

PROJECT REPORT

ECE 569 - INTRODUCTION TO ROBOTIC SYSTEMS

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Introduction:

OpenRAVE is an open-source platform used to simulate and plan motion of many robots. The software allows seamless creation and interface of many plugins. The software was developed by Rosen Diankov at CMU.

During the course of this project using a PUMA 560 robot, forward and inverse kinematics was studied. For various input angles the position and orientation of the gripper was calculated. Using this position and orientation and the decision equations the original configuration was re-calculated. The error is studied.

Forward Kinematics:

Notation:

$\theta[i-1]$, $d[i-1]$, $\alpha[i-1]$ and $a[i]$ are the joint parameters corresponding to the joint i . This notation was followed for the ease of programming (The array index begins from 0)

In order to obtain the orientation and position of a link with respect to another link, HTM matrices were used.

By applying chain rule the position and orientation of gripper was obtained.

$${}^{(i-1)}A(i) = \begin{bmatrix} \text{float}(\cos(\theta)) & -\text{float}(\cos(\alpha))\text{float}(\sin(\theta)) & \text{float}(\sin(\alpha))\text{float}(\sin(\theta)) & a\text{float}(\cos(\theta)) \\ \text{float}(\sin(\theta)) & \text{float}(\cos(\alpha))\text{float}(\cos(\theta)) & -\text{float}(\sin(\alpha))\text{float}(\cos(\theta)) & a\text{float}(\sin(\theta)) \\ 0 & \text{float}(\sin(\alpha)) & \text{float}(\cos(\alpha)) & d \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$${}^0A1 = \begin{bmatrix} \text{float}(\cos(\theta[0])), & -\text{float}(\cos(\alpha[0]))\text{float}(\sin(\theta[0])), & \text{float}(\sin(\alpha[0]))\text{float}(\sin(\theta[0])), & \text{float}(a[0])\text{float}(\cos(\theta[0])), \\ \text{float}(\sin(\theta[0])), & \text{float}(\cos(\alpha[0]))\text{float}(\cos(\theta[0])), & -\text{float}(\sin(\alpha[0]))\text{float}(\cos(\theta[0])), & \text{float}(a[0])\text{float}(\sin(\theta[0])), \\ 0, & \text{float}(\sin(\alpha[0])), & \text{float}(\cos(\alpha[0])), & \text{float}(d[0]), \\ 0, & 0, & 0, & 1 \end{bmatrix}$$

$${}^1A2 = \begin{bmatrix} \text{float}(\cos(\theta[1])), & -\text{float}(\cos(\alpha[1]))\text{float}(\sin(\theta[1])), & \text{float}(\sin(\alpha[1]))\text{float}(\sin(\theta[1])), & \text{float}(a[1])\text{float}(\cos(\theta[1])), \\ \text{float}(\sin(\theta[1])), & \text{float}(\cos(\alpha[1]))\text{float}(\cos(\theta[1])), & -\text{float}(\sin(\alpha[1]))\text{float}(\cos(\theta[1])), & \text{float}(a[1])\text{float}(\sin(\theta[1])), \\ 0, & \text{float}(\sin(\alpha[1])), & \text{float}(\cos(\alpha[1])), & \text{float}(d[1]), \\ 0, & 0, & 0, & 1 \end{bmatrix}$$

$${}^2A3 = \begin{bmatrix} \text{float}(\cos(\theta[2])), & -\text{float}(\cos(\alpha[2]))\text{float}(\sin(\theta[2])), & \text{float}(\sin(\alpha[2]))\text{float}(\sin(\theta[2])), & \text{float}(a[2])\text{float}(\cos(\theta[2])), \\ \text{float}(\sin(\theta[2])), & \text{float}(\cos(\alpha[2]))\text{float}(\cos(\theta[2])), & -\text{float}(\sin(\alpha[2]))\text{float}(\cos(\theta[2])), & \text{float}(a[2])\text{float}(\sin(\theta[2])), \\ 0, & \text{float}(\sin(\alpha[2])), & \text{float}(\cos(\alpha[2])), & \text{float}(d[2]), \\ 0, & 0, & 0, & 1 \end{bmatrix}$$

```

3A4=
[float(cos(theta[3])),      -float(cos(alpha[3]))*float(sin(theta[3])),      float(sin(alpha[3]))*float(sin(theta[3])),
      float(a[3])*float(cos(theta[3])),
float(sin(theta[3])),      float(cos(alpha[3]))*float(cos(theta[3])),      -float(sin(alpha[3]))*float(cos(theta[3])),
      float(a[3])*float(sin(theta[3])),
0,      float(sin(alpha[4])),      float(cos(alpha[4])),      float(d[4]),
0,      0,      0,      1      ]

```

```

4A5=
[float(cos(theta[4])),      -float(cos(alpha[4]))*float(sin(theta[4])),      float(sin(alpha[4]))*float(sin(theta[4])),
      float(a[4])*float(cos(theta[4])),
float(sin(theta[4])),      float(cos(alpha[4]))*float(cos(theta[4])),      -float(sin(alpha[4]))*float(cos(theta[4])),
      float(a[4])*float(sin(theta[4])),
0,      float(sin(alpha[4])),      float(cos(alpha[4])),      float(d[4]),
0,      0,      0,      1      ]

```

```

5A6=
[float(cos(theta[5])),      -float(cos(alpha[5]))*float(sin(theta[5])),      float(sin(alpha[5]))*float(sin(theta[5])),
      float(a[5])*float(cos(theta[5])),
float(sin(theta[5])),      float(cos(alpha[5]))*float(cos(theta[5])),      -float(sin(alpha[5]))*float(cos(theta[5])),
      float(a[5])*float(sin(theta[5])),
0,      float(sin(alpha[5])),      float(cos(alpha[5])),      float(d[5]),
0,      0,      0,      1      ]

```

Multiplying the matrices gives the position of the gripper.

```

A_02=matrixmult (A_01,A_12)
A_24=matrixmult (A_23,A_34)
A_46=matrixmult (A_45,A_56)
A_04=matrixmult (A_02,A_24)
A_06=matrixmult (A_04,A_46)

```

Here matrixmult is a function that multiplies the matrices.

In order to get the configuration the following equations were used:

$$\text{arm_calc} = (-d[3] * \sin(\theta[1] + \theta[2]) - a[2] * \cos(\theta[1] + \theta[2]) - a[1] * \cos(\theta[1]))$$

if arm_calc >= 0:

ARM = 1

else:

ARM = -1

$$\text{elbow_calc} = d[3] * \cos(\theta[2]) - a[2] * \sin(\theta[2])$$

if elbow_calc >= 0:

ELBOW = ARM

else:

ELBOW = -ARM

$$\text{wrist_calc_s} = s[0] * z4[0] + s[1] * z4[1] + s[2] * z4[2]$$
$$\text{wrist_calc_n} = n[0] * z4[0] + n[1] * z4[1] + n[2] * z4[2]$$

if wrist_calc_s > 0:

WRIST = 1

if wrist_calc_s < 0:

WRIST = -1

if wrist_calc_s == 0:

if wrist_calc_n >= 0:

WRIST = 1

else:

WRIST = -1

Inverse Kinematics:

Given the end effector position and orientation, obtaining the robot configuration is required quite many a times.

In order to do so we use three methods:

1. Circle Equation:

In the circle equation to solve $a \cdot \sin(x) + b \cdot \cos(x) = c$

We use

$$r = \sqrt{a^2 + b^2}$$

and let $a/r = \cos(y)$ and $b/r = \sin(y)$

Dividing both sides by r gives

$$\sin(x+y) = c/r$$

$$\text{or } x = \arcsin(c/r) - y$$

Thus we obtain the required angles.

Obtained solution for PUMA 560 robot:

All possible solutions:

$$\text{calculated_thetaA}[0] = 180/\pi * (\text{atan2}(py, px) - \text{atan2}(d[1], \sqrt{px*px + py*py - d[1]*d[1]}))$$

$$\text{calculated_thetaB}[0] = 180/\pi * (\text{atan2}(py, px) - \text{atan2}(d[1], -\sqrt{px*px + py*py - d[1]*d[1]}))$$

$$g_{214} = \cos(\text{theta}[0]) * px + \sin(\text{theta}[0]) * py$$

$$g_{224} = -pz$$

$$d_const = g_{214} * g_{214} + g_{224} * g_{224} - d[3] * d[3] - a[2] * a[2] - a[1] * a[1]$$

$$e_const_square = 4 * a[1] * a[1] * a[2] * a[2] + 4 * a[1] * a[1] * d[3] * d[3]$$

$$\text{calculated_thetaA}[2] = 180/\pi * (\text{atan2}(d_const, \sqrt{e_const_square - d_const * d_const}) - \text{atan2}(a[2], d[3]))$$

$$\text{calculated_thetaB}[2] = 180/\pi * (\text{atan2}(d_const, -\sqrt{e_const_square - d_const * d_const}) - \text{atan2}(a[2], d[3]))$$

$$f = g_{214} - a[1] * \cos(\text{theta}[2])$$

$$p_{xx} = -(d[3] * \cos(\text{theta}[2]) - a[2] * \sin(\text{theta}[2]))$$

$$p_{yy} = d[3] * \sin(\text{theta}[2]) + a[2] * \cos(\text{theta}[2]) + a[1]$$

$$\text{rad} = g_{214}$$

```
calculated_thetaA[1]=180/pi*(atan2(pyy,pxx) -atan2(rad,sqrt((pxx*pxx + pyy*pyy)-rad*rad)) )  
calculated_thetaB[1]=180/pi*(atan2(pyy,pxx) -atan2(rad,-sqrt((pxx*pxx + pyy*pyy)-rad*rad)) )
```

```
calculated_thetaA[3]= 180/pi*atan2( -sin(theta[0])*ax + cos(theta[0])*ay ,  
cos(theta[1]+theta[2])*(cos(theta[0])*ax +sin(theta[0])*ay) - az*(sin(theta[1]+theta[2])) )  
calculated_thetaB[3]= 180 + 180/pi*atan2( -sin(theta[0])*ax + cos(theta[0])*ay ,  
cos(theta[1]+theta[2])*(cos(theta[0])*ax +sin(theta[0])*ay) - az*(sin(theta[1]+theta[2])) )
```

```
calculated_thetaA[4]=180/pi*atan2(  
cos(theta[3])*(cos(theta[1]+theta[2])*(cos(theta[0])*ax+sin(theta[0])*ay)-  
sin(theta[1]+theta[2])*az)+sin(theta[3])*(-sin(theta[0])*ax +cos(theta[0])*ay) ,  
sin(theta[1]+theta[2])*(cos(theta[0])*ax + sin(theta[0])*ay) +az*cos(theta[1]+theta[2])) )
```

```
calculated_thetaA[5]=180/pi*atan2(-  
sin(theta[3])*(cos(theta[1]+theta[2])*(cos(theta[0])*nx+sin(theta[0])*ny) -  
sin(theta[1]+theta[2])*nz) + cos(theta[3])*(-sin(theta[0])*nx + cos(theta[0])*ny) , -  
sin(theta[3])*(cos(theta[1]+theta[2])*(cos(theta[0])*sx+sin(theta[0])*sy) -  
sin(theta[1]+theta[2])*sz) + cos(theta[3])*(-sin(theta[0])*sx + cos(theta[0])*sy) )
```

The actual solution:

```
if ARM==1:
```

```
    theta[0] = calculated_thetaB[0]  
    theta[1] = calculated_thetaB[1]
```

```
else:
```

```
    theta[0]=calculated_thetaA[0]  
    theta[1]=calculated_thetaA[1]
```

```
if ARM*ELBOW==1:
```

```
    theta[2]=calculated_thetaA[2]
```

```
else:
```

```
    theta[2]=calculated_thetaB[2]
```

```
theta[3]=calculated_thetaA[3]
```

```
theta[4]=calculated_thetaA[4]
```

```
theta[5]=calculated_thetaA[5]
```

2. Using half angle method:

In this method to solve equation of the type $a \cdot \sin(x) + b \cdot \cos(x) = c$

we let

$$u = \tan(\theta/2)$$

$$\text{then } \sin(\theta) = 2u / (1 + u^2)$$

$$\text{and } \cos(\theta) = (1 - u^2) / (1 + u^2)$$

Finally we get a quadratic in u and the solution gives us $\tan(\theta/2)$.

Taking inverse gives us θ .

All Possible Solutions:

$$\text{calculated_theta_halfA}[0] = 180/\pi * 2 * \text{atan2}(-px + \sqrt{px*px+py*py-d[1]*d[1]}, d[1]+py)$$

$$\text{calculated_theta_halfB}[0] = 180/\pi * 2 * \text{atan2}(-px - \sqrt{px*px+py*py-d[1]*d[1]}, d[1]+py)$$

$$g_{214} = \cos(\theta[0]) * px + \sin(\theta[0]) * py$$

$$g_{224} = -pz$$

$$d_const = g_{214} * g_{214} + g_{224} * g_{224} - d[3] * d[3] - a[2] * a[2] - a[1] * a[1]$$

$$e_const_square = 4 * a[1] * a[1] * a[2] * a[2] + 4 * a[1] * a[1] * d[3] * d[3]$$

$$\text{calculated_theta_halfA}[2] = 180/\pi * 2 * \text{atan2}(2 * a[1] * d[3] + \sqrt{e_const_square - d_const * d_const}, d_const + 2 * a[1] * a[2])$$

$$\text{calculated_theta_halfB}[2] = 180/\pi * 2 * \text{atan2}(2 * a[1] * d[3] - \sqrt{e_const_square - d_const * d_const}, d_const + 2 * a[1] * a[2])$$

$$f = g_{214} - a[1] * \cos(\theta[2])$$

$$p_{xx} = -(d[3] * \cos(\theta[2]) - a[2] * \sin(\theta[2]))$$

$$p_{yy} = d[3] * \sin(\theta[2]) + a[2] * \cos(\theta[2]) + a[1]$$

$$rad = g_{214}$$

$$\text{calculated_theta_halfA}[1] = 180/\pi * 2 * (\text{atan2}(-p_{xx} + \sqrt{p_{xx} * p_{xx} + p_{yy} * p_{yy} - rad * rad}), rad + p_{yy})$$

$$\text{calculated_theta_halfB}[1] = 180/\pi * 2 * (\text{atan2}(-p_{xx} - \sqrt{p_{xx} * p_{xx} + p_{yy} * p_{yy} - rad * rad}), rad + p_{yy})$$

$$\text{calculated_theta_halfA}[3] = 180/\pi * \text{atan2}(-\sin(\theta[0]) * ax + \cos(\theta[0]) * ay, \cos(\theta[1] + \theta[2]) * (\cos(\theta[0]) * ax + \sin(\theta[0]) * ay) - az * (\sin(\theta[1] + \theta[2])))$$

$$\text{calculated_theta_halfB}[3] = 180 + 180/\pi * \text{atan2}(-\sin(\theta[0]) * ax + \cos(\theta[0]) * ay, \cos(\theta[1] + \theta[2]) * (\cos(\theta[0]) * ax + \sin(\theta[0]) * ay) - az * (\sin(\theta[1] + \theta[2])))$$

```

calculated_theta_halfA[4]=180/pi*atan2(
cos(theta[3])*(cos(theta[1]+theta[2])*(cos(theta[0])*ax+sin(theta[0])*ay)-
sin(theta[1]+theta[2])*az)+sin(theta[3])*(-sin(theta[0])*ax +cos(theta[0])*ay) ,
sin(theta[1]+theta[2])*(cos(theta[0])*ax + sin(theta[0])*ay) +az*cos(theta[1]+theta[2]) )

```

```

calculated_theta_halfA[5]=180/pi*atan2(-
sin(theta[3])*(cos(theta[1]+theta[2])*(cos(theta[0])*nx+sin(theta[0])*ny) -
sin(theta[1]+theta[2])*nz) + cos(theta[3])*(-sin(theta[0])*nx + cos(theta[0])*ny) , -
sin(theta[3])*(cos(theta[1]+theta[2])*(cos(theta[0])*sx+sin(theta[0])*sy) -
sin(theta[1]+theta[2])*sz) + cos(theta[3])*(-sin(theta[0])*sx + cos(theta[0])*sy) )

```

The actual solution is:

```

if ARM==1:

```

```

    theta[0]=calculated_theta_halfB[0]

```

```

    theta[1]=calculated_theta_halfB[1]

```

```

else:

```

```

    theta[0]=calculated_theta_halfA[0]

```

```

    theta[1]=calculated_theta_halfA[1]

```

```

if ARM*ELBOW==1:

```

```

    theta[2]=calculated_theta_halfB[2]

```

```

else:

```

```

    theta[2]=calculated_theta_halfA[2]

```

```

theta[3]=calculated_theta_halfA[3]

```

```

theta[4]=calculated_theta_halfA[4]

```

```

theta[5]=calculated_theta_halfA[5]

```

3. Using geometric method:

In this method the geometric structure of the robot is used to calculate the configuration.

```

p=[A_04[0][3], A_04[1][3], A_04[2][3]]

```

```

px=p[0]

```

```

py=p[1]

```

```

pz=p[2]

```

```

temp=sqrt(px*px+py*py-d[1]*d[1])

```

```

geometry_calculated_theta[0] = 180/pi*atan2( (-ARM*py*temp-px*d[1])/(px*px+py*py) , (-
ARM*px*temp+py*d[1])/(px*px+py*py) )

```


$R = \sqrt{p_x^2 + p_y^2 + p_z^2 - d[1] \cdot d[1]}$

$r = \sqrt{p_x^2 + p_y^2 - d[1] \cdot d[1]}$

$\sin_alpha = -p_z / R$

$\cos_alpha = -ARM \cdot r / R$

$\cos_beta = (a[1] \cdot a[1] + R \cdot R - d[3] \cdot d[3] - a[2] \cdot a[2]) / (2 \cdot a[1] \cdot R)$

$\sin_beta = \sqrt{1 - \cos_beta^2}$

$\sin_theta_2 = \sin_alpha \cdot \cos_beta + (ARM \cdot ELBOW) \cdot \cos_alpha \cdot \sin_beta$

$\cos_theta_2 = \cos_alpha \cdot \cos_beta - (ARM \cdot ELBOW) \cdot \sin_alpha \cdot \sin_beta$

$geometry_calculated_theta[1] = 180 / \pi \cdot \text{atan2}(\sin_theta_2, \cos_theta_2)$

$R = \sqrt{p_x^2 + p_y^2 + p_z^2 - d[1] \cdot d[1]}$

$\cos_phi = (a[1] \cdot a[1] + d[3] \cdot d[3] + a[2] \cdot a[2] - R \cdot R) / (2 \cdot a[1] \cdot \sqrt{d[3] \cdot d[3] + a[2] \cdot a[2]})$

$\sin_phi = ARM \cdot ELBOW \cdot \sqrt{1 - \cos_phi^2}$

$\sin_beta = d[3] / (\sqrt{d[3] \cdot d[3] + a[2] \cdot a[2]})$

$\cos_beta = \text{fabs}(a[2]) / (\sqrt{d[3] \cdot d[3] + a[2] \cdot a[2]})$

$\sin_theta_3 = \sin_phi \cdot \cos_beta - \cos_phi \cdot \sin_beta$

$\cos_theta_3 = \cos_phi \cdot \cos_beta + \sin_phi \cdot \sin_beta$

$geometry_calculated_theta[2] = 180 / \pi \cdot \text{atan2}(\sin_theta_3, \cos_theta_3)$ ## theta 4, theta 5 and theta 6

$z3 = [A_03[0][2], A_03[1][2], A_03[2][2]]$

$cross = [z3[1] \cdot approach[2] - approach[1] \cdot z3[2], approach[0] \cdot z3[2] - z3[0] \cdot approach[2], z3[0] \cdot approach[1] - z3[1] \cdot approach[0]]$

$cross_mod = \sqrt{cross[0]^2 + cross[1]^2 + cross[2]^2}$

if $cross_mod == 0$:

$\sigma = 0$

else:

$cross = [cross[0] / cross_mod, cross[1] / cross_mod, cross[2] / cross_mod]$

$s_prod = [s[0] \cdot cross[0] + s[1] \cdot cross[1] + s[2] \cdot cross[2]]$

 if $s_prod == 0$:

$\sigma = [n[0] \cdot cross[0] + n[1] \cdot cross[1] + n[2] \cdot cross[2]]$

 else:

$\sigma = s_prod$

```

if sigma>=0:
    M= WRIST
else:
    M= -WRIST

```

```

temp1= (M* (cos(pi/180*geometry_calculated_theta[0])* approach[1] –
sin(pi/180*geometry_calculated_theta[0])* approach[0] ))

```

```

geometry_calculated_theta[3] = 180/pi*atan2( temp1 ,
M*((cos(pi/180*geometry_calculated_theta[0])*cos(pi/180*geometry_calculated_theta[1]+pi
/180*geometry_calculated_theta[2])*approach[0]) +
(sin(pi/180*geometry_calculated_theta[0])*cos(pi/180*geometry_calculated_theta[1]+pi/180
*geometry_calculated_theta[2])*approach[1]) -
(sin(pi/180*geometry_calculated_theta[1]+pi/180*geometry_calculated_theta[2])*approach[
2])) )

```

```

C1=cos(pi/180*geometry_calculated_theta[0])
S1=sin(pi/180*geometry_calculated_theta[0])
C23=cos(pi/180*geometry_calculated_theta[1] + pi/180*geometry_calculated_theta[2])
S23=sin(pi/180*geometry_calculated_theta[1] + pi/180*geometry_calculated_theta[2])
C4=cos(pi/180*geometry_calculated_theta[3])
S4=sin(pi/180*geometry_calculated_theta[3])

```

```

geometry_calculated_theta[4] = 180/pi*atan2 ( (C1*C23*C4 - S1*S4)*approach[0] +
(S1*C23*C4 + C1*S4)*approach[1] - C4*S23*approach[2] , C1*S23*approach[0] +
S1*S23*approach[1] + C23*approach[2] )

```

```

geometry_calculated_theta[5] = 180/pi*atan2 ((-S1*C4 - C1*C23*S4)*n[0] + (C1*C4 -
S1*C23*S4)*n[1] + (S4*S23)*n[2] , (-S1*C4 - C1*C23*S4)*s[0] + (C1*C4 - S1*C23*S4)*s[1] +
(S4*S23)*s[2] )

```

```

if FLIP==1:
    geometry_calculated_theta[3] = geometry_calculated_theta[3]+pi
    geometry_calculated_theta[4] = - geometry_calculated_theta[4]
    geometry_calculated_theta[5] = geometry_calculated_theta[5]+pi

```

The geometry_calculated_theta is the actual theta