

Governing Equations for elastic bodies

unknown

- 3 displacements u_i
 - 6 strains ϵ_{ij}
 - 6 stresses σ_{ij}
 - density (important when $\alpha \neq 0$) ρ
- } 15

Known

- 6 displacement-strain relations, $[\epsilon] = \frac{(\nabla u + \nabla u^T)}{2}$
- 3 equilibrium equations, $\nabla \cdot \sigma + f = \rho a$
- 1 continuity equation $\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho v) = 0$

10 equations

- we need constitutive relationships

$$\sigma_{ij} = \sigma_{ij}(\epsilon_{ij}, \underbrace{\alpha}_{\substack{\text{material} \\ \text{rheological} \\ \text{parameters}}})$$

For elastic bodies,

use **Hooke's law** ie $\sigma_{ij} \propto \epsilon_{ij}$
linear

$$\sigma_{ij} = \underbrace{C_{ijkl}}_{81 \text{ parameters for generalized Hooke's Law}} \epsilon_{kl}$$

→ in a homogenous & isotropic medium,

$$C_{ijkl} \rightarrow [\lambda, G]$$

Lamé's parameters

Hooke's law : $\sigma_{ij} = \lambda \epsilon_{kk} \delta_{ij} + 2G \epsilon_{ij}$ [equation 6]

$$\epsilon_{kk} = (\epsilon_{11} + \epsilon_{22} + \epsilon_{33})$$

$$[\sigma] = \lambda \epsilon_{kk} [I] + 2G [\epsilon]$$

→ λ, G can be measured directly in a solid

→ some related material properties [commonly used]

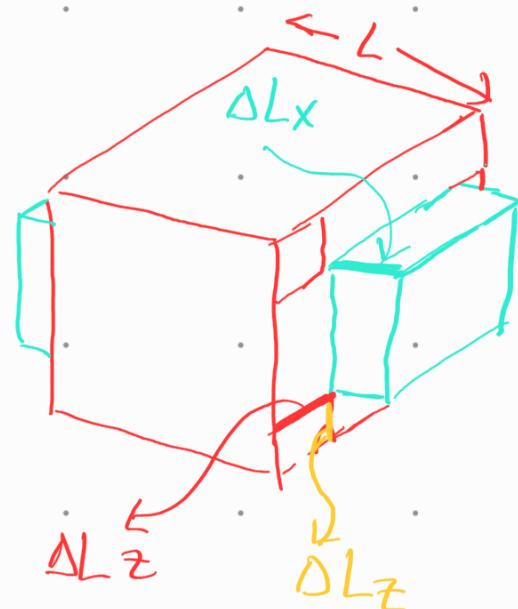
$$1. K = \lambda + \frac{2}{3}G = -V \frac{dP}{dV}$$
 bulk modulus

$$2. \nu = \frac{\lambda}{2(\lambda + G)} \rightarrow \text{Poisson's Ratio}$$

$$F/A = -\left(\frac{\epsilon_y}{\epsilon_x}\right) = -\left(\frac{\epsilon_z}{\epsilon_x}\right)$$

$$3. G = \frac{\tau_{xy}}{2\epsilon_{xy}}$$

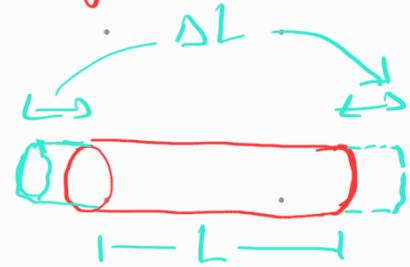
shear modulus / rigidity



$$4. E = G \frac{(3\lambda + 2G)}{(\lambda + G)}$$
 → Young's Modulus

$$= 2G_1(1+\nu)$$

$$= \frac{|\sigma|}{|\epsilon|} \rightarrow \frac{\text{axial stress}}{\text{axial strain}}$$



$$\epsilon_{11} = \frac{1}{E} (\sigma_{11} - \nu (\sigma_{22} + \sigma_{33}))$$

$$\epsilon_{22} = \frac{1}{E} (\sigma_{22} - \nu (\sigma_{11} + \sigma_{33}))$$

$$\epsilon_{33} = \frac{1}{E} (\sigma_{33} - \nu (\sigma_{11} + \sigma_{22}))$$

tri-anisotropic
stress &
strain

Hooke's Law in 3-d

— we generally use (G_1, ν)

$$\begin{bmatrix} \sigma_{11} & \sigma_{12} & \sigma_{13} \\ \sigma_{21} & \sigma_{22} & \sigma_{23} \\ \sigma_{31} & \sigma_{32} & \sigma_{33} \end{bmatrix} = 2G_1 \begin{bmatrix} \epsilon_{11} & \epsilon_{12} & \epsilon_{13} \\ \epsilon_{21} & \epsilon_{22} & \epsilon_{23} \\ \epsilon_{31} & \epsilon_{32} & \epsilon_{33} \end{bmatrix} + \lambda \epsilon_{kk} \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

$$\begin{bmatrix} \sigma_{11} \\ \sigma_{22} \\ \sigma_{33} \\ \sigma_{23} \\ \sigma_{13} \\ \sigma_{12} \end{bmatrix} = \frac{2G_1}{(1-2\nu)} \begin{bmatrix} 1-\nu & \nu & \nu & 0 & 0 & 0 \\ \nu & 1-\nu & \nu & 0 & 0 & 0 \\ \nu & \nu & 1-\nu & 0 & 0 & 0 \\ 0 & 0 & 0 & \frac{1-2\nu}{2} & 0 & 0 \\ 0 & 0 & 0 & 0 & \frac{1-2\nu}{2} & 0 \\ 0 & 0 & 0 & 0 & 0 & \frac{1-2\nu}{2} \end{bmatrix} \begin{bmatrix} \epsilon_{11} \\ \epsilon_{22} \\ \epsilon_{33} \\ \epsilon_{23} \\ \epsilon_{13} \\ \epsilon_{12} \end{bmatrix}$$

6 equations

Apply this to momentum conservation

$$\nabla \cdot \underline{\sigma} + \underline{f} = \underline{\rho a}$$

$$(\underline{\sigma}_{ij,j} \text{ or } \underline{\sigma}_{ij,j}) \leftarrow \underline{\sigma} = \underline{\sigma}^T$$

$$(\lambda \sum_{kk} \delta_{ji} + 2G \underline{\epsilon}_{ji})_{,j} \quad \begin{matrix} \text{insert Hooke's law} \\ \text{to } [\underline{\sigma}] \end{matrix}$$

$$(u_{k,k}) \quad \frac{1}{2}(u_{j,i} + u_{i,j})$$

$$(\lambda u_{k,k} \delta_{ji} + G(u_{j,i} + u_{i,j}))_{,j}$$

$$\lambda u_{j,i,j} + G(u_{j,i,j} + u_{i,j,j}) + f_i = \rho a_i$$

$$(\lambda + G) u_{j,i,j} + G u_{i,j,j} + f_i = \rho a_i$$

- vector/tensor notations

$$\nabla \cdot \underline{\sigma} + \underline{f} = \underline{\rho a}$$

$$\nabla \underline{u} = \begin{bmatrix} u_{1,1} & u_{2,1} & u_{3,1} \\ u_{1,2} & u_{2,2} & u_{3,2} \\ u_{1,3} & u_{2,3} & u_{3,3} \end{bmatrix}$$

$$\nabla \cdot (\lambda \underline{\epsilon}_{kk} \underline{I} + 2G[\underline{\epsilon}]) + \underline{f} = \underline{\rho a}$$

$$\lambda \nabla \cdot \begin{bmatrix} \nabla \cdot \underline{u} & 0 & 0 \\ 0 & \nabla \cdot \underline{u} & 0 \\ 0 & 0 & \nabla \cdot \underline{u} \end{bmatrix} + G \nabla \cdot (\nabla \underline{u} + \nabla \underline{u}^T) + \underline{f} = \underline{\rho a}$$

$$\lambda \begin{bmatrix} \frac{\partial (\nabla \cdot \underline{u})}{\partial x_1} \\ \frac{\partial (\nabla \cdot \underline{u})}{\partial x_2} \\ \frac{\partial (\nabla \cdot \underline{u})}{\partial x_3} \end{bmatrix} + G \nabla^2 \underline{u} + G \nabla \cdot \nabla \underline{u}^T + \underline{f} = \underline{\rho a}$$

$$\begin{bmatrix} \nabla^2 u_1 \\ \nabla^2 u_2 \\ \nabla^2 u_3 \end{bmatrix} \quad \begin{bmatrix} u_{1,11} + u_{2,12} + u_{3,13} \\ u_{1,21} + u_{2,22} + u_{3,23} \\ u_{1,31} + u_{2,32} + u_{3,33} \end{bmatrix}$$

$$\nabla (\nabla \cdot \underline{u})$$

$$(\lambda + G) \nabla(\nabla \cdot \underline{u}) + G \nabla^2 \underline{u} + \underline{f} = \underline{\rho a}$$

$$\underline{a} = \frac{\partial^2 \underline{u}}{\partial t^2}$$

Elastic-wave
equation

i.e.

$$(\lambda + G) \nabla(\nabla \cdot \underline{u}) + G \nabla^2 \underline{u} + \underline{f} = \underline{\rho} \frac{\partial^2 \underline{u}}{\partial t^2}$$

\underline{u} → 3 unknowns, 3 equations

(λ, G, ρ) → known for material

Elasto-statics → $\underline{a} \rightarrow 0$

$$(\lambda + G) [\nabla \cdot (\nabla \underline{u})] + G (\nabla^2 \underline{u}) + \underline{f} = 0$$

If we take the time-derivative

$$(\lambda + G) [\nabla \cdot (\nabla \underline{v})] + G (\nabla^2 \underline{v}) + \underline{f}(t) = 0$$

Quasi-static equilibrium [elastic body]

Simplifying geometries

Anti-plane

in-plane

$$\underline{u} = [u_1, 0, 0]$$

$$\frac{\partial(\underline{u})}{\partial x_1} = 0$$

$$\underline{u} = [0, u_2, u_3]$$

$$\frac{\partial(\underline{u})}{\partial x_1} = 0$$

3 equilibrium equations

$$(\lambda + G_1) [u_{1,11} + u_{2,12} + u_{3,13}] + G_1 [u_{1,11} + u_{1,22} + u_{1,33}] + f_1 = 0$$

$$(\lambda + G_1) [u_{1,21} + u_{2,22} + u_{3,23}] + G_1 [u_{2,11} + u_{2,22} + u_{2,33}] + f_2 = 0$$

$$(\lambda + G_1) [u_{1,31} + u_{2,32} + u_{3,33}] + G_1 [u_{3,11} + u_{3,22} + u_{3,33}] + f_3 = 0$$

Anti-plane strain : $G_1 (u_{1,22} + u_{1,33}) + f_1 = 0$

Plane-strain :

$$(\lambda + G_1) [u_{2,22} + u_{3,23}] + G_1 [u_{2,22} + u_{2,33}] + f_2 = 0$$

$$(\lambda + G_1) [u_{2,32} + u_{3,33}] + G_1 [u_{3,22} + u_{3,33}] + f_3 = 0$$

