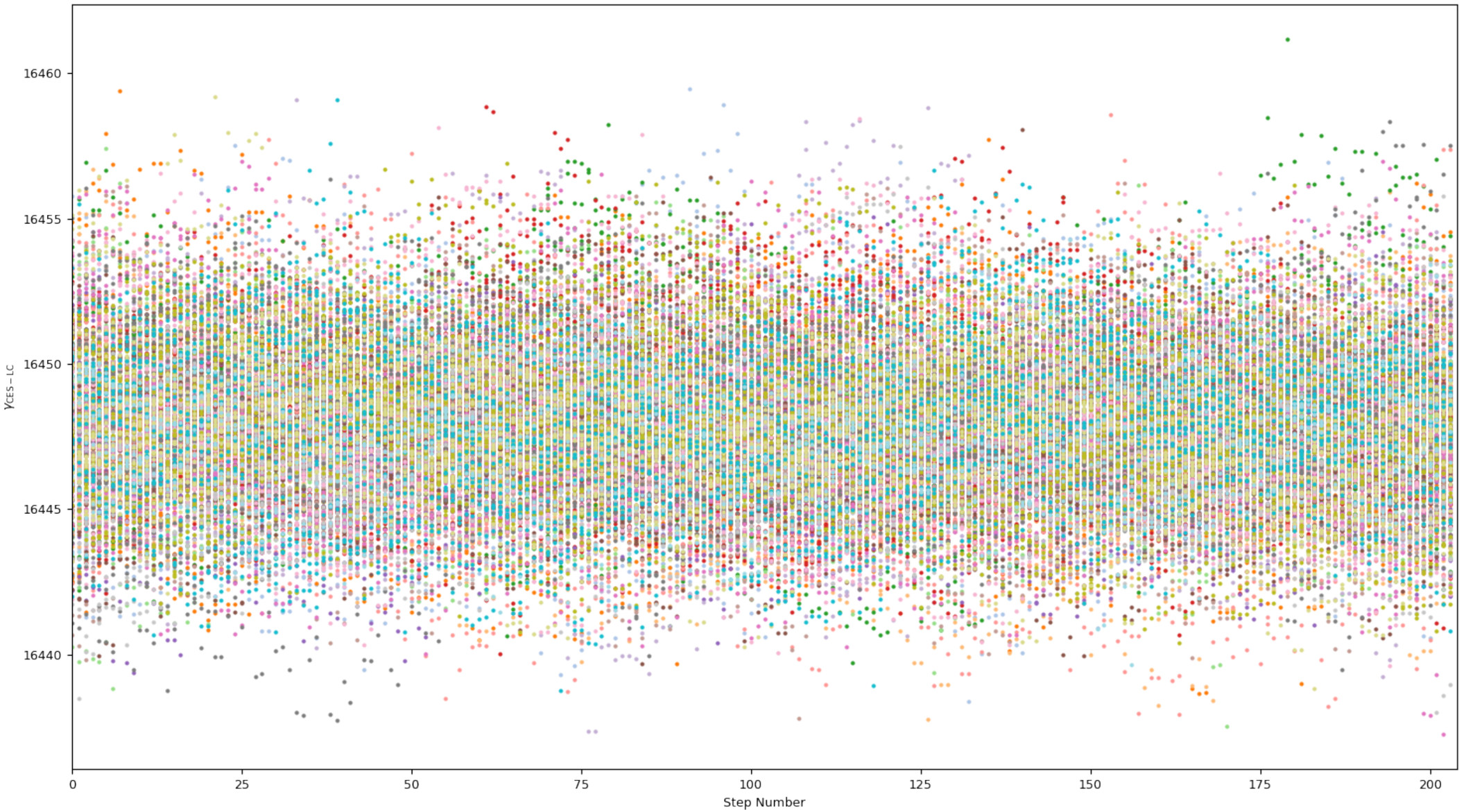
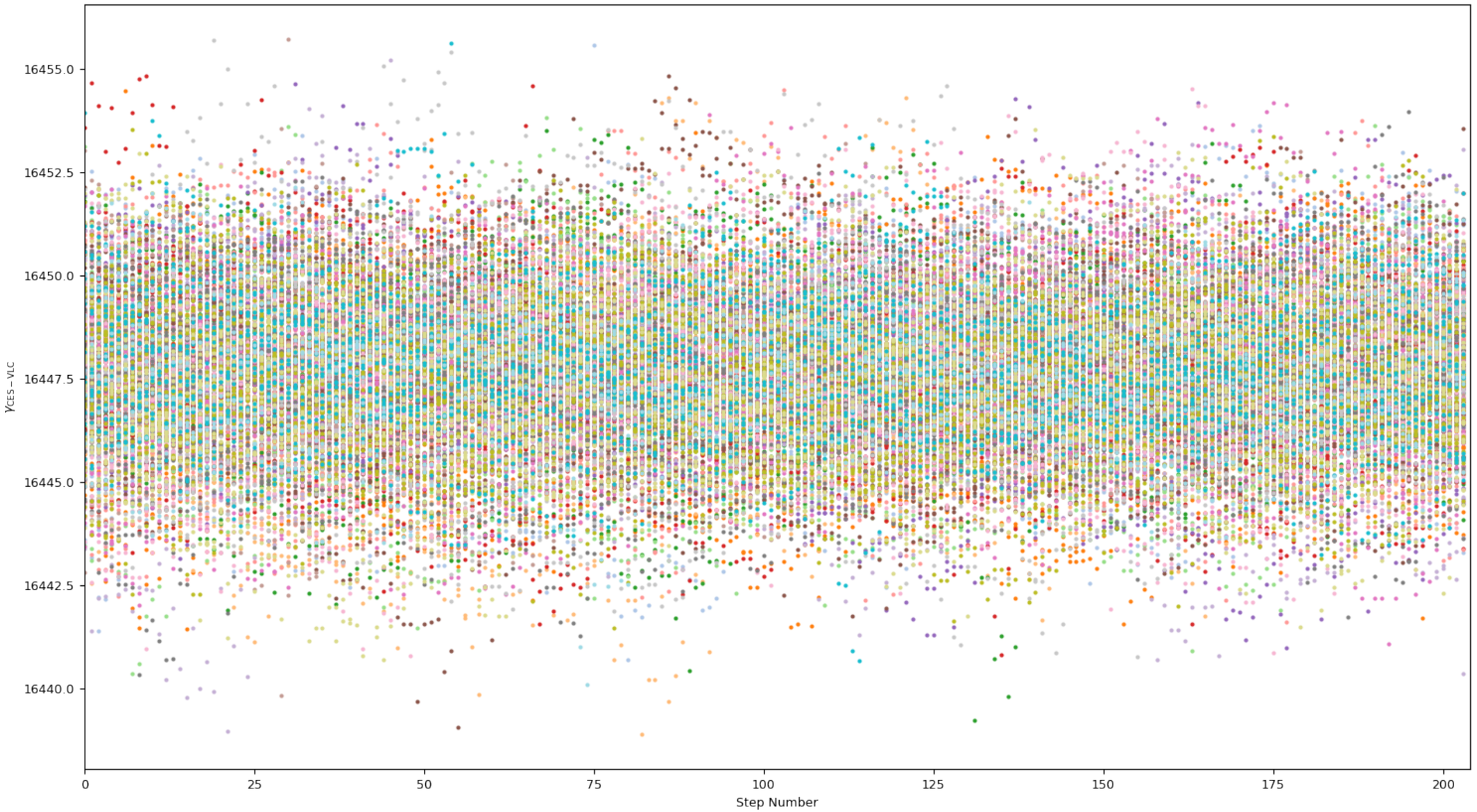
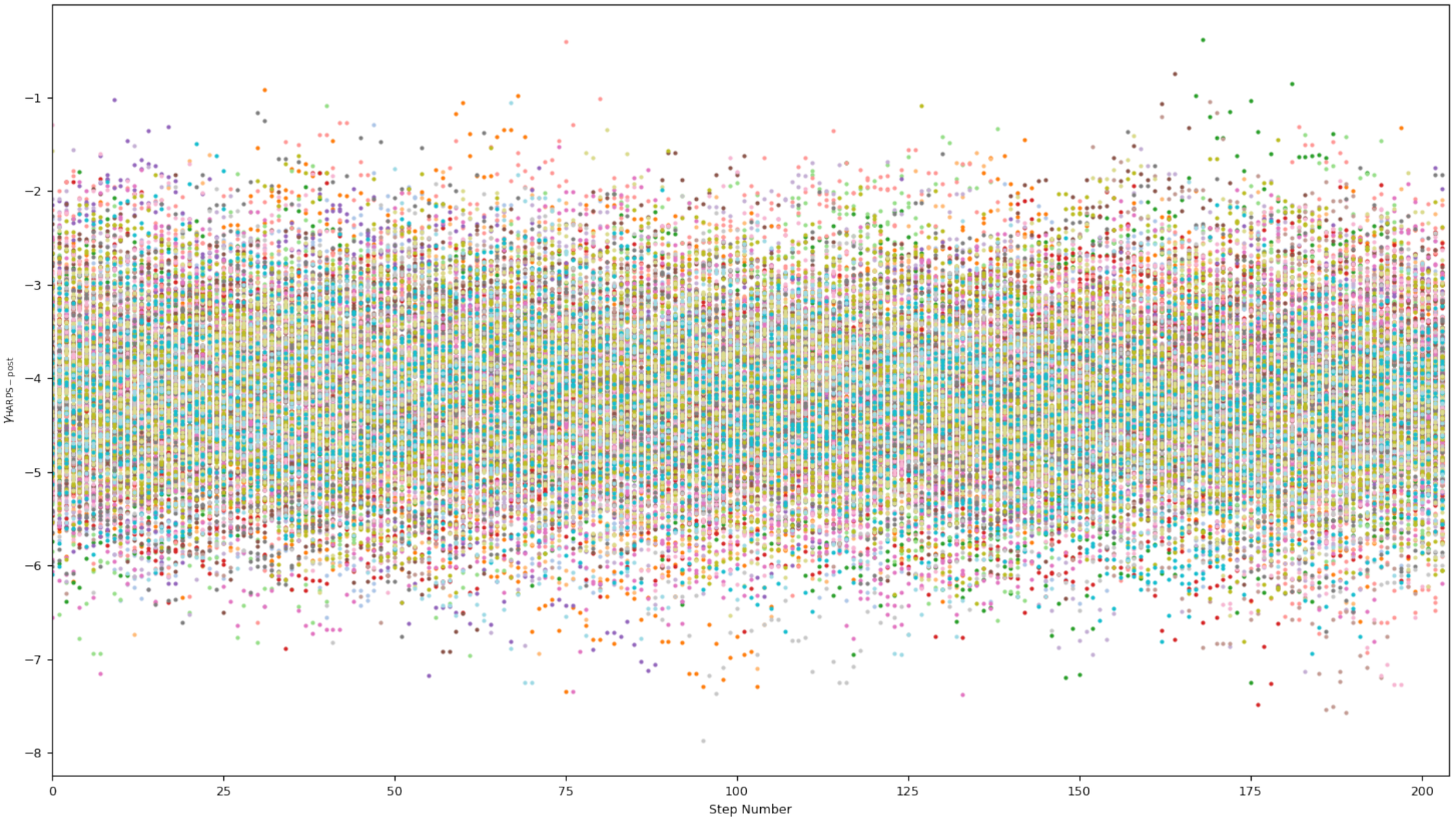
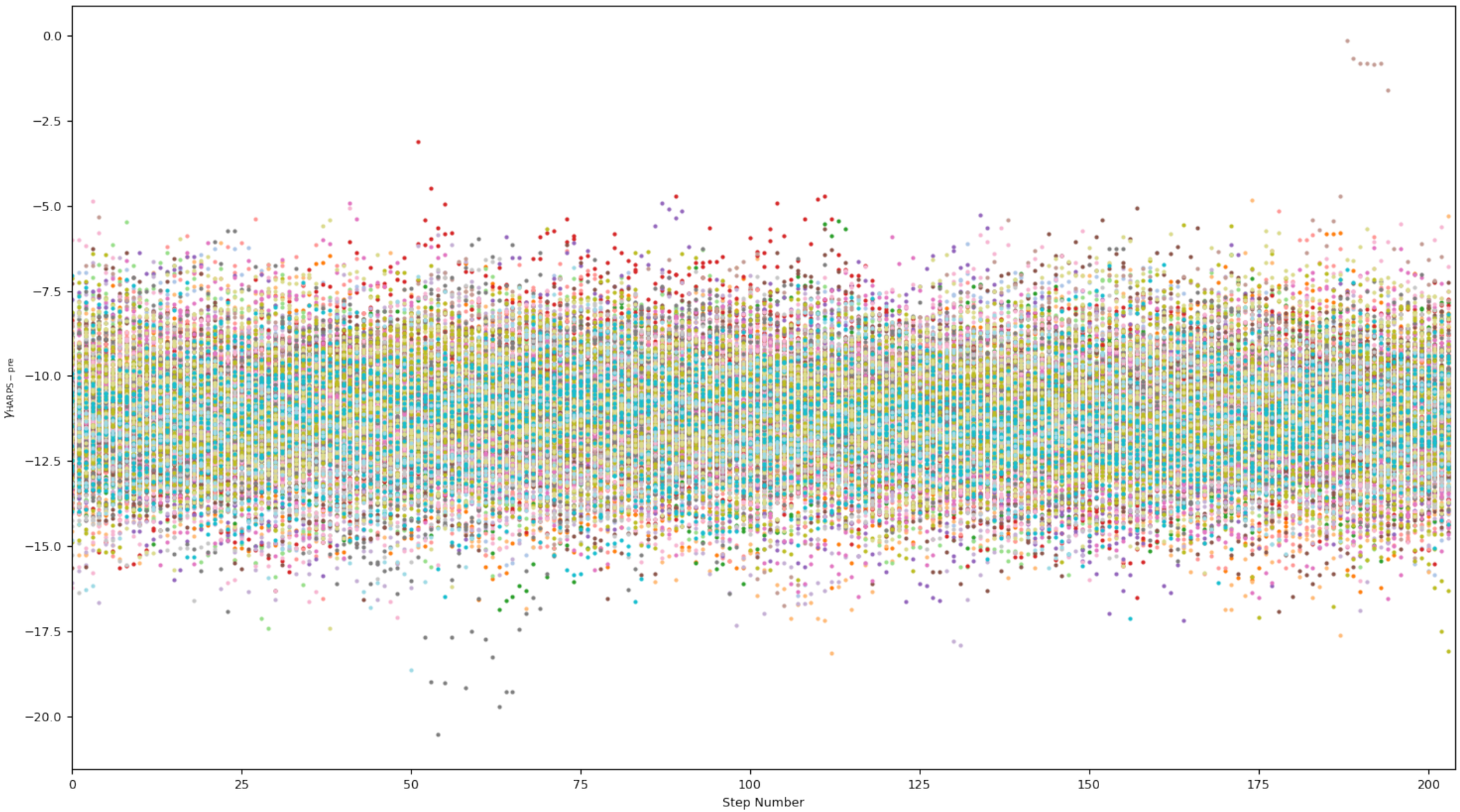
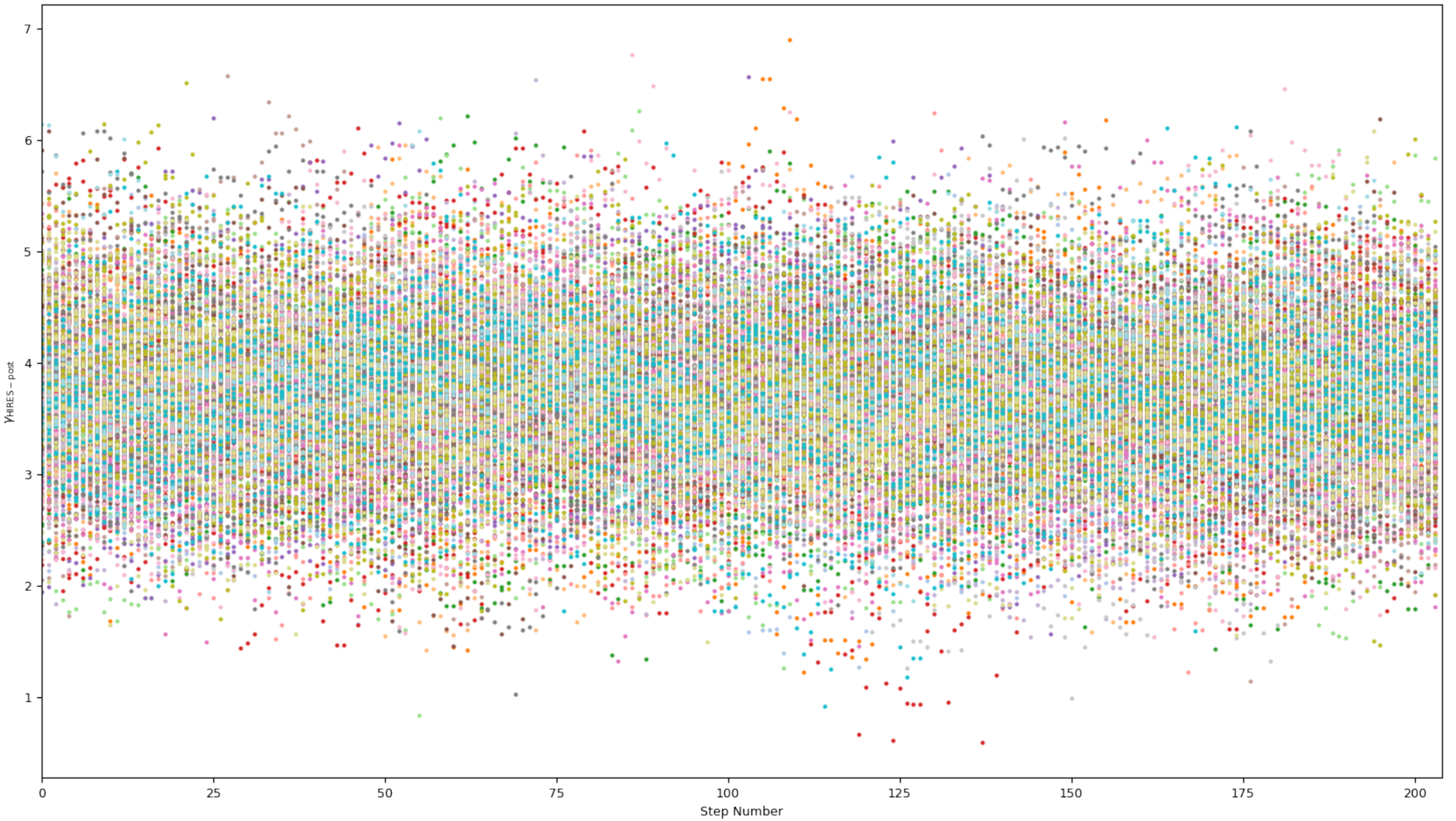

16460
16455
16450
16445
16440
Y_{CES-LC}
0
25
50
75
100
125
150
175
200
Step Number

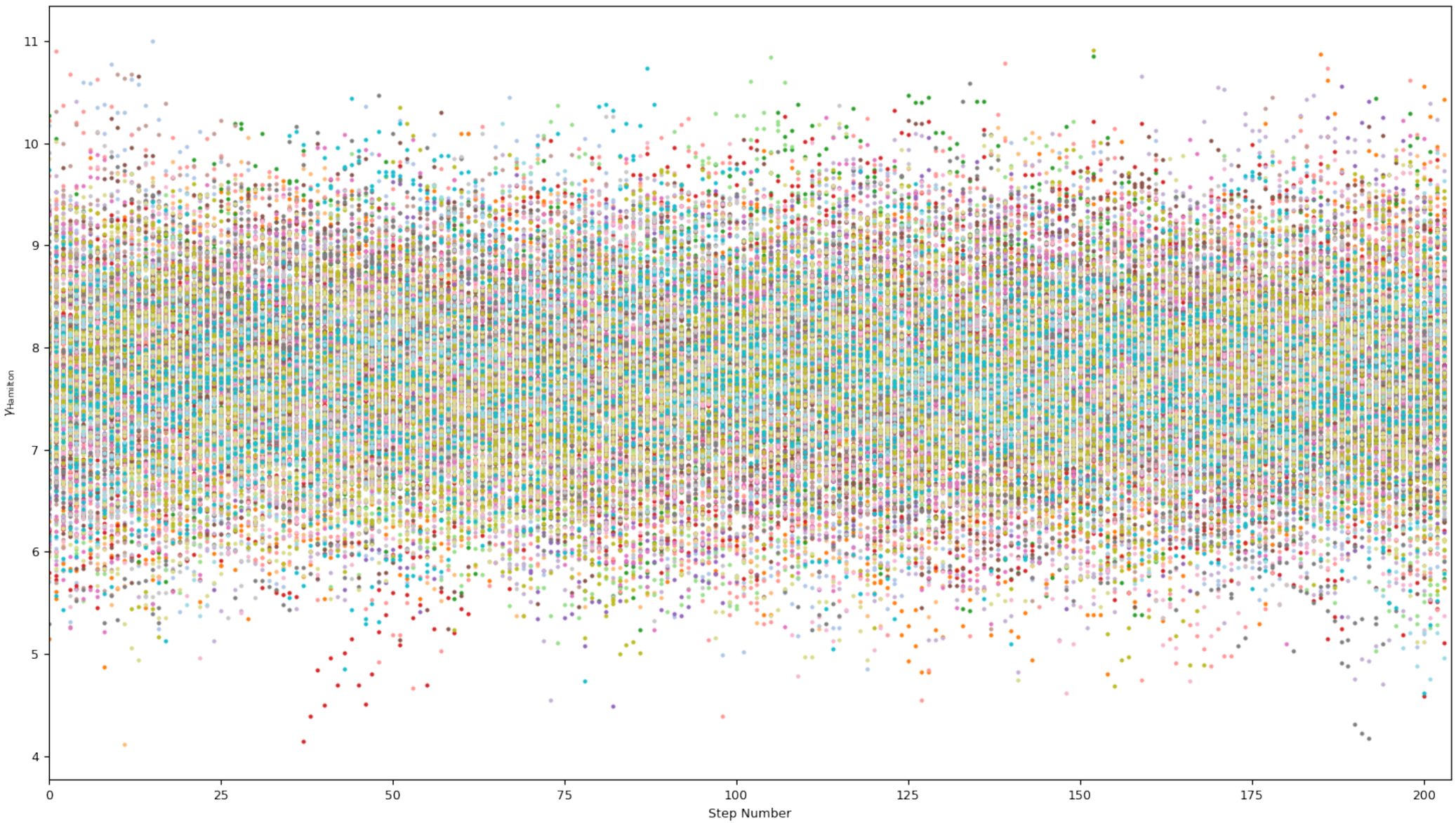

16455.0
16452.5
16450.0
16447.5
16445.0
16442.5
16440.0
$Y_{CES-VLC}$
0
25
50
75
100
125
150
175
200
Step Number

0
−2
−4
−6
−8
−10
y_{EXPRES}
0
25
50
75
100
125
150
175
200
Step Number

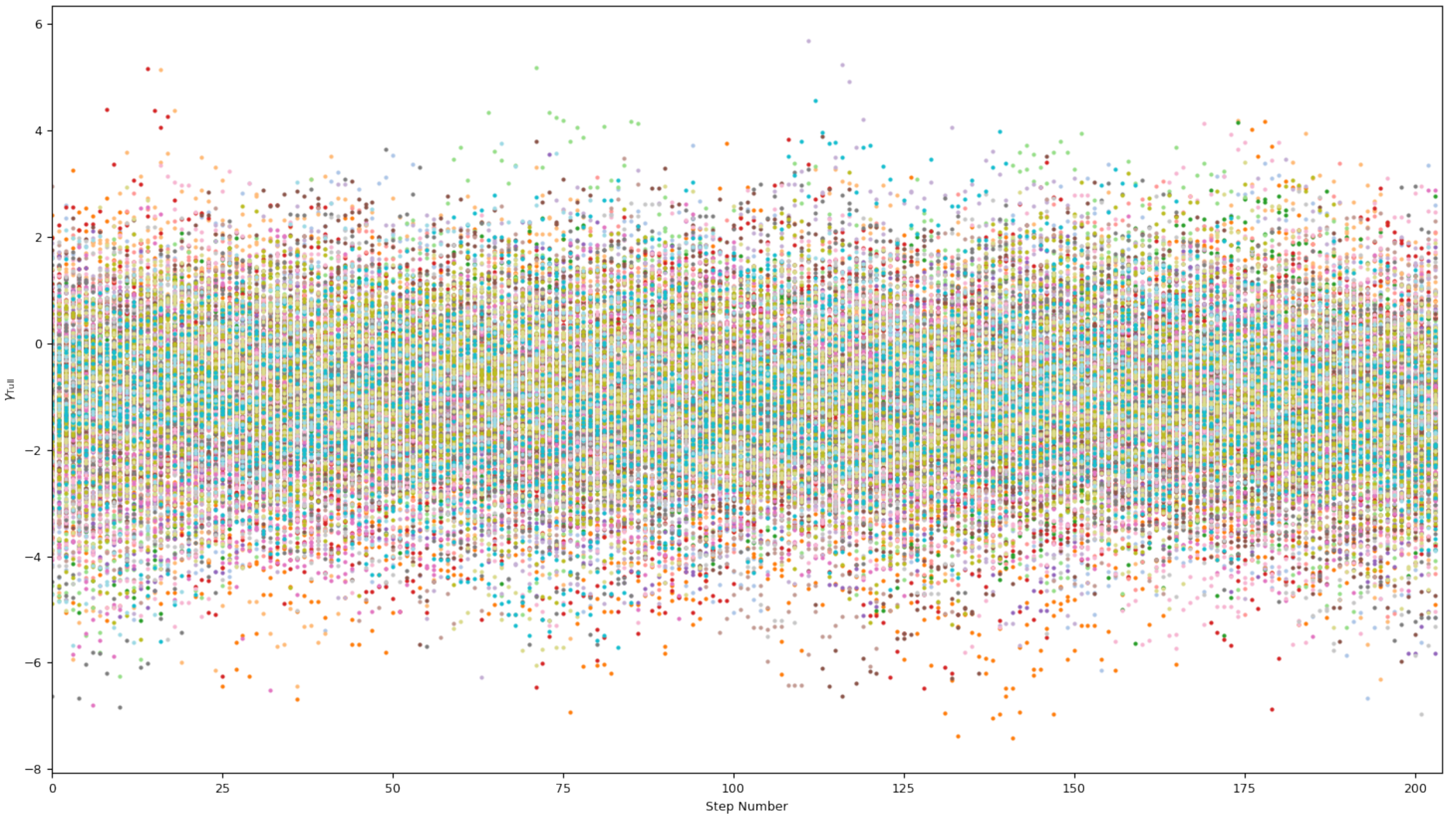

−1
−2
−3
−4
−5
−6
−7
−8
$\gamma_{HARPS-post}$
0
25
50
75
100
125
150
175
200
Step Number


0.0
−2.5
−5.0
−7.5
−10.0
−12.5
−15.0
−17.5
−20.0
$y_{HARPS-pre}$
0
25
50
75
100
125
150
175
200
Step Number

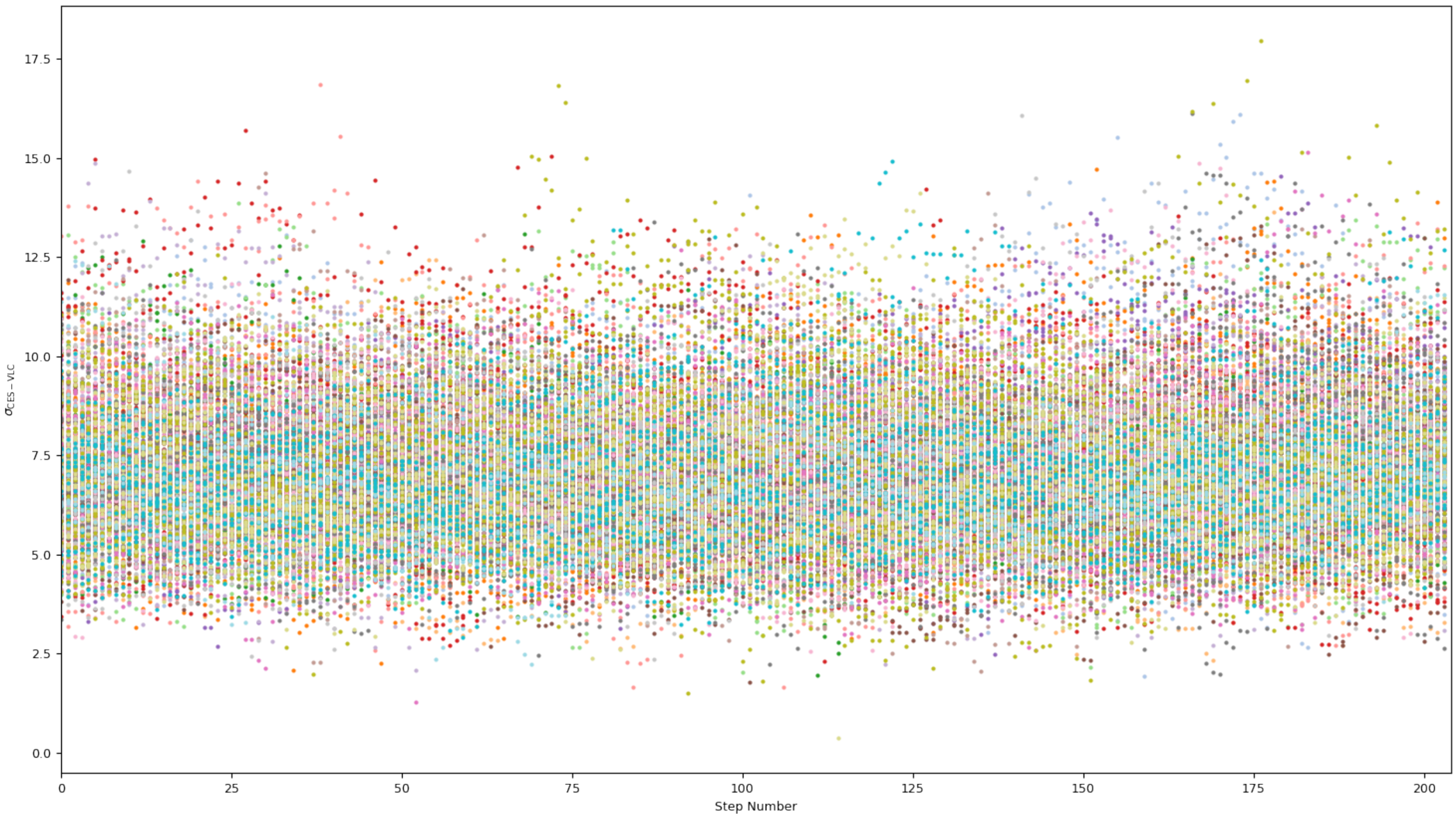

7
6
5
4
3
2
1
$y_{HIRES-post}$
0
25
50
75
100
125
150
175
200
Step Number

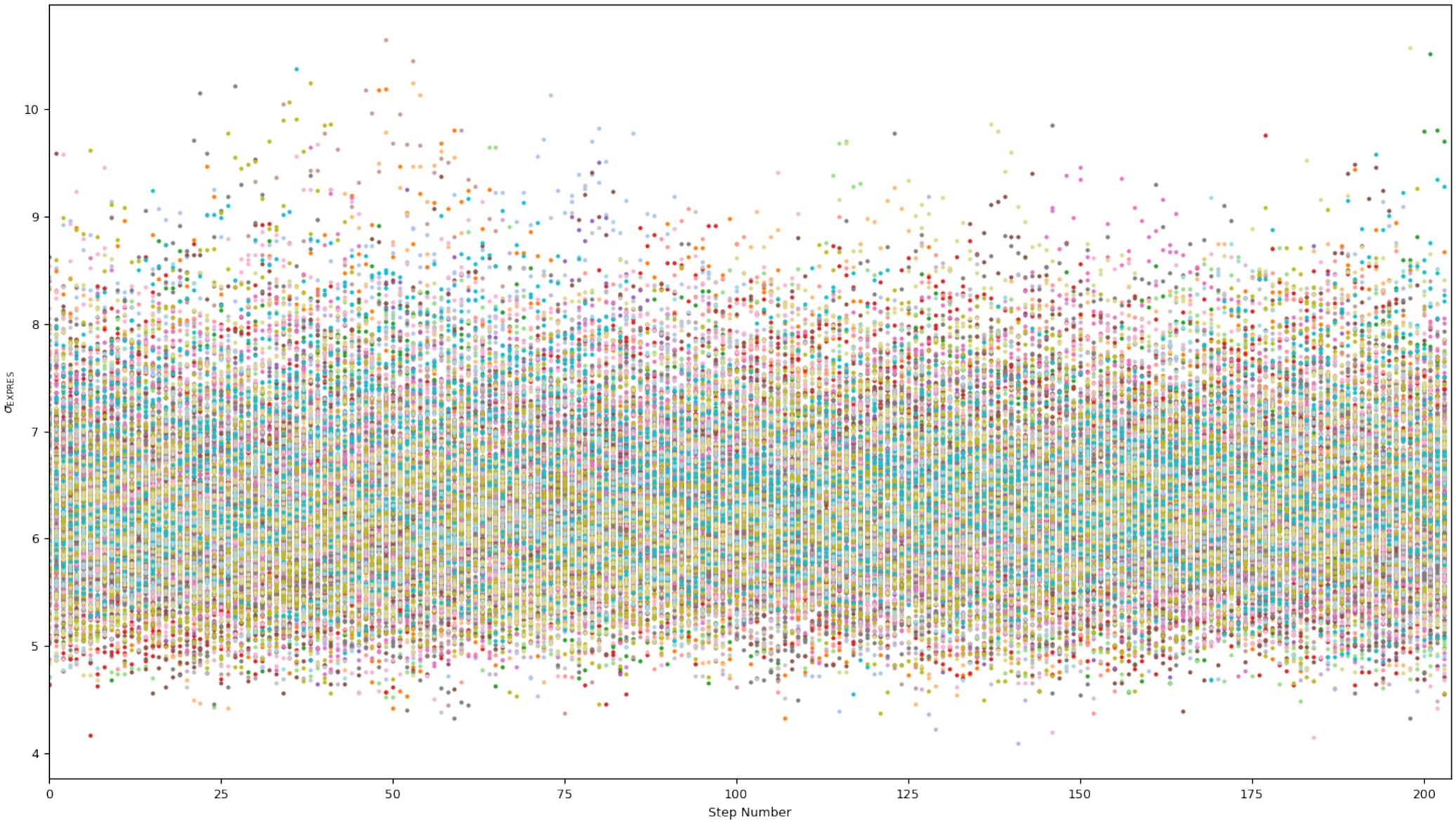

11
10
9
8
7
6
5
4
$Y_{Hamilton}$
0
25
50
75
100
125
150
175
200
Step Number

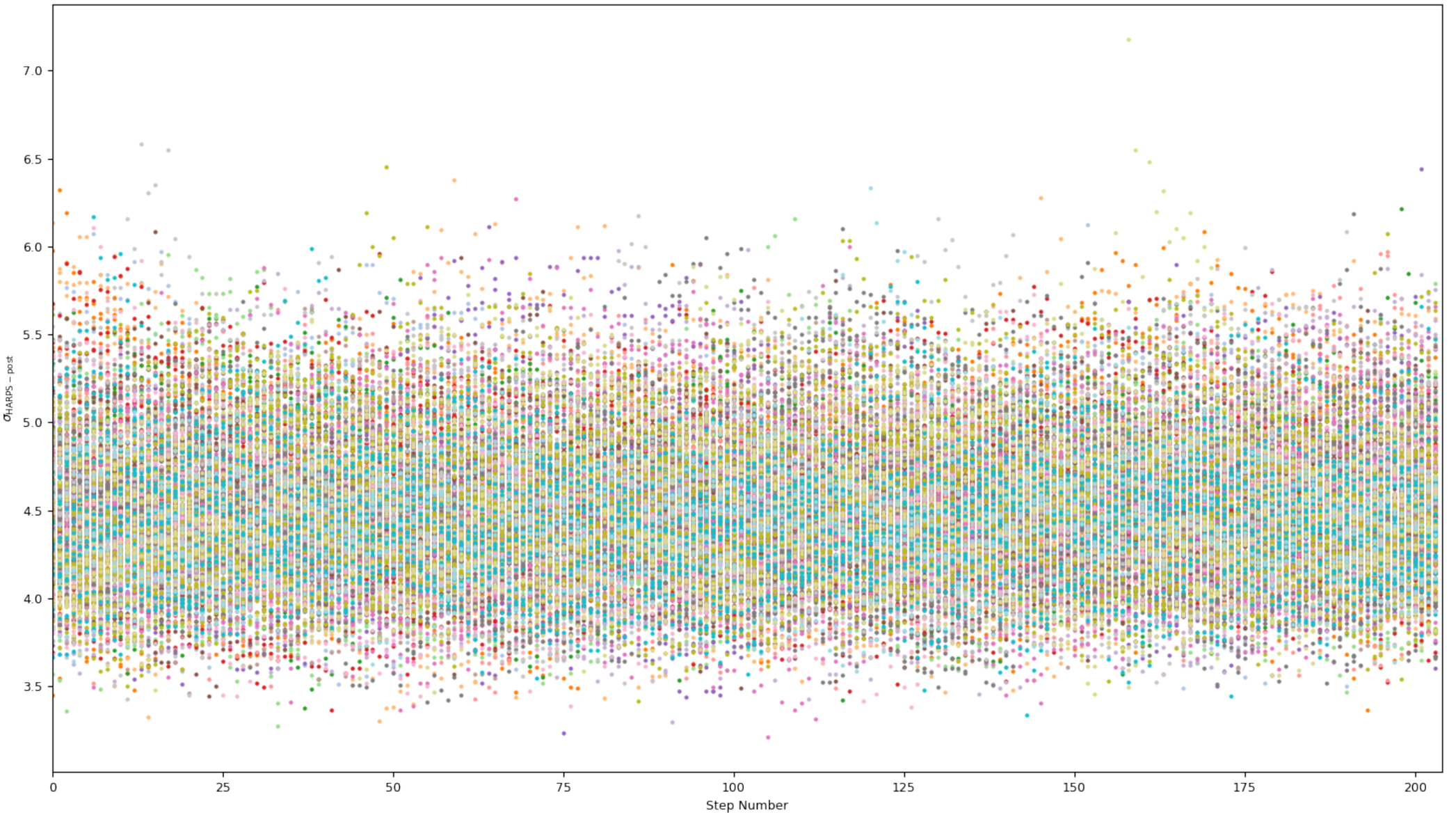
2
1
0
−1
−2
−3
γ_{Levy}
0
25
50
75
100
125
150
175
200
Step Number

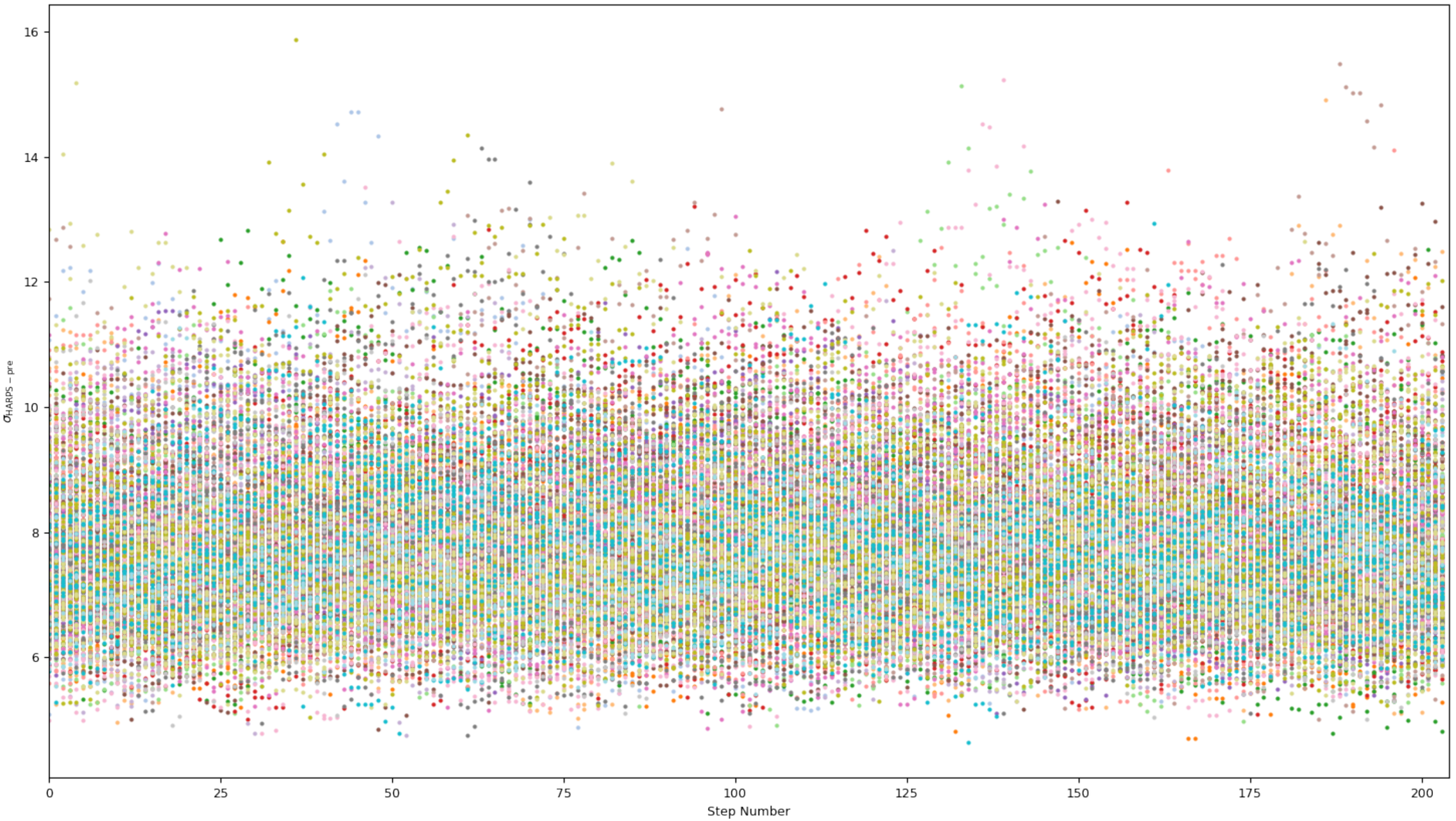

6
4
2
0
−2
−4
−6
−8
y_{Full}
0
25
50
75
100
125
150
175
200
Step Number

25
20
15
10
5
σ_{CES-LC}
0
25
50
75
100
125
150
175
200
Step Number


17.5
15.0
12.5
10.0
7.5
5.0
2.5
0.0
$\sigma_{CES-VLC}$
0
25
50
75
100
125
150
175
200
Step Number


10
9
8
7
6
5
4
σ_{EXPRES}
0
25
50
75
100
125
150
175
200
Step Number


7.0
6.5
6.0
5.5
5.0
4.5
4.0
3.5
$\sigma_{\mathrm{HARPS-post}}$
0
25
50
75
100
125
150
175
200
Step Number


16
14
12
10
8
6
$\sigma_{HARPS-pre}$
0
25
50
75
100
125
150
175
200
Step Number

10
9
8
7
6
$\sigma_{HIRES-post}$
0
25
50
75
100
125
150
175
200
Step Number

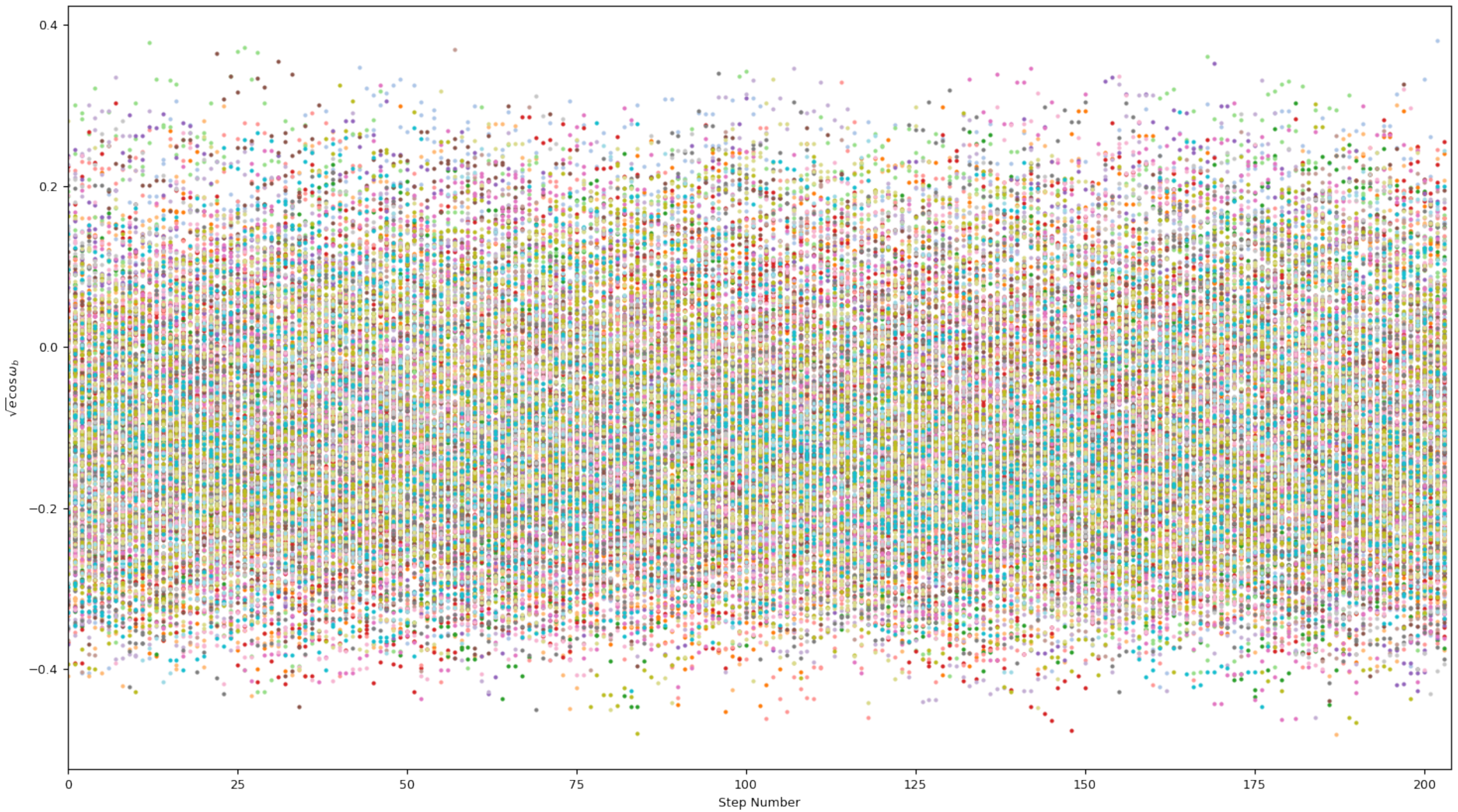
13
12
11
10
9
8
σ_{Hamilton}
0
25
50
75
100
125
150
175
200
Step Number

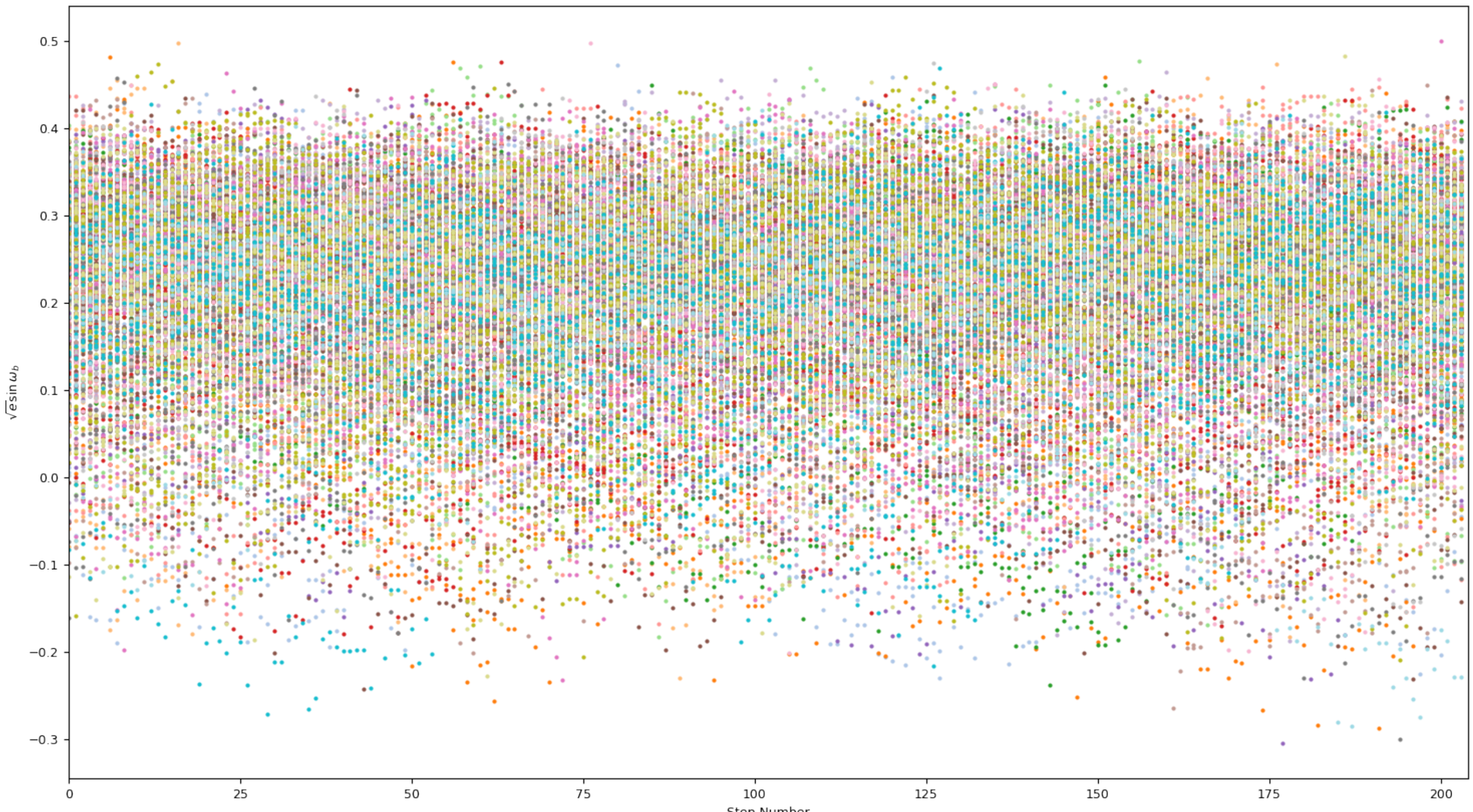
10
9
8
7
6
σ_{Levy}
0
25
50
75
100
125
150
175
200
Step Number

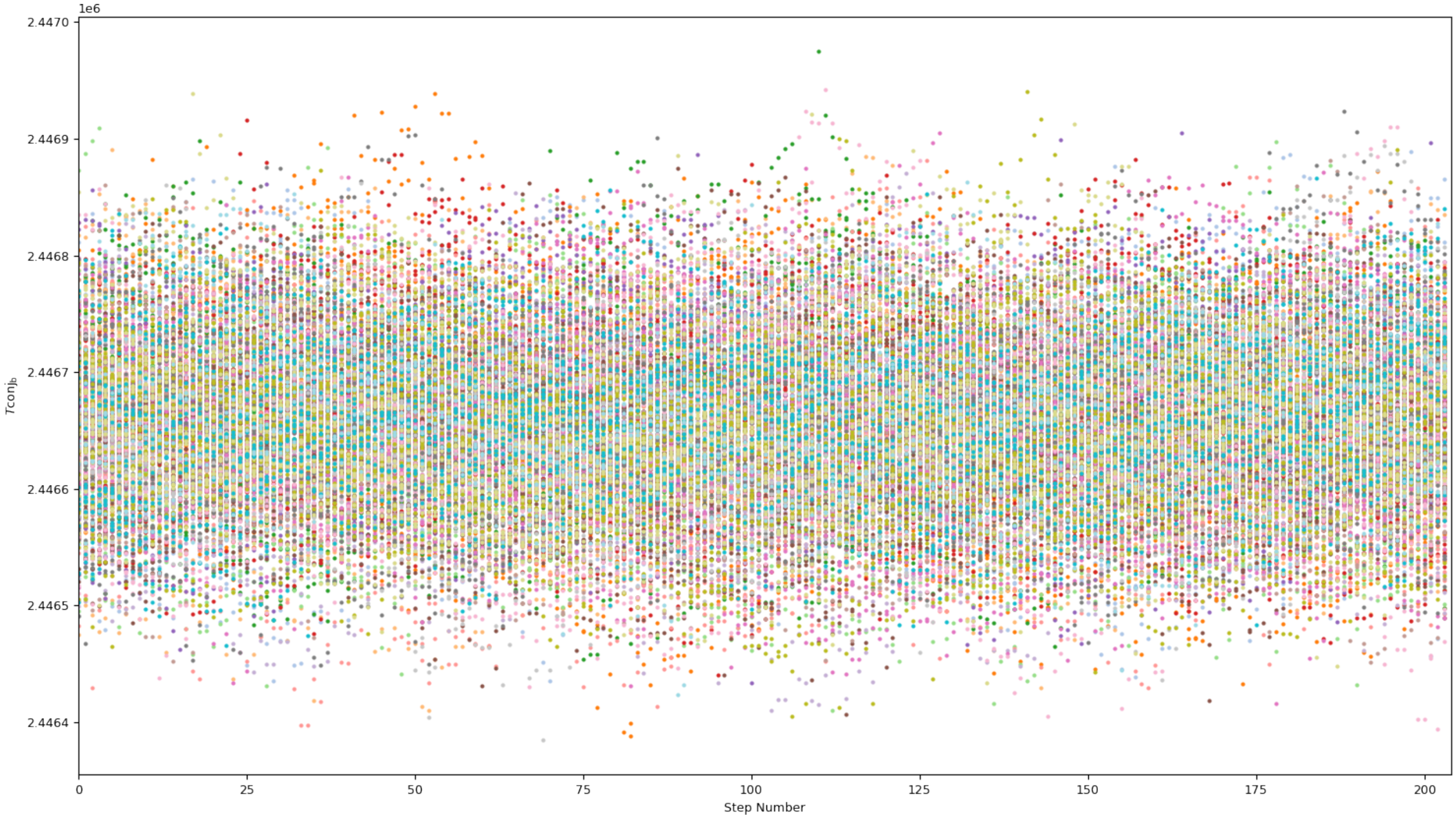
12
10
8
6
4
2
0
σ_{Tull}
0
25
50
75
100
125
150
175
200
Step Number

13
12
11
10
9
K_b
0
25
50
75
100
125
150
175
200
Step Number

2760
2740
2720
2700
2680
2660
2640
2620
P_b
0
25
50
75
100
125
150
175
200
Step Number


0.4
0.2
0.0
−0.2
−0.4
$\sqrt{e}\cos\omega_b$
0
25
50
75
100
125
150
175
200
Step Number


0.5
0.4
0.3
0.2
0.1
0.0
−0.1
−0.2
−0.3
$\sqrt{e}\sin\omega_b$
0
25
50
75
100
125
150
175
200
Step Number


1e6
2.4470
2.4469
2.4468
2.4467
2.4466
2.4465
2.4464
Tconj_b
0
25
50
75
100
125
150
175
200
Step Number