.9	0.038	0.243	1.1077	3.8	548.8	801		
XPS.9	0.9	0.038	0.243	1.1077	2.9	531.2	750.1		
XPS.10	0.9	0.038	0.243	1.1077	1.9	513.6	702.1		
XPS.11	0.9	0.038	0.243	1.1077	1	496	656.8		
XPS.12	0.9	0.038	0.243	1.1077	0.1	478.5	614.1		
XPS.13	0.9	0.038	0.243	1.1077	-0.8	460.9	569.2		
Zun.					-0.8	461	569	-	
površina									
Okolica					-1	461	562		

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Analiza netransparentne konstrukcije

Naziv: Strop

Tip: Strop proti neogrevanemu prostoru

	d	λ	ρ	Cp	μ	R	S _d	
	[m]	[W/mK]	[kg/m³]	[J/kg K]	[-]	[m ² K/W]	[m]	
Beton	0,150	2,040	240	0	960	60,0	0,074	9,000
Steklena volna	0,300	0,034	23		1030	1,0	8,824	0,300

Prikaz temperature v konstrukciji

```
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ctx.rect(xAxis.getPixelForValue(temp[1].x), yAxis.top, xAxis.getPixelForValue(temp[temp.length -
2].x) - xAxis.getPixelForValue(temp[1].x), yAxis.bottom-yAxis.top); ctx.fill(); temp.forEach((value,
index) => { if (index > 0 && index Prikaz tlaka in kondenzacije
```

	d	λ	R [m ² K/W]	S _d	Т	p _{dei}	p_{nas}	g_d	M _a
	[cm]	[W/mK]		[m]	[°C]	[Pa]		[g/m² m]	[g/m ²]
Prostor					20	1028	2337	-	
Notr.					19.8	1028	2304		
površina									
Beton	15	2.04	0.074	9	19.6	479.2	2279.3		
Steklena	0.8	0.034	0.245	0.0083	19	478.7	2199.9		
volna.1									
Steklena	0.8	0.034	0.245	0.0083	18.5	478.2	2122.9		
volna.2									
Steklena	0.8	0.034	0.245	0.0083	17.9	477.7	2048.4		
volna.3									
Steklena	0.8	0.034	0.245	0.0083	17.3	477.1	1976.1		
volna.4									
Steklena	0.8	0.034	0.245	0.0083	16.7	476.6	1906.1		
volna.5									
Steklena	0.8	0.034	0.245	0.0083	16.2	476.1	1838.2		
volna.6									

			2·····						
	d [cm]	λ [W/mK]	R [m²K/W]	Տ _d [m]	T [°C]	p _{dej} [Pa]	p _{nas} [Pa]	g _c [g/m² m]	M _a [g/m²]
Steklena volna.7	0.8	0.034	0.245	0.0083	15.6		1772.5		
Steklena volna.8	0.8	0.034	0.245	0.0083	15	475.1	1708.8		
Steklena volna.9	0.8	0.034	0.245	0.0083	14.5	474.6	1647.2		
Steklena	0.8	0.034	0.245	0.0083	13.9	474.1	1587.5		
volna.10 Steklena	0.8	0.034	0.245	0.0083	13.3	473.6	1529.7		
volna.11 Steklena	0.8	0.034	0.245	0.0083	12.8	473.1	1473.8		
volna.12 Steklena	0.8	0.034	0.245	0.0083	12.2				
volna.13									
Steklena volna.14	0.8	0.034	0.245	0.0083	11.6		1367.3		
Steklena volna.15	0.8	0.034	0.245	0.0083	11.1	471.6	1316.7		
Steklena volna.16	0.8	0.034	0.245	0.0083	10.5	471	1267.7		
Steklena	0.8	0.034	0.245	0.0083	9.9	470.5	1220.3		
volna.17 Steklena	0.8	0.034	0.245	0.0083	9.3	470	1174.5		
volna.18 Steklena	0.8	0.034	0.245	0.0083	8.8	469.5	1130.2		
volna.19 Steklena	0.8	0.034	0.245	0.0083	8.2	469	1087.3		
volna.20 Steklena	0.8	0.034	0.245	0.0083	7.6				
volna.21									
Steklena volna.22	0.8	0.034	0.245	0.0083					
Steklena volna.23	0.8	0.034	0.245	0.0083	6.5	467.5	967.3		
Steklena volna.24	0.8	0.034	0.245	0.0083	5.9	467	929.9		
Steklena volna.25	0.8	0.034	0.245	0.0083	5.4	466.5	893.9		
Steklena	0.8	0.034	0.245	0.0083	4.8	466	859.1		
volna.26 Steklena	0.8	0.034	0.245	0.0083	4.2	465.4	825.5		
volna.27 Steklena	0.8	0.034	0.245	0.0083	3.6	464.9	793		
volna.28 Steklena	0.8	0.034	0.245	0.0083	3.1	464.4	761.7		
volna.29 Steklena	0.8	0.034	0.245	0.0083	2.5	463.9	731.5		
volna.30 Steklena	0.8	0.034	0.245	0.0083					
volna.31									
Steklena volna.32	0.8	0.034	0.245	0.0083					
Steklena volna.33	0.8	0.034	0.245	0.0083	0.8	462.4	647		
Steklena volna.34	0.8	0.034	0.245	0.0083	0.2	461.9	620.9		
Steklena volna.35	0.8	0.034	0.245	0.0083	-0.3	461.4	593.7		
Steklena	0.8	0.034	0.245	0.0083	-0.9	460.9	566.4		
volna.36 Zun.					-0.9	461	566		
površina Okolica					-1	461	562		

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Tocke", "data": dejanskiTlakTocke, "borderColor": "rgb(75, 50, 20)", "showLine": true } ] }, "plugins":
[{ beforeDraw: chart => { var ctx = chart.ctx; var xAxis = chart.scales.x; var yAxis = chart.scales.y;
ctx.fillStyle = "lightgray"; ctx.rect(xAxis.getPixelForValue(nasicenTlak[1].x), yAxis.top,
xAxis.getPixelForValue(nasicenTlak[nasicenTlak.length - 2].x) -
xAxis.getPixelForValue(nasicenTlak[1].x), yAxis.bottom-yAxis.top); ctx.fill();
nasicenTlak.forEach((value, index) => { if (index > 0 && index < nasicenTlak.length - 1) { var x = } }
xAxis.getPixelForValue(nasicenTlak[index].x); var yTop =
yAxis.getPixelForValue(nasicenTlak[index].y); ctx.save(); ctx.strokeStyle = '#404040';
ctx.beginPath(); ctx.moveTo(x, yAxis.bottom); ctx.lineTo(x, yAxis.top); ctx.stroke(); ctx.restore(); }
}); } }], "options": { "scales": { x: { type: "linear", position: "bottom", min: -0.10, max: 9.3 + 0.1 } },
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```

Ovoj cone "Ogrevana cona"

<u>← Nazaj</u>

Zaporedna št. kon Št. enakih Orientacija Naklon Toplotna prehodno Površina Faktor		° W/m²K m²		Tp1 1 0 0,125 200,0 1,30	Ts1 1 0 0,111 200,0 1,00	V1 1 S 90 1,000 3,0 1,00	15,0	5,0	O1 2 V 90 0,820 1,0 1,00	9 0,8 1	01 2 5 90 320 ,0
	U×A×	d _f W/K		32,5	22,1	3,0	10,2	3,7	0,8	0	,8
Faktor senčenja ol	koliških ovir	jan feb mar apr maj jun jul avg sep okt nov	1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000	1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000	1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000 1,000	1,000 0,993 0,964 0,945 0,953 0,984 1,000 1,000	0 0,984 0 0,982 8 0,980 4 0,978 6 0,793 8 0,788 4 0,799 0 0,843 0 0,986	0,936 0,913 0,895 0,888 0,895 0,889 0,889 0,887 0,908 0,930 0,956	0,938 0,938 0,937 0,937 0,939 0,937 0,935 0,943 0,948	1,0 0,9 0,9 0,9 0,9 0,9 1,0 1,0	000 000 000 994 978 971 974 988 000 000
Mesečno sončno c H _{sol,m} (Wh/m²m)	jan feb mar apr maj jun jul avg sep okt nov dec	dec št. dni 31 28 31 30 31 30 31 30 31 30 31	7967 11480 19654 30810 37200 42510 39370 32240 23610 16306 9720 7006	1,000 28427 48468 85529 121470 151714 158220 169539 146909 100620 59241 29490 21638	48468 85529 121470 151714 158220 169539 146909 100620 59241 29490	11480 19654 30810 4 37200 42510 39370 32240 23610 16300 9720	14446 22484 441664 58440 71333 69660 73129 66619 45420 628113 15960	5 43431 4 59752 4 72354 0 69870 1 65999 0 66774 9 74803 0 72000 7 56451	14446 22484 41664 58440 71331 69660 473129 66619 45420 28117	79 114 190 300 370 420 390 320 230 160 97	967 480 654 810 200 510 370 240 610 306 720
Transmisijske toplotne izgube Q (kWh/m)	ΔT :r,m	št. dni	OGREVAN	IJE							
jan	21	31 69	90,7	348,7	470,8	48,7	169,5	181,3	26,9	26,9	196 3,4
feb	19	28 56	54,5 2	295,6	384,7	39,8	138,5	148,2	22,0	22,0	161
mar	15	31 49	93,4 2	284,3	336,3	34,8	121,1	129,5	19,2	19,2	5,2 143
apr	11	30 35	50,1 2	290,2	238,6	24,7	85,9	91,9	13,6	13,6	7,7 110 8,7
maj	6	31 19	97,3 2	279,4	134,5	13,9	48,4	51,8	7,7	7,7	740 ,8
jun	3	30 9	5,5 2	258,6	65,1	6,7	23,4	25,1	3,7	3,7	481
jul	1	31 3	2,9 2	259,0	22,4	2,3	8,1	8,6	1,3	1,3	,8 335 ,9
avg	1	31 3	2,9 2	259,0	22,4	2,3	8,1	8,6	1,3	1,3	,3 335 ,9
sep	5	30 15	59,2 2	266,5	108,5	11,2	39,1	41,8	6,2	6,2	638 ,6

okt	10	31	328,9	230,7	224,2	23,2	80,7	86,3	12,8	12,8	999 ,7
nov	16	30	509,3	285,5	347,1	35,9	125,0	133,7	19,8	19,8	147 6,2
dec	20	31	657,8	337,9	448,4	46,4	161,4	172,7	25,6	25,6	187 5,8
Transmisijske toplotne izgube	ΔΤ	št. dni	HLAJENJE								Sku paj
Q _{tr,m} (kWh/m) jan	27	31	888,1	348,7	605,3	62,7	217,9	233,1	34,6	34,6	242
feb	25	28	742,7	295,6	506,2	52,4	182,2	194,9	28,9	28,9	4,8 203
mar	21	31	690,7	284,3	470,8	48,7	169,5	181,3	26,9	26,9	1,9 189
apr	17	30	541,1	290,2	368,8	38,2	132,8	142,0	21,1	21,1	9,1 155
maj	12	31	394,7	279,4	269,0	27,9	96,9	103,6	15,4	15,4	5,2 120
jun	9	30	286,5	258,6	195,2	20,2	70,3	75,2	11,1	11,1	2,2 928
jul	7	31	230,2	259,0	156,9	16,2	56,5	60,4	9,0	9,0	,3 797
avg	7	31	230,2	259,0	156,9	16,2	56,5	60,4	9,0	9,0	,3 797
sep	11	30	350,1	266,5	238,6	24,7	85,9	91,9	13,6	13,6	,3 108
okt	16	31	526,3	230,7	358,7	37,1	129,1	138,1	20,5	20,5	5,0 146
nov	22	30	700,3	285,5	477,3	49,4	171,8	183,8	27,2	27,2	1,0 192
dec	26	31	855,2	337,9	582,9	60,4	209,8	224,5	33,3	33,3	2,6 233
5 1 v		v	00051/44	_							7,2
Dobitki sončnega obsevanja Qsol,m		št. dni	OGREVANJI	E							Sku paj
, , ,	jan	31	-25,73	0,00	-40,84	-2,11	96,81	272,20	10,91	5,80	317 ,1
	feb	28	-20,97	0,00	-36,88	-1,91	154,64	369,00	17,41	8,99	490 ,3
	mar	31	-19,53	0,00	-40,84	-2,11	291,00	436,05	33,01	16,03	713 ,6
	apr	30	-12,65	0,00	-39,52	-2,05	410,40	412,91	46,76	25,66	841
	maj	31	-10,22	0,00	-40,84	-2,11	501,42	386,37	57,32	30,65	,5 922 ,6
	jun	30	-6,44	0,00	-39,52	-2,05	395,35	358,18	56,12	35,00	796
	jul	31	-9,07	0,00	-40,84	-2,11	412,48	391,39	58,75	32,37	,6 843
	avg	31	-12,85	0,00	-40,84	-2,11	380,91	438,31	53,33	26,69	,0 843 ,4
	sep	30	-16,47	0,00	-39,52	-2,05	271,87	431,98	36,34	19,52	701
	okt	31	-21,31	0,00	-40,84	-2,11	194,75	345,18	22,14	13,10	,7 510 ,9
	nov	30	-23,83	0,00	-39,52	-2,05	107,75	209,40	12,12	7,38	,9 271 ,2
	dec	31	-26,24	0,00	-40,84	-2,11	80,53	192,47	8,94	4,96	,2 217 ,7

Dobitki sončnega št. dni obsevanja Qsol,m (kWh/m)

Analiza sNES "Testni Projekt"

<u>← Nazaj</u>

Kazalniki energijsk	e učinkovitosti	stavbe
		Količina (kWh/an)
Neutežena dovedena energija	E _{del,an}	9180
za delovanje TSS	aci,aii	
	E _{w,del,an}	17235
delovanje TSS	w,uei,aii	
Obnovljiva primarna energija	E _{Pren.an}	9180
dovedene energije	-rien,an	3233
Neobnovljiva primarna energija	F _{Daron} on	8055
dovedene energije	-Filleli,ali	
Skupna primarna energija	E _{Ptot.an}	17235
	i—Ptot.an	
		Vrednost (%)
Razmernik obnovljivih virov		53
energije ROVE		
Minimalni zahtevani razmernik		50
ROVE _{min}]
Ustreza minimalni zahtevi		DA
Ostreza minimalni zantevi		Vrednost (-)
Korekcijski faktor razmernika		1.0
ROVE X _{OVE}		1,0
Kompenzacijski faktor		0,8
razmernika ROVE Y _{ROVE}		0,0
IdZITIEITIIKA KOVE I _{ROVE}		l .
Korekcijski faktor dovoljene		1,0
skupne primarne energije		1,0
glede na vrsto stavbe X.		
Korekcijski faktor dovoljene		1,0
skupne primarne energije		1,0
glede na leto uveljavitve X _p		
Kompenzacijski faktor potrebne		1,2
toplote za ogrevanje Y _{H.nd}		1,2
topiote za ogrevanje r _{H.nd}		<u> </u>
		Količina (kWh/an)
Specifična potrebna skupna	E:	108
primarna energija	E' _{Ptot,an}	100
	 	103
	E' _{Ptot,kor,an}	103
primarna energija Dovoljena specifična potrebna	C'	75
	E' _{Ptot,kor,an}	/3
skupna primarna energija		75
Korigirana dovoljena specifična	E Ptot,kor,dov,an	75
potrebna skupna primarna 		
energija		
Ustreza minimalni zahtevi		NE
		1 1/1/2
		Vrednost (kg/an)
Izpusti ogljikovega dioksida	$M_{CO2,an}$	2255