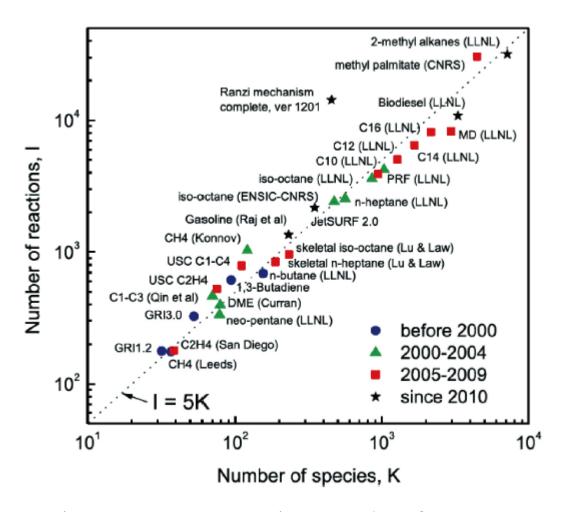
# Topic 6 Chemical mechanisms

Examine ways in which mechanisms are constructed, their dependence on rate and thermodynamic data, their evaluation using experimental targets and the optimization of component rate constants using direct and indirect data

Numbers of species and reactions in mechanisms for combustion of hydrocarbon fuels (Lu and Law, Prog En Comb Sci, 2009, 35, 192, updated Yuan et al, Science China (Chemistry), 2017, 60, 1391)



- Larger mechanisms require thousands of rate constants.
- Can't measure them all calculation essential

#### Hierarchical approach to combustion mechanisms

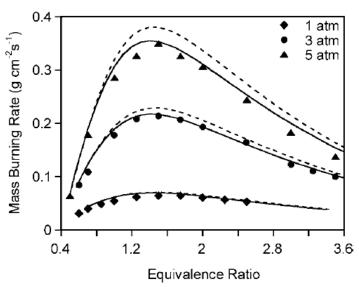
- Westbrook and Dryer, Proc. Comb. Inst. 18 (1981)
   749-766, Prog. Energy Combust. Sci. 10 (1981) 1-57.

   Construction of comprehensive, hierarchical chemical mechanisms.
- Build mechanisms up with increasing complexity  $O_2$  + (i)  $H_2$  (ii)  $CO/H_2O$  (iii)  $CH_4$  .....
- Use evaluated rate data where available

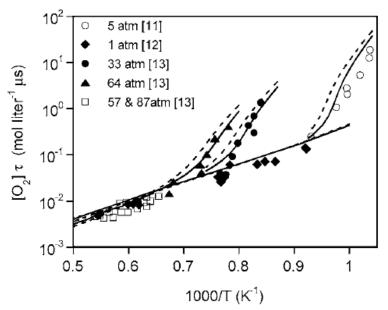
### Examples of $H_2 + O_2$ mechanisms

- Li et al. Int J Chem Kinet 36, (2004) 566-575 based on earlier mechanism by Mueller et al. Updated Burke et al, Int J Chem Kinet 44: 444-474, 2012
- Konnov, Combustion and Flame 152 (2008) 507-528.
   Examination of uncertainties in rate coefficients based on earlier (2004) mechanism
- Hong et al., Comb and Flame, 158, (2011) 633-644
- Keromnes et al Comb and Flame 160 (2013) 995-1011.

#### Testing mechanisms against global observables: Li et al



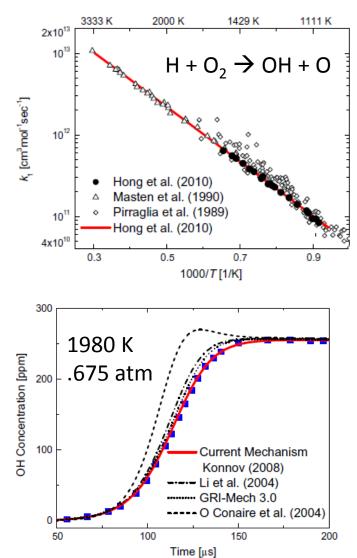
**Figure 7** Laminar flame mass burning rate at 1, 3, and 5 atm for  $H_2/O_2/He$  mixture ( $O_2:He=1:7$ ). Symbols: experimental data [7]; solid lines: the present model; dashed lines: the model of Mueller et al. [1].

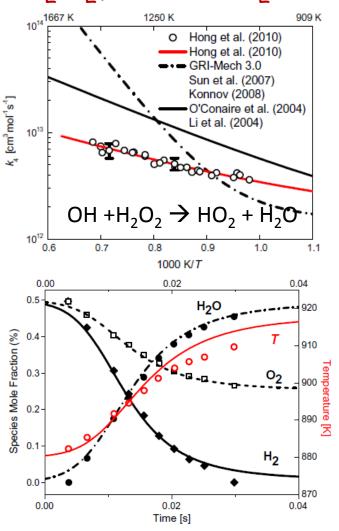


**Figure 11** Ignition delay of  $H_2/O_2/Ar$  mixtures in shock tubes. Initial conditions:  $H_2 = 8.0\%$ ,  $O_2 = 2.0\%$  at 5 atm [11];  $H_2 = 1.0\%$ ,  $O_2 = 2.0\%$  at 1 atm [12];  $H_2 = 2.0\%$ ,  $O_2 = 1.0\%$  at 33, 57, 64, and 87 atm [13]. Symbols: experimental data [11–13]; solid lines: the present model; dashed lines: Mueller et al. [1]. Ignition delay time for the cases of Ref. [11] is defined by the maximum of OH concentration; for Ref. [12], as the time when OH concentration reaches  $1 \times 10^{-6}$  mol/L; and for Ref. [13], by the maximum of  $\frac{d[OH]}{dt}$ .

#### Hong et al.

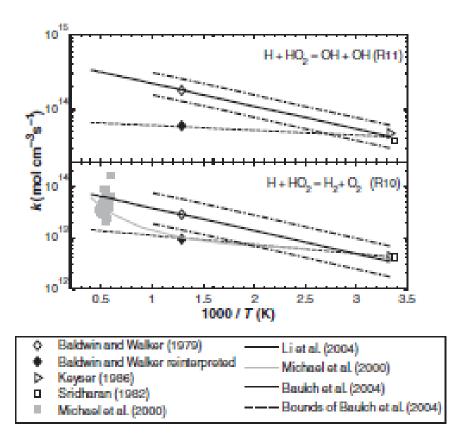
# Revised mechanism using own shock tube data on $H + O_2 \rightarrow OH + O$ , $H_2O_2 + M$ , $OH + H_2O_2$ , $OH + HO_2$

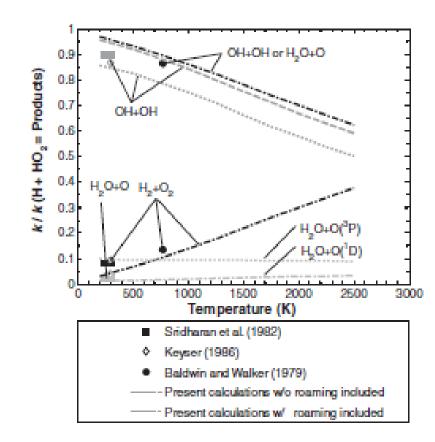




Species profiles, 880 K, 0.3 atm

#### Burke et al.

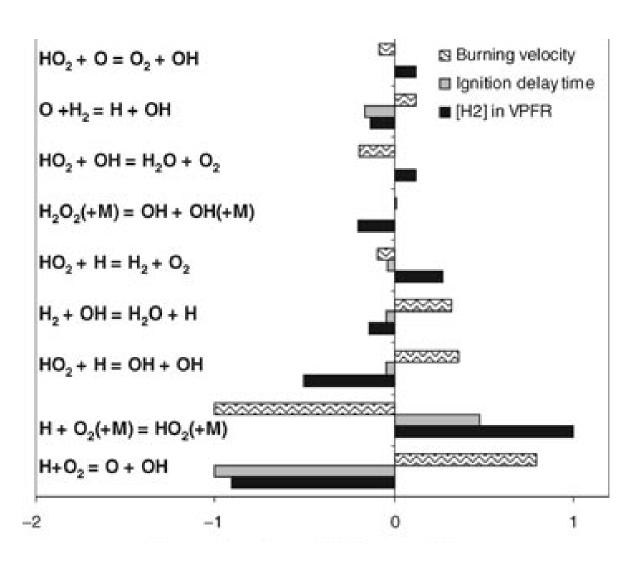




 $H + HO_2$ 

Branching ratios

## Sensitivity analysis (Burke et al



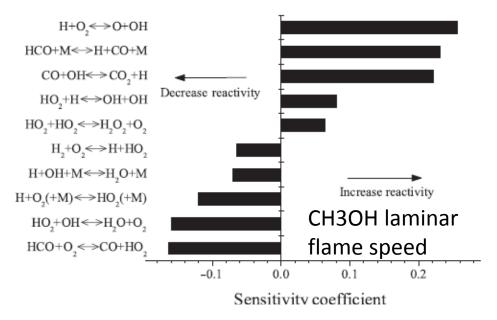
# A Hierarchical and Comparative Kinetic Modeling Study of C1-C2 Hydrocarbon and Oxygenated Fuels Metcalfe et al, Int J Chem Kinet, 45, 638 (2013)

Table I Range of Experimental Devices Used for Mechanism Validation

Fuel	Shock Tube	Jet-Stirred Reactor	Flow Reactor	Flame Speed	Flame Speciation
Methane	✓	✓	✓	✓	
Ethane	✓	✓		✓	
Ethylene	✓	✓	✓	✓	✓
Acetylene	✓	✓	✓	✓	✓
Formaldehyde			✓		✓
Acetaldehyde	✓	✓	✓		
Methanol	✓	✓	✓	✓	
Ethanol	✓	✓	✓	✓	✓
Methane/ethane	✓	✓		✓	
Temperature (K)	833-2500	800-1260	600-1400	295-600	300-2300
Pressure (atm)	0.65-260	1–10	1.0-59.22	1–10	0.026-0.05
Equivalence ratio $(\phi)$	0.06-6.0	0.25-5.0	0.05-5.0	0.4-2.2	0.75-2.4

 Mechanisms evaluated using ignition delays, laminar burning velocities and flame speeds,

#### Examples of sensitivity analyses and and optimised rate data



Ο, CH, 77777777777 CH, HCO Thermochemistry H CH.O sensitivity analysis H,O ĆΟ methane/air ignition CH,O ÓН delay times Η CH,OH S<sup>0</sup> ( 298 K) O CHO H<sup>o</sup> (298 K) H,O, HO, CH<sub>3</sub>O

0.0

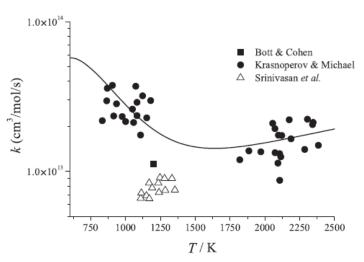
Sensitivity coefficient

0.1

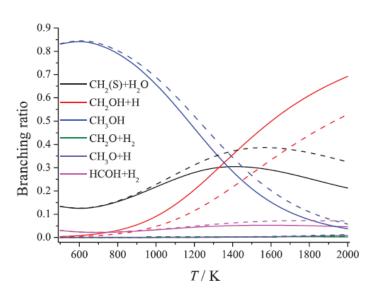
0.2

-0.1

-0.2



Recommended  $k(CH_3 + OH)$ 



Reaction channels in CH<sub>3</sub>+OH vs theory

# More complex mechanisms 1. Oxidation of C1-C5 Alkane Quinternary Natural Gas Mixtures at High Pressures Energy Fuels 2010, 24, 1521-1528

- Rapid compression machine and shock tube
- detailed chemical kinetic mechanism
- Mixtures of  $CH_4/C_2H_6/C_3H_8/n-C_4H_{10}/n-C_5H_{12}$  studied in the temperature range 630-1550 K, in the pressure range 8-30 bar, and at equivalence ratios of 0.5, 1.0, and 2.0 in air
- Mechanism: NUIG Combustion Chemistry Centre, Natural Gas III mechanism, 2011. Available at <a href="http://c3.nuigalway.ie/naturalgas3.html">http://c3.nuigalway.ie/naturalgas3.html</a>. (See more recent developments later in lecture)

## More complex mechanisms 2. Curran et al, low T dimethyl ether oxidation

$$CH_3O\dot{C}H_2 \xrightarrow{282} CH_2O + \dot{C}H_3$$

$$CH_3OCH_2\dot{O}_2 \stackrel{287}{\longleftrightarrow} CH_3O\dot{C}H_2 + O_2$$

$$CH_3OCH_2\dot{O}_2 \stackrel{293}{\longleftrightarrow} \dot{C}H_2OCH_2O_2H$$

$$\dot{C}H_2OCH_2O_2H \stackrel{294}{\longleftrightarrow} CH_2O + CH_2O + \dot{O}H$$

$$\dot{O}_2CH_2OCH_2O_2H \stackrel{295}{\longleftrightarrow} \dot{C}H_2OCH_2O_2H + O_2$$

$$\dot{O}_2CH_2OCH_2O_2H \stackrel{296}{\longleftrightarrow} HO_2CH_2OCHO + OH$$

$$HO_2CH_2OCHO \stackrel{297}{\longleftrightarrow} \dot{O}CH_2OCHO + OH$$

$$\dot{O}CH_2OCHO \stackrel{298}{\longleftrightarrow} CH_2O + HCO_2$$

$$\dot{O}CH_2OCHO \stackrel{298}{\longleftrightarrow} CH_2OCH_2OCHO$$

 $HOCH_2OCO \xrightarrow{304} HOCH_2O + CO$ 

 $HOCH_2OCO \xrightarrow{305} CH_2OH + CO_2$ 

$$\varepsilon_a = \Delta H_{\rm rxn} + {\rm ring \ strain} + E_{\rm abst}$$

$$E_{\rm abst} = 12.7 + (\Delta H_{\rm rxn} \times 0.37)$$

Most of rate coefficients have not been measured and were estimated - e.g. through relations with thermodynamic data.

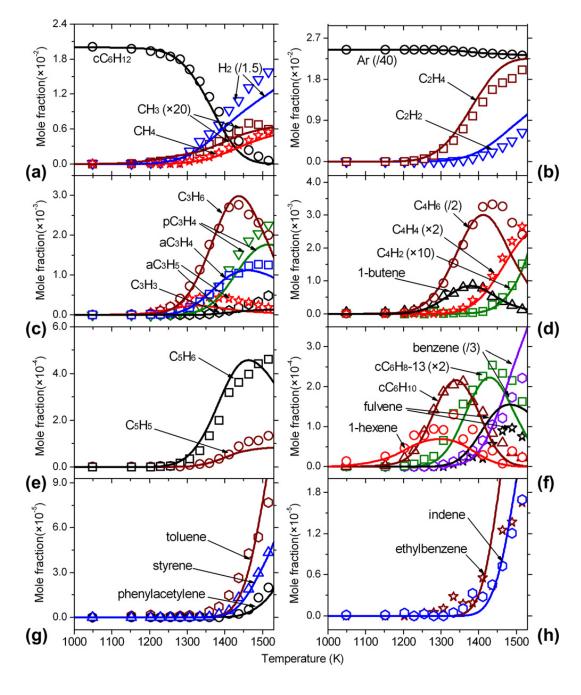
Int J Chem Kinet, 2000, 32, 741

See discussion in Topic 7

### Larger Molecules 1. Cyclohexane pyrolysis Wang et al, Comb and Flame 159 (2012) 2243-2253

Skimmer
Quartz Nozzle
Oven
Heating Wire
Thermocouple
Gas Inlet

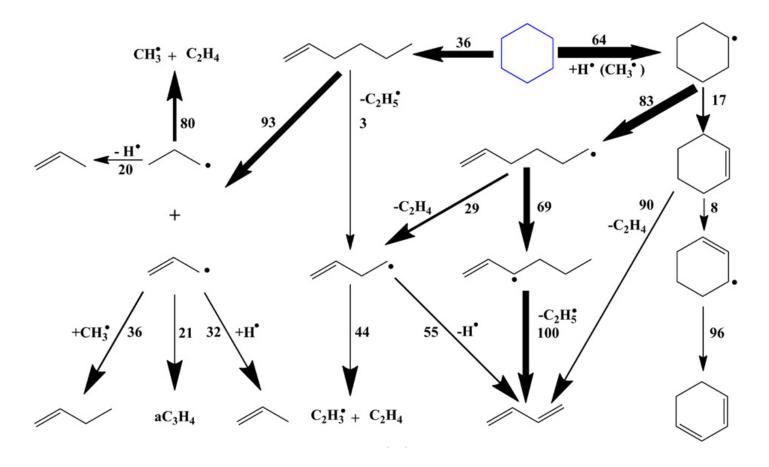
- Heated flow reactor, 950 to 1520 K, synchrotron VUV photoionization mass spectrometry.
- 30 species identified by photoionization efficiency (PIE) spectra, including some radicals like methyl, propargyl, allyl and cyclopentadienyl radicals, and stable products (e.g., 1-hexene, benzene and some aromatics).



# Observed products vs temperature

- Open symbols experiment; full lines simulations
- Mechanism based on earlier work at Hefei and on A High-temperature Chemical Kinetic Model of n-alkane (up to ndodecane), Cyclohexane, and Methyl-, ethyl-, npropyl and n-butylcyclohexane Oxidation at High Temperatures, JetSurF Version 2.0, September 19, 2010. <http://melchior.usc.edu/ JetSurF/ JetSurF2.0>.

#### Rate of production analysis of cyclohexane pyrolysis at 1360 K

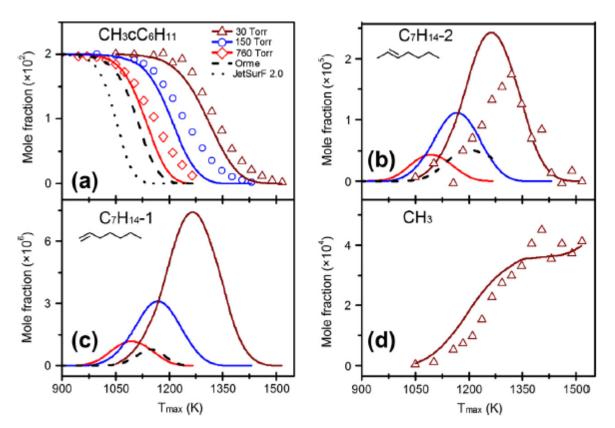


 Thickness of arrows denotes relative rate, numbers show percentage conversion

#### Larger molecules 2

Experimental and kinetic modeling study on methylcyclohexane pyrolysis and combustion, Wang et al, Comb and Flame, 161 (2014) 84-100

 synchrotron vacuum ultraviolet photoionization mass spectrometry combined with molecular-beam sampling was used to investigate the species formed during the pyrolysis of methylcyclohexane and in premixed flame of methylcyclohexane.



Solid lines: Wang et al mechanisms
Other mechanisms at 760 Torr

Mechanism based on cyclohexane mechanism; development also included Theoretical calculations of abstraction by H

### Comprehensive mechanisms:

#### 1. AramcoMech2.0

- Kinetic and thermochemical properties of a large number of  $C_1$ - $C_4$  based hydrocarbon and oxygenated fuels over a wide range of experimental conditions. Developed by Curran et al., at NUI Galway.
- Developed in a hierarchical way 'from the bottom up', starting with a  $H_2/O_2$  sub-mechanism, followed by a C1 sub-mechanism and has grown to include larger carbon species such as ethane, ethylene, acetylene, allene, propyne, propene, n-butane, isobutane, isobutene, 1-butene and 2-butene, and oxygenated species including formaldehyde, acetaldehyde, methanol, ethanol, and dimethyl ether.
- Validated against a large array of experimental measurements including data from shock tubes, rapid compression machines, flames, jet-stirred and plug-flow reactors.

#### References

- Y. Li, et al. The Oxidation of 2-Butene: A High Pressure Ignition Delay, Kinetic Modeling Study and Reactivity Comparison with Isobutene and 1-Butene Proceedings of the Combustion Institute (2017) 36(1) 403-411.
- C-W. Zhou et al. " A Comprehensive experimental and modeling study of isobutene oxidation", Combust. Flame (2016) 167 353-379.
- U. Burke, et al., " A Detailed Chemical Kinetic Modeling, Ignition Delay time and Jet-Stirred Reactor Study of Methanol Oxidation", Combust. Flame (2016) 165 125-136.
- S.M. Burke, et al., "An experimental and modeling study of propene oxidation. Part 2: Ignition delay time and flame speed measurements", Combust. Flame (2015) 162(2) 296-314.
- S.M. Burke et al., "An experimental and modeling study of propene oxidation. Part 1: Speciation measurements in jet-stirred and flow reactors", Combust. Flame (2014) 161(11) 2765-2784.
- W.K. Metcalfeet al., "A hierarchical and comparative kinetic modeling study of  $C_1$ - $C_2$  hydrocarbon and oxygenated fuels", Int. J. Chem. Kinet. (2013) 45(10) 638-675.
- A. Kéromnès, et al.
   "An Experimental and Detailed Chemical Kinetic Modelling Study of Hydrogen and Syngas Mixtures at Elevated Pressures" Combustion and Flame (2013) 160 995-1011.
- Web site: <a href="http://www.nuigalway.ie/c3/aramco2/frontmatter.html">http://www.nuigalway.ie/c3/aramco2/frontmatter.html</a>

#### **USC** Mechanism:

#### http://ignis.usc.edu/Mechanisms/USC-Mech%20II/USC\_Mech%20II.htm

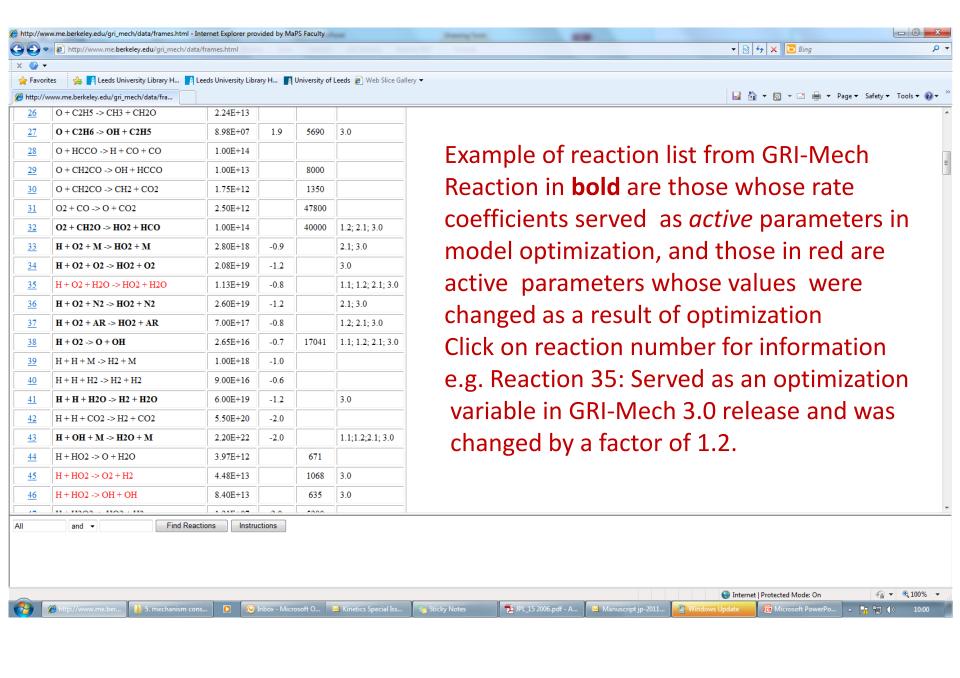
- Incorporates the recent thermodynamic, kinetic, and species transport updates relevant to high-temperature oxidation of hydrogen, carbon monoxide, and C1-C4 hydrocarbons. This model was developed on the basis of:
  - Optimised H2/CO combustion
  - GRI-Mech 1.2, 3.0
  - Comprehensive mechanism for ethene and ethyne combustion
  - Mechanism for C3 and 1,3 butadiene combustion
- Validated with:
  - Ignition delays
  - Species profiles in shock tube oxidation studies
  - Laminar flame speeds
  - Flow reactor data
  - Burner stabilized flame data

## Development of a tuned mechanism GRI-Mech

- G.P. Smith, D.M. Golden, M. Frenklach, N.W.Moriarty, B. Eiteneer, M. Goldenberg, C.T. Bowman, R. Hanson, S. Song, W.C. Gardiner, Jr., V.Lissianski, Z. Qin, Available at: <a href="http://www.me.berkeley.edu/gri\_mech/">http://www.me.berkeley.edu/gri\_mech/</a>
- GRI-Mech is a list of elementary chemical reactions and associated rate constant expressions
- Sensitivity tests against target experimental data allow selection of rate parameters for tuning
- process of automatic simultaneous parameter optimization, to get the parameter set for each successive release of GRI-Mech. Strict constraints keep the rate parameters within predetermined bounds based on
  - evaluations of the uncertainties in measurements of the rates of elementary reactions
  - applications of conventional reaction rate theory

#### GRI-Mech contd

- GRI-Mech is optimized <u>as a whole</u>, substitutions, further selective tuning should not be done.
- All reactions treated as reversible; thermodynamic data (based on NASA, Technion) provided.
- to use the input files directly you need the Chemkin-II programs
- GRI-Mech 3.0 has 53 species, 325 reactions, with associated rate and thermodynamic data.
- Optimized for methane as a fuel. Includes C2 and propane chemistry.
- Optimized against chosen targets in ranges: T = 1000 to 2500 K, p =10 Torr to 10 atm,  $\phi$  = 0.1 to 5 for premixed systems
- http://akrmys.com/public/chemkin/CKm\_inp.html.en
- http://www.reactiondesign.com/products/chemkin/

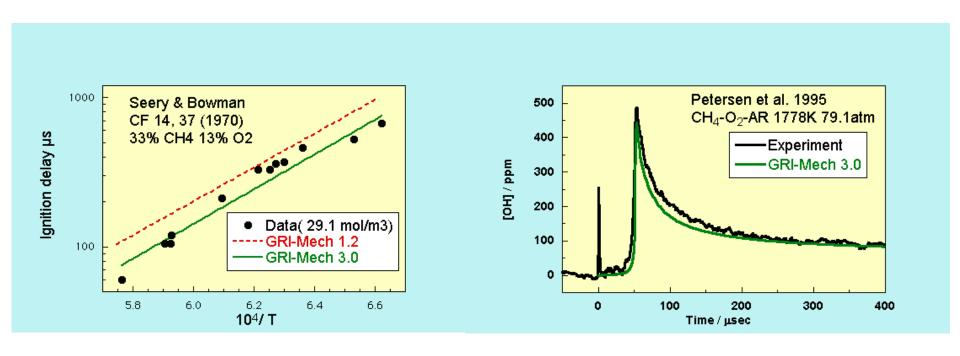


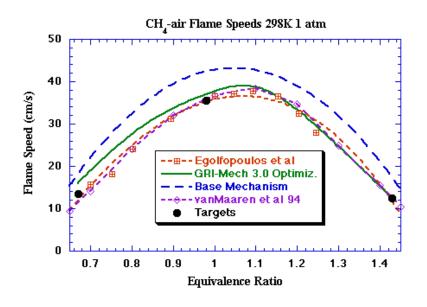
### Thermodynamic and kinetic data for reaction 35

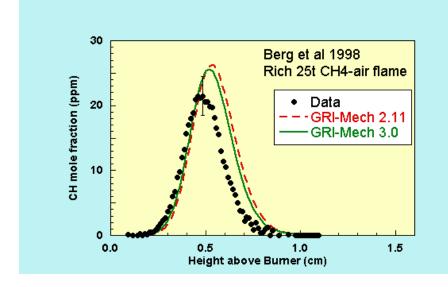
Temp	delta-S	delta-H	kf	kr	Keq
(K)	(cal/mol K)	(kcal/mol)	(mol,	cm3,s)	(cm3/mol)
200	01 7	40.1	1 400.17	E EOE 10	0 (45.25
300	<b>-</b> 21.7	-49.1	1.48E+17	5.59E-19	2.64E+35
500	<b>-</b> 23.4	<b>-</b> 49.8	1.00E+17	5.63E-05	1.78E+21
1000	<b>-</b> 25 <b>.</b> 1	<b>-</b> 51.0	5.90E+16	1.61E+06	3.68E+10
1500	<b>-</b> 25.7	<b>-</b> 51.7	4.34E+16	4.31E+09	1.01E+07
2000	-26.0	<b>-</b> 52 <b>.</b> 2	3.49E+16	2.03E+11	1.72E+05
2500	-26.1	<b>-</b> 52.4	2.94E+16	1.91E+12	1.55E+04
3000	-26.2	-52.6	2.57E+16	8.05E+12	3.19E+03

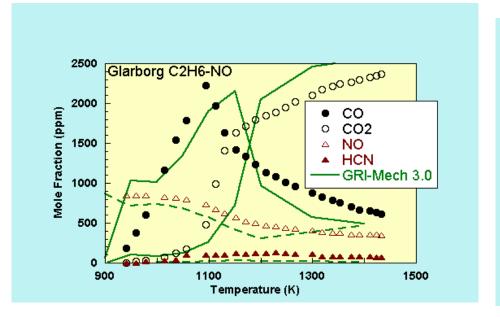
### Optimisation against a wide list of targets

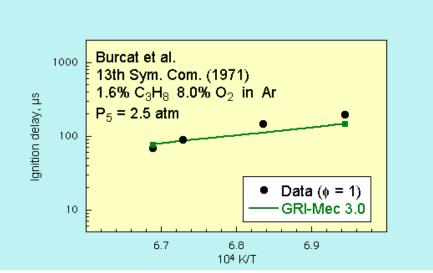
 Shock tube ignition delay and species profiles, reactors, laminar flame speed, prompt NO, HCN oxidation, reburning. Examples:











# Engagement of the community in mechanism development PrIMe Frenklach, Proc Comb Inst 31 (2007) 125-140

Discussed the future of predictive combustion models through what he termed Process Informatics which "relies on three major components: proper organization of scientific data, availability of scientific tools for analysis and processing of these data, and engagement of the entire scientific community in the data collection and analysis."

### Current site: https://prime.cki-know.org/

- The PrIMe project started from informal discussions in 2001.
- Depository and Library. PrIMe Data Warehouse consists, conceptually, of two parts: Depository and Library. The Depository is a repository of data provided by the community. The only requirement for the acceptance of the data into the Depository is the data-record completeness, which is checked electronically with the use of data schemas. The Library is a set of data evaluated by the PrIMe Work Groups (PWG). A set of primekinetics codes is being developed to assist in both initial submission and PWG-evaluation of the data.

# Current site: https://prime.cki-know.org/PrIMe Group directory 1

<u>Name</u>	Subscribers	<u>Description</u>
<u>BioFuels</u>	9	BioFuels
Burner-stabilized premixed flames	33	Burner-stabilized premixed flames
<u>CO-C2</u>	69	H2/O2/C0 + C1/C2 hydrocarbon pyrolysis and oxidation
<u>C3-C4</u>	47	C3-C4 hydrocarbon pyrolysis and oxidation
<u>C5-C16</u>	35	C5-C16 hydrocarbon pyrolysis and oxidation
<u>C6 + aromatics</u>	20	C6 + aromatic hydrocarbon pyrolysis and oxidation
Cyber-numerics	33	Cyber-numerics
<u>Diffusion flames</u>	22	Diffusion flames

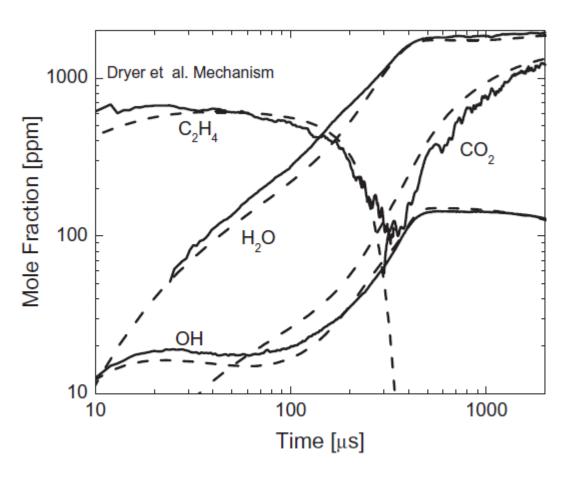
### PrIMe Group directory 2

Flow reactors	2	Flow reactors	Spectroscopy	7	Spectroscopy
<u>Industrial</u>	13	Industrial	Stirred	_	Stirred
Laminar		Laminar	<u>reactors</u>	9	reactors
premixed flames	32	premixed flames (global properties)	<u>Test</u>	1	For testing only
<u>N</u>	8	Nitrogen containing	<u>Thermo</u>	42	Thermodyna mic data
<u>P-dependence</u>	15	Pressure dependence of	<u>Transport</u>	11	Transport data
		reactions	<u>TST</u>	25	Transition-
<u>Quantum</u>	2	Quantum	<u>131</u>	23	State theory
chemistry		chemistry	<u>Turbulent</u>	1	Turbulent
ReactionDesign	24	ReactionDesign	<u>flames</u>	1	flames
Shock tubes	35	Shock tubes			
<u>Soot</u>	67	Soot			

### Systematic provision of targets

- E.g. Davidson et al. Combustion and Flame 157 (2010) 1899-1905: Multi-species time-history measurements during n-heptane oxidation behind reflected shock waves
- 1300-1600 K, 2 atm (Ar) 300 ppm n-heptane, 3300 ppm oxygen ( $\phi = 1$ )
- Monitoring:
  - n-Heptane and ethylene, IR gas laser absorption, 3.39 and 10.53  $\mu$ m, resp.
  - OH UV laser absorption at 306.5 nm
  - $CO_2$  and  $H_2O$  tunable IR diode laser absorption at 2.7 and 2.5  $\mu$ m, resp.

# Example of experimental measurements and comparison with existing mechanism



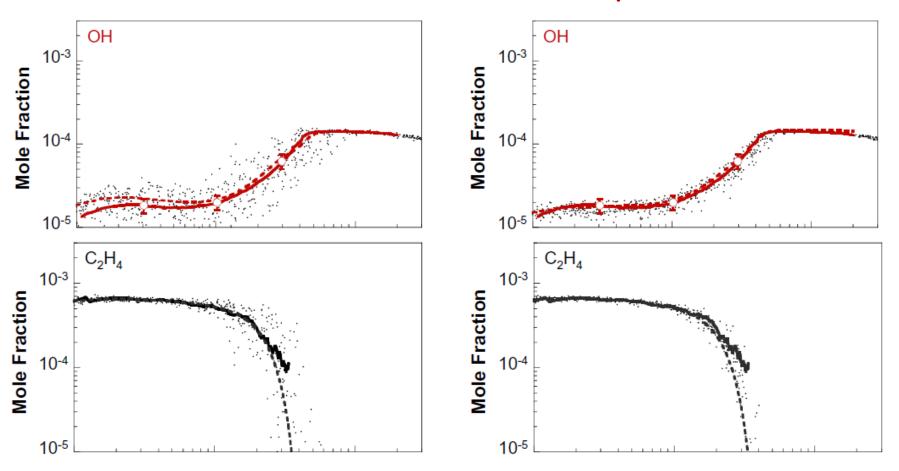
**Fig. 7.** Comparison of laser-absorption measurements with the Dryer et al. model [4]. Reflected shock wave conditions: 1494 K, 2.15 atm, 300 ppm n-heptane/O<sub>2</sub>/argon,  $\phi = 1$ .

### Use of target data from Davidson et al. Sheen and Wang, Combustion and Flame 158 (2011) 645-656 (quotes from abstract) Combustion kinetic modeling using multispecies time

histories in shock-tube oxidation of heptane

- Precise nature of measurements of Davidson et al. impose critical constraints on chemical kinetic models of hydrocarbon combustion.
- while an as-compiled, prior reaction model of n-alkane combustion can be <u>accurate</u> in its prediction of the detailed species profiles, the kinetic parameter uncertainty in the model remains too large to obtain a precise prediction of the data.
- Constraining the prior model against the species time histories within the measurement uncertainties led to notable improvements in the <u>precision</u> of model predictions against the species data as well as the global combustion properties considered.
- accurate data of <u>global</u> combustion properties are still necessary to predict fuel combustion.

### Model measurement comparisons



• Experimental (solid lines) and computed (dashed lines: nominal prediction; dots: uncertainty scatter). The open circles and the corresponding error bars designate data used as Series 1 targets and  $2\sigma$  standard deviations, respectively. Left panel: prior model (Model I). Right panel: posterior model (Model II).

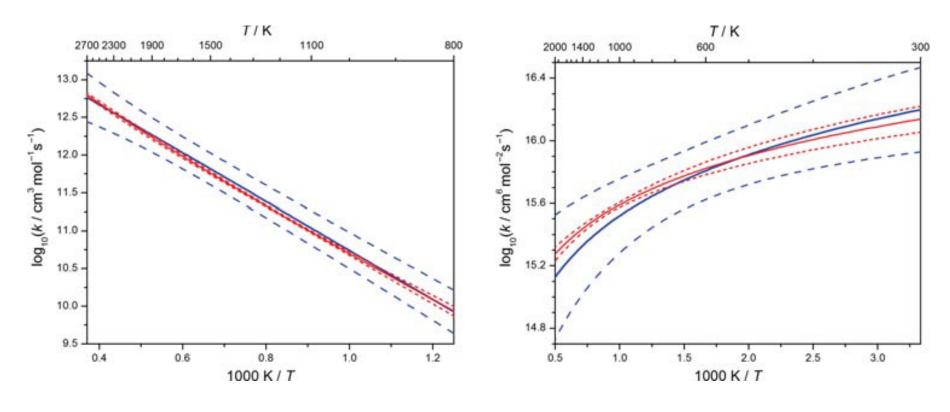
#### Turanyi et al. Determination of Rate Parameters Based on Both Direct and Indirect Measurements

International Journal of Chemical Kinetics 2012 DOI 10.1002/kin.20717

(R1): 
$$H + O_2 = OH + O$$
  
(R2):  $H + O_2 + M = HO_2 + M$  (low-pressure limit,  $M = N_2$  or  $Ar$ )

- new approach that takes into account both direct and indirect measurements and optimizes all influential rate parameters
- First, the domain of feasibility of the Arrhenius parameters is determined from all of the available direct measurements (see topic 5).
- the optimal Arrhenius parameters are then sought within this domain to reproduce the selected direct and indirect measurements
- 9 direct measurements for reaction (R1) (745 data points)
- 10 direct measurements for reaction (R2) (258 data points)
- 11 ignition time measurements (79 data points) were taken into account.
- A new fitting algorithm and a new method for error calculation were developed to determine the optimal mean values and the covariance matrix of all parameters

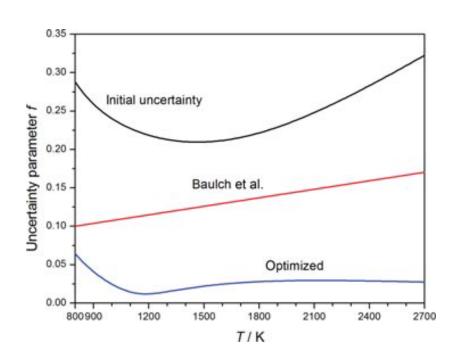
#### Arrhenius plots and uncertainties

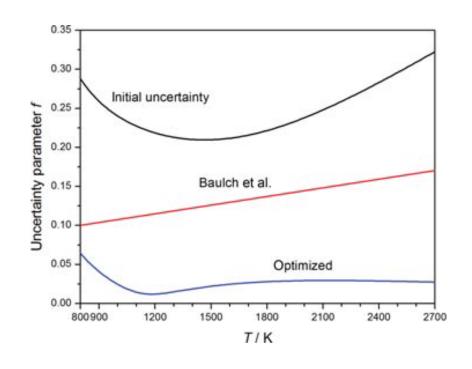


Arrhenius plots of the initial and optimized main values and uncertainty limits for reaction (R1):  $H + O_2 = OH + O$ . Thin solid blue line: initial value, recommended by Baulch et al.; blue dashed lines: initial uncertainty limits; red line: optimized rate coefficient; red dashed lines: optimized uncertainty limits.

Arrhenius plots of the initial and optimized main values and uncertainty limits for reaction (R2):  $H + O_2 + N_2 = HO_2 + N_2$  (low-pressure limit). Thin solid blue line: initial value, recommended by Baulch et al.; blue dashed lines: initial uncertainty limits; red line: optimized rate coefficient; red dashed lines: optimized uncertainty limits.

#### Uncertainty parameters for reactions R1 and R2.





Uncertainty parameter (f) as a function of temperature for reaction (R1): H + O2 = OH + O, according to the evaluation of Baulch et al. [3] (red line), and f calculated from the covariance matrix of the Arrhenius parameters in two different ways: The "initial uncertainty" belongs to the kmin(T) and kmax(T) functions (black line), and the "optimized" belongs to the optimized rate parameters (blue line).

Uncertainty parameter (f) as a function of temperature for reaction (R2): H + O2 + N2 = HO2 + N2 (low-pressure limit) according to the evaluation of Baulch et al. (red line), and f calculated from the covariance matrix of the Arrhenius parameters in two different ways: The "initial uncertainty" belongs to the kmin(T) and kmax(T) functions (black line), and the "optimized" belongs to the optimized rate parameters (blue line).

Table VII The Determined Covariances of the Rate Parameters

	$lnA_1$	$n_1$	$E_1/R$	$lnA_2$	$n_2$	m (Ar)
In A <sub>1</sub> n <sub>1</sub> E <sub>1</sub> IR In A <sub>2</sub> n <sub>2</sub> m (Ar)	1.0609 × 10 <sup>0</sup>	$-1.2149 \times 10^{-1}$ $1.3924 \times 10^{-2}$	$2.3661 \times 10^{2}$ $-2.6989 \times 10^{1}$ $5.3824 \times 10^{4}$	$-4.4080 \times 10^{-1}$ $4.9745 \times 10^{-2}$ $-1.0438 \times 10^{2}$ $3.3293 \times 10^{-1}$	$6.3586 \times 10^{-2}$ $-7.1782 \times 10^{-3}$ $1.5020 \times 10^{1}$ $-4.7993 \times 10^{-2}$ $6.9222 \times 10^{-3}$	$-3.0367 \times 10^{-3}$ $3.5276 \times 10^{-4}$ $-6.0886 \times 10^{-1}$ $7.4402 \times 10^{-4}$ $-1.1576 \times 10^{-4}$ $9.2352 \times 10^{-5}$

Table VIII The Determined Correlations of the Rate Parameters

	$\ln A_1$	$n_1$	$E_1/R$	ln A <sub>2</sub>	$n_2$	m (Ar)
In A <sub>1</sub>	1	-0.99957	0.99015	-0.74170	0.74199	-0.30679
$n_1$		1	-0.98586	0.73062	-0.73116	0.31108
$E_1/R$			1	-0.77976	0.77814	-0.27309
In A2				1	-0.99973	0.13418
n <sub>2</sub>					1	-0.14478
m (Ar)						1

**Table I** Evaluated and Optimized Rate Parameters for Reaction  $H + O_2 = OH + O(R1)$ 

Reference	$A (cm^3 mol^{-1} s^{-1})$	n	E/R (K)	f	T Range (K)
Baulch et al. [3]	$2.07 \times 10^{14}$	-0.097	7560	0.1 at 800 K, 0.2 at 3500 K	800-3500
Li et al. [41]	$3.55 \times 10^{15}$	-0.41	8359	_	_
Ó Conaire et al. [42]	$1.91 \times 10^{14}$	0	8278	_	_
Konnov [43]	$2.06 \times 10^{14}$	-0.097	7564	0.176	800-3500
Hong et al. [44]	$1.04 \times 10^{14}$		7705		1100-3370
This work	$3.003 \times 10^{10}$	0.965	6158	0.025 at 1000 K,	950-3550
				0.022 at 1500 K,	
				0.029 at 2000 K	

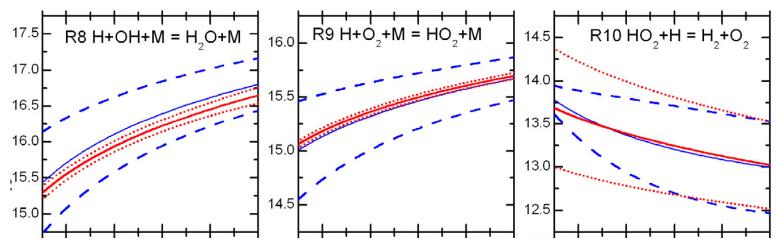
 $\textbf{Table II} \quad \text{Evaluated Rate Parameters for Low-Pressure Limit Reaction H} + O_2 + M = HO_2 + M \text{ (R2)}$ 

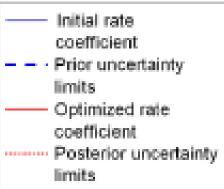
Reference	Bath Gas	$A (cm^6 mol^{-2} s^{-1})$	n	E/R (K)	f	T Range (K)
Baulch et al. [3]	N <sub>2</sub>	$2.65 \times 10^{19}$	-1.3	0	0.1 at 298 K,	298-2000
Baulch et al. [3]	Ar	$6.9\times10^{18}$	-1.2	0	0.2 at 2000 K 0.1 at 298 K, 0.2 at 2000 K	298-2000
Li et al. [41]	N <sub>2</sub>	$6.37 \times 10^{20}$	-1.72	261.8	_	_
Li et al. [41]	Ar	$9.04 \times 10^{19}$	-1.50	246.7	_	_
Ó Conaire et al. [42]	N <sub>2</sub>	$3.482 \times 10^{16}$	-0.41	-561.5	_	_
Konnov [43]	N <sub>2</sub>	$5.70 \times 10^{19}$	-1.4	0	0.079	300-2000
Konnov [43]	Ar	$7.43 \times 10^{18}$	-1.2	0	0.079	300-2000
Hong et al. [44]	$N_2$	$2.65 \times 10^{19}$	-1.3	0	_	_
Hong et al. [44]	Ar	$6.81 \times 10^{18}$	-1.2	0	_	_
This work	N <sub>2</sub>	$7.856 \times 10^{18}$	-1.100	0	0.032 at 800 K, 0.018 at 1000 K, 0.045 at 1500 K	300-1850

## Optimization of a hydrogen combustion mechanism using both direct and indirect measurements Varga et al, Proc Comb Inst 35 (2015) 589-596

- Optimisation of Keromnes mechanism using ignition measurements from shock tubes (566 datapoints, 43 datasets) and rapid compression machines (219/19) + flame velocities (364/59)
- Sensitivity analysis showed that parameters for 11 elementary reactions could be optimised. Also utilized 1749 direct k measurements from 56 datasets, with prior uncertainty ranges
- Analysis provides new mechanism including new k(T)s, with covariance matrix and T dependent posterior uncertainty ranges
- Demonstrate much reduced overall error function compared with 13 earlier mechanisms

#### Examples of results for rate constants





- Global parameter optimization from Int J Chem Kinet, 44 (2012) 284 - 302
- Based on minimization of objective function:

$$E(p) = \frac{1}{N} \sum_{i=1}^{N} \frac{1}{N_i} \sum_{j=1}^{N_i} \left( \frac{Y_{ij}^{mod} - Y_{ij}^{exp}}{\sigma(Y_{ij}^{exp})} \right)^2$$

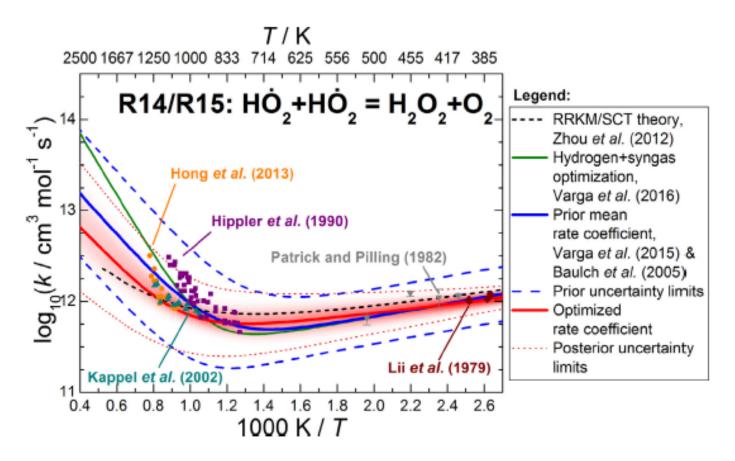
where N is the total number of datasets and  $N_i$  is the number of datapoints in the ith dataset.  $\sigma(Y_{ij}^{exp})$  is the experimental std deviation in the jth datapoint, ith dataset

## Comparison of the performance of several recent syngas combustion mechanisms

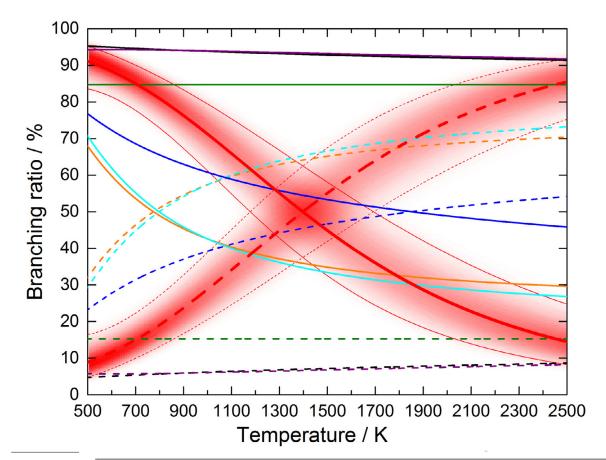
Olm et al Comb and Flame 162 (2015) 1793-1812

- Used same objective function approach to compare performance of 16 syngas (wet CO) mechanisms ignition studies in shock tubes and rapid compression machines, flame velocities and species concentration measurements from flow reactors, shock tubes and jet-stirred reactors. 4970 data points in 408 datasets from 52 publications.
- Some observations not well modelled.
- Five mechanisms performed better than others.
- influence of poorly reproduced experiments and weighting on the performance of the mechanisms investigated
- analysis of local sensitivity coefficients showed the influence of selected reactions and helped identify those reactions that require more attention

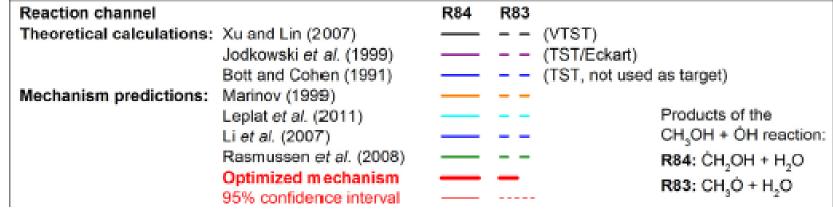
## Uncertainty quantification optimized methanol, formaldehyde combustion mechanism (Olm et al, Comb & Flame 2017, 186, 45)



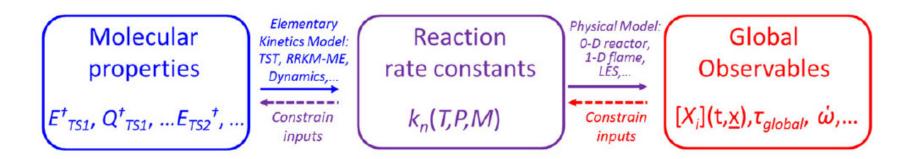
- The prior uncertainty limits are large especially at high T, reflecting substantial disagreements between direct experimental datasets (se Topic 2). Also theory gives lower values.
- The extensive set of indirect measurements (24900 points from 265 datasets) change the optimized k and substantially narrow the uncertainty limits



Channel Yields  $CH_3OH + OH \rightarrow$   $CH_2OH + H_2O (R84)$   $CH_3O + H_2O (R83)$ 



Harnessing the Combined Power of Theoretical and Experimental Data through Multiscale Informatics M P Burke, Int J Chem Kinet 2016, 48,

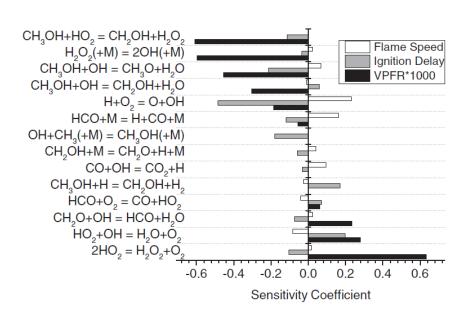


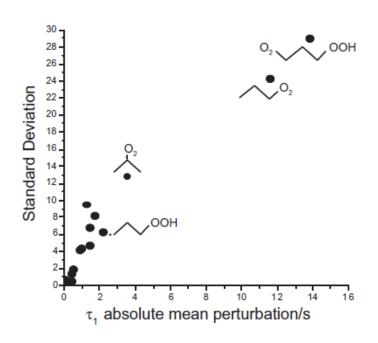
- Approach integrates information from a wide variety of sources and scales:
  - Theoretical parameters, e.g. TS energies, with constrained uncertainties
  - Through elementary kinetics models to rate constants, with propagated uncertainties
  - Through physical models to global observables, such as ignition delay times, with propagated uncertainties

## The role of sensitivity and uncertainty analysis in combustion modelling (A 5 Tomlin, Proc Comb Inst 34 (2013) 159-176)

- significant uncertainties in the data used to parameterise combustion models still exist.
- input uncertainties propagate through models of combustion devices leading to uncertainties in the prediction of key combustion properties.
- focus efforts on those parameters which drive predictive uncertainty, which may be identified through sensitivity analysis.
- Paper discusses how sensitivity and uncertainty analysis can be incorporated into strategies for model improvement

#### Local and global sensitivities





Sensitivity coefficients for flow reactor, shock tube and laminar premixed flame studies of methanol combustion

Global screening methods: Morris analysis for enthalpies of formation with respect to time to cool flame for propane oxidation Investigation of the effect of correlated uncertain rate parameters via the calculation of global and local sensitivity indices

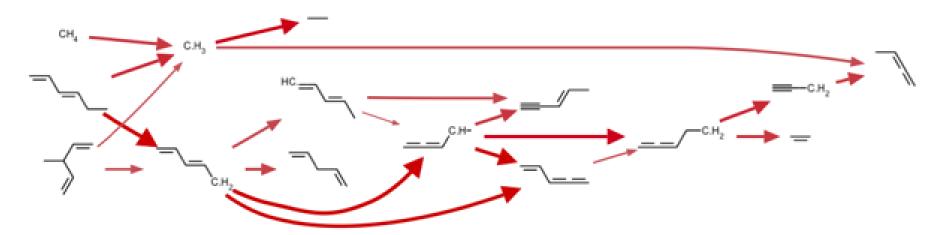
Valko et al, J Math Chem (2018) 56:864-889

- Applied to mechanism used to model ignition delay times in syngas / air (15 species, 48 reactions)
- Most of the parameters have large correlated sensitivity indices and the correlation between the parameters has a high influence on the results.
- The parameters belonging to <u>five</u> elementary reactions only, have significant final marginal sensitivity indices.
- Results of the global sensitivity analysis were compared with the corresponding results of local sensitivity analysis for the syngas-air combustion system. The same set of reactions was indicated to be important by both approaches

#### Automatic mechanism generation

W H Green et al <a href="http://ReactionMechanismGenerator.github.io">http://ReactionMechanismGenerator.github.io</a>

- Open source software, Reaction Mechanism Generator (RMG) is an automatic chemical reaction mechanism generator that constructs kinetic models composed of elementary chemical reaction steps using a general understanding of how molecules react.
- Latest version RMG-Py, written in Python
- CanTherm, developed and distributed as part of RMG-Py, can be used as a stand-alone application for Thermochemistry, Transition State Theory, and Master Equation chemical kinetics calculations
- · Website includes a guide to the theory used in RMG
- Flux diagram for the pyrolysis of 1,3-hexadiene, an example model generated with RMG, showing the net carbon flux at an instant near the end of the simulation



#### RMG - an example

- Harper et al. Comprehensive reaction mechanism for n-butanol pyrolysis and combustion, Combustion and Flame 158 (2011) 16-41
- 263 species and 3381 reactions. Constructed using Reaction Mechanism Generator
- tested against recently published data jet-stirred reactor mole fraction profiles, opposed-flow diffusion flame mole fraction profiles, autoignition delay times, and doped methane diffusion flame mole fraction profiles - and newly acquired n-butanol pyrolysis experiments.

#### Approach

- Base mechanism GRI 3.0 with N chemistry removed.
- Where possible use published data for rate coefficients
- For some important p dependent reactions, calculate high pressure limit using canonical TST using electronic structure calculations.
- Methods available for calculating p dependence.
- Mechanism contains reaction rate constants for 147 different pressure-dependent networks, e.g.  $C_4H_9$
- Extensive testing against experiments, and sensitivity analysis

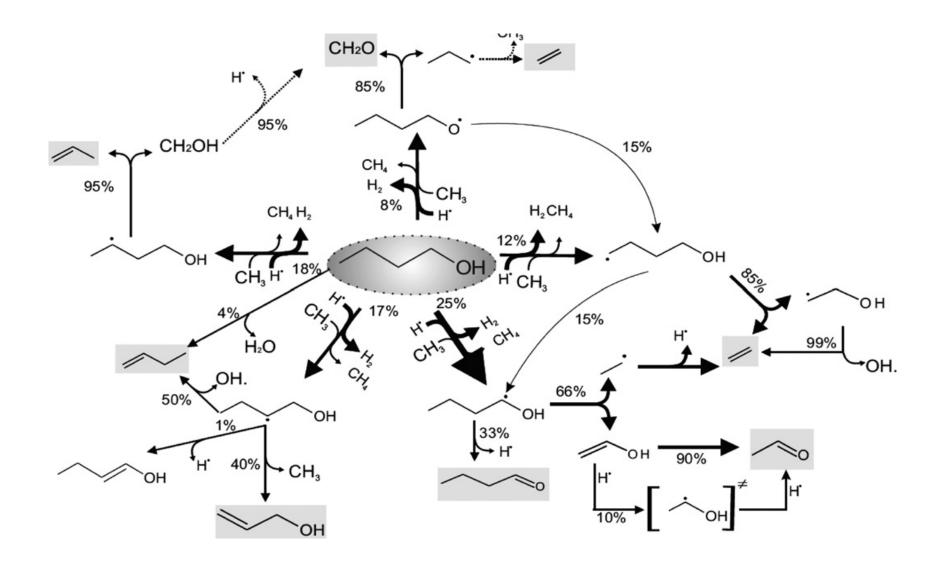
#### Example of reaction network: butyl

1-butyl isomerization to 2-butyl (via three- and four-member ring transition states)

the two beta-scission reactions of 1-butyl radical forming H atom + 1-butene and ethane + ethyl radical

the three beta-scission reactions of 2-butyl radical, forming H atom + 1-butene, H atom + 2-butene, and propene + methyl radical.

#### Example of reaction pathway analysis



## Automatic estimation of pressure-dependent rate coefficients within RMG

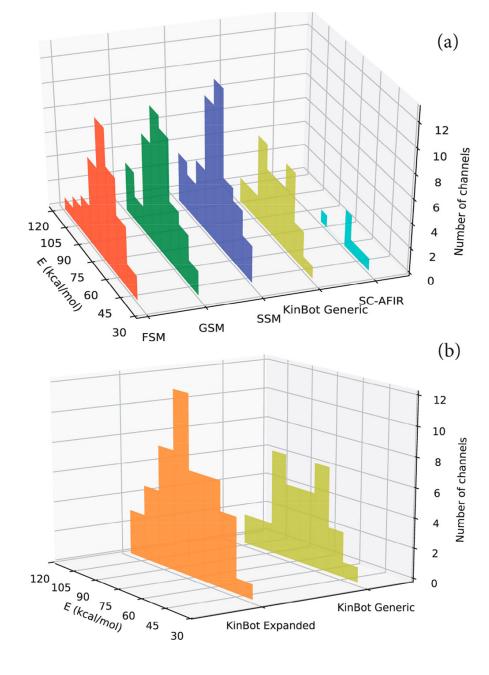
Allen et al. Phys. Chem. Chem. Phys., 2012, 14, 1131-1155

- A general framework for accurately and efficiently estimating the phenomenological pressure-dependent rate coefficients for reaction networks of arbitrary size and complexity using only high-pressure-limit information. Method includes:
- two methods of estimating the density of states of the species in the network, including a new method based on characteristic functional group frequencies.
- three methods of simplifying the full master equation model of the network to a single set of phenomenological rates.

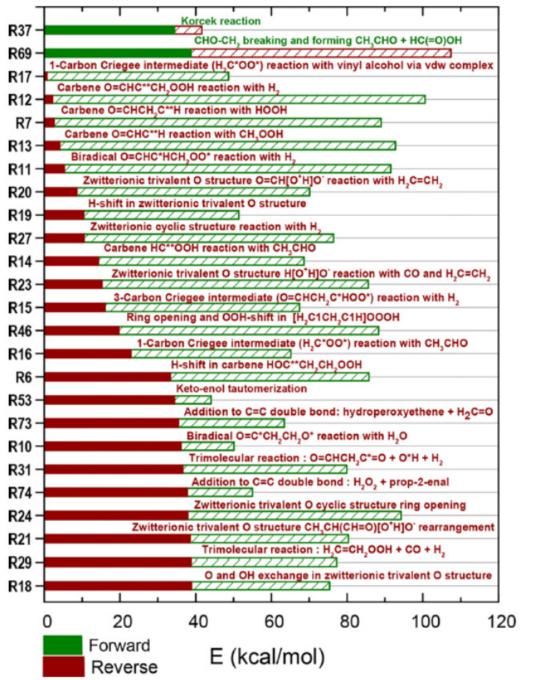
# Unimolecular Reaction Pathways of a $\gamma$ -Ketohydroperoxide from Combined Application of Automated Reaction Discovery Methods

Grambow et al, J Am Chem Soc, 2018, 140, 1035

- Combination of density functional theory with automated transition state search algorithms
- Applied to unimolecular reactions of 3hydroperoxypropanal (CH(O)CH<sub>2</sub>CH<sub>2</sub>OOH) using several different approaches
- 75 elementary unimolecular reactions were found, 68 of these were previously unknown and completely unexpected.
- Several of these involve low barrier reactions that may be relevant in combustion and atmospheric chemistry



### Histogram of energy barriers using different methods



Energy barriers of 25 reactions with energy barriers below 40 kcal/mol

Korcek reaction

#### Some additional references on RMG

- ComputerPhysicsCommunications 203 (2016) 212-225 Reaction Mechanism Generator: Automatic construction of chemical kinetic mechanisms
- Combustion and Flame 160 (2013) 2343-2351 Hansen et al. The predictive capability of an automatically generated combustion chemistry mechanism: Chemical structures of premixed isobutanol flames
- Computers and Chemical Engineering 52, (2013), 35-45 Magoon and Green Design and implementation of a next-generation software interface for on-the-fly quantum and force field calculations in automated reaction mechanism generation