

Green's functions

(Elastostatic equilibrium in anti-plane)

$$G \nabla^2 u + f = 0$$

In cartesian coordinates, $\frac{\partial^2 u_1}{\partial x_2^2} + \frac{\partial^2 u_1}{\partial x_3^2} + \frac{f}{G} = 0$

In polar coordinates, $\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial u_1}{\partial r} \right) + \frac{f}{G} = 0$

Defining ∇ in polar coordinates (r, θ)

$$r = \sqrt{x_2^2 + x_3^2}$$

$$\theta = \tan^{-1} \left(\frac{x_3}{x_2} \right)$$

$$\begin{bmatrix} \hat{r} = \cos \theta \hat{x}_2 + \sin \theta \hat{x}_3 \\ \hat{\theta} = -\sin \theta \hat{x}_2 + \cos \theta \hat{x}_3 \end{bmatrix}$$

length increment $d\hat{r} = d(r \hat{r})$

$$\hat{r} \text{ — unit vector } [\text{no dependence on } r] = dr \hat{r} + r d\hat{r} \quad \text{--- ①}$$

using chain rule

$$d\hat{r} = \frac{\partial \hat{r}}{\partial r} dr + \frac{\partial \hat{r}}{\partial \theta} d\theta$$

$$\frac{\partial \hat{r}}{\partial \theta} = \hat{\theta}$$

$$d\hat{r} = \hat{\theta} d\theta \quad \text{--- ②}$$

Apply ② in ①,

$$d\hat{r} = dr \hat{r} + r d\theta \hat{\theta} \quad \text{--- ③}$$

So we have a scalar θ and a vector $\hat{\theta}$

so now let's consider any scalar ϕ and its length increment $d\phi \leftarrow$ scalar length change.

in cartesian coordinates,

$$d\phi = \frac{\partial \phi}{\partial x_2} dx_2 + \frac{\partial \phi}{\partial x_3} dx_3$$

$\phi(x_2, x_3)$

$$d\phi = (\nabla \phi) \cdot d\underline{x} \quad \text{where } d\underline{x} = \begin{bmatrix} dx_2 \\ dx_3 \end{bmatrix}$$

in polar coordinates,

$$\phi(r, \theta) \quad d\phi = \nabla \phi \cdot d\underline{r} \quad \leftarrow \begin{array}{l} \text{length increment of } \underline{x} \\ \text{length increment of } \underline{r} \end{array}$$

from chain rule,

$$d\phi(r, \theta) = \frac{\partial \phi}{\partial r} dr + \frac{\partial \phi}{\partial \theta} d\theta$$

$$\frac{\partial \phi}{\partial r} dr + \frac{\partial \phi}{\partial \theta} d\theta = \nabla \phi \cdot d\underline{r} \quad \text{--- (4)}$$

insert (3) into (4) $\curvearrowright (dr \hat{i} + r d\theta \hat{\theta})$

$$\frac{\partial \phi}{\partial r} dr + \frac{\partial \phi}{\partial \theta} d\theta = A_1 dr + A_2 r d\theta$$

$$\Rightarrow \boxed{\nabla = \left[\frac{\partial}{\partial r} \hat{i} + \frac{1}{r} \frac{\partial}{\partial \theta} \hat{\theta} \right]} \quad \text{--- (5)}$$

Divergence in polar coordinates ($\nabla \cdot \underline{u}$)

Consider a vector field $\underline{u} = u_r \hat{r} + u_\theta \hat{\theta}$

from (5), we know $\nabla = \begin{bmatrix} \frac{\partial}{\partial r} & \hat{r} \\ \frac{1}{r} \frac{\partial}{\partial \theta} & \hat{\theta} \end{bmatrix}$

So divergence $\nabla \cdot \underline{u} = \nabla \cdot \begin{bmatrix} u_r & \hat{r} \\ u_\theta & \hat{\theta} \end{bmatrix}$

$$= \hat{r} \cdot \left(\frac{\partial (u_r \hat{r})}{\partial r} + \frac{\partial (u_\theta \hat{\theta})}{\partial \theta} \right)$$

$$+ \frac{\hat{\theta}}{r} \cdot \left(\frac{\partial (u_r \hat{r})}{\partial \theta} + \frac{\partial (u_\theta \hat{\theta})}{\partial r} \right)$$

$$= \hat{r} \cdot \left(\frac{\partial u_r}{\partial r} \hat{r} + u_r \frac{\partial \hat{r}}{\partial r}^0 + \frac{\partial u_\theta}{\partial r} \hat{\theta} + u_\theta \frac{\partial \hat{\theta}}{\partial r}^0 \right)$$

$$+ \frac{\hat{\theta}}{r} \cdot \left(\frac{\partial u_r}{\partial \theta} \hat{r} + u_r \frac{\partial \hat{r}}{\partial \theta}^1 + \frac{\partial u_\theta}{\partial \theta} \hat{\theta} + u_\theta \frac{\partial \hat{\theta}}{\partial \theta}^1 \right)$$

$$= \cancel{\frac{\partial u_r}{\partial r}} + \cancel{u_r \frac{\partial \hat{r}}{\partial r}} + \cancel{\frac{\partial u_\theta}{\partial r}} + \cancel{u_\theta \frac{\partial \hat{\theta}}{\partial r}}$$

$$\frac{1}{r} \frac{\partial}{\partial r} (r u_r) + \frac{1}{r^2} \frac{\partial^2 u_r}{\partial \theta^2}$$

$$\boxed{\nabla \cdot \underline{u} = \frac{1}{r} \left[\frac{\partial}{\partial r} (r u_r) + \frac{\partial u_\theta}{\partial \theta} \right]} - (6)$$

\Rightarrow Laplacian in polar coordinates ($\nabla \cdot \nabla \phi$)
 — apply (5) & (6),

$$\nabla \cdot \nabla \phi = \nabla \cdot \left(\frac{\partial \phi}{\partial r} \hat{r} + \frac{1}{r} \frac{\partial \phi}{\partial \theta} \hat{\theta} \right)$$

$$= \frac{1}{r} \left[\frac{\partial}{\partial r} \left(r \frac{\partial \phi}{\partial r} \right) + \frac{\partial}{\partial \theta} \left(\frac{1}{r} \frac{\partial \phi}{\partial \theta} \right) \right]$$

$$\boxed{\nabla^2 \phi = \frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial \phi}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 \phi}{\partial \theta^2}} - (7)$$

Coming back to elastostatic equilibrium [anti-plane geometry]

$$\underbrace{\nabla^2 u}_{\text{Laplace's equation}} + \frac{f}{G} = 0$$

Laplace's
equation

Poisson's equation

$\frac{f}{G} \rightarrow$ source term

Poisson's equation

$$\nabla^2 u = 0 \rightarrow (x_2, x_3) \rightarrow ax_2 + bx_3$$

general solutions

$$\left\{ \begin{array}{l} a(x_2^2 - x_3^2) + bx_2x_3 \\ \exp(ux_3)[a \cos ux_2 + b \sin ux_2] \end{array} \right.$$

$\rightarrow (r, \theta) \rightarrow a \ln r$

general solutions

$$\left\{ \rightarrow \left(a \frac{r^m + b}{r^m} \right) \left(c \cos m\theta + d \sin m\theta \right) \right.$$

- These solutions obey linear superposition
- Uniqueness → only when we match boundary conditions. limit of Gaussian

The source term is a boundary condition)

⇒ point source $\delta(x_2)\delta(x_3)$ or $\delta(r)$
 for any location $(y_2, y_3) \rightarrow \delta(x_2 - y_2)\delta(x_3 - y_3)$

in polar coordinates, $\delta(r) = \frac{1}{2\pi r} \delta(r)$

$$\iint_{x_2 x_3} \delta(\underline{x}) dx_2 dx_3 = \iint_0^{2\pi} \delta(r) dr r d\theta = 1$$

property of Delta-dirac function /
 point source

$$\Rightarrow \nabla u + \left(\frac{f}{G} \right) = 0$$

source terms
→ Delta-dirac function

solution $u(x_2, x_3)$ at $r=0$

or $u(r, \theta)$ is a Greens function solution

⇒ response of the full-space to a unit body force at the source -

This has huge implications since any force distributions can be decomposed as

$$f(x_2, x_3) = \iiint_{-\infty}^{\infty} \delta(x_2 - y_2) \delta(x_3 - y_3) f(y_2, y_3) dy_2 dy_3$$

Break f into a number of point sources & sum

The Greens functions can then be used to compute the weighted sum ⇒ displacements

$$\Rightarrow \nabla \underbrace{\xi(x_2, x_3; y_2, y_3)}_{\text{source}} + \underbrace{\delta(x_2 - y_2) \delta(x_3 - y_3)}_G = 0$$

$$\Rightarrow u_i(x_2, x_3) = \iint_{-\infty}^{\infty} \xi(x_2, x_3; y_2, y_3) f(y_2, y_3) dy_2 dy_3$$

Because u_1 is a response to a point force, we expect it to decay only radially,
 $\Rightarrow u_1 = u_1(r)$ [no θ dependence]
 \rightarrow makes computing Greens functions easier.

So the governing PDE in polar coordinates,

$$\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial u}{\partial r} \right) = \frac{s(r)}{2\pi r}$$

$\underbrace{-f(r)}$

The solution is found by

integrating twice $\boxed{u_1(r) = \frac{1}{2\pi} \ln r}$

in (x_2, x_3) $\boxed{u_1(x_2, x_3) = \frac{1}{4\pi} \ln(x_2^2 + x_3^2)}$

Greens Function for a point source at $(y_2, y_3) = (0, 0)$

$$G(x_2, x_3; y_2, y_3) = \frac{1}{4\pi} \ln((x_2 - y_2)^2 + (x_3 - y_3)^2)$$

These Greens Functions are defined in a full space, if we want to introduce a free-surface, we need to match the boundary condition.

x_2 traction-free

$$x_3 \quad (y_2, y_3) \quad \begin{bmatrix} 0 & \Gamma_{12} & \Gamma_{13} \\ \Gamma_{12} & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \quad \begin{bmatrix} 0 \\ 0 \\ -1 \end{bmatrix} \quad \Rightarrow \begin{bmatrix} -\Gamma_{13} \\ 0 \\ 0 \end{bmatrix}$$

Boundary condition is $\Gamma_{13}(x_2, x_3=0) = 0$.

$$\Gamma_{13} = \frac{G}{2} \frac{\partial u_1}{\partial x_3} \Big|_{x_3=0} = 0. \text{ This is solved by introducing image sources at } (y_2, -y_3)$$

$$\Rightarrow \boxed{g(x_2, x_3; y_2, y_3) = \frac{1}{4\pi} \left\{ \ln((x_2-y_2)^2 + (x_3-y_3)^2) + \ln((x_2-y_2)^2 + (x_3+y_3)^2) \right\}}$$

Half-space Green functions

Equivalent body-forces & BCs

- We used the source term in Poisson's eqn to describe a force applied at a location (y_2, y_3) , and it only existed as $\delta(y_2)\delta(y_3)$
- Now when we need a finite length source, we build on the same principles.

The equivalent body force density f is given from the divergence of the moment density tensor.

$$m_{ij} = G \underbrace{\varepsilon_{ij}^{(i)}}_{\text{stress tensor}} \leftarrow \text{inelastic strain tensor}$$

[only defined on the fault plane]

Equilibrium equation applied at the fault,

$$\nabla \cdot m + f = 0.$$

$$\Rightarrow f = -\nabla \cdot \bar{m} = -\nabla \cdot (G \varepsilon^{(i)})$$

$$f_i = -G \varepsilon_{ji,j}^{(i)} \quad \begin{matrix} \text{slip vector} \\ \text{not a unit vector} \end{matrix}$$

$$\varepsilon^{(i)} = \frac{1}{2} (\hat{n} \otimes \underline{r} + \underline{r} \otimes \hat{n})$$

$$\text{for a vertical fault } \hat{n} = \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix}, \underline{r} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

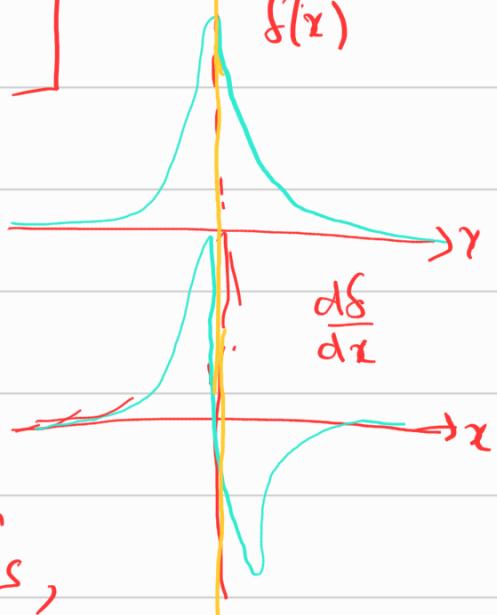
$$\text{only } \varepsilon_{12}^{(i)} = \varepsilon_{21}^{(i)} \neq 0$$

$$= \frac{S}{2} \delta(x_2) \Pi \left(\frac{x_3}{w} \right)$$

$$\Rightarrow m = \begin{bmatrix} 0 & 2G\varepsilon_{12}^{(i)} & 0 \\ 2G\varepsilon_{21}^{(i)} & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

$$\text{so } f = -\nabla \cdot m = \begin{bmatrix} -2G\varepsilon_{21,2}^{(i)} \\ 0 \end{bmatrix}$$

$$f_i = -2G \underset{\delta\text{-derivative}}{\cancel{s}} \frac{\partial \delta(x_2)}{\partial x_2} \pi\left(\frac{x_3}{w}\right)$$



Use this with our full-space GFs,

$$U_i(x_2, x_3) = -\frac{S}{4\pi} \iint_{-\infty}^{\infty} f_i(y_2, y_3) \ln\left(\frac{(x_2-y_2)^2 + (x_3-y_3)^2}{w^2}\right) dy_2 dy_3$$

$\frac{f}{G}$ source

$$= -\frac{S}{4\pi} \iint_{-\infty}^{\infty} \frac{\partial \delta(y_2)}{\partial y_2} \ln\left(\frac{(x_2-y_2)^2 + (x_3-y_3)^2}{w^2}\right) \pi\left(\frac{y_3}{w}\right) dy_2 dy_3$$

• use δ -identity, $\int \delta(x-a) f(x) dx = f(a)$

$$\bullet \text{ we } \int_{-\infty}^{\infty} \pi\left(\frac{x}{w}\right) f(x) dx = \int_{-w/2}^{w/2} f(x) dx .$$

$$= -\frac{S}{4\pi} \int_{-w/2}^{w/2} \frac{2(x_2 - 0)}{x_2^2 + (x_3 - y_3)^2} dy_3$$

$$= -\frac{S}{2\pi} \int_{-w/2}^{w/2} \frac{x_2}{x_2^2 + (x_3 - y_3)^2} dy_3 = -\frac{S}{2\pi} \left[\tan^{-1} \frac{x_3 - y_3}{x_2} \right]_{-w/2}^{w/2}$$

$y_3 = \frac{w}{2}$

$$\int_{-\frac{w}{2}}^{\frac{w}{2}} x_2 + (x_3 - y_3)^2 \, dx_2 = \frac{2\pi}{2} \left[\begin{array}{l} x_2 \\ y_3 = \frac{-w}{2} \end{array} \right]$$

$$U_1(x_2, x_3) = \frac{S}{2\pi} \left[\tan^{-1} \frac{x_3 + \frac{w}{2}}{x_2} - \tan^{-1} \frac{x_3 - \frac{w}{2}}{x_2} \right]$$

Full-space solution for finite fault located at $(0, 0)$ with width w

To move the source location to (y_2, y_3)

$$U_1(x_2, x_3) = \frac{S}{2\pi} \left[\tan^{-1} \frac{x_3 - y_3 + \frac{w}{2}}{x_2 - y_2} - \tan^{-1} \frac{x_3 - y_3 - \frac{w}{2}}{x_2 - y_2} \right]$$

To account for free-surface i.e half-space, add image solution at $(y_2, -y_3)$

$$U_1(x_2, x_3) = \frac{S}{2\pi} \left[\tan^{-1} \frac{x_3 - y_3}{x_2 - y_2} \right]_{y_3 = \frac{-w}{2}}^{y_3 = \frac{w}{2}} + \frac{S}{2\pi} \left[\tan^{-1} \frac{x_3 + y_3}{x_2 - y_2} \right]_{y_3 = -\frac{w}{2}}^{y_3 = \frac{w}{2}}$$

$$u_1(x_2, y_3) = \frac{5}{2+1} \left| \tan \frac{x_3 - y_3}{x_2 - y_2} \right|$$

Curvilinear
Notation

