



materials

Food Packaging Materials and Technologies

Edited by
Cornelia Vasile and Morten Sivertsvik
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Food Packaging

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Materials and Technologies

Special Issue Editors

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Contents

About the Special Issue Editors	vii
Preface to "Food Packaging: Materials and Technologies"	ix
Cornelia Vasile	
Polymeric Nanocomposites and Nanocoatings for Food Packaging: A Review	
Reprinted from: <i>Materials</i> 2018, 11, 1834, doi:10.3390/ma11101834	1
Raluca Nicoleta Darie-Niță, Cornelia Vasile, Elena Stoleru, Daniela Pamfil, Traian Zaharescu, Liliana Tarțău, Niță Tudorachi, Mihai Adrian Brebu, Gina Mihaela Pricope, Raluca Petronela Dumitriu and Karol Leluk	
Evaluation of the Rosemary Extract Effect on the Properties of Polylactic Acid-Based Materials	
Reprinted from: <i>Materials</i> 2018, 11, 1825, doi:10.3390/ma11101825	50
Sandra Madalina Constantin, Frederic Buron, Sylvain Routier, Ioana Mirela Vasincu, Maria Apotrosoaei, Florentina Lupașcu, Luminița Confederat, Cristina Tuchilus, Marta Teodora Constantin, Alexandru Sava and Lenuța Profire	
Formulation and Characterization of New Polymeric Systems Based on Chitosan and Xanthine Derivatives with Thiazolidin-4-One Scaffold	
Reprinted from: <i>Materials</i> 2019, 12, 558, doi:10.3390/ma12040558	83
Bogdan Silvestru Munteanu, Liviu Sacarescu, Ana-Lavinia Vasiliu, Gabriela Elena Hitruc, Gina M Pricope, Morten Sivertsvik, Jan Thomas Rosnes and Cornelia Vasile	
Antioxidant/Antibacterial Electrospun Nanocoatings Applied onto PLA Films	
Reprinted from: <i>Materials</i> 2018, 11, 1973, doi:10.3390/ma11101973	102
Valentina Siracusa, Santina Romani, Matteo Gigli, Cinzia Mannozzi, Juan Pablo Cecchini, Urszula Tylewicz and Nadia Lotti	
Characterization of Active Edible Films based on Citral Essential Oil, Alginate and Pectin	
Reprinted from: <i>Materials</i> 2018, 11, 1980, doi:10.3390/ma11101980	120
Elena Butnaru, Elena Stoleru, Mihai Adrian Brebu, Raluca Nicoleta Darie-Nita, Alexandra Bargan and Cornelia Vasile	
Chitosan-Based Bionanocomposite Films Prepared by Emulsion Technique for Food Preservation	
Reprinted from: <i>Materials</i> 2019, 12, 373, doi:10.3390/ma12030373	134
Stanislav Kotsilkov, Evgeni Ivanov and Nikolay Kolev Vitanov	
Release of Graphene and Carbon Nanotubes from Biodegradable Poly(Lactic Acid) Films during Degradation and Combustion: Risk Associated with the End-of-Life of Nanocomposite Food Packaging Materials	
Reprinted from: <i>Materials</i> 2018, 11, 2346, doi:10.3390/ma11122346	151
Lucía Rodríguez-Parada, Pedro F. Mayuet and Antonio J. Gámez	
Evaluation of Reliefs' Properties on Design of Thermoformed Packaging Using Fused Deposition Modelling Moulds	
Reprinted from: <i>Materials</i> 2019, 12, 478, doi:10.3390/ma12030478	166
Lucía Rodríguez-Parada, Pedro F. Mayuet and Antonio J. Gámez	
Custom Design of Packaging through Advanced Technologies: A Case Study Applied to Apples	
Reprinted from: <i>Materials</i> 2019, 12, 467, doi:10.3390/ma12030467	186

About the Special Issue Editors

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Preface to "Food Packaging: Materials and Technologies"

Food Packaging: Materials and Technologies book describes how polymeric materials are used in the obtainment of bioactive, biodegradable, smart food packaging and also as biomaterials to solve some healthcare problems. Polymeric nanomaterials (synthetic and/or natural) used for these purposes described in this book are: active nanocoatings, electrospun nanofibres and nanoparticles, multifunctional nanoparticles, etc.

As key features of the book it can be mentioned: it is demonstrated how the properties of polymeric degradable materials can be used to create more efficient ways to prevent food spoilage and prolong food service life; can help in solving problems in the field through the latest technologies and formulations.

The target of our volume is to bring in the attention of the readers on the importance to develop new materials and technologies in the field of food packaging that will become active, smart and biodegradable to satisfy the requirements and consumer demands.

In this volume are collected reviews and original papers about new receipts of polymeric blends, bio(nano)composites and nanocoatings with multifunctional properties as antibacterial, antioxidant, good barriers to gases and/or water, etc., keeping satisfactory mechanical and thermal characteristics or improving them. These goals have been achieved by using both new synthetized compounds as xanthine derivatives with thiazolidin-4-one, new types of vegetable extracts, nanoclays, graphene and carbon nanotubes and modern methods of preparation as emulsion/solvent casting, electrospinning/electrospraying, etc.

Special attention was given to biodegradation of new polymeric materials, kinetic studies of bioactive compounds release in simulated media, testing of the new elaborated materials for food preservation and prolonged self-life and risk associated with the end-of-life of nanocomposites used as food packaging materials. Two papers present interesting results on design of packaging manufactured by thermoforming, for special case of apple packaging.

The book gives a broad perspective on the topic for researchers, postgraduate students and professionals in the fields of food industry and biomedical fields and medicine.

The editors and contributors of all presented materials will be pleased to receive creative and useful criticism to further improve their work in the future

Cornelia Vasile, Morten Sivertsvik

Special Issue Editors

Review

Polymeric Nanocomposites and Nanocoatings for Food Packaging: A Review

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Abstract: Special properties of the polymeric nanomaterials (nanoscale size, large surface area to mass ratio and high reactivity) individualize them in food packaging materials. They can be processed in precisely engineered materials with multifunctional and bioactive activity. This review offers a general view on polymeric nanocomposites and nanocoatings including classification, preparation methods, properties and short methodology of characterization, applications, selected types of them used in food packaging field and their antimicrobial, antioxidant, biological, biocatalyst and so forth, functions.

Keywords: polymer; nanocomposites; nanocoatings; food packaging; risks; smart nanomaterials

1. Introduction

Nanoscience and nanotechnology applications to the agriculture, food sector and food safety are relatively recent compared with their use in cosmetics and personal care products (60%), paints and coatings, catalysts and lubricants, security printing, drug delivery and pharmaceuticals, medical therapeutics and diagnostics, energy production, molecular computing and structural materials [1–4]. Over \$17.8 billion worldwide investment was made in 2010 for research and development in nanotechnology and this will grow to \$3 trillion by 2020. Food packaging sector counts for ~50% market value for all nanotechnology-enabled products. Annual growth rate is 11.65%. Nanotechnology is mainly applied in extremely high gas barriers packaging materials with antimicrobial properties and in nanoencapsulants for the delivery of nutrients, flavours, or aromas [5,6].

According to regulation (EC) = No 1935/2004 a good packaging should have the following functions: “to protect the food from dirt or dust, oxygen, light, pathogenic microorganisms, moisture and a variety of other destructive or harmful substances. Packaging must also be safe under its intended conditions of use, inert, cheap to be produced, lightweight, easy to dispose or to reuse, able to withstand extreme conditions during processing or filling, impervious to a host of environmental storage and transport conditions and resistant to physical abuse” [7].

Nanomaterials are applied in packaging and food safety are in various forms such as: polymer nanocomposites with high barrier properties, intelligent packaging, nanocoatings, surface biocides, active packaging, silver nanoparticles as antimicrobial agents, nutrition and nutraceuticals, nanosensors and assays for the detection of food relevant analytes (gases, small organic molecules and food-borne pathogens) and bioplastics.

Main recent development areas in packaging field are:

- (I) *Improved packaging* which offers improved mechanical properties as flexibility, enhanced barrier properties against water, gases, taint, durability, temperature/moisture stability, and so forth;
- (II) *Active/bioactive food packaging* offers antimicrobial, antioxidant or biocatalytic functions. It can be obtained by the incorporation of active/bioactive compounds into matrices used in existing packaging materials, or by the application of coatings with the mentioned functionality through

physical or chemical surface modification. Active packaging is applied in food packaging, pharmaceuticals and consumer goods in order to improve shelf life, safety, or quality of packaged foods. Coating option is advantageous because the bulk properties of the packaging materials are preserved almost intact by using a minimum amount of active agent required to impart efficacy and therefore also cost is reduced.

- (III) *Smart/intelligent packaging* as a promising area for active packaging coating is developed by manufacture of nano(bio)sensors which can indicate quality of foodstuffs, of nano(bio)switch to release preservatives and nano-coatings as antimicrobial, antifungal, antioxidant, barrier coatings, external stimuli responsive materials and self-cleaning food contact surfaces. Intelligent inks such as nanoparticles and reactive nanolayers allow analyte recognition at nanoscale. Printed labels are applied to indicate: temperature, time, pathogen, freshness, humidity, integrity [8]. Smart packaging may monitor various parameters such as: temperature, oxygen, pH, moisture and so forth [9–11] of packaged products.

2. Polymeric Nanocomposites

Polymeric nanocomposites are mainly obtained by dispersing of nanoscale filler into a polymeric matrix.

Polymers commonly used in food packaging as either matrices or substrates for bioactive coatings are synthetic undegradable as low density and high density polyethylene (LDPE and HDPE), polypropylene (PP), polyethylene terephthalate (PET), ethylene vinyl alcohol (EVOH) copolymer, polyamide (PA), polystyrene (PS) and degradable ones as polyhydroxyalkanoates (polyhydroxybutyrate (PHB), poly(hydroxybutyrate-*co*-hydroxyvalerate) (PHBV)), poly(lactic acid) (PLA), polycaprolactone (PCL), polyvinyl alcohol (PVOH) and biopolymers as polysaccharides and proteins with critical issue on water resistance, migration and permeability and so forth. These properties may be improved by adding reinforcing compounds (nanofillers), forming bionanocomposites [12]. Because of the different characteristics, their application in food packaging is specific. For example, HDPE is used as milk bottles and bags, LDPE for trays and general-purpose containers, PP has a high melting point, being ideal for hot-fill liquids, films and microwavable containers, while PET is clear, tough and has good gas and moisture barrier properties, so it is used for soft drink bottles, beverages and mineral waters, carbonated drinks and so forth [13]. While synthetic polymers generate huge waste quantity and have an environmental negative impact, by using degradable polymers these problems are avoid, because they are biocompatible and safe to use. However, most degradable polymers are in the research stage or their cost is high, some food packaging based on PLA (the cheapest bio-based material) and poly(butylene adipate-*co*-terephthalate) (PBAT) based packaging is used in Europe, Japan and North America [14,15].

Moreover, recently, a series of biodegradable nanocomposite films based on PBAT and reinforced with an organophilic layered double hydroxide OLDH (0.5–4 wt %) nanosheets were scale-up fabricated. Xie et al. reported such materials with “outstanding thermal, optical, mechanical and water vapour barrier properties a 37% reduction in haze and a 41.9% increase of tensile strain at break better than the pure PBAT film and commercial polyethylene packing materials” [16].

The active agents used in active packaging and coatings include antimicrobials, antioxidants and enzymes which control microbial growth, inhibit oxidative degradation reactions and offer a targeted biocatalysis that maintains food safety and quality and controls spoilage.

The most used nanofillers and nanoreinforcements are: clay montmorillonite (MMT) and kaolinite and silicate nanoplatelets (two-dimensional layers, which are 1 nm thick and several microns long), silica nanoparticles, carbon nanotubes, graphene nanosheets, silver, zinc oxide, titanium dioxide, copper and copper oxides, starch nanocrystals, cellulose nanofibres and nanowhiskers, chitosan and chitin whiskers and others. In respect with their geometry isodimensional nanoparticles have three nanometric external dimensions while nanotubes or whiskers are elongated structures with two external dimensions on nanometre scale and the third is larger (Figure 1) [17–19]. Other classification

is zero-dimensional, one-dimensional, two-dimensional and three-dimensional nanostructured materials [20]. Nanofibres may be also known as nanowire (electrically conducting nanofibre), nanotube (hollow nanofibre) and nanorods (solid nanofibre) [12].

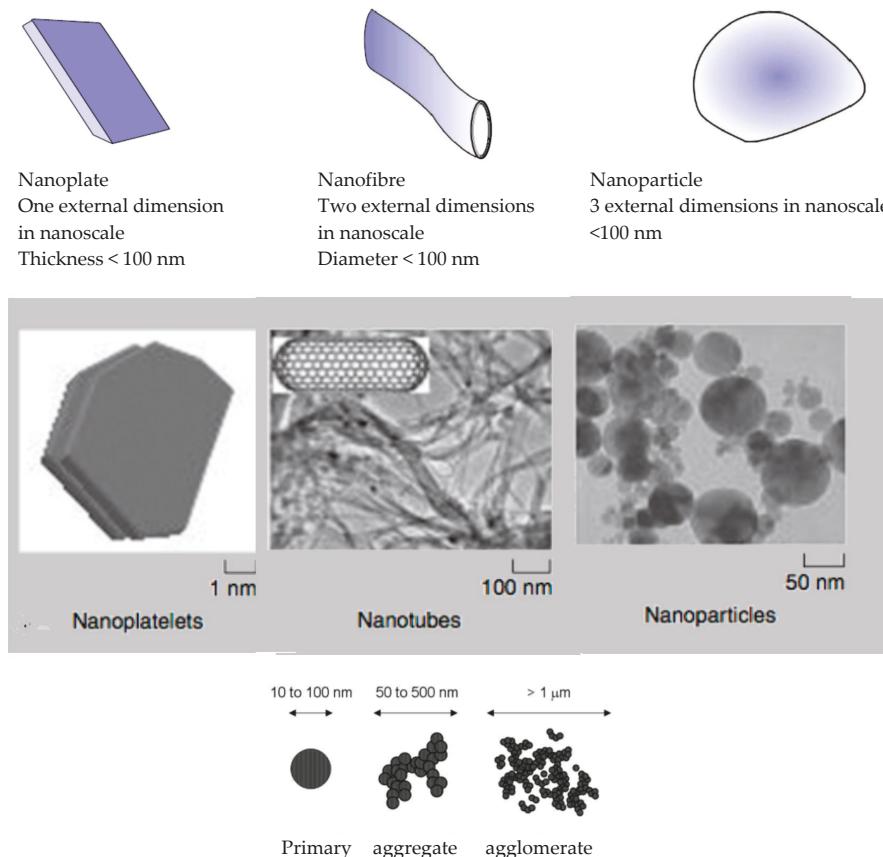


Figure 1. Representative images for nanofillers for nanocomposites. adapted from [17–19].

When only one dimension is in the nanometre range, the composites are known as polymer-layered silicate nanocomposites [21,22]. The role of nanofillers and nanoreinforcements in composites consists in the enhancement of the mechanical, thermal (glass transition, melting and degradation temperature) and barrier properties by increasing path length for gas diffusion, changes in surface wettability and hydrophobicity and so forth. For food packaging they may offer antimicrobial activity, oxygen scavengers, enzyme immobilization, biosensing and so forth. Nanocomposites usually represent significant changes in properties at low loads <5 wt % of nanofillers and <2% volume. Also, nanocomposites improve the stability of sensory properties, such as flavour, better maintenance of colour and texture, increased product stability through the food chain and less spoilage. It is well-known that the interfacial region in nanocomposites is extremely large, therefore the interaction of the polymer with the nanoparticles is strong and this will change the polymer mobility and relaxation dynamics, decreases chain mobility due to nanomodification and that means an increase in Tg [23].

Nanocomposites may improve both thermal and environmental dimensional stability. Two factors are considered responsible for improving the thermal stability in thermoplastic nanocomposites with

respect to the neat matrix: (i) the chemical composition and morphology of the nanocomposites is different from that of the pristine polymer; (ii) the thermal motion of the polymer molecules is restricted by the filler nanoparticles. Incorporation of nanofillers in thermoplastics usually led to a marked increase in the melt viscosity, especially in the range of low frequencies.

Several types of polymer nanocomposites are known depending on the nanofiller used as mentioned above. Examples include UV absorbers to prevent UV degradation of plastic polymers (e.g., nano-titanium dioxide, iron oxides, silica, alumina), titanium nitride (TiN) used to improve the strength of materials, nano-calcium carbonate-polymer composites, biodegradable starch and/or polylactic acid with various nanoclay composites, gas barrier coatings and so forth [24–28].

2.1. Preparation Methods

The preparation methods for polymer nanocomposites should assure a good dispersion of nanofiller into matrix to obtain intercalated or exfoliated structures [29–33]. The exfoliated nanocomposites are also classified as ordered and disordered exfoliations. Partial exfoliation is an intermediate morphology between intercalation and exfoliation. Significant variations in physical and mechanical properties of polymer nanocomposites are directly correlated with the differences in morphology [34].

There are two main strategies to obtain nanostructures and consequently polymer nanocomposites and nanocoatings—Table 1—so called “top down” or *ex situ* synthesis (attachment of nanoparticles to the polymer matrices prepared into different step) and “bottom up” or *in situ* synthesis methods (e.g., *in situ* polymerization, spin coating, casting) [35]. In the “top-down” approach the nanoparticles are produced in a separate step and then they are dispersed in polymer (direct mixing of the filler into a polymeric matrix, ball milling and application of severe plastic deformation.), melt, or monomer solution which is then polymerized or nanostructures are generated by mechanical disintegration (milling) of the previous prepared material. In the “bottom-up” approach, the nanostructures are built up in a chemical process consisting in generation of nanoparticles inside polymer matrix or monomer polymerizing solution by chemical, thermal or photolytic decomposition of some precursors. Bottom-up approaches may be in gas-phase or in liquid phase such as: sol-gel processing, chemical syntheses, spraying, plasma or flame sputtering, spinning to make thin polymer fibres, chemical vapour deposition (CVD), laser pyrolysis, atomic or molecular condensation, electrodeposition, supercritical fluid synthesis, and so forth [36], while among the top-down techniques it is possible to include the energetic mechanical milling, sonication and so forth.

The preparation method determines both the concentration and distribution of the nanofillers and nanoreinforcements into the polymer [37].

The *in-situ* polymerization technique was widely used to obtain different kinds of nanocomposites such as those based on poly (vinyl acetate), nylon 6, *in situ* synthesis of poly(urethanes) PU in *in dimethylformamide* (DMF), emulsion polymerization of styrene in water and many others [38,39].

Solution mixing or *solvent casting* involves the vigorous stirring or ultrasonication of the nanoparticles in a polymer solution before casting in a mould and then evaporating the solvent. Both water and organic solvents can be used to prepare nanocomposites with either thermoplastics or thermosets. The removal of organic solvent after casting has environmental implications. The polarity of the solvent is a critical characteristic which influences the intercalation of the polymer into the space between the clay platelets. Nanocomposites are prepared by *emulsion polymerization* of acrylates in silica sols. By using this technique, it is possible to achieve a homogeneous distribution of silica nanoparticles into polymer at silica content up to 50% in the nanocomposites.

Table 1. Methods for preparation of polymer nanocomposites.

Method	Method to Obtain Nanocomposites	Results
In situ polymerization: emulsion and miniemulsion polymerization	dispersing fine nanofiller and nanoreinforcement in a monomer	monomers interact with the nanofiller surface and form a uniform suspension
Solution casting and latex method or solvent processing	1. filler dispersal in the polymer solution 2. solvent evaporation 3. freeze-drying and hot-pressing 4. freeze-drying, extruding and hot-pressing the mixture. 5. surfactant addition 6. grafting of long chains onto nanofiller surface	sandwiched multilayer structures forming of filler-rich layers polymer polarity-based results The dispersion of nanoparticles in the nanocomposite film strongly depends on the processing technique and conditions
Direct addition/extruder Blending, melt processing Shear mixing	1.addition of filler directly into the melted polymer 2. blending either by (mechanical mixer and extruder)	target: to obtain uniform distribution of the nanofillers in a polymer matrix
Deposition or layer (LBL) assembly	Layer-by-layer deposition	sequential substrate dipping in clay and polycation solutions were adopted to make the coating Multilayer films
Dispersion and chemical reaction	UV-curing in presence of photo-initiator; casting, evaporating the solvent	cross-linked nanocomposites
Electrospinning	development of electrospun nanofibers	nanofibres with different morphologies

At industrial scale of the *extrusion* or *melt processing*, the compounding of the components of a nanocomposite material is performed in a single or twin-screw extruder where the mixture of polymer and the nanofiller is a melt state. The shear and elongational stress applied with mixer during process help to break the filler agglomerates and uniformly dispersing them into the polymer matrix. As end products, films and other items can be formed from blend by profile injection moulding, extrusion, blow moulding. The intrinsic lack of thermal stability of many active/bioactive compounds which can be lost through degradation and evaporation during the heat transfer and high shear that also could degrade both the polymer and the nanofillers (as carbon nanotubes) limit the applicability of this preparation method. The homogeneous distribution of active agents into matrix is difficult. Processing at high shear or sonication techniques are used to deaggregate or exfoliate the clusters and to increase the surface area exposed to the polymer. Polymers able to interact with nanofillers give a good dispersion.

Shear mixing: Low-shear mixing or high-shear mixing can be used for incorporating solid nanoparticles into a liquid polymer. Under these conditions and if the nanoparticles are compatible with the selected polymer, the mixing will disrupt the nanoparticle aggregates and disperse the polymer matrix into the nanoparticle layers or onto the nanoparticle surfaces. The dispersion degree of the nanofiller and the filler/matrix interaction can be generally improved by (i) using surface-treated filler to reduce aggregation phenomena and (ii) incorporating a compatibilizer or a tensioactive agent within the polymer matrix (such as maleic anhydride grafted polypropylene).

LBL and electrospinning techniques are described in the nanocoatings section.

2.2. Types of Polymer Nanocomposites Used in Food Packaging

Some types of nanocomposites used in food packaging are given in Table 2 [12,33].

2.2.1. Montmorillonites (MMT) Containing Nanocomposites

The polymer–clay morphologies are classified in (1) tactoid, (2) intercalated and (3) exfoliated. In the *tactoid structures* due to the poor affinity of nanoclay with the polymer, the interlayer space of the clay gallery will not expand, the components do not mix each other and nanocomposites are not formed. In *intercalated structures* a moderate affinity between polymer and clay exists hence they are characterized by moderate expansion of the clay interlayer but the shape remains unchanged, polymer chains are able to penetrate the basal spacing of clay, mixing of components being homogeneous.

A high affinity between polymer and nanoclay promotes separation of the clay clusters into single sheets within the continuous polymer matrix resulting a homogeneous dispersion as the *exfoliated structures* which determine important changes in properties of the nanocomposites in respect with those of neat polymer.

Generally, MMT behaves as an effective reinforcement/filler, offering a high surface area and large aspect ratio. However, in many cases the compatibility with the matrix should be improved both by organophilization of the filler, the use of surfactants or compatibilizers. By these ways better exfoliated structure and better mechanical properties are achieved for nanocomposites. Clay layers constitute a barrier to gases and water, forcing them to follow a tortuous path, nanocomposites showing improved oxygen and water vapour barrier properties and some of them as Cloisite 93A, Cloisite 30B and Dellite High Pressure Sodium HPS offer also antimicrobial activity against both Gram-positive and Gram-negative bacteria, excepting fungus *Candida albicans* [40]. In many cases the mechanical properties are improved, glass transition and thermal degradation temperatures increase but some nanoclays decrease transparency of the films [12].

Table 2. Some examples of nanofillers intended to be used in nanocomposites for food packaging (for many examples see also recent reviews on this subject [41–44]).

Type of Nanofiller	Matrix	Preparation	Properties/Applications	Ref
Organoclay	LDPE and HDPE	melt mixing using PE grafted with maleic anhydride as compatibilizer-exfoliation	oxygen permeability of PE decreases gradually with the clay concentration, reaching a maximum reduction of ~30% for 15 wt % MMT; dynamic moduli increase showing pseudo solid-like behaviour at clay concentrations higher than 8 wt %.	[45]
Nanolayers of Nanotex™ from NanoBioMatters LTD Spain	PE	melt processing	very good barrier properties	[46]
4% MMT	EPDM	melt processing	decreased N ₂ permeability by 30%	[46]
Bentonite	PLA	solution casting	improve strength and modulus; decreased elongation at break	[47]
5% MMT	PVOH	casting	90% reduction in water permeability retaining optical clarity	[46]
MMT	proteins and polysaccharides	casting	60% reduction in water permeability	[46]
1.1%–4%–10% Various unmodified and organically modified MMT, Cloisite 25A, Nanotex™	PLA, PCL, PHA, PHBV Strach	monolayer packaging	reduction of oxygen and water permeability	
MMT	chitosan films	solvent casting	exfoliated and intercalated structure depending on MMT amount, tensile strength of a chitosan film was enhanced and elongation-at-break decreased	[48]
MMT	poly (ε-caprolactone) (PCL)	electrospinning	improved mechanical properties even elongation at break	[49]
Anionic sodium MMT exfoliated	cationic polyacrylamide on a PET substrate	Layer-by-layer (LbL) self-assembly multilayer film	oxygen transmission rate (OTR) decreased as a function of number of bilayers deposited, until a negligible value—below 0.005 cm ³ (m ² /day atm)—for a 30-bilayer film, microwaveable and with a good optical transparency (higher than 90%), it was presented as a good candidate for aluminium foil replacement in food packaging	[50]
5% Clay ZnO stabilized with sodium carboxymethylcellulose	thermoplastic starch; gelatinized starch film; glycerol plasticized-PEA starch	melt extruded	improve the mechanical strength of biopolymers, decreased water vapour permeability by using only 5% (w/w) of clays; the highest exfoliation and best improvement in mechanical properties, exfoliated clay.	[51,52]

Table 2. Cont.

Type of Nanofiller	Matrix	Preparation	Properties/Applications	Ref
1 wt % and 5 wt % of modified (surfactant-modified) and un-modified cellulose nanocrystals,	PLA	solvent casting method in the presence of surfactant	reductions of 34% in water permeability for the cast films with 1 wt % of surfactant modified-CNC; good oxygen barrier properties; the migration level of the studied nano-biocomposites was below the overall migration limits required by the current normative for food packaging materials in both non-polar and polar simulants.	[53]
Up to 3% cellulose nanocrystals CNCs	PLA	extrusion, twin-screw extruder	water vapour permeability decreased gradually with increasing addition of CNCs up to 3%; good oxygen barrier properties; enhanced barrier and mechanical properties	[54]
Cellulosic nanoparticles in chloroform and layered silicates; whiskers	PLA		An improvement in storage modulus over the entire temperature range for both nanoreinforcements together with shifts in the tan delta peaks for both nanoreinforcements to higher temperatures; reduction in the oxygen permeability for the bentonite nanocomposite but not for the MCC nanocomposite. The amount of light being transmitted through the nanocomposites was reduced compared to pure PLA indicating that both nanoreinforcements were not fully exfoliated	[47,55]
cellulose whiskers extracted from IPEA hull fibres with different hydrolysis times, which resulted in different aspect ratios.	PEA starch matrix		The composite produced by using the whiskers with the highest aspect ratio exhibited the highest transparency and best tensile properties; enhances thermomechanical properties, reduces the water sensitivity and keeps biodegradability; Tg increases; moisture resistance improved	[56,57]
cellulose whiskers	PVOH	solution casting, water solvent casting	the modulus increased by orientation of reinforcement under magnetic field	[58]
cellulose nanowhiskers	k/l carrageenan	casting	high crystallinity, enhanced water barrier of carrageenan	
	PLA	casting	improved barrier properties to gases and vapours, fully renewable biocomposites for biopackaging	[59]
Bacterial cellulose nanowhiskers	EVOH or PLA	electrospinning	increased thermal stability	
Bacterial cellulose nanowhiskers	EVOH	melt compounding	enhanced barrier and mechanical properties of EVOH	

Table 2. Cont.

Type of Nanofiller	Matrix	Preparation	Properties/Applications	Ref
30 wt % of Straw cellulose whiskers	poly(styrene-co-butyl acrylate) latex film	freeze-drying and moulding a mixture of aqueous suspensions	modulus more than a thousand times higher than that of the bulk matrix	[60]
Aqueous suspensions of polysaccharide (cellulose, chitin or starch) nanocrystals tunicin (the cellulose extracted from a tunicate—a sea animal) whiskers, wheat straw or sugar beet cellulose nanocrystals, potato starch nanocrystal and squid pen and Riftia tubes chitin whiskers	hydrophobic polymers as: styrene and butyl acrylate [poly(S-co-BuA)] poly[β-hydroxy-octanoate] (PHO) polyvinylchloride (PVC), waterborne epoxy, natural rubber (NR) and polyvinyl acetate (PVAc), poly(styrene-co-heptyl acrylate)	dispersion of these nanocrystals in non-aqueous media is possible using surfactants or chemical grafting; long chain surface chemical modification; mixing and casting the two aqueous suspensions; freeze-drying and hot-pressing or freeze-drying, extruding and hot pressing; mixture extrusion and hot pressing; mixture emulsion polymerization	films; larger latex particle size results in higher mechanical properties	[30]
aqueous suspension of polysaccharide nanocrystals	hydrosoluble or hydrodispersible polymers as: reinforced starch, silk fibroin, poly(oxyethylene), polyvinyl alcohol, hydroxypropyl cellulose, carboxymethyl cellulose or soy protein isolate	mixing and casting the aqueous solutions, freeze-drying and hot-pressing		
starch nanocrystals	waterborne polyurethane	solution casting; chemical grafting of starch nanocrystals	enhanced strength, elongation and Young's modulus. The chemical grafting of the starch nanocrystals onto SBNs did not affect positively the strength and elongation, because such a treatment inhibited the formation of physical interaction and increasing network density in nanocomposites	[61]
Coating of cotton and tunicin whiskers by a surfactant phosphoric ester of polyoxyethylene (9-nonyl phenyl ether leads to stable suspensions in toluene and cyclohexane or chloroform	atactic polypropylene, isotactic polypropylene, or (EVA)	dispersion in non-aqueous medium, casting	decreased mechanical properties	[62,63]
Chitin whiskers	protein isolate thermoplastics	solution-casting technique	improved not only the tensile properties (tensile strength and elastic modulus) of the matrix but also its water resistance	[64]
chitin whiskers	chitosan films	solution-casting technique	improved chitosan films tensile strength until a whisker content of 2.46%, while higher increases of whiskers contents resulted in decreasing strength. Improved water resistance of the films.	[65]
chitosan-triopolyphosphate (CS-TPP) nanoparticles	hydroxypyropyl methylcellulose (HPMC) films	solution-casting technique	improved mechanical and barrier properties of the films	[66]
carbon-based graphene, 20 to 60 nm in thickness and 0.5 to 25 µm in diameter, at 1 to 5 wt % loading	Poly(methyl methacrylate) (PMMA)	dispersion at 30 °C by high speed shearing methods	heat resistant, high barrier nanocomposites promising in food packaging, increase the glass transition temperature of PMMA	[67]

MMT containing nanocomposites show many advantages in respect of neat corresponding polymeric matrices; they are lighter, stronger, more heat-resistant, offer improved barrier against gases, moisture and volatiles materials, antimicrobial properties and so forth. They are produced by Nanocor Inc. (Arlington Heights, IL, USA) and Southern Clay Products, Inc. (Gonzales, TX, USA), Mitsubishi Gas Chemical (New York, NY, USA) and other units using as matrices Nylon-6, PE, PET and EVOH. Films, PET bottles and multilayer films from nanocomposites are obtained to prolong the shelf life of a variety processed meats, cheese, confectionery, cereals and boil-in-bag foods and so forth [8,68,69].

2.2.2. Bionanofibrils

Biopolymer nanofibrils with dimensions of angstrom to hundreds of nanometre scales arise from renewable resources, are widely available at low-cost, offering exceptional biocompatibility, biodegradability, flexibility and the availability of multiple reactive sites for introducing novel functionalities. Because of the natural origin and well-defined supramolecular assemblies and geometries they exhibit exceptional mechanical properties mainly a unique combination of strength and toughness. Their biological functions allow the interactions with the surrounding environment performing a variety of specific functions in living systems and also serving as building blocks stabilized by non-covalent interactions in material science. The nanofibrillar biopolymers are potential candidates for high-performance and functional bionanocomposites as strong, sustainable, stimuli responsive and biocompatible materials for a wide range of applications such as environmental, energy, food packaging, optical and biomedical [70,71]. The combination of biological and synthetic components frequently shows synergistic effects because of strong interfacial interactions that significantly enhance the structural performance and facilitate added functionalities of nanocomposites. In some bionanocomposites, novel synthetic nanoparticles (graphene, carbon nanotubes, mineral nanoparticles, metallic nanoparticles and so forth) were efficiently combined with biological components to achieve superior electrical and thermal conductivity, controlled gas barrier properties, complex actuation and unique optical properties [72]. The biopolymer nanofibrils as cellulose nanofibrils (CNF), chitin nanofibrils (ChNF), silk nanofibrils (SNF) and collagen nanofibrils (CoNF) are most abundant nanofibrils in nature. The nanocellulose and silk nanofibrils, are representatives of classes of polysaccharides and polypeptides [73].

Both top-down and bottom-up strategies have been developed to exfoliate and regenerate bionanofibrils.

Nanocellulose is a term referring to nano-structured cellulose. This may be either cellulose nanocrystal (CNC), cellulose nanofibers (CNF) also called microfibrillated cellulose, or bacterial nanocellulose, which refers to nano-structured cellulose produced by bacteria (BC). They are renewable abundant raw materials derived from wood and plants. As biodegradable fibre-reinforcement for polymeric bionanocomposites, they also offer excellent tensile properties, non-toxicity, high thermal conductivity and optical transparency as indispensable requirements for advanced food packaging.

Cellulose-based nanoreinforcements (as cellulose microfibrils or nanofibers and microcrystalline cellulose). Cellulose microcrystals may contain also amorphous areas. Nanofibres have nanosized diameters (dimension range of 2–20 nm, depending on the bionanofibril origin) and lengths in the micrometre range. Whiskers are crystalline parts and are known as nanocrystals, nanorods, or rod like cellulose microcrystals with lengths ranging from 500 nm up to 1–2 µm and about 8–20 nm or less in diameter and high aspect ratios. Microcrystalline cellulose has 200–400 nm in length and an aspect ratio of about 10 [12]. Their dimensions affect the properties of nanocomposites. Nanocellulose can be extracted via enzymatic pre-treatments, tempo oxidation and chemical extraction, while CNC are extracted generally via acid hydrolysis with sulfuric acid [74–76].

Polysaccharide nanoparticles as aqueous suspensions hydrosoluble (or at least hydrodispersible) or latex-form polymers are obtained. The dispersion of nanocrystals into non-aqueous media is also possible using surfactants or chemical grafting. These are other possibilities for processing of the nanocomposites. The surface of the polysaccharide nanocrystals is covered with reactive hydroxyl

groups, which provide the possibility of their extensive chemical modification using grafting agents bearing a reactive end group and a long compatibilizing tail [30]. The surface chemical modification of the cellulose biofibres leads to improved interfacial adhesion between the fibres and the matrix, resulting in enhanced mechanical properties and thermal stability. CNC coatings are also transparent, nontoxic and sustainable. CNCs are highly crystalline and easily dispersed in water, therefore the structure can be controlled to eliminate free volume and to improve barrier properties of the materials. They offer to coatings a higher density and packing that reduces diffusion pathways and drastically improves oxygen, carbon dioxide and water vapour permeability properties which are similar with those of EVOH commercial food packaging material. Their use is also associated with biodegradability and sustainability [77]. *Bacterial cellulose (BC) nanofibrils* randomly-oriented as web-like form show full potential as reinforcement. To orient the nanofibrils a controlled stretching of BC hydrogel was performed by Rahman and Netravali [78,79]. They obtained a BC-reinforced soy protein soy protein isolate (SPI) by vacuum-assisted SPI resin impregnation into BC hydrogel and then stretching the resin impregnated BC hydrogel. Aligned BC nanofibrils were produced by cultivating them inside polydimethylsiloxane (PDMS) tubes followed by wet-stretching. Due to higher BC nanofibrillar orientation, the stretched BC-SPI green composites showed significant improvement in their tensile properties. Cellulose nanofibrils were produced from commercial bleached cellulose pulps after 30 passages in a SuperMasscolloider Grinder (MASUKO SANGYO CO., Kawaguchi, Saitama, Japan), or using mechanical processes [80]. Films were prepared by a casting method. BC-reinforced PLA showed enhanced barrier and mechanical properties [81].

Hybrid nanocomposites, where two different nanoparticles CNC/metallic nanoparticles CNF/clay and CNC/clay) are incorporated into the polymer have been also obtained. [82] PLA-based nanocomposites with CNF, 1–5% nanocrystalline cellulose (CNC) and 1–5% nanoclay (CloisiteTM 30B) for food packaging use led to up to a 90% reduction in the oxygen transmission rate (OTR) and 76% reduction of water vapour transmission rate (WVTR), significant increase in thermomechanical resistance and increased crystallisation kinetics. [83,84] The incorporation of nanoparticles will increase the tortuosity within the material and that this increases barrier properties.

The corona treatment leads to the quality improvement of fabrics and composites. It was applied with good for surface modification and physical and mechanical properties of nanofibril containing films useful for printing and packaging materials such as eucalyptus and pinus nanofibril films [85]. After the corona discharge and subsequent exposure to oxygen from air hydroxyl, carbonyl and other functional groups are formed by breaking C-C bonds and interaction with active species from plasma (see below). After such treatment, the Eucalyptus nanofibril films showed increased tensile strength due to their higher crystalline index and nanofibril dimensions.

Chitin nanofibrils were directly extracted from crab shells through a green deprotonation-assisted liquid exfoliation procedure. By aqueous re-dispersibility after freezing/air/thermal drying, hybridization with other two-dimensional nanomaterials, (e.g., graphene and transitional metal dichalcogenides) was performed. Plasticized PLA with 1 and 5 wt % chitin nanocrystals (ChNC) nanocomposite after orientation, showed a ‘shish-kebab’ morphology in the drawn tapes. Singh et al. reported improved mechanical and thermal properties. The tensile strength increased and the elongation at break increased from 5% to 60% for the nanocomposite with 5 wt % ChNC and a draw ratio of 3 because of the synergistic effects of the ChNC in the nanocomposite and their alignment of the ChNC together with the polymer chains induced by the solid-state drawing [86].

Silk fibres. A variety of artificial spinning methods have been applied to produce regenerated SNFs. Ling et al. developed a bioinspired spinning method [87]. They prepared nematic silk microfibril solution, highly viscous and stable by partially dissolving silk fibres into micro-fibrils. The hierarchical structures in natural silks was maintained in solution which was spun into regenerated silk fibres by direct extrusion in the air. In this way, polymorphic and hierarchical regenerated silk fibres with physical properties beyond natural fibre construction were generated. By further functionalization

with a conductive silk/carbon nanotube coating, responsive materials to changes in humidity and temperature can be produced.

The following surface modification were applied: Poly (ethylene glycol) PEG-grafted rod-like cellulose microcrystals [88], alkenyl succinic anhydride acylating the surface of cellulose nanocrystals, crab shell chitin whiskers [89], waxy maize starch nanocrystals [90] and tunicin whiskers used then to reinforce some plastics [91,92] their performance depending on type of matrix.

Starch nanocrystals show platelet morphology with thicknesses of 6–8 nm. Their incorporation lead to improve some properties of PVOH [93] and pullulan [94].

2.2.3. Other Types of Nanofillers

Carbon nanotubes (CNT). Tensile strength/modulus of PVOH [95], PP [96], PA [97] are improved by addition of CNTs.

Silica nanoparticles ($nSiO_2$) improve mechanical and/or barrier properties of PP [98], mainly when maleic anhydride grafted polypropylene (PP-g-MA) is used as a compatibilizer [99], of PVOH [100] or of starch matrix [101].

Halloysite (HAL) represents a class of natural, non-toxic, non-swelling silicates, stable even at very high temperatures and show a good encapsulation and release capacity for bioactive compounds (anticorrosion, antimicrobial, drugs, flame retardant, microcrack self-healing). They have a wide variety of applications including also as fillers and reinforcements for polymers. The HAL particles can adopt a variety of morphologies, as elongated tubules known as halloysite nanotubes (HNT), short tubular, spheroidal and platy particle shapes, the first one being the most common [102]. HAL can be incorporated into different polymers to obtain non-degradable and degradable nanocomposites with versatile properties some of them being attractive for potential uses in food packaging [103]. The HNT-incorporated polymer nanocomposites can be prepared by various processing routes such as melt blending, melt spinning, water-assisted extrusion process, methods involving hydrogen bonding and charge transfer mechanism, solution casting, co-coagulation or co-curing processes, in situ or emulsion polymerization techniques for nondegradable nanocomposites and solution casting, coagulation, electrospinning for HNT-containing degradable nanobiocomposites. HNTs containing nanocomposites exhibit remarkable mechanical performance and their properties can be tailored by HAL surface modification [104], by nanocomposites composition and by the preparation methods optimization. HAL nanofillers act as ethylene gas absorbers. This gas causes softening and aging of fruits and vegetables; limits the migration of spoilage-inducing gas molecules within the polymer matrix. Active food packaging materials as HNT/PE nanocomposite films showed higher ethylene scavenging capacity and OTR and WVTR than neat PE films. Due to their ethylene scavenging activity and good water vapour and oxygen barrier properties, the nanocomposite films slow down the ripening process of bananas and retain the firmness of tomatoes and also slowed down the weight loss of strawberries and aerobic bacterial growth on chicken surfaces. HNT/PE nanocomposite films contribute to food safety improving the quality and shelf life of fresh food products [105]. Starch/halloysite/nisin nanocomposite films inhibited activity of *Listeria monocytogenes*, *Clostridium perfringens* and *Staphylococcus aureus* in skinned milk agar being active and useful barrier to control food contamination [106]. HNTs loaded with lysozyme, as nano-hybrid antimicrobial was incorporated into a poly (ϵ -caprolactone) (PCL) matrix at 10 wt % and then the films were submitted to a cold drawn process. The films exhibit a controlled release of lysozyme being for specific active packaging requirements [107].

Graphene as atomically thin carbon sheets improve physical properties of host polymers at extremely small loading. Nanocomposites containing graphene are obtained by top-down strategies starting from graphite oxide, solvent- and melt-based strategies [108]. Such nanocomposites offer extremely high barrier performance at even very low graphene loadings, which is interesting for food packaging [109].

Metallic nanoparticle incorporated into food contact polymeric matrices enhance mechanical and barrier properties, prevent the photodegradation of plastics and are effective antimicrobials (as salts, oxides and colloids, complexes) such as AgNP [110]. Copper, zinc and titanium NP are also useful in food safety and technology. Copper is an efficient sensor for humidity and titanium oxide has resistance to abrasion and UV-blocking performance [111].

Lignin nanoparticles were tested for their antioxidant, antimicrobial activities and potential biological being effectively used as active agents towards different pathogen strains when is combined with PVA, chitosan CH, natural polymers and so forth [112,113].

Multifunctional nanocomposites contain usually a mixture of micro- and nanostructured materials such as essential oils, natural extracts and metal nanoparticles with antimicrobial/antioxidant agents/biological functions and they are also interesting for food contact materials.

2.2.4. Bioplastics–Biopackaging

Increased use of the synthetic packaging materials (as films, bottles, trays and so forth) has led to serious ecological problems due to their non-biodegradability and waste accumulation. Biopolymers derived from natural resources as plants (starch, cellulose and their derivatives, proteins), animal (proteins, polysaccharides) and microbial products, such as polyhydroxybutyrate have been extensively studied in the bio-based nanocomposites field [114] because of their good biocompatibility, degradability [115] and recyclability [116]. The starch-clay biodegradable nanocomposites were investigated for several applications including food packaging. Some restrictions are encountered on the use of biodegradable or natural polymers in food packaging since they have poor barriers and mechanical properties, high permeability to gases, such as oxygen and water vapour because of their hydrophilic nature with a few exceptions, such as caseinates, which show excellent barrier performance, even better than PET [117]. Nanoreinforcements can improve barrier properties and have a positive impact on the oxidation stability, thermal and mechanical characteristics and eventually bionanocomposites show the good biodegradability comparing with conventional polymeric matrices. Polymer cross-linking and graft copolymerization of natural polymers with synthetic monomers/polymers are other alternatives of promising values in biodegradable packaging. The complete replacement of synthetic polymers with degradable ones is almost impossible to achieve and even unnecessary, at least for specific applications the use of biodegradable polymers is desirable. No doubt, In the future biopackaging will be increasingly developed [46,118].

Protein-based nanocomposites. In commercial applications, the following animal derived proteins used are: casein, whey protein, collagen, egg white and fish myofibrillar protein. The plant-based proteins also under large scale application consideration include soybean protein, zein (corn protein) and wheat gluten. Compared with non-ionic polysaccharide films, protein films, due to their more polar nature and more linear (non-ring) structure and lower free volume offer better oxygen barrier properties and lower water vapour permeability [119]. The transparent films based on whey protein show good oxygen barrier and TiO₂ or ZnO were added to form nanocomposites with improved antimicrobial properties [120–122] used to fabricate food-grade, biodegradable packaging materials. Chen et al. and Yu et al. showed that the addition of small amounts (<1 wt %) of TiO₂ nanoparticles significantly increased the tensile properties of whey protein film (from 1.69 to 2.38 MPa). Soy protein nanocomposite films exhibited reduced water vapour permeability, improved elastic modulus and tensile strength compared with neat polymer [123,124]. Zein as biodegradable polymer is used in the food industry as a coating agent [125]. It is less water sensitive than other biopolymers but shows high water vapour permeability and low tensile strength when compared with commodity polymers. To ameliorate its inherent brittleness, plasticizers may be used.

2.2.5. Degradability and Recyclability of Nanocomposites

Bionanocomposites (BNC) can be recycled/valorised or treated together with other organic wastes in composting facilities and produce compost, as valuable soil conditioners and fertilizers

and so forth [126]. They are high-performance biodegradable materials, based on plant, animal and other natural materials, therefore these are safely decomposed into CO₂ consumed during plant photosynthesis, water and humus through the activity of microorganisms [127]. This behaviour refers to with BNC with degradable polymeric matrices like poly(lactic acid) (PLA), poly(butylene adipate-co-terephthalate) and thermoplastic starch which undergo degradation after various time period. Different biodegradation conditions can be considered: hydrolytic, composting, enzymatic, according to the final applications and the post-use of the new developed materials [128].

Combining the individual advantages of starch/synthetic or natural polymers and nanoparticles (cellulose nanocrystals, clay, TiO₂, layered silicate and so forth) starch-based completely biodegradable materials with potential applications in food industry as edible films were prepared. [129].

The effect of the nanofillers on degradability and compostability of bioplastics depends on their type. PLA/Laponite biocomposites showed the greatest microbial attachment on the surface (biofilm is formed), while PLA/ organo-montmorillonite (OMMT) had the lowest biofilm formation because of the inhibitory effect of this NP during biodegradation test. Nanoclays influence the polymer bacterial degradation due to the affinity of the bacterium towards clay. The addition of nanoclays during composting process increases the PLA degradation rate due to the presence of hydroxyl groups from the silicate layers of these clays. As an example, due to the hydrophilic nature of nanocellulose, the cellulose nanocrystals (CNCs) increased the disintegrability rate of PLA.

PLA bio-nanocomposite films containing nanoclay with organo-modified (with methyl, tallow, bis-2-hydroxyethyl, quaternary ammonium montmorillonite), Halloysite nanotubes and Laponite® RD, MMT showed a significantly higher mineralization of the films in comparison to the pristine PLA, mainly attributed to the reduction in the PLA lag time. PLGA/CNT films were degraded by hydrolytic degradation [130]. CNTs insignificantly modifies the kinetics and the mechanism of the hydrolytic erosion with respect to the neat PLGA, while CNTs functionalized with carboxylic groups accelerated the hydrolytic degradation and the weight loss of the PLGA matrix of the nanocomposites.

MWCNTs reduce the biodegradation rate of PCL in the presence of *P. aeruginosa*, systematically as the CNT loading increased from 0.1 to 10% w/w [131].

3. Polymer Nano-Coatings in Food Packaging

A coating is defined as a coherent layer formed from a single or multiple applications of a coating material to a substrate. Nanocoatings are ultra thin layers on the nanoscale <1–100 nm thick built-up onto surfaces [132,133]. Nanocoatings do not modify the surface topography, they do not fill in defects or make a smooth surface like a paint does, and they also do not stand up to abrasion and wear. They are used to impart a particular chemical or physical function(s) to a surface as gas-barrier coatings, hydrophilic/hydrophobic or oleophobic properties, improve corrosion resistance and enhance insulating or conductive properties [134].

Nanocoatings can be built up with thickness of one molecular or multiple molecular layers. Nanocoatings are applied to various substrates such as metals, glass, ceramics, polymers and so forth (Figure 2) [135,136]. Some nanocoatings are polymers, either polymerized in-situ or prior to application. “Smart coatings” are coatings with multifunctional additional functions some also assuring thermal insulation, controlled release of active ingredients or self-healing functions.

Additives are added to a coating material in very small quantities. They can modify a large variety of properties, for instance, flow behaviour, surface tension, gloss, structure, UV and weather resistance. Depending on the desired function, nanotechnology-based functional coatings uses some nanomaterials as in the case of antimicrobial coatings containing silver, titanium dioxide, zinc oxide, some organic bioactive agents as polysaccharides, proteins, spice and herb extracts as essential and vegetable oils, bacteriocins (ex: Nisaplin®, nisin, pediocins), organic acids for food packaging or hygienic surfaces. Nanomaterial-containing coatings offer high performance materials and better processing properties than conventional coatings (e.g., increased indentation resistance, high elasticity, fast drying, no expansion after contact with water, high water vapour permeability).

3.1. Types of Nanocoatings

Several types of nanocoatings are known in food packaging applications as: nanocoating inside package, outside package, sandwiched as a layer in laminated multilayer packaging films, polymer with nanocoating with high barrier properties, edible coatings and films on a wide variety of foods which serve as moisture, lipid and as gas barriers [137], vacuum deposited aluminium coatings on plastic films, coating of the surfaces of glass food and beverage containers (bottles, jars) with organosilanes, nanosurface biocides and so forth

Nanosilica-coated films onto PET, Nylon and so forth, replace polyvinylidene fluoride (PVDF) coated films and oxide evaporated films, for processed meat products (beef meta, sausage, ham and so forth, fresh food like rare fish, sushi, dried fish and so forth, bakery, sandwiches, snack, candy, nut products with high fat) and so forth [28], offering oxygen and moisture barrier and aroma preservation increased self-life and decreased production cost, good printability and laminating machinability, are eco-friendly, no dioxines are formed during incineration, excellent mechanical and optical properties (retaining bulk properties of base film).

Nano surface biocides (using as nanoparticles: nanosilver as metallic Ag, AgNO₃, ZnO, TiO₂, MgO) are obtained by incorporation such nanomaterials with antimicrobial properties onto packaging surface. Such food contact nano surface containing biocides maintain the hygienic conditions when applied to reusable food containers such as boxes and crates and inside liners of refrigerators and freezers.

The most known coating technologies are immobilization using covalent (non-migratory) and non-covalent (migratory), layer-by-layer deposition, photografting chemistries and embedding for controlled release, schematically represented in Figure 2 [135–140].

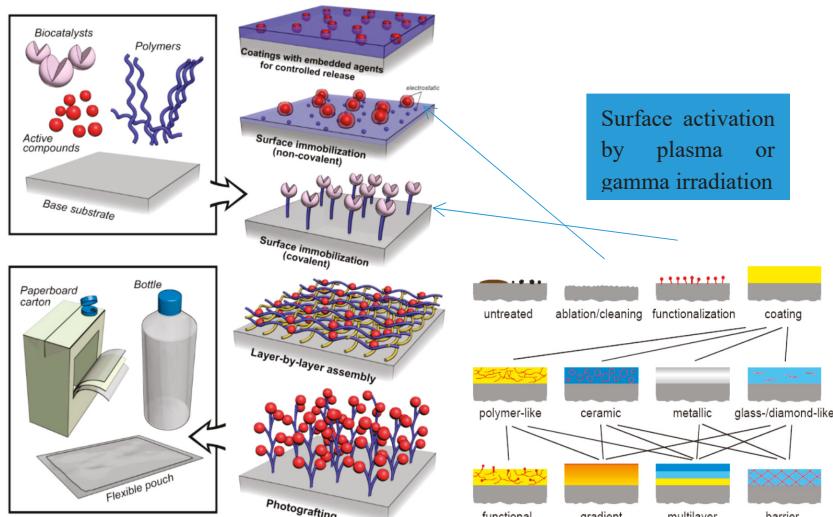


Figure 2. Summary of coating technologies (adapted from [135–140]).

In coating technology which uses the embedded agents for controlled release, the active agent is intended to migrate to the packaged good (embedding, non-covalent immobilization, some layer-by-layer deposition techniques) while in non-migratory technologies, the active agent is intended to remain stable in the packaging matrix (in covalent immobilization, some layer-by-layer deposition techniques, photografting). Some techniques to prepare nanocoating are similar with those for nanocomposites obtaining, some are adapted and other are specific for this purpose. In some

cases, the nanocoatings application required specialized equipment and complex procedures, such as, chemical vapour deposition or plasma spray techniques.

The active agents are expected to migrate and exert their specific antimicrobial, antioxidant, biocatalytic, or nutraceutical functions within a packaged food. Active compounds are incorporated into polymeric materials by extrusion/blending and pip-coating techniques or solution casting.

3.2. Coatings Procedures

3.2.1. Solution Casting

Solution casting consists of dissolving the polymer in a suitable solvent and simultaneously incorporating the active compound of interest, followed by pouring this mix solution onto an inert surface. By the solvent evaporation, the films with desired functionality (antimicrobial, antioxidant, pharmaceutical, biocatalytic and so forth) result. It is mainly used at laboratory scale and can be translated at industrial scale by coupling with a wet-coating station and roll-to-roll system [141]. However, it has some limitations both for practical and commercial application because the most of the interesting polymers used in food packaging dissolve only at high temperatures and in certain organic solvents [142], which will affect both the stability and effectiveness of many active/bioactive compounds of interest. Therefore, the incorporation of active compounds through solution casting has mainly applied when biodegradable polymers dissolved at milder temperatures, such as poly(lactic acid), poly(butylene adipate-*co*-terephthalate) and cellulose derivatives, PVOH and so forth [143]. Butnaru et al. obtained films by casting and dried in a vacuum oven with controlled temperature using solutions of highly viscous chitosan from crab shells where food grade vegetable oils (clove, thyme and rosehip seeds oils) were incorporated were homogenized by ultrasonication [144].

3.2.2. Extrusion

In commercial extrusion, the active compounds with polymeric materials in melted state, in a single or twin screw extruder by heat transfer where are incorporated a blend is obtained from which films can be formed. It also has serious limitations due to the intrinsic lack of thermal stability of many active compounds as it was already mentioned above, which can be lost either through degradation and evaporation. During the heat transfer involved in these unit operations the homogeneous distribution of active agent into matrix is difficult. The active compound release is controlled by packaging material characteristics such as the degree of affinity between it and the matrix, morphology and porosity and also by medium temperature. Multilaminated system in which the layer that harbours the active compound is covered by an adjacent layer could act as a barrier slowing release rate. In such case the bulk properties as tensile and thermal are changed therefore the coating technique is preferred.

3.2.3. Sol-Gel Procedure

Sol-gel procedure is extensively used in obtaining of nano-based coatings. A viscous colloidal-sol is applied to a surface by dip, spray or spin coating processes onto surface. The thickness of the obtained layers varies from a few nanometres thick to 0.5 and 3 μm . The process occurs at low temperature, in a short time, is low energy consuming and more important without disruption of the structure or functionality of biocomplexes or organic aggregates, the nanocoating as a gel may exhibit a porous 3D network [145].

3.2.4. Spraying Solution with Compressor Gun

There several types of sparaying guns as manual and automatic spray guns with air compressors, etc. Manual spray guns are available in various configurations to suit a wide range of applications and processes. HVLP (high volume low pressure) gun offers the following advatages: the spraying is controllable, high transfer efficiency, can be used for a wide variety of materials, it is inexpensive to

maintain because needs a reduced preparation and clean-up, is portable, the material consumption is reduced by 40%.

Their applications are: painting, food industry, pharmaceutical, dyestuff coating, oil, lubricating, rubber solution spray, textile spray, water based materials/paints, etc.

They are already applied on a large scale both by individuals and industrially.

3.2.5. Surface Immobilization

Surface immobilization of the bioactive compounds was performed for a wide range of inert hydrophobic packaging polymeric materials. Surface modification of polymers can be performed either by physical, chemical (wet) or biological methods. Physical methods are preferred over chemical techniques because they offer greater precision, ease of process control and environment friendliness. Classical physical methods for modifying polymer surfaces include flame and corona treatment, ultraviolet light, gamma-ray, ion-beam techniques, low-pressure plasma and laser treatment. Physical methods either modify the surface layer or an extraneous layer is deposited on the top of the existing material—*coating*. The main advantage of plasma treatments is that the modification is restricted to the uppermost layers of the substrate, thus not affecting the overall desirable bulk properties. To achieve approximately similar surface modification, gamma irradiation should apply only in mild controlled conditions [146,147].

The physical methods are widely used due to their easier industrial scalability, no liquid reagents of any kind are needed in their application, thus is avoided the accumulation and handling of harmful waste [148]. The main effect of the surface activation methods is the formation of reactive species on the polymer surface like oxygenated groups as carbonyl, hydroxyl and carboxylic acid groups or nitrogen containing groups depending on discharge gas used in plasma device or after air exposure. On activated polymer surface bioactive compound can be either covalent or non-covalent immobilized Figure 2. Non-covalent way is based on electrostatic interactions when substrate and bioactive compound show opposite net charges, while ligand–receptor interactions, like in the case of biotin–avidin [149] are specific for affinity immobilization.

Covalent attachment/conjugation of bioactive compounds to functionalized polymer surfaces is realized by: hydrophilic, bifunctional, and/or branched spacer molecules. The main advantage of covalent immobilization is high stability of the formed layer and the active compound does not migrate into the packaged food product to affect its quality and safety. Active agents can be covalently linked directly to the polymer surface or by use of a spacer or crosslinker, which either share a permanent covalent bond between the polymeric substrate and the bioactive compound, or promotes covalent bond formation between the activated substrate and the bioactive compound without forming part of that link (“zero-length” crosslinkers). It can also perform optimization of the surface functionalization by using a polyfunctional agent, increased number of functional groups, tethering a bioactive compound to a solid substrate via a spacer molecule, covalently attach a bioactive compound to the functionalized polymer surface via an intermediary. The immobilization technologies are potential versatile as once functional groups are introduced to the polymer surface, a range of bioactive agents (e.g., enzymes, peptides) can be immobilized through standard chemical or bioconjugation techniques [150].

Plasma and gamma rays assisted nanocoating and immobilization. Plasma treatment and gamma irradiation are energetic processing methods that create reactive spots to which either oxygen- or nitrogen containing groups can be implemented on surface and functional groups and radicals are created depending on the type of discharge gas/atmosphere used inside reactors. The energy levels of entities generated in cold plasma are comparable to the bond energies of organic compounds and thus can facilitate surface functionalization reactions. The extent of functionalization can be controlled by selecting the discharge parameters [139]. On polymer surfaces three main effects can be obtained depending on the treatment conditions: a cleaning effect, an increase of microroughness surface and functionalization. According to the literature data acidic surfaces are obtained by O₂ and air plasma

activation of inert surface of synthetic polymers [151] and amphoteric surfaces are obtained by N₂ plasma activation [152,153], in all cases after exposure to air for the same period of time of about 1 min. Nitrogen containing functionalities originate from plasma treatment itself and also, very likely, from the post-reaction with the venting gas. The oxygen atoms are both in the form of alcohol (C-OH) or/and carbonyl (C=O) groups, epoxy groups and radicals, while the nitrogen atoms appear as amino (C-NH₂) groups. In order to develop new multifunctional active polymeric surfaces with special properties for food packaging applications based on inert polymer such as *polyolefins* or *polylactic acid* and *polyalkanoates*, the following solutions have been applied:

- a. Activation of polymeric substrates by non-solvent, environment friendly methods by using of gamma-ionizing radiation or cold plasma gas discharge.
- b. Stable layers have been deposited onto activated polymeric substrates using different coupling agents for covalent linking of active/bioactive formulations.
- c. Selected bioactive compounds were: chitosan/chitin, lactoferrin, vitamin E, natural vegetable oils with high content of antioxidant compounds as phenols or flavonoids mixtures.

Covalent grafting of bioactive compounds onto inert polymeric surfaces occurs by a two-step procedure:

Step I. Polymeric surface activation.

Surface activation techniques are applied in order to introduce the desired type and quantity of reactive functional groups which are able then to covalently attach a bioactive compound. The polymeric films/papers were exposed both to corona and to high-frequency plasma (air or nitrogen were used as discharge gas). The most important feature of irradiated polymers is the possibility of grafting for certain structures, because the radical sites are available for coupling. γ -exposure of polymeric films/papers was carried out in an irradiation machine at various irradiation doses from 2–30 kGy absorbed in air, at room temperature. Surface functionalization because of implementation of polar groups and radicals onto substrate surface provides desired changes in physical properties of the substrate surface (e.g., wettability, improved adhesion and biocompatibility, interaction with surrounding media) [154]. Although physical adsorption may be useful in some applications, covalent immobilization provides the most stable controllable bonds, between the bioactive compound and the functionalized polymer surface [155]. Optima conditions of activation by each method or compound to be linked were established by varying the exposure parameters and determination of the dependence of the surface wettability and morphology on these [146,147,156–162].

Step II. Covalent bonding/grafting of bioactive compound onto activated polymeric surfaces.

After the corona, plasma discharge or γ -irradiation pre-treatment, the polymer surface was enriched with oxygen-containing groups, such as carboxyl, carbonyl, hydroxyl, ester groups and/or nitrogen containing groups. The covalent attachment between a polymeric surface and an active compound is achieved by formation of amide, ether, ester and thioester bonds, created between the hydroxyl, amine, imine, carboxylic acid and thiol groups of the active compounds of interest which may possess intrinsically (or are incorporated in their structure) and the functional groups created on the substrate [156,157,163,164]. After cold plasma/ γ -ray exposure the polymeric films/fibres/papers were removed from the treatment chamber and then immersed into the bioactive compound solution (chitosan (CHT), grape seed oil, clove oil, etc.). The dipping/immersion, spreading or electrospinning/electrospraying of such solution onto activated surface lead to coat of the activated surface. For covalent bonding of CHT or other bioactive compounds onto activated surfaces, the Ethyl-3-[3-dimethylaminopropyl] carbodiimide hydrochloride) (EDC), -N-hydroxysuccinimide (NHS) or 1'-Carbonyldiimidazole (CDI) coupling agents were used.

Comparing various methods of chitosan deposition onto cold plasma and γ -irradiation activated PE surface it was established that for the same concentration of the chitosan solution the most efficient method was the immersion in respect with homogeneity of surface and thickness of deposited layer

but the electrospraying appeared to be more versatile method, because it allows a more precise control of the chitosan content deposited onto the surface by varying the deposition time.

Attenuated Total Reflectance Fourier Transform Infrared spectroscopy (ATR-FTIR), X-ray photoelectron spectroscopy (XPS) and potentiometric titration proved CHT presence on the PE surface and also new bonds are evidenced mainly amide groups or ester groups because of interaction of $-NH_2$ or $-OH$ groups of CHT with carboxyl group implemented on PE or PLA surface by radiation activation of surface. Other reactions were also possible because of the high reactivity of the active species created by plasma exposure/gamma irradiation and the functional groups of chitosan [157,165]. Chitosan coating improved the oxygen barrier properties of PE (Oxygen Transmission Rate (OTR) of PE decreased 3 times being of $1066\text{ mL}/(\text{m}^2 \cdot \text{day})$ while OTR of the uncoated PE is $3833.36\text{ mL}/(\text{m}^2 \cdot \text{day})$). The potentiometric and polyelectrolyte titrations, zeta potential determination showed that some amount of chitosan desorbed faster from the surface until equilibrium was reached and also that the grafted chitosan layer was more stable than the physically adsorbed one. In the case of grafting, a thin chitosan layer was irreversibly immobilized on the PE surface. The obtained materials combine the antibacterial, antifungal, bioadhesivity, biocompatibility, biodegradability of chitosan [146,150,156,157,163–167], with the biological functions and antioxidative activity of vitamin E. Vitamin E is also known for its activity to prevent cell membrane damage by inhibiting peroxidation of membrane phospholipids and disrupting free radical chain reactions induced by formation of lipid peroxides [168].

The pH responsiveness was evidenced by contact angle measurements using buffered solutions with pH varying in the 2–11 range and it appears by sudden switching from hydrophilic to hydrophobic surface at critical pH ≈ 6 . The contact angle of the polyethylene surface remains constant over the entire studied pH range (Figure 3).

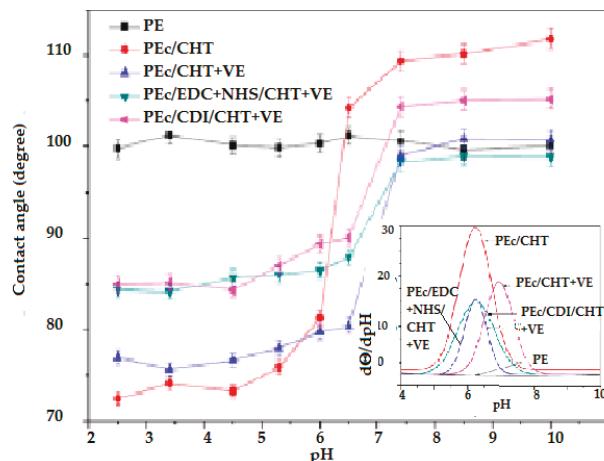


Figure 3. Contact angle (θ) versus pH titration curves and derivative curves of $d\theta/dpH$ (insert) for chitosan/vitamin E-coated PE films adapted from [157].

Also, vegetable oils (clove oil, argan oil, thyme oil, tee tree oil and so forth) and combinations chitosan/vegetable oils have been tested to combine antimicrobial activity of CHT with those of vegetable oils and their antioxidant, biological function and nutrition [169]. They were covalently immobilized both on the activated substrate of PE and PLA and the results indicated their synergism in preventing microbial growth on fresh crude cheese, beef meat, poultry minced meat and fresh apple juice [136,140,146]. Both plasma activation and γ -irradiation have great influence on the antimicrobial activity being known that they are relatively simple and quite safe microbial sterilization techniques

that are utilized in a variety of applications for their low operating costs and non-polluting capabilities. In the case of lactoferrin immobilization it was established that gamma irradiated samples showed higher activities than those nitrogen plasma activated [150].

Lignocellulosic materials usually display a very low microbial resistance and microbial contaminations might be an additional issue to be taken into account. Conferring antibacterial activity to lignocellulose-based products may represent a main functional property which is useful not only for advanced food packaging [113] but also for textile applications. This can be realized by incorporation of aldehydes, epoxy, carboxylic acids and so forth [160,170] followed by attachment of some phenolic structures which can react at different extents with plasma/ γ -irradiated activated surfaces and therefore they will be grafted on the lignocellulosic material surface to develop covalently bound antimicrobial products. The cellulose/chitin mixture and kraft paper were modified using different types of plasma: air, oxygen, nitrogen and argon activation followed by reaction with various phenolic compounds such as p-a-hydroxybenzoic acid (HBA), galic acid (GA) eugenol (Eu) and grape seed oil (GO) and rosehip seed oil (RO) and it was found efficient for inhibiting growth of microorganisms onto fresh crude cheese and beef meat. [160,171]. The antimicrobial activity was increased up to 100%. The rosehip seeds oil imparted the best antimicrobial properties to cellulose/chitin mix substrate. As functionalizable substrate is a biodegradable polymer and surface treatment was realized by physical methods of activation (cold plasma and gamma irradiation in mild conditions), the obtaining of the materials with desired surface properties avoided the harmful environmental concerns.

3.2.6. Wet Methods

Wet Methods involve both corrosive liquids to which the polymer substrates are directly exposed, like piranha solution (dissolved hydrogen peroxide and sulfuric acid), combined sodium hydroxide and sulfuric acid, chromic acid, potassium permanganate and nitric acid [172] and graft copolymerization. The first method has not a wide applicability but graft copolymerization received a wide scientific and applicability interest.

3.2.7. Photografting

Photografting method is a free radicals photografting procedure which occurs onto a polymer surface exposed to UV light in the 315–400 nm range in the presence of photoinitiators (e.g., benzophenone, anthraquinone, thioxanthone, phenyl azide, polymers, curcumin) and monomers which usually bear ketone groups [173]. The active agent can be directly incorporated during photografting, or by its subsequent immobilization after grafting of a polymer chain with reactive functional groups (e.g., acrylic acid).

3.2.8. Biological Methods

Biological methods consist in: pre-adsorption of proteins, drug, enzyme immobilization, cell seeding and pre-clotting [174].

3.2.9. Chemical Vapour Deposition (CVD)

In typical CVD, the substrate is exposed to one or more volatile precursors, which react and/or decompose on the substrate surface to produce the desired deposit [175]. Diamond-like carbon (DLC) has been investigated as coating materials for industrial applications due to its outstanding characteristics such as high hardness, wear resistance, chemical inertness and biological compatibility. The demand for polymeric materials has also been increasing and highly functionalized polymers are much desired for wider applications to the production materials ranging from biomaterials to eco-friendly materials. In order to modify the polymers for highly-functionalized and highly biocompatible materials, DLC can be effectively nanocoated on polymeric materials, especially on

polymeric surfaces through CVD methods. By nanocoating such DLC, a new type of polymer/DLC nanocomposite could be established for the use in biomedical devices and food packaging.

3.2.10. Atomic Layer Deposition (ALD) Method

VTT Technical Research Centre of Finland developed a fully recyclable nanocoating for food and pharmaceuticals [176] which is thin, light and air-tight, conformal and pinhole-free coating which follows the contours of the coated material, with excellent gas permeation resistance for packaging materials by ALD method. These thin bio-based packaging materials have gas permeability properties similar to those of existing dry food packages and pharmaceutical blister packs protecting the products from humidity, drying or oxidation. ALD coating allows integrating different functions into the packaging material, such as prevent water, oxygen, humidity, fats and aromas from permeating the packaging and protect the surface from stains and bacterial growth. The ALD technology improves the humidity tolerance and performance of bio-polymers, reducing the need for oil-based plastics.

3.2.11. Layer-by-Layer Assembly

By layer-by-layer assembly deposition can prepare active packaging coatings by the incorporation of active agents either between layers or within the structure of an individual polyelectrolyte [177]. Onto a polymeric activated substrate can be deposited by mutual attraction of polyelectrolytes with opposite charges or even by covalently attached of a polyelectrolyte such as proteins, polysaccharides, synthetic polymers of successive alternate layers [135,178]. Deposition can be accomplished either by submersion of the substrate into polyelectrolyte solutions or by spraying of solutions onto the substrate. The depositions are the presence optimized by adjusting the pH of their solutions for a full protonation or deprotonation, by maximizing of charge [179]. Between layers can be either only electrostatic interactions [180], and/or covalent bonds through the use of crosslinkers. The number of deposited layers is limited by a saturation state characterized by a thickness and stability of the system [181,182]. Jokar et al. produced coatings by the layer-by-layer deposition method. LDPE films were ultrasonically washed with acetone, functionalised in dilute aqueous solution of polyethylenimine for 10 min and sequentially dipped into anionic silver colloid dispersions containing PEG-capped silver NPs or cationic chitosan for 10 min. Silver particles were 18–32 nm and 22–30 nm in size in melt-blended and coated composites, respectively and their migration in simulated media as water, 10% ethanol, 3% acetic acid and apple juice depends on silver concentration and temperature [183]. Covalently bonded multi-layered films were assembled also using the LBL techniques by using polymers bearing functional groups capable of reacting with one another or with a bi-functional agent (diamines, diimides or dialdehydes). Covalent cross-linking increased the modulus and stability of the films.

3.2.12. Ultrasonic Nozzle Systems for Nanotechnology Coating Applications

Sono-Tek ultrasonic nozzles are suitable to depositing precision nanotechnology coatings for spray applications in research as well as production volume spray processes [184]. Uniform nanolayers of solutions onto any size or width substrate (including moving webs of material) are deposited and nano-suspensions are homogeneously dispersed onto a substrate, including suspensions that tend to agglomerate easily which are continuously break due to the mechanical vibration of the nozzle which is much efficient than air spraying. Sono-Tek systems employ the ultrasonic nozzle technology which enables to be easily scaled up from R&D to high volume production.

3.2.13. Plasma Nano-Coating of Beverage Cans

Interior and possibly even exterior coating of the aluminium cans and tubes is required in the food industry because the direct contact between the product and the packaging can lead to aluminium corrosion and the food could spoil. For example, the pasteurization increases corrosive impact on packaging. PlasmaPlus® coating technique uses the plasma jets deposit micro-fine glass-like nano-coats

which form a highly effective protective film on the packaging with minimum material usage. Plasma coats provide a perfect quality imprinting [185]. Nobile et al. [186] produced the coating in polyethylene oxide on the surface of PE film by plasma-based vapour deposition. Transmission electron microscopy (TEM) imaging revealed AgNPs about 90 nm in size deposited on the films. The migration of silver ions from nanosilver coatings onto PE films studied by immersion in distilled water, acidified malt extract broth and apple juice at 44 °C for 5 days. It was found that the silver content in the solutions was the highest in the distilled water simulant (1–1.9 mg/kg), with lower concentrations in the malt extract broth and apple juice (0.2–0.38 mg/kg).

3.2.14. Electrospinning/Electrospraying

Electrospinning/electrospraying has recently gained much attention because of its versatility in processing a wide range of polymer and biopolymer materials. It has the ability to produce fibre/particle diameters within the submicron and nano range using electric field which cannot be achieved by using conventional-generating technologies. Nanofibers have wide applications in industry such as food packaging coatings, composite materials, carbon nano tubes, inorganic fibres and tissue scaffolds, filtration, medical, membranes and so forth [187]. Electrospinning has been used to create a well-dispersed “concentrate” or master batch that will act as a carrier of well dispersed nanoparticles. It is an electro-hydrodynamic process, comprising electrospraying and electrospinning techniques which produces nanostructured fibre-based and particle-based materials both in laboratory and industrial scale. The devices used for the mono-axial and co-axial electrospinning/electrospraying method is presented in Figure 4.

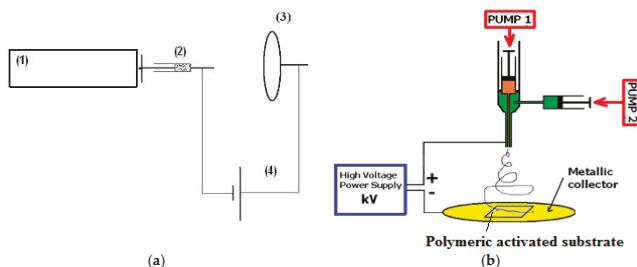


Figure 4. Representative experimental set-up of the uniaxial (a): (1) pump; (2) syringe; (3) collector; (4) high direct voltage (0 to 30 kV) power supply; or coaxial (b) electrospinning device used for immobilization of vegetable oil into chitosan and bioactive layer deposition onto polymeric activated substrate adapted from [146]; Vasile et al. (2016).

In monoaxial electrospinning the device consists of a direct current high voltage supply, a metal plate collector sustaining the polymeric substrate, a pump and a syringe oriented perpendicularly to the metal plate with the low diameter needle (Figure 4a). A high direct voltage (0 to 30 kV) between the metal plate and the syringe needle is applied. The polymer solution is extruded through the needle tip by the syringe pump at a constant flow rate. At the point of ejection (the needle tip), is created a polymer jet because of the electric charge repulsion outgoing the solution surface tension. Based on electrostatic field between nozzle (needle tip) and collector, the dry polymer or solution are collected on the surface of collector screen. On the collector a very thin polymer layer is deposited, whose morphology as nanofibres or nanoparticles, depends on rheological properties of the solution [156] and composition of electrospinnable solutions [157,188]. This device has some disadvantages such as drying which can be controlled by the distance between nozzle and collector.

In co-axial electrospinning two syringes are used one of them being provided with a co-axial needle oriented with the needle perpendicular to the metal plate. It offers the possibility of depositing a bioactive layer/coating containing two bioactive compounds onto activated surface achieving the

encapsulation of less stable or liquid compound (as vegetable oils) into a polymeric one so core-shell morphology is obtain which can increase the coating functionality and protection of the labile bioactive component and also the use of nanomaterials in other technology. Encapsulation of the vegetable oils in chitosan was achieved by coaxial electrospinning method and immediately a coating of the nanoparticles/nanofibres was deposited onto polymeric substrate [146,189]. This technique may also be used with one of the two syringes with the polymeric solution and the other one with the same solvent able to dissolve the polymeric matrix. This approach is to improve the processability, being particularly interesting to scale up the electrospinning technique from lab scale to the industrial sector.

Electrospun fibres have a very high specific surface and porosity and they are able to encapsulate active substances. A wide range of applications are known for such fibres as improvement of physico-chemical and functional properties of biopolymer based materials by means of a controlled release of active compounds or by enhancing the dispersion of nano-additives into the biopolymer matrices. The nano encapsulation/ entrapment can reduce the amount of active ingredients needed to obtain certain functionality and also their controlled release [158,188,190]. Nanofiber-based systems for antimicrobial food packaging and food contact surface applications contain antimicrobial fibre-base mats as coating of the packaging material, improve their activity in maintaining an optimal effect during the food storage period. Furthermore, the high surface to volume ratio of electrospun mats offer an efficient and prolonged delivery of loaded bioactive compounds.

An antimicrobial active multilayer system was obtained from a commercial polyhydroxyalkanoate substrate (PHA) and an electrospun PHA coating with in situ-stabilized silver nanoparticles (AgNPs) with satisfactory thermal, mechanical, barrier and antibacterial properties. It reduced the bacterial population of *Salmonella enterica* below the detection limits at very low silver loading of 0.002 ± 0.0005 wt %. Also, polylactic acid (PLA)/Silver-NP/Vitamin E bionanocomposite has been prepared by electrospinning and they showed a good antimicrobial activity against both gram positive and gram-negative bacteria [190]. As a result, this method provides an innovative route to generate fully renewable and biodegradable antimicrobial materials for food packages and food contact surfaces [191]. The choice of the manufacturing process depends on specific application requirements of the coating. As an example, the percent reduction against the fungus *A. Níger* after 14 days, for the three multilayer samples coated with AgNP/polyethylene nanocomposites with the silver nanocomposite layer of AgNO_3 suspension (black) all at 1.0 wt % of silver content depends on the coating method, the most efficient being spraying one which gave a reduction of more than 70% while laminated and casting method reduction were of 20% and 45%, respectively [192].

4. Applications

Nanocomposites and nanocoatings applications in food packaging depend both on the properties of matrices/substrates and activity of ingredients. Nanoclay composites (usually montmorillonites) are used as flexible and rigid food packaging because of their excellent barrier characteristics in packaging of processed meats, cheese, confectionery, cereals and boil-in-the bag foods, items obtained by extrusion-coating process together with the paperboard are useful for fruit juice and dairy products and the beer and carbonated drinks bottles are manufactured by co-extrusion processes. For example, the PET bottles contain nanocore and nylon beer bottles with nanoclays show improved barrier characteristics. The active agents functions include antimicrobial, antifungal, antioxidant, biocatalyst, external stimuli responsiveness, additives that absorb undesirable component from food such as ethylene, moisture and odour and so forth They are incorporated into matrix or coating to enhance the quality and shelf life of the food and are released in a controllable manner, the procedure being much efficient than direct addition into the food because they may react with other food components and loss their activity or affect food sensorial characteristics.

There are many formulations including such antimicrobials, antioxidants and biocatalysts, some of them being summarized in Tables 3 and 4.

Table 3. Formulations including antimicrobials as bioactive compounds intended to use in food packaging.

Active Agent	Substrate or Matrix	Technique	Characteristics/Observations	Ref.
Antimicrobials				
Essential oils; adhesion promoters (e.g., acrylic or vinyl) resins or nitrocellulose) and fixatives	common packaging materials	different coating or spraying	controlled release	[193]
Bacteriocins (ex: Nisaplin® nisin, pediocins); Spice and herb extracts; Organic acids, microencapsulated nisin	polycaprolactone alginate, crosslinked chitosan/cellulose nanocrystal	crosslinking reaction under γ -irradiation	nano-cellulose/PLC and alginate/cellulose nanocrystal based edible films and ready-to-eat meat	[194]
Silver nanoparticles AgNP	poly(3-hydroxybutyrate-co-3-hydroxyvalerate)	extrusion/blending	sustained release of antimicrobial silver ions in food applications	[195]
Silver	poly(l-lactide)	melt-compounding	significant inhibition of microbial growth; migration rates below values reported by international imposed limits	[196]
AgNP/ peptide/ cellulose nanocrystals	PLA	solvent casting	the composite showed its biodegradation extent of 69.94% (after 90 days), offering good biodegradability for use as a material for the production of degradable plastic bags. The aging, hydrolytic degradation and biodegradation of PLA-based films could be tailored by Ag kaolinite incorporation	[197]
AgNP/kaolinite	PLA and poly(butylene adipate-co-terephthalate)	blow films	compression-moulding, 180 °C and 1.8 MPa for 5 min; coated with PHBV and PHBV/AgNPs ultrathin fibre mats produced by electrospinning followed by an annealing step; electrospun coating ($\sim 0.71 \pm 0.01$ mg/cm ²)	[198]
AgNP	PVOH	mixing a colloidal solution	improved thermal properties, enhancing stability and increasing T _g	[199]
2 wt % Ag-NPs	polyamide 6	thermal reduction of silver ions during the melt processing of a PA6/silver acetate mixture	effective against E. coli	[200,201]
TiO ₂ /Ag grafted with γ -aminopropyltriethoxysilane nano-Ag 35%, nano-TiO ₂ 40%, kaolin 25% (30%)	PVC	mixing	good antibacterial properties by photocatalytic bacterial inactivation	[202]
ZnO/Cu/Ag	PLA	high-speed mixer; extruded by a twin-screw extruder and then film was obtained	Ag-NPs retarded the senescence of jujube, a Chinese fruit.	[203]
		melt processing	Antimicrobial materials	[189]

Table 3. Cont.

Active Agent	Substrate or Matrix	Technique	Characteristics/Observations	Ref.
Antimicrobials				
cellulose nanocrystal/silver nanohbrids bi-functional nanofillers—10 wt % CNC-Ag	poly(3-hydroxybutyrate-co-3-hydroxyvalerate)	solution casting	high performance nanocomposites with improved thermal, mechanical and antibacterial properties against both Gram-negative <i>E. coli</i> and Gram-positive <i>S. Aureus</i> of PHBV. Reduced water uptake and water vapour permeability; lower migration level in both non-polar and polar simulants because of increased crystallinity and improved interfacial adhesion. Great potential applications in the fields of food, beverage packaging and disposable overwrap films.	[204]
30 µm thick coating containing 2–6% cinnamon essential oil	PP	spreading	controlled release, total inhibition against <i>Aspergillus flavus</i> and <i>niger</i> and <i>Penicillium roqueforti</i> and <i>Penicillium expansum</i> .	[205]
4% thyme and oregano essential oils	corona treated LDPE	ionizing treatment and directly extrusion	controlled release, inhibit <i>Escherichia coli</i> 0157:H7, <i>Salmonella Typhimurium</i> and <i>Listeria monocytogenes</i> , changes in barrier properties	[206]
Organic-inorganic hybrid coatings, poly(vinyl alcohol) with improved water resistance	poly(ethylene terephthalate) and oriented polypropylene	sol-gel technique condensation of hydroxylated monomers and polymers into a network	multilayer materials for packaging applications	[207]
Antifungal agent natamycin was embedded in a tetraethyl orthosilicate/EVOH gel	plasma treated PLA films	sol-gel	antimicrobial coatings; controlled release; inhibit mould growth on cheese stored for 30 days	[208]
Nanosilver or chitosan	LDPE	melt-blended and layered deposited silver	silver ion migration from the nanocomposites into the food simulants and apple juice was less than the cytotoxicity-level concentration (10 mg kg^{-1}) in all cases over 30 days	[209]
Antimicrobial photocatalysis (e.g., TiO ₂)	PLA multi-layered hybrid coatings	sol-gel technique	Controlled release, antimicrobial	[210]
Polydiacetylene liposomes containing cinnamaldehyde as liposome-encapsulated cinnamaldehyde	amine-functionalized silane monolayer on Piranha treated glass or amine-functionalized PLA films	nanoencapsulation and immobilization of cinnamaldehyde	2–3 logarithmic reductions of <i>Listeria innocua</i> (2–3 logarithmic reductions), <i>Listeria monocytogenes</i> and <i>Salmonella</i> Typhimurium / negative effect on CO ₂ gas barrier properties. There was no significant difference in the effectiveness of antimicrobial films versus the coatings. Antimicrobial packaging may be used alone, or in combination with flash pasteurization, in preventing foodborne illness due to post processing contamination of ready-to-eat meat products.	[211]
Sorbitic acid and/or lauric arginate ester and chitosan and nisin	PLA or corona treated PLA	treated with solution-coated polyactic acid (PLA) films	[212,213]	

Table 3. Cont.

Active Agent	Substrate or Matrix	Technique	Characteristics/Observations	Ref.
	Antimicrobials			
Peptide nisin entrapped in polyethylene oxide brushes grown on silane modified silicon wafers which protected nisin.	polyethylene oxide	entrainment	inhibition of Gram positive bacterium <i>Pediococcus pentosaceus</i> over a period of seven days	[214]
Pullulan Powder was rendered cationic by reaction with an amine terminated silane as 3-aminopropyltrimethoxysilane	antimicrobial pullulan	immobilization	inhibits <i>Staphylococcus aureus</i> and <i>Escherichia coli</i>	[215]
Enzyme lysozyme	covalently attached onto UV-ozone treated EVOH films	immobilization via carbodiimide chemistry	inhibits <i>Listeria monocytogenes</i>	[216]
(3-Bromopropyl)triphenylphosphonium	poly(butylene adipate-co-terephthalate) functionalized with a quaternary phosphonium compound, (3-bromopropyl)triphenylphosphonium	immobilization by azide-alkyne “click” reaction	inhibits <i>Escherichia coli</i>	[217]
SO_2	multi-layered film made of PA and PE was subjected to atmospheric plasma treatment (Ar , Na_2O and SO_2) on the PA side of the films	immobilization	inhibits <i>Escherichia coli</i> (82%), <i>Staphylococcus aureus</i> (86%), <i>Listeria monocytogenes</i> (63%), <i>Bacillus subtilis</i> (79%) and <i>Candida albicans</i> (75%)	[218]
Chitosan (polycation) and κ -carrageenan (polyanion)	aminated PET	layer-by-layer assembly	improved gas barrier properties	[219,220]
Lysozyme: κ -carrageenan alternated with two layers of the antimicrobial enzyme lysozyme	amine-functionalized PET films	layer-by-layer assembly	improved oxygen and water vapour permeability	[221]

Table 4. Formulations including antioxidants and biocatalysts as bioactive compounds intended to use in food packaging.

Antioxidants			
Citrus oil	plasma treated PET trays	spray deposition of citrus oil in methanol	controlled release; antioxidant activity with cooked turkey meat and retained activity after six months of storage [222,223]
Rosemary extract	LDPE plastic wrap or a polymeric carrier	applied direct onto LDPE plastic wrap or with a polymeric carrier	controlled release; 0.45 mg rosemary cm^{-2} [224]
α -Tocopherol	paperboard using a vinyl acetate-ethylene copolymer as a carrier for controlled release	solvent casting coating at a concentration of 3%	antimicrobial and antioxidant coating; controlled release [225]
gallic acid	chitosan	immobilization by carbodiimide assisted reaction	reduced oxidation of peanuts [226]
Metal oxide coatings Aluminium oxide or silicon oxide	biaxially oriented polypropylene and polyethylene terephthalate film substrates	reactive evaporation using an industrial high-speed vacuum deposition technique boat-type roll-to-roll metalizer	transparent barrier coatings based on aluminium oxide or silicon oxide fulfill requirements such as product visibility, microwaveability or resealability reduce oxygen diffusion [227,228]
Tannic acid and poly(allylamine hydrochloride)	glass slides	layer-by-layer assembly	the number of bilayers increases in overall scavenging activity [229]
Caffeic acid	polypropylene packaging materials coating	photografting	prevent oxidative degradation of ascorbic acid in orange juice [230]
Acrylic acid	metal chelating active packaging coatings PP films, PP-g-PAA	photografting	prevent lipid oxidation in food emulsions [231-233]
Hydroxamic acid photografted Polyhydroxamate chelators Plant-derived phenolic compounds, metal chelating	PP	<i>in situ</i> polymerization of a mixture of catechol and catechin and oxidative polymerization with laccase and in alkaline saline and photografting	surface adhesion properties upon polymerization; non-migratory iron chelating active packaging material biomimetic iron chelating active packaging material, inhibit oxidation of food [234-236]
Lignosulfonate	Alginate	Solution casting	Antioxidant and UV protective films [113]
Biocatalysis			
Lactase blended into polyethylene oxide nanofibers	oxygen scavenging	electrospinning-enzymes or other active agents are incorporated into polymer nanofibers	controlled release, retained up to 93% of free enzyme activity [237,238]
Lactase	attachment of lactase to polyethylene films;	immobilization β -galactosidase bound to amine-functionalized PE films by a dialdehyde tether; polyethylene glycol tether size influences the attachment	reduce milk lactose in package; retained activity of immobilized lactase [239,240]
Lactase conjugated to nanomaterials	lactase immobilization onto nanostructures	lactase was attached to carboxylic acid functionalized magnetic nanoparticles 18 nm, 50 nm and 200 nm in diameter using carbodiimide chemistry.	retained activity of immobilized lactase; reducing the particle size of magnetic nanoparticles can increase the activity retention of conjugated lactase [241]
Lactase and polyethylamine, glutaraldehyde	lactase covalently bound to low-density polyethylene	layer-by-layer assembly	more enzyme is immobilised but diffusion is difficult [242]

Table 4. Cont.

Glucose oxidase	electrospun Polyvinyl acetate/chitosan/tea extract fibres	electrospinning	reduce oxygen in packaged foods	[243]
Glucose oxidase	chitosan	LbL films	biosensors	[244]
Oxalate oxidase, oxygen-reducing enzymes in coatings and films for active packaging	extrusion-coated liner of polypropylene on top of the coating.	entrapment in a latex polymer matrix	protective packaging gas carbon dioxide; oxygen scavenging in active packaging; retained catalytic activity through entrainment in a latex polymer matrix	[245]
Laccase-catalysed reduction of oxygen	it was possible to use lignin derivatives as substrates for the enzymatic reaction.	laccase-catalysed reaction created a polymeric network by cross-linking of lignin-based entities,	resulted in increased stiffness and water-resistance of biopolymer films	[238]
Catalase	layered haemoglobin/PS	Immobilization	create a physical and chemical protective barrier	[229,246]
Fungal haringinase	cross-linking, naringinase to polyvinyl alcohol and alginate	immobilization	bitterness reduction in grapefruit juice	[247,248]
Protease, trypsin and endoproteases	PP, PVOH and PS	photografting, carbonyl-imide chemistry -covalently couple enzymes (via amine groups) to carboxylic acid groups poly(ethylene) glyco-methacrylate and 4-vinyl-2,2-dimethylazolactone	antibody analysis in enzyme reactors	[249]
Hydrolyse urease	photografted polytetrafluoroethylene	photografting	remove urea from beverages and foods	[250]
Glucose oxidase catalase for oxygen scavenging activity	low-density polyethylene and paper board multilaminate or combinations of LDPE, PP and PLA	industrial lamination	scaled-up production in tetra pack pilot plant, scavenge oxygen to improve food shelf life	[251]
Poly(sloxane-based healing agents	acrylate matrix	polymer coatings coaxial electrospinning	self-healing polymer coating systems	[252]

4.1. Antimicrobial/Antibacterial

Nanomaterials are more and more used to target bacteria in textile industry, marine transport, medicine and food packaging as antibacterial coatings and other materials [253]. Antimicrobial packaging role is to control the growth of pathogenic and/or spoilage microorganisms in packaged products. The diminishing and control bacterial colonization by the modification of the surfaces can be achieved [254]. As antimicrobial agents, essential oils, organic acids, peptides, enzymes and biopolymers are applied and nanoparticles like AgNP, MgO, CuO, Cu, ZnO, Cd selenide/telluride, chitosan, carbon nanotubes are used. Antimicrobial plant extracts from many plants and fruits such as thyme, clove and tea tree, rosemary oil or powder [169], sea buckthorn (*Hippophaë rhamnoides* L.) leaves and inner bark of pine trees (*Pinus silvestris*) [255] used in food packaging provide a healthy alternative. They contain aromatic and phenolic compounds that are responsible for their antibacterial properties and antioxidant activities. They can be applied as components in chitosan films or nanofibres obtained by electrospinning deposited on PLA [256]. Such essential or cold press oils exhibited selective antibacterial and/or antifungal effect both as a solvent extract and as a coating against three food spoilage fungi—*Fusarium graminearum*, *Penicillium corylophilum* and *Aspergillus brasiliensis*—and three potential pathogenic food bacteria as *Staphylococcus aureus*, *Escherichia coli* and *Listeria monocytogenes* and also against *Pseudomonas aeruginosa*.

TiO₂ and ZnO are non-toxic and approved by FDA as GRAS. TiO₂ nanoparticles exhibiting bactericidal and fungicidal effect against *Salmonella choleraesius*, *Vibrio parahaemoliticus*, *Staphylococcus aureus*, *Diaporthe actinide* and *Penicilium expansum*. It was ultrasonically dispersed ethylene-vinyl alcohol copolymer films to obtain active packaging. It showed excellent bactericidal property under UV light [257]. Because of their very small dimensions, the nanomaterials are able to attach many biological molecules, therefore showing a greater efficiency [258]. ZnO is efficient both against Gram-positive and Gram-negative bacteria. NanoZnO coated films exhibit antimicrobial effects against *L. Monocytes* and *S. Enteritis*.

Have been proposed several mechanisms for the antimicrobial activity of nanoparticles as: directly interactions with microbial cells and interruption of the trans-membrane electron transfer, disrupting/penetrating the cell envelope, oxidizing cell components or producing secondary products as reactive oxygen species (ROS) or dissolved heavy metal ions. Secondary processes also can occur. For example, the antibacterial activity of silver ion is reduced by the protein rich food because it can bind the cysteine, methionine, lysine and arginine [259]. Nanosilver antimicrobial activity is explained by adhesion to the cell surface, degrading lipopolysaccharides and damaging the membranes, largely increasing permeability, by penetration inside bacterial cell, damaging DNA [260] and releasing antimicrobial Ag⁺ ions by AgNPs dissolution which then bind to electron donor groups in biological molecules containing sulphur, oxygen or nitrogen [261]. Silver ions can be released to destroy food spoilage. They show also a high temperature stability and low volatility. Nanosilver is useful as coatings component where the antimicrobial action occurs at the surface as on containers, mugs, dishes, cutlery, fridges, chopping boards and so forth [262]. It was found effective against numerous species of bacteria including *E. Coli*, *Enterococcus faecalis*, *Staphylococcus aureus* and *Epidermidis*, *Vibrio cholera*, *Pseudomonas aeruginosa* and *putida* and *fluorescens* and *oleovorans*, *Shigella flexneri*, *Bacillus anthracis* and *subtilisi* and *Cereus*, *Proteus mirabilis*, *Salmonella enterica typhimurium*, *Micrococcus luteus*, *Listeria monocytogenes* and *Klebsiella pneumoniae* [1,263] some of them presenting resistance to other potent chemical antimicrobials. Migration studies for nanosilver containing PE composites or coatings [264] in different simulants as malt broth, apple juice, distilled water and 10% ethanol showed good results.

The NanoBioMatters highly efficient antimicrobial product and BactiBlock® technology are based on silver-functionalized nanoclay. MgO and ZnO nanoparticles could provide cheap, safe alternative to expensive nano-sized silver as a heavy metal not suitable for human contact. The combinations of α-tocopherol with nisin or chitosan as coating or biocomposites confer both antimicrobial and antioxidative properties [136,140,225].

Antimicrobial activity of the chitosan and engineered nanoparticles is explained by several mechanisms including interactions between positively charged chitosan and negatively charged cell membranes, increased membrane permeability and rupture and leakage of intracellular material. They are ineffective at pH values above 6 because of the absence of protonated amino groups [265]. Another two antimicrobial mechanisms as chelation of trace metals by chitosan, inhibiting enzyme activities and, in fungal cells, penetration through the cell wall and membranes to bind DNA and inhibit RNA synthesis were also proposed [167].

Carbon nanotubes also have antibacterial properties. They are efficient against *E. coli*, possibly because puncture microbial cells [266] but is possible to be cytotoxic to human cells, to skin and lungs in processing stages rather than for consumers, therefore their migration to food must be carefully controlled.

4.2. Antioxidant

Oxidative degradation of food products happens during transport and storage producing lipid rancidity, colour loss (e.g., oxidation of carotenoids, chlorophyll, anthocyanins) and vitamin degradation. The antioxidants (e.g., free radical scavengers, metal chelators, singlet oxygen quenchers, oxygen scavengers) are commonly incorporated in food packaging by blending with polymers during processing (mixing, extrusion) [267,268]. The antioxidant active packaging technologies include oxygen scavengers, manufactured as sachets or labels and by the development of migratory and non-migratory antioxidant coatings. In the first case is possible a controlled release of an antioxidant (migration is 20 times less than the legal limits for the European Union) and sometimes does not requiring direct contact with the food [269]. Non-migratory antioxidant coatings may also be applied by covalent immobilization by means of the functional groups on the surface of packaging materials and shows advantages that do not alter sensorial properties of the packaged food product [270].

4.3. Biocatalytic

Enzymes onto solid support materials provide biocatalytic coatings for active packaging by catalysing some reactions. Biocatalysts are used in ingredients production and breakdown of undesirable components which are harmful or may decrease product quality. Biocatalysts are very sensitive, therefore the immobilization method onto and into solid supports must preserve their thermostability, optima pH and solvent stability and usually so-called “in-package processing” is applied to avoid changes during processing, transport and storage. Antimicrobial enzymes (e.g., lysozyme) are incorporated into active packaging coatings via blending, non-covalent binding for controlled release and covalent immobilization [150,271,272]. Their compatibility with matrix can be achieved by surface functionalization and cross-linking techniques [273]. The thermostability and pH stability of the bound enzyme determines the success of the coating method.

4.4. Barrier Applications of Polymer Nanocomposites

A critical issue in food packaging is that of migration and permeability [170,274] to atmospheric gasses, water vapour, or substances contained within both in the food being packaged or even the packaging material itself. As examples, in packages for fresh fruits and vegetables high barriers to migration or gas diffusion are undesirable because their shelf-life depends on oxygen for sustained cellular respiration while the plastics for carbonated beverage containers must have high oxygen and carbon dioxide barriers to prevent oxidation and decarbonation of the beverage contents. Though polymers possess numerous advantages their major drawback is an inherent permeability to gasses and other small molecules. PET provides a good barrier to oxygen (6–8 nmol/ms GPa) while this is very low for HDPE (200–400 nmol/ms GPa). The situation is opposite in respect with barrier against water vapour [170]. Oxygen and carbon dioxide barriers are necessary for plastics used for carbonated beverage containers. EVOH exhibits excellent oxygen transmission rate (OTR) values under dry conditions but under very humid conditions (relative humidity > 75%) it can

possess OTR values more than an order of magnitude higher due its swelling and plasticization in the presence of diffused water molecules [275]. Bio-derived polysaccharide (starch, chitosan, pullulan) based packaging show even larger dependence of their OTR on humidity level, which has severely limited their usefulness. Thermoplastic biopolymers like PLA or polycaprolactones (PCLs) have good tolerance to moisture [276]. Because of the tortuosity effect created by the presence of highly crystalline CNCs (1% CNC) in the PLA-based nanocomposites, which increased degree of crystallinity all barrier properties are significantly improved (WVP (lower ~ 40%; OP ~75% than neat PLA films). PLA/CNC with 1% nanofiber showed also improved of elongation at break [277–279]. Because of this specific dependence, complex multilayer films (by co-extrusion) [280] or polymer blends and composites are often preferred [281]. A high oxygen barrier, water sensitive material like EVOH was sandwiched between two layers composed relatively hydrophobic polyethylene [172]. Multilayer films and polymer blending require the use of additional additives and adhesives that complicate their regulation by federal agencies and arise recycling difficulties. Polymer nanocomposites (PNCs) should solve most of the above-mentioned problems.

4.5. Stimuli Responsive Nanocomposites/Nanocoatings

Stimuli responsive nanocomposites/nanocoatings prepared using “stimuli-responsive,” “smart,” “intelligent” or “environmentally sensitive” polymers [282–285]. These polymers respond to environmental changes by changing their conformation, solubility, hydrophilic/hydrophobic balance, reaction rate, swelling and release behaviour (for hydrogels) and molecular recognition. Their response to the external changes are reversible, “switching” may occur repeatedly and occurs in a narrow interval of stimuli variation. Responsive polymers have found applications as free chains dissolved in aqueous solutions, as covalently or noncovalently crosslinked hydrogels and immobilized adsorbed or surface-grafted onto solid surfaces [286]. Surfaces modified with stimuli-responsive polymers dynamically modify their physico-chemical properties in response to changes in their environmental conditions. Stimuli-responsive surfaces have been created by the immobilization of reversible thermally responsive elastin-like polypeptide, on a glass surface [287]. The distance-dependent colorimetric properties of gold nanoparticles, enable to determine the effect of different variables on the lower critical solution temperature (LCST) at the solid–water interface. A poly(ethyleneimine)-poly(dimethylsiloxane) mixed brush switched spontaneously from the hydrophilic state in water to the hydrophobic one in air, therefore materials show a poor adhesion in a changeable environment. The surface coatings fabricated from mixed poly (ethylene oxide) (PEO)-poly(dimethylsiloxane) brushes or from fluorinated nanoparticles were adaptive to liquid and vapour environments so that the surfaces were spontaneously transformed to non-sticky states in air and in water. Smart and self-healing coatings have been also prepared. Colloidal particles obtained by the emulsion copolymerization of acrylate and fluorinated acrylate monomers form stratified film morphologies in superhydrophobic surfaces [288]. Thermoresponsive poly(*N*-isopropylacrylamide)-based microgels and assemblies have a diverse range of applications for example, biosensing, smart coatings and so forth [289].

Sensory Packaging is a category of devices used in intelligent packaging as nanosensors to monitor and report on the condition of food, communicate the degradation of product or microbial contamination and give information on history of storage, avoiding inaccurate expiration date increasing security and food safety. It helps food industry and retailers to know if the food package has been opened or tampered. This could be achieved by using a nanocrystalline indicator in form of an oxygen intelligence ink printable on most surfaces. This ink contains an UV light activated nanocrystalline particles of a semiconductor (usually TiO₂) or nanoposphorous particles. These particles are white in daylight but will fluoresce when exposed to light of certain wavelengths. The colour pigments can be also used as micro-colour codes in packaging and labelling applications. The development of sensory packaging which monitor the conditions of pharmaceuticals and foods are those affected by changes in temperature, humidity and shock. Nanobarcodes developed by Nanoplex

are written into fluorescent microspheres by photobleaching. Coating on PET bottles will expand the packaging of sensitive juice or beer beverages

5. Possible Risks

Consumers are hesitant to buy nanotechnology foods or food with nanotechnology packaging. However, some results suggest that nanotechnology packaging is more beneficial than nanotechnology foods. The main concern with the application of the nanotechnology in food packaging is related to the fact that the very small sizes of the nanoparticles have different chemical and physical properties in respect of macroscale materials and it is possible they could cause health problems. New packaging materials must have good barrier properties to oxygen, carbon dioxide, water vapour and flavour compounds. This controlled release packaging is another example of a nanomaterial application in active packaging. Nanoclays can be used as carriers for the active agents with high efficacy because it is highly dispersed in the polymeric matrix and, hence, exposed more efficiently to the substance on which it is required to act. Potential implications for consumer safety are migration of nanoparticles. They can enter into body through ingestion, inhalation or dermal contact leading to health effects of exposure to some insoluble, persistent nanoparticles. Such health effects are currently not known. Nanoparticles also migrate to foodstuffs with possible adverse effects on food quality. Other concern is with degradability of bio-polymers and formation of degradation products with possible adverse effects. Also, may appear potential environmental impacts of nano-polymer composites and some problems with end-of-life treatments as recycling, re-use and disposal. Detecting the migration of nanomaterials requires more sensitive analytical techniques due to the complexity of the nanomaterials and because they represent only a very small portion of the bulk food. Migration into food can cause both undesirable organoleptic changes (migration of TiO₂ into lipid matrix results in rancidity) and in some cases nanoparticles of bioactive compounds are intended to be released deliberately.

A considerable number of migration studies were found for nanosilver containing polymer composites or coatings. Overall the results from these studies suggest the production method of nanocomposites (e.g., incorporation or coating, surfactant modification), starting silver concentration, temperature, time and choice of contact medium are all factors which may have an effect on the extent of silver ion migration into food simulants. In general, the rate of migration increases when nanosilver is coated onto the food packaging material or surfactants are added, when the storage temperature and length of storage increases and the acidity of the contact medium increases. There appears to be a specific time of storage, after which a steady state release of silver is achieved. This is supported also by a repeat contact migration experiments, which found silver migration decreased considerably (by an order of magnitude) after first contact. Nevertheless, there is some evidence to suggest that if silver nanoparticles do migrate into food/food simulants, they would most likely dissolve quickly into ionic silver. The majority of the migration studies found for nanosilver food packaging composites have shown levels of migration of ionic silver into foods and food simulants below the European specific migration limit (SML) of 0.05 mg Ag/kg food, suggesting low consumer exposure and subsequently low risk of adverse effects. However, there are also several studies, in which migration exceeded this limit. This indicates that for new food packaging products containing nanosilver, the migration experiments should be conducted in each particular case. Migration of intact nanoparticles into food simulants is negligible, implying consumer exposure to these materials is likely low. This suggests there is low potential for safety issues related to the nanosize level of the materials incorporated into food packaging. If they migrate in nanoparticulate form, it would be anticipated at the resulting low concentration in food that many of the metal oxide nanoparticulates would likely dissolve into their ionic forms upon contact with acid foods or stomach acid. Theoretically, potential consumer exposure to nanomaterials incorporated into food packaging will appear if: they migrate into foodstuffs or drinks from the packaging, or if the nanocomposite polymers degrade and 'dissolve' into food or drinks. Migration can theoretically occur if nanoparticles desorb from the surface of the packaging material due to weak bonding at the surface (only really relevant for coatings), diffuse into foods as a

result of a concentration gradient, or dissolve resulting in ions released into food [209,290]. However, currently, there are no internationally protocols or standards concerning nanomaterials characterization or to assess their implications on the consumers health [291–293]

6. Commercial Level

The companies producing nanoreinforced food packaging materials are Color Matrix Corporation manufacturing Imperm a high barrier nylon multilayer bottles films; Mitsubishi Gas Chemical Comp. Nanocore producing NANO-N-MXD6 for PET bottles; Lanxess for Durethan KU2-2601; Honeywell polymer with Aegis NC and OX as coating PA6 on paperboard and coinjection PET bottles [33], NanoSealTM Barrier Coating and Bairicade XTTM Barrier Coating (from NanoPack Inc, Wayne, PA, USA) described as a water based coating comprised of a master batch and a liquid dispersion of clay platelets ('nano' or particle size is not mentioned). The coating is applied to traditional packaging films to enhance gas barrier properties and is stated to be approved for indirect food contact (i.e., used with dry and moderately dry food applications).

Nanocor Inc. Developed Imperm® as multilayer PET bottle and sheets is used to improve barrier properties and Nylon MXD6 Nylon MXD6-Ultra Barrier System [294], Duretham® KU 2-2601 (LanXess GmbH, Cologne, Germany) nylon nanocomposites for films and paper coating designed for medium barrier applications, requiring excellent clarity; Aegis® (Honeywell, NJ, USA) a polymerized nanocomposite film incorporating an active oxygen scavengers and passive nanocomposite clay particles.

"Micro-pore-plugging" film as single nanolayer on PET, manufactured by Tera-Barrier, provides transparency and stretchability for applications in food, medical and other packaging markets. Coating of 400 nm is obtained by slot die and has WVTR (40 °C and 100% RH) of 5×10^{-2} g/(m² day), transparency 86% (PET 87%) at 550 nm, stretchability > 5%, average roughness 10.3 nm. Sidel trade name used for less sensitive foods are a coating of about 200 nm thick obtained inside PET bottle wall by acetylene plasma.

Barrier films are manufactured by Clariant and Nanocore from PP and respectively Nylon with organoclay for packaging or PET beer bottle.

Purdue University developed a large-scale manufacturing process that may change the way some grocery store foods are packaged. This new manufacturing process uses cellulose nanocrystals as advanced barrier coatings for food packaging. The Purdue manufacturing technique is a roll-to-roll manufacturing process using waterborne polymer systems being scalable [77]. By their studies it appreciated that food packaging is a growing billion-dollar market and overall predicted growth is expected to reach 6 percent by 2024. Advanced barrier coatings, which help to protect grocery items such as foods and beverages, are growing by as much as 45 percent each year.

7. Conclusion and Future Trends

The global trade of active food packaging was estimated to be around US \$12,000,000,000.00 in 2017 [295]. The active food packaging market is dominated by oxygen scavenging and moisture absorption applications [296,297]. Consideration must also be given to requirements of different regulatory agencies, under the jurisdiction of the Food and Drug Administration (in the United States), the European Food Safety Authority (in the European Union), or for each country. Non-migratory technologies produced by either covalent immobilization, cross-linked layer-by-layer deposition, or some photografted coatings offer a potential regulatory benefit. Migration testing using standardized simulants (water, 3% acetic acid, 15% ethanol, olive oil, iso-octane and 95% ethanol) must be performed to quantify levels of migrants in packaged product systems [298]. A benefit to coatings over bulk material modification is that bulk material properties should remain intact. However, the influence of the coating on processability, thermomechanical properties, barrier properties and seal strength must be characterized [299]. Rigorous application tests must also be performed to ensure that neither material conversion steps nor end use result in delamination of active coatings. Many of the coatings

technologies have potential for scalability to roll-to-roll, high throughput coating operations. Finally, while incorporation of active agents and specialized packaging processes will indeed increase material cost, the opportunities for new products, enhanced safety and reduced waste of packaged goods highlight the potential for increasing product value through smart integration of active biodegradable packaging coatings.

Nanotechnology has the potential to generate new food products and new food packaging. Analyses of individual data showed that the importance of naturalness in food products and trust were significant factors influencing the perceived risk and the perceived benefit of nanotechnology foods and nanotechnology food packaging [300–303].

Nanotechnology has been found to be a promising technology for the food packaging industry. It has proven capabilities that are valuable in packaging foods, including improved barriers; mechanical, thermal and biodegradable properties; and applications in active and intelligent food packaging including anti-microbial agents and nanosensors, respectively. However, the use of nanocomposites in food packaging might be challenging due to the reduced particle size of nanomaterials and the fact that the chemical and physical characteristics of such tiny materials may be quite different from those of their macro-scale counterparts. Migration studies must be conducted to determine the amounts of nanomaterials released into the food matrices [292]. Nanoscale dimensions can increase significantly the physical interactions, physico-chemical and chemical interfaces in materials [304]. The morphologies obtained for the nanocomposites and the ability to modify the interfaces are essential to maximize the properties. Surface treatment and intensive in optima conditions mixing are key solutions determining the nanomaterials performance. The combinations between nanofillers/matrix and bioactive compounds allow wide possibilities of mechanical, thermal, optical, electrical, barrier properties and multifunctionality to create good food packaging materials. Coating technology has undergone a wide variety of changes in the last few years to become a flexible coating process for innovative surface functions. Today, barriers and multifunctional surfaces can meet complex requirements for a wide range of applications in a variety of sectors. New technological solutions for upgrading smart products as other emerging trends are developing.

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Article

Evaluation of the Rosemary Extract Effect on the Properties of Polylactic Acid-Based Materials

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Abstract: New multifunctional materials containing additives derived from natural resources as powdered rosemary ethanolic extract were obtained by melt mixing and processed in good conditions without degradation and loss of additives. Incorporation of powdered rosemary ethanolic extract (R) into poly(lactic acid) (PLA) improved elongation at break, rheological properties, antibacterial and antioxidant activities, in addition to the biocompatibility. The good accordance between results of the chemiluminescence method and radical scavenging activity determination by chemical method evidenced the increased thermoxidative stability of the PLA biocomposites with respect to neat PLA, with R acting as an antioxidant. PLA/R biocomposites also showed low permeability to gases and migration rates of the bioactive compounds and could be considered as high-performance materials for food packaging. In vitro biocompatibility based on the determination of surface properties demonstrated a good hydrophilicity, better spreading and division of fibroblasts, and increased platelet cohesion. The implantation of PLA/R pellets, was proven to possess a good in vivo biocompatibility, and resulted in similar changes in blood parameters and biochemical responses with the control group, suggesting that these PLA-based materials demonstrate very desirable properties as potential biomaterials, useful in human medicine for tissue engineering, wound management, orthopedic devices, scaffolds, drug delivery systems, etc. Therefore, PLA/R-based materials show promising properties for applications both in food packaging and as bioactive biomaterials.

Keywords: powdered rosemary ethanolic extract; poly(lactic acid); bioactive food packaging; biomaterials

1. Introduction

The use of natural additives is gaining increasing interest in the development of new multifunctional materials as a key for new active materials strategies. Different natural essential oils have been proposed for incorporation into the polymer matrices to improve the functionality as well as the products (food and pharmaceuticals) quality and safety.

The action of natural additives is essential in reducing or even eliminating some of the main spoilage causes, such as rancidity, color loss/change, active compounds losses, dehydration, microbial proliferation, senescence, gas build-up, and off-odors, etc. [1].

Nature offers several solutions to obtain appropriate antioxidants with higher activity than those which are synthesized. Ethanolic extraction is a method by which the highest quantity of phenolic compounds can be extracted from plant leaves. Isolated compounds, as well as crude ethanol extract, showed antibacterial activities against four Gram-negative bacteria strains, *Escherichia coli*, *Pseudomonas aeruginosa*, *Klebsiella pneumoniae*, and *Enterobacter aerogenes* [2], in addition to antioxidant activity because the content in phenolic compounds is preserved [3].

The use of extracts from rosemary (*Rosmarinus officinalis*) as food preservatives is well established [4,5]. A broad range of beneficial health effects can be attributed to rosemary, such as antidepressant, antihypertensive, antiproliferative, antibacterial, antiatherogenic, hypocholesterolemic, hepatoprotective, and anti-obesity properties. The biological properties of rosemary are attributed to the contribution of its different bioactive compounds belonging mainly to the classes of phenolic acids, flavonoids, diterpenoids, and triterpenes. Rosemary samples have the highest levels of flavonoids and other compounds such as carnosol, rosmarinidiphenol, rosmadial, rosmarinic acid, and carnosic acid [6]. It was found to be very efficient to protect food against lipid oxidation [7] and is known as rosemary active packaging [8]. Antioxidative efficiency is imparted by at least 20 specific phenols, the most effective compounds are carnosol, rosmarinic acid, and carnosic acid, followed by caffeic acid, rosmanol, rosmadial, genkwanin, and cirsimarinin. Rosemary extracts derived from *Rosmarinus officinalis* L. contain several compounds which have been shown to possess antimicrobial, antioxidative, anti-inflammatory, antiviral, and anti-tumor functions. Literature reports either rosmarinic acid, an ester of caffeic acid and 3,4-dihydroxyphenyllactic acid or/and the phenolic diterpenes carnosol and carnosic acid as the principal antioxidative components of the rosemary extract (Figure 1) [9,10].

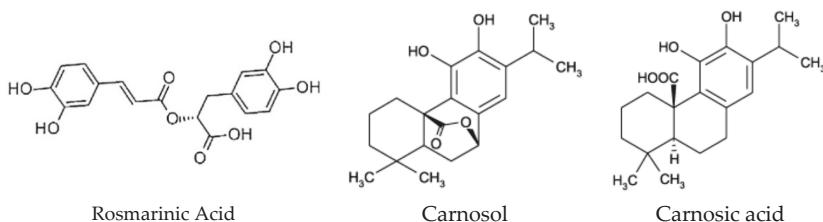


Figure 1. Chemical structure of the major antioxidative compounds in rosemary extracts.

Almost 90% of the rosemary leaf extract's antioxidant activity can be attributed to carnosol and carnosic acid [11].

Knowing that oxidative stress plays a determinant role in the pathogenesis of liver diseases, at this moment the antioxidant products from natural sources are being increasingly used to treat various pathological liver conditions. Due to its antioxidant and antimicrobial properties, rosemary essential oil (REO) is already largely used in the food industry as a preservative, while additionally possessing other health benefits. In addition to free radical scavenging activity, the REO mediates the hepatoprotective effects by activating the physiological defense mechanisms. Rašović et al. [12] have found 29 chemical compounds of a selected REO, and the main ones identified were 1,8-cineole (43.77%), camphor (12.53%), and α -pinene (11.51%). The essential oil they tested has exerted hepatoprotective effects on rats with carbon tetrachloride-induced acute liver damage, at doses of 5 mg/kg and 10 mg/kg, by diminishing aspartate transaminase (AST) and alanine aminotransferase (ALT) activities by up to two-fold and preventing lipid peroxidation in liver homogenates. Moreover, pre-treatment with the tested essential oil for seven days has significantly reversed the activities of antioxidant enzymes

(such as catalase, peroxidase, glutathione peroxidase, and glutathione reductase) in liver homogenates, mainly using a dose of 10 mg/kg.

Polylactic acid (PLA) is one of the well-known biodegradable, biocompatible, non-toxic, and eco-friendly polyesters. The low cost and attractive materials properties of PLA would open many applications. Despite the great advantages of PLA, it presents poor toughness, thus its use in obtaining materials that require high deformation capabilities is limited. There are several ways to improve PLA's processability, flexibility, and ductility, such as: blending with polymers, copolymerization with other monomers, plasticization using biocompatible plasticizer, or incorporation of filler materials [13]. The most promising method to increase PLA flexibility for film manufacturing as well as to improve the compatibility between PLA and other additives in the blend has been proven to be blending with low-molecular-weight polymers, which act as plasticizers [14]. An efficient plasticizer for PLA must reduce the glass transition temperature and the crystallinity, not migrate and show miscibility with the matrix, and possess a low volatility and a lack of toxicity [15]. Depending on the targeted application, there are various types of plasticizers for PLA, but in view of obtaining sustainable materials, mostly eco-friendly plasticizers are used today [16]. Literature shows possible plasticizers used for PLA processing, such as, oligomeric lactic acid, L-lactide, poly(ethylene glycol) (PEG), epoxidized soybean oil (USE), citrate esters, glycerol, and glucose monoesters [14,17]. Among these, the most common and suitable plasticizer for PLA has been reported to be low-molecular-weight PEG due to its miscibility, biodegradability, glass transition temperature (T_g) reduction, and approval for food-contactable materials [13,17]. The major characteristics of PEG are its biocompatibility, water solubility, and low cost that recommend its use in biomaterials composition [18].

PLA and its composites are currently being extensively studied to obtain degradable food packaging and are also widely used in human medicine for tissue engineering, wound management, orthopedic devices, biomedical and clinical applications in scaffolds, bone fixation devices such as screws and plates, surgical suture and meshes, medical implants, drug delivery systems, etc. [19–22].

As natural additives are too volatile to be directly used in the processing technologies, a viable alternative is to incorporate these compounds into materials as natural active additives with the possibility to be released from the material of interest and to reduce their volatility. The release rate of active substances such as antioxidants from a packaging material can be evaluated through migration studies, usually performed using food simulants and conditions specified in the European food packaging regulations [23,24]. As it is desirable to place the samples in contact with the food simulant in the worst foreseeable conditions of time and temperature pertaining to actual use, and as increasing the temperature accelerates the migration, the conditions for the release studies were 40 °C for a minimum of ten days with a 50% aqueous ethanol solution used as a food simulant. This is known as a modified D1 food simulant, which is assigned as a conventional simulant selected for foods with lipophilic character, oil-in-water emulsion character, hydrophilic foods containing relevant amounts of organic ingredients, and for hydrophilic alcohol-containing foods with over 20% alcohol content. Generally, food simulant D1 can be considered to be the most severe aqueous food simulant for hydrophilic non-acidic foods [23]. Since ethanol is commonly used as a food simulant, the 50% aqueous ethanol solution was chosen to perform these tests in order to comply with the latest approved directives on migration testing (EU EC. No. 10/2011) [23]. Through ethanol sorption in the PLA matrix, voids or swelling of the film can occur, facilitating penetration within PLA chains and promoting the migration of the active substances [25,26].

In this paper antimicrobial and antioxidant activity was offered to the PLA by mixing with ethanolic rosemary extract as a powder. This was obtained by alcoholic extraction of the rosemary leaves followed by precipitation [27].

2. Experimental

2.1. Materials

Polylactic acid (PLA) obtained from renewable resources from NatureWorks LLC (trade name: PLA 2002D, Minnetonka, MN, USA) is a transparent material with a melt flow index of 5–7 g/10 min (conditions 210 °C/2.16 kg) and a content of 96% L-lactide and 4% isomer D. Average molecular weight determined by GPC was 4475 kDa. It has a density of 1.25 g/cm³, melting point of 152 °C, glass transition temperature of 58 °C. The crystallinity depends on the isomer content and thermal history. Water permeability at 25 °C was 172 g/m²·day and percentage of biodegradation/mineralization is 100% [16].

Poly(ethylene glycol) (PEG) BioUltra 4000 purchased from Sigma-Aldrich (St. Louis, MO, USA) was used as a plasticizer.

Powdered rosemary ethanolic extract (R) was obtained following a previously reported procedure by the solvent extraction method in a Soxhlet unit [27] involving the alcoholic extraction of the rosemary leaves followed by precipitation. Fresh rosemary leaves were collected from local farms, dried at ambient temperature and subsequently milled, cleaned, and powdered in a grinder (Laboratory of Radiation Chemistry, INCDIE-ICPE CA. Bucharest, Romania). The vegetal material was then refluxed in 2 L of ethanol at 65–75 °C for 10 h during continuous extraction in the Soxhlet apparatus (Laboratory of Radiation Chemistry, INCDIE-ICPE CA. Bucharest, Romania). The extract in ethanol solution was subjected to precipitation induced by the addition of water as non-solvent and a solid phase was finally filtered, washed with acetone, dried in air, and further dried under vacuum at ambient temperature. A greenish-yellow fine powder was obtained and stored in desiccators to avoid the absorption of moisture.

All other reagents were of analytical grade purity.

The composition of the rosemary ethanolic extracts was detailed and studied because of the importance of its biological activity in various applications. As previously mentioned in the introduction, the rosemary extracts, especially the ones derived from the leaves, are usually herbal products used as natural antioxidant and flavoring agents in food processing and cosmetics. In the present study, the phenolic and flavonoids contents have been determined according to the following methods.

2.1.1. Determination of Total Phenolic Content

Total phenols content was determined using Folin-Ciocalteu's reagent (FC) method as presented in the work of Scalbert et al. [28]. Powdered rosemary extract (0.01 g) was added to 10 mL methanol and then 0.1 mL of methanolic solution was diluted with 0.4 mL of double distilled H₂O. FC/H₂O solution (1:10 v/v) (1 mL) was added to 0.5 mL diluted methanol/R extract and left for 10 min at 25 °C after a strong mixing. A 2 mL solution of 15% sodium carbonate (Na₂CO₃·10H₂O) was added, and after 1 h of incubation, the absorbance was read at 740 nm with a Cary 60 UV-Vis spectrophotometer (Agilent Technologies, Santa Clara, CA, USA) against a freshly prepared blank sample. The blank sample contained 0.1 mL methanol without powdered rosemary ethanolic extract, 0.4 mL of water, 1 mL FC reagent solution, and 2 mL of Na₂CO₃·10H₂O solution. Solutions of gallic acid (used as standard) in methanol of different concentrations (0.01–1 mg/mL) were prepared and based on the measured absorbance at 740 nm, the calibration curve was drawn. The obtained calibration curve was then used for the determination of the total phenolics content expressed as mgGAE/g dw (mg of gallic acid equivalent per g of dry weight). The determination was made in triplicate and an average value was obtained. The resulted total phenolic content was of 112.5 mg GAE/g dw.

2.1.2. Determination of Total Flavonoids Content

Total flavonoid content was determined by the aluminum chloride colorimetric assay [29]. A quantity of 1 mL of extract (1 mg/mL powdered rosemary ethanolic extract) or standard Quercetin

(of different concentrations) was added to 4 mL of H₂O. Then, at different time intervals the following solutions were added consecutively: 0.30 mL of 5% NaNO₂; 0.3 mL of 10% AlCl₃ after 5 min; and 2 mL of 1 M NaOH after another 5 min. At the end, the volume was made up to 10 mL with H₂O, mixed, and absorbance was measured against the blank sample at 510 nm. The total content of flavonoids was expressed as mg Quercetin Equivalents (QE)/g dw. The measurement was made in triplicate and an average value was reported. Thus, a total flavonoids content of 261.5 (mg QE/g dw) was found.

The obtained values both for phenolic and flavonoids content of the powdered ethanolic rosemary extract are close to those found in the literature, which explain, in part, its good antioxidant properties [30].

2.2. PLA-Based Blends Processing

PLA-based blends were prepared using different amounts of powdered ethanolic rosemary extract (R) by incorporation into a PLA matrix in the melt state. Before mixing, drying of the additives and PLA was done in a vacuum oven (Binder, Tuttingen, Germany) for 6 h at a temperature of 80 °C. The compounding was performed for 10 min, at 175 °C, and 60 rpm, by means of a Brabender mixer (30EHT, Duisburg, Germany). A Carver press (Wabash MPI, IN, USA) and special parameters for compression molding (175 °C, or 165 °C for PLA/R blends, pre-pressing for 3 min at 50 atm and a pressing for 2 min at 150 atm) were used to obtain specimens for different analyses. Both films (thickness of ~0.15 mm), as well as sheets (thickness of ~1 mm), were prepared for different analyses that required specific thickness. Sheets were used for mechanical (tensile) and rheological tests (1 mm distance between parallel plates) while films were used for spectral characterization, permeability tests, etc. The compositions of the prepared systems are shown in Table 1.

Table 1. Compositions of the prepared poly(lactic acid) (PLA)-based systems.

No.	Sample	PLA (wt %)	Powdered Rosemary Ethanolic Extract (R) (wt %)	PEG (wt %)
1	PLA	100	-	-
2	PLA/0.25R	99.75	0.25	-
3	PLA/0.5R	99.5	0.5	-
4	PLA/0.75R	99.25	0.75	-
5	PLA/PEG	80	-	20
6	PLA/PEG/0.5R	79.5	0.5	20

2.3. Investigation Methods

2.3.1. Processing Behavior

Processing behavior was evaluated by analysis of processing characteristics following the torque-time curves registered during blending on a Brabender mixer.

2.3.2. Scanning Electron Microscopy (SEM)

The samples were fixed on copper supports for the SEM investigation and the surface of the films was examined as such, without metal coating. An Environmental Scanning Electron Microscope (ESEM) type Quanta 200 Instrument (FEI Company, Hillsboro, TX, USA) was used, operating at 25 kV with secondary electrons in low vacuum mode (LFD detector).

2.3.3. ATR-FTIR Spectroscopy

A Bruker VERTEX 70 spectrometer (Ettlingen, Germany) was used to record the Attenuated Total Reflectance-Fourier Transformed Infrared ATR-FTIR spectra by a 4 cm⁻¹ resolution. Both the spectra of samples as well as background were recorded in the wavenumber interval of 4000–600 cm⁻¹, and the OPUS program was used for the processing of spectra.

2.3.4. Stress-Strain Measurements

Tensile measurements were performed at room temperature on dumbbell-shaped samples, by means of an Instron Single Column machine (3345, Norwood, MA, USA), according to EN ISO 527-2/2012. The load cell was of 1 kN, the loading speed was of 10 mm/min, and the gauge length was 40 mm. Young's modulus, tensile strength at break, and strain at break have been evaluated.

2.3.5. Dynamic Rheology

An Anton Paar rheometer (MCR301, Graz, Austria) was used to study the rheological properties of the PLA/R composites. Oscillatory frequency sweeps were performed using a geometry with a parallel plate of 25 mm in diameter, at 175 °C, and a strain of 10% (linear viscoelasticity region) in the range between 0.05 to 500 rad/s.

2.3.6. Differential Scanning Calorimetry (DSC)

Thermal analysis of PLA/R composites was performed under a nitrogen atmosphere by means of a TA Instruments Q20 Dynamic Scanning Calorimeter (New Castle, DE, USA). Each sample of ~10 mg was cooled down to 0 °C and heated up to +250 °C, which was below the glass transition and above the melting temperature of the materials. After the first heating run, each sample was kept for 2 min and then cooled down to 0 °C with a cooling rate of 5 °C/min and reheated up to 250 °C with a heating rate of 10 °C/min. As PLA is a semicrystalline polymer with a low crystallinity, the cooling rate must be slower than the heating rate in order to increase the crystallinity. An empty crucible was used as a reference. The parameters achieved through the DSC experiments were the glass transition temperature, cold crystallization, as well as the melting temperature and crystallinity. The degree of crystallinity of the investigated samples was obtained by dividing the melting enthalpy of the sample by $\Delta H_m = 93.7 \text{ J/g}$ [31], which is equilibrium enthalpy of PLA sample with 100% crystallinity (PLA 100%).

2.3.7. Thermogravimetry–Infrared Spectroscopy/Mass Spectrometry (TG-FTIR/MS) Coupled Analysis (TG-FTIR/MS)

The thermal behavior of the samples and evolved gases analyses were performed using a TG-FTIR/MS system. The system is equipped with a thermobalance STA 449F1 Jupiter (Netzsch, Germany), spectrophotometer FTIR model Vertex-70 Bruker, (Ettlingen, Germany) and mass spectrometer QMS 403C Aeolos (Netzsch, Germany). The thermogravimetric analyzer was calibrated for temperature and sensitivity using the melting point of some standard metals (Hg, In, Sn, Bi, Al) from –38.5 °C to 800 °C. The temperature reproducibility was ± 2 °C. The heating program was between 30–600 °C, with a $10 \text{ }^{\circ}\text{C min}^{-1}$ heating rate and nitrogen as a carrier gas with a flow rate of 50 mL min^{-1} . The samples (7–8 mg) were heated in an open Al_2O_3 crucible, and Al_2O_3 was used as the reference material. The gases released during the thermal degradation were transferred by two isothermal transition lines to the FTIR and mass spectrometer. The transfer line to the FTIR spectrophotometer is heated at 190 °C, the gases are introduced in TGA-IR external modulus (gas cell V = 8.7 mL) and the spectra are recorded on a $600\text{--}4000 \text{ cm}^{-1}$ domain with a resolution of 4 cm^{-1} . The acquisition of FTIR spectra in 3D was done with OPUS 6.5 software (Ettlingen, Germany) that measures from the start and synchronizes across all the apparatus. On the other hand, the transfer line to the mass spectrometer is heated at 300 °C and the volatile degradation products are directly transferred to an electron impact ion source of 70 eV. The data acquisition was achieved with Aeolos® 7.0 software (Netzsch, Germany), in the scan bar graph mode on the range $m/z = 1\text{--}300$.

2.3.8. Chemiluminescence

Chemiluminescence (CL) spectra were recorded on small-weight samples (max. 5 mg) by means of a LUMIPOL 3 unit (SAS, Bratislava, Slovakia) instrument as non-isothermal dependencies of the

recorded intensity on the temperature of samples. The temperature interval used for measurements started from room temperature until 250 °C, and a low error (± 0.5 °C) was associated with measured temperatures. CL measurements were performed in air under static conditions using different heating rates, namely 2, 3.5, 5, and 10 °C/min. The intensity values of CL were normalized to sample mass for their reliable comparison.

2.3.9. Antioxidant Activity Evaluation

The ABTS•⁺ (2,2'-azino-bis(3-ethylbenzothiazoline-6-sulfonic acid) diammonium salt radical cation scavenging assay can be used to assess the antioxidant activity of both hydrophilic and hydrophobic compounds. To obtain the ABTS•⁺ radical cation, 2.5 mL of 7 mM ABTS is mixed with 2.5 mL 14.7 mM potassium persulphate (KPS) aqueous solutions and the mixture is left in the dark, at room temperature, for 16 h. By the direct reaction between ABTS and KPS, the ABTS•⁺ radical cation is generated, which is a blue-green chromophore, that can undergo a reduction reaction in the presence of an antioxidant. This reaction determines a loss of absorbance at 750 nm. Using Equation (1), the antioxidant capacity was calculated and the resulting values were expressed as percentage inhibition.

$$\text{Inhibition}(\%) = \left[\frac{A_{\text{control}} - A_{\text{sample}}}{A_{\text{control}}} \times 100 \right] \quad (1)$$

In the case of polymeric composites, the reaction mixture consisted of adding different volumes (mL) of the reaction mixture and 2 mL of ABTS radical solution. The reaction mixture was obtained by placing 80 mg of sample in 5 mL ethanol and stirred for 24 h at room temperature (20 °C).

2.3.10. Antimicrobial Activity

The antimicrobial activity against *Bacillus cereus*, *Salmonella typhymurium*, and *Escherichia coli*, included four experimental steps as follows. The first stage was the sterilization of samples in an autoclave at 110 °C and 0.5 bars for 20 min. The second step consisted in the American Type Culture Collection (ATCC) culture bacteria contamination where the preparation of ATCC cultures was done by seeding of the pre-enrichment medium and incubation for 24 h at 37 °C; then, the colonies were counted in 0.1 mL culture by selective culture medium separation; and 0.1 mL bacterial culture ATCC was seeded using a sterile swab samples surface. The third step consisted in the incubation of samples contaminated with the ATCC for 24 h at 25 °C in the dark, in sterilized glass Petri dishes, repeated for another 24 h incubation. The last step involved the identifying of target germs. The following standardized methods of bacteriology procedures were used, according to standards in force: SR ISO 16649—*E. coli*; ISO 7932:2004 ISO 21871:2006(en)—*Bacillus cereus*, SR EN ISO 6579—*Salmonella* spp.

2.3.11. Gas Permeability

The gas transmission rates of CO₂ and O₂ were recorded by means of a Lyssy L100-5000 (Systech Instruments Ltd., Johnsburg, IL, USA) manometric gas permeability tester (~4 h to equilibrium for CO₂ and ~7 h to equilibrium for O₂). Specimens with 108 mm × 108 mm × 0.2 mm dimensions were used. Four determinations were made for each sample and the average value was reported.

2.3.12. Migration Study

The migration of the active components belonging to the powdered rosemary ethanolic extract from the different polymeric PLA-based films was investigated by a total immersion migration test (EC, 1997) [32] using 50% aqueous ethanolic solution as a food simulant assigned for fatty foods which frequently undergo oxidation [33]. The release studies were performed at 40 °C for a minimum of 10 days by keeping the samples in an oven, and the selected testing conditions simulate storage at ambient temperature for an unlimited duration. The migration tests were performed with pieces of

films of about 1 cm² in 5 mL of simulant. A blank test for the simulant and each type of control sample was carried out previously.

Aliquots of ~1 mL withdrawn from the release medium at predetermined time intervals were analyzed at 285 nm by means of a Cary 60 UV-VIS spectrophotometer (Agilent Technologies, Santa Clara, CA, USA) by scanning from 200 to 600 nm. Samples were run in quartz cuvettes with a 1 mm path length.

The active components' concentrations were calculated based on the calibration curve previously determined at 285 nm for the main components of rosemary extract, since for rosmarinic acid the λ_{\max} values are reported in literature as 254, 290, and 328 nm, and for carnosol and carnosic acid at 283 and 246 nm [34,35]. The chosen λ_{\max} value can be attributed to overlapped maxima corresponding to rosemary extract active ingredients since all of them contain the aromatic double bond.

The corresponding release curves were represented as time-dependent plots of the cumulative percentage of active component released.

In order to evaluate the migration kinetic parameters and to establish the release mechanism involved, the release data were fitted first to the Korsmeyer-Peppas model using the Equation (2) [36,37]:

$$M_t/M_\infty = k \cdot t^n \quad (2)$$

The migration data were also fitted to the Higuchi kinetic model, using the Equation (3):

$$M_t/M_\infty = k_H \cdot t^{1/2} \quad (3)$$

where M_t/M_∞ represents the fraction of bioactive compound (s) released at time t , n is the release exponent and k and k_H are the release rate constants for each model considered.

The power law release exponent n describes the release mechanism from a thin polymer sample: a value of $n = 0.5$ corresponds to a Fickian diffusion mechanism, $0.5 < n < 1$ to non-Fickian/anomalous transport, $n = 1$ to Case II transport, and $n > 1$ to super case II transport [36,37].

2.3.13. Biocompatibility Evaluation

In Vitro Biocompatibility Evaluation—Contact Angle (CA) and Surface Free Energy (SFE).

By the sessile drop method, the contact angle (CA) of the polymeric sample surfaces was measured using a CAM-200 instrument from KSV (Helsinki, Finland) at room temperature and a controlled humidity. A 1 μ L drop of water was placed on the film's surface and after 10 s the static contact angle was recorded. To evaluate the wettability at least ten contact angle CA measurements were realized in different locations on the surface and the obtained average values were used further. For more details on the method see references [38,39]. To determine the surface free energy (SFE) components, the CA at equilibrium between the film surface and three pure liquids (in addition to water, methylene iodide, and formamide were used, as-purchased at maximum obtainable purity) were measured by fitting the drop profile using the Young-Laplace equation [40–43]. The acid/base (LW/AB) approach of van Oss and Good, see Equation (4) [44,45], was used to calculate the total SFE and its components, namely the dispersive component, also named the Lifshitz–van der Waals interaction, (γ_{sv}^{LW}) and polar Lewis acid-base interactions (γ_{sv}^{AB}), respectively, see Equation (5). The acid-base interactions are subdivided into electron donor γ_{sv}^- (Lewis base) and electron acceptor γ_{sv}^+ (Lewis acid) parts, see Equations (4)–(6). The subscripts “ lv ” and “ sv ” denote the liquid-vapor and surface-vapor interfaces.

$$(1 + \cos \theta) \gamma_{lv} = 2 \left(\sqrt{\gamma_{sv}^{LW} \gamma_{lv}^{LW}} + \sqrt{\gamma_{sv}^+ \gamma_{lv}^-} + \sqrt{\gamma_{sv}^- \gamma_{lv}^+} \right) \quad (4)$$

$$\gamma_{sv}^{AB} = 2 \sqrt{\gamma_{sv}^+ \gamma_{sv}^-} \quad (5)$$

$$\gamma_{sv}^{TOT} = \gamma_{sv}^{LW} + \gamma_{sv}^{AB} \quad (6)$$

where θ is the contact angle, γ_{sv} is the liquid's total surface tension, and γ_{lv}^{LW} and γ_{sv}^{LW} are the apolar (dispersive) Lifshitz–van der Waals components of the liquid and the solid, respectively, whereas $\gamma_{sv}^+ \gamma_{lv}^-$ and $\gamma_{sv}^- \gamma_{lv}^+$ are the Lewis acid–base contributions of either the solid or the liquid phase as indicated by the subscripts. To determine the total surface free energy of the solid material (γ_{sv}^{TOT}) a system based on Equation (4) must be used. To solve the resulting systems of equations it is necessary to use at least three test liquids with known γ_{lv} , γ_{lv}^{LW} , γ_{lv}^- , and γ_{lv}^+ , see Table 2 [45–48].

Table 2. Surface tension parameters (mN/m) of the liquids used for contact angle measurements.

Liquid	γ_{lv}^{TOT}	γ_{lv}^{LW}	γ_{lv}^{AB}	γ_{lv}^+	γ_{lv}^-
Water	72.80	21.80	51.00	25.50	25.50
Formamide	58.00	39.00	19.00	2.28	39.6
Methylene iodide	50.80	50.80	0.00	0.72	0.00
Red blood cells (rbc) [49]	36.56	35.2	1.36	0.01	46.2
Platelets (p) [49]	118.24	99.14	19.1	12.26	7.44

The manner in which the surface of the materials interacts with the constituents of blood, such as platelets and red blood cells, determines if the tested materials are blood compatible. Evaluating the surface/interfacial free energy of a material can represent an *in vitro* method to determine biocompatibility. Equation (7) was used to establish if the obtained materials present blood compatibility, where $W_{s/rbc}$ and $W_{s/p}$ denote the red blood cells and platelets work spreading [49]. When a biomaterial is exposed to blood it can cause the adhesion of blood cells onto surface, and the extent of this adhesion will determine the life of the implanted biomaterials. By such cells adherence to biomaterial surfaces the coagulation and immunological cascades could be activated [50].

$$W_s = W_a - W_c = 2 \left(\sqrt{\gamma_{sv}^{LW} \gamma_{lv}^{LW}} + \sqrt{\gamma_{sv}^+ \gamma_{lv}^-} + \sqrt{\gamma_{sv}^- \gamma_{lv}^+} \right) - 2\gamma_{lv} \quad (7)$$

where W_s —work of spreading (the negative free energy associated with spreading liquid over the solid surface); W_a —work of adhesion (defined as the work required separating the liquid and solid phases) and W_c —work of cohesion (defined as the work required separating a liquid into two parts) [41].

In Vivo Biological Evaluation

White male Wistar rats (200–250 g) were used in the experiment. The animals were housed under a standard laboratory environment (relative humidity 55–65%, chamber temperature 23.0 ± 2.0 °C and 12 h of light: Dark sequence (lights on at 6:00 a.m.) and fed with a specific diet and water ad libitum, excluding the time of the investigations. Before the assessment, the animals were positioned on a raised wire mesh, under a clear Plexiglass container and allowed 2 h to familiarize themselves to the testing room.

Rats were randomly assigned into eight groups of six animals each according to the following protocol: Group 1: Control (C)—distilled water; Group 2: R—powdered rosemary ethanolic extract; Group 3: PLA; Group 4: PLA/0.25R; Group 5: PLA/0.50R; Group 6: PLA/0.75R; Group 7: PLA/PEG; and Group 8: PLA/PEG/0.5R.

In the first day of the investigations, under general anesthesia (with ketamine 50 mg/kg body weight and xylazine 10 mg/kg body weight), the samples (weighing 62 mg) were placed subcutaneously, in one side in the rat's dorsal region, after a small incision, and subsequently sutured. Cotton pellets, of 62 mg, impregnated with distilled water (0.3 mL) and respectively with R solution (0.3 mL), were subcutaneously inserted into control animals. Pellets and the implanted samples behaved like foreign materials generating a subacute inflammatory response.

The in vivo biocompatibility of PLA-based materials containing rosemary ethanolic extract was evaluated by estimating the influences on the hematological and serum biochemical tests and on certain immune system parameters [51,52].

After certain time intervals (24 h and 7 days) following the implantation of PLA-based materials containing rosemary ethanolic extract, 0.3 mL of blood samples were collected from retro-orbital plexus and the following parameters were determined: Blood count, aspartate transaminase (AST), alanine aminotransferase (ALT), and lactic dehydrogenase (LDH) activity, as well as, serum urea and creatinine levels [53].

At the same time in the experiment, the serum complement activity, and the phagocytic capacity of peripheral neutrophils (Nitro Blue Toluene—NBT test) were also established [54]. These parameters belong to specific tests used to quantify the influence of pharmacologic agents on the immune defense capacity of laboratory animals [55].

The data were expressed as mean $+/-$ standard deviation (S.D.) and processed using SPSS variant 17.0 for Windows 10, to estimate the differences between the control group and the groups receiving the investigated substances. The values of coefficient *p* (probability) below 0.05 compared with those of the control group were considered to be statistically significant.

Ethics statement: The experimental research protocol was approved by the local Animal Ethics Committee of the “Grigore T. Popa” University of Medicine and Pharmacy, Iași, Romania, in strict observance of the international ethical regulations on laboratory animal work (AVMA Guidelines on Euthanasia, 2007). Biocompatibility tests were performed according to the “Grigore T. Popa” University of Medicine and Pharmacy guidelines for the handling and use of experimental animals and in accordance with the recommendations and policies of the International Association for the Study of Pain [56].

Each animal was used only once and the length of the experiments was kept as short as possible. For ethical considerations, all the animals were euthanized at the end of the experiment [57].

3. Results and Discussion

Films and sheets resulting from the melt mixing process are transparent and homogeneous and at high R concentration show a little yellowing.

3.1. Processing Behavior

The torque-time curves were registered during blending in a Brabender mixer in order to evaluate the processing behavior by analyzing torque values at different mixing times. Melt processing characteristics of PLA and its blends—Table 3—are not changed by the incorporation of the powdered rosemary ethanolic extract.

Table 3. Melt processing characteristics of PLA and its blends with rosemary solid extract.

Sample	TQ _{max1} (Nm)	TQ _{1min} (Nm)	TQ _{max2} (Nm)	TQ _{5min} (Nm)	TQ _{final} (Nm)
PLA	66.4	17.2	-	13.3	10.2
PLA/0.25R	73.8	15.7	-	11.2	10.2
PLA/0.5R	72.0	17	-	11.4	10.5
PLA/0.75R	74.6	17.6	-	11.1	10.1
PLA/PEG	12.9	0.9	-	7.3	6.5
PLA/PEG/0.5R	10.1	2.8	-	7.3	5.7

TQ_{max1}—maximum torque; TQ_{1min}—torque after one minute of mixing; TQ_{max2}—maximum torque after 1.5 min of mixing; TQ_{5min}—torque after 5 min of mixing (half processing time); TQ_{final}—torque at the end of mixing.

A sharp change in the melt mixing behavior was recorded in the presence of a plasticizer. PEG improved the melt flow, the materials being easily processed as all torque characteristics decreased. PEG favors the processing of polymers due to the increased chain mobility, therefore improving macromolecular movement. This effect was previously observed by other authors for various types

of blends containing PLA and PEG, for example in PLA/PEG/organoclays nanocomposites [13] or PLA/PHB blends [58]. No oxidation occurred during processing.

3.2. SEM Results

SEM images, presented in Figure 2, show a homogeneous distribution of the rosemary powder in the PEG plasticized PLA samples without agglomeration, which happens in the absence of the plasticizer.

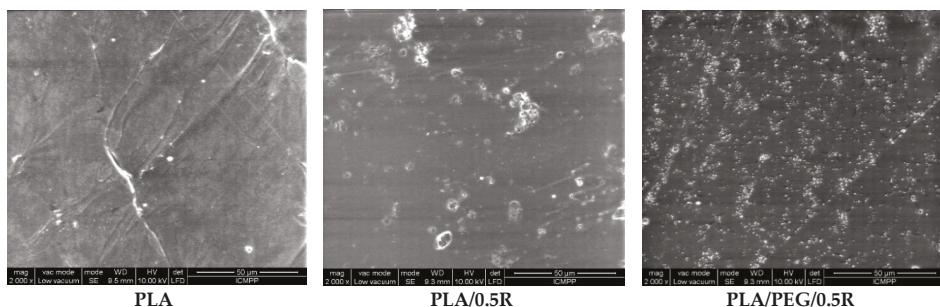


Figure 2. SEM images of PLA, PLA/0.5R and PLA/PEG/0.5R. PEG is defined as poly(ethylene glycol) and R is defined as rosemary ethanolic extract.

From SEM images, the histograms of the distribution of the particle dimensions were evaluated and are shown in Figure 3. For the PLA/0.5R sample, an average dimension of the particles of $14.2 \mu\text{m}$ was found while for PLA/PEG/0.5R this was approximately $4.1 \mu\text{m}$. Therefore, the incorporation of PEG into the PLA-based composites improves the R distribution, with the sample being more homogenous and the particles dimension histogram being narrower.

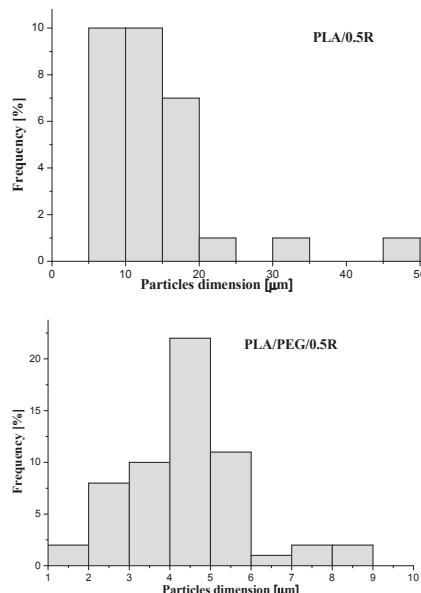


Figure 3. The distribution of particle dimensions determined from SEM images.

3.3. ATR-FTIR Data

The ATR-FTIR spectra of the PLA prior to and after loading with powdered rosemary ethanolic extract are presented in Figure 4. The IR spectrum of the PLA presents a strong band at 1749.3 cm^{-1} due to C=O stretching of the carbonyl group, while the bending vibration of this group appears at 1267.1 cm^{-1} . The bands at 867.9 cm^{-1} and 754.1 cm^{-1} are assigned to the amorphous and respectively crystalline phases of PLA. The IR bands at 2995.2 and 2945.1 cm^{-1} are assigned to the CH stretching as ν_{as} CH_3 and ν_{s} CH_3 modes.

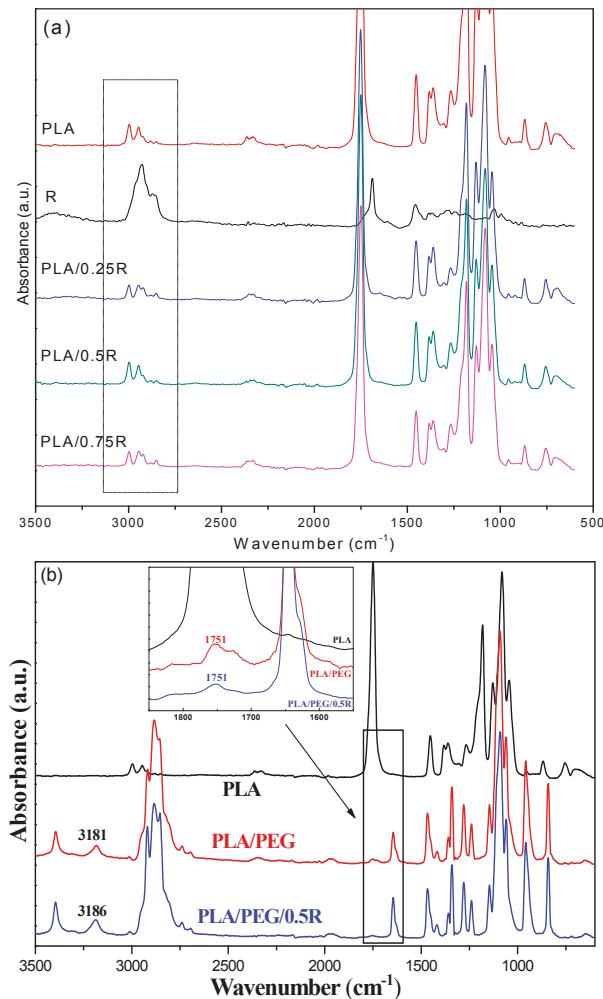


Figure 4. FTIR spectra of the neat PLA and the PLA/rosemary blends (a) and PLA/PEG/R (b); insert spectrum highlights details of different spectral regions.

The components of powdered rosemary ethanolic extract have different groups in their structures (such as COOH, C=O, phenolic) with corresponding absorption bands in the region of $1750\text{--}1600\text{ cm}^{-1}$. The R sample exhibits a relatively sharp band with a maximum at 1692 cm^{-1} corresponding to C=O vibrations, which are also present in the samples loaded with powdered rosemary ethanolic extract.

The rosemary constituents are mainly aromatic compounds and the band appearing at 1026 cm^{-1} is attributed to the deformation vibration of C–H bonds from aromatic rings [59].

The shape of the bands in the 2500 – 3500 cm^{-1} region, see the highlighted region of Figure 4a, are specific for each sample, as they are a coupling of the bands of PLA and R with insignificant shifts, while in the case of the systems containing plasticized PLA the bands' shift indicates some interactions between components due to the better distribution of the components. These bands are associated with the stretching modes of C–H overlapped with the –OH stretch from alcohols, carbonyl in aldehydes, and carboxyl groups [60].

3.4. Mechanical Properties

The Young's modulus and tensile strength increase after incorporation of R into PLA and decrease in plasticized PLA, while as is expected, the elongation at break increased and is two times higher for plasticized systems containing R– as revealed in Figure 5. An increase in the elongation at break and a decrease in the tensile strength for PLA/PEG4000 blends were previously reported [61], with ~7% elongation at break for the PLA/PEG4000 blend [62]. The mechanical properties are kept within satisfactory limits with improved elasticity for plasticized samples in the presence of R. Examples in the literature present a lack of systems containing PLA/rosemary, mostly using essential oils; therefore, it is difficult to compare results with different types of materials processed in other conditions. A PLA-based compound comprising rosemary essential oil showed a slightly decreased elongation at break by 2.8% [63].

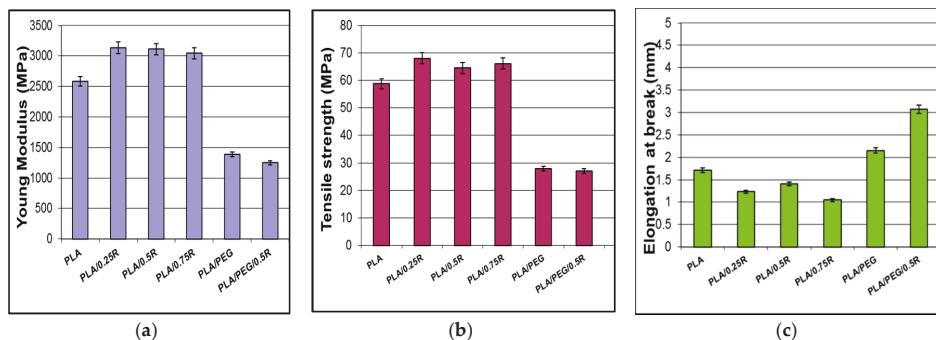


Figure 5. Mechanical properties of the PLA/R and PEG-plasticized PLA/R: (a) Young's modulus; (b) tensile strength; (c) elongation at break.

3.5. Rheological Behavior

The incorporation of the powdered rosemary ethanolic extract in the PLA films led to a decrease of all studied rheological parameters: Storage modulus (G'), loss modulus (G''), and complex viscosity, as presented in Figure 6a,b. A predominantly viscous behavior ($G'' > G'$) can be noticed both for PLA and for the PLA-based composites. The loss modulus dependence on the deformation frequency presents the same decreasing trend for the composites investigated with the differences becoming more pronounced at low frequencies. The results obtained are supported by those found by other authors comparing various formulations with that containing rosemary; the flow curve of the rosemary-containing formulation is the lowest one [64].

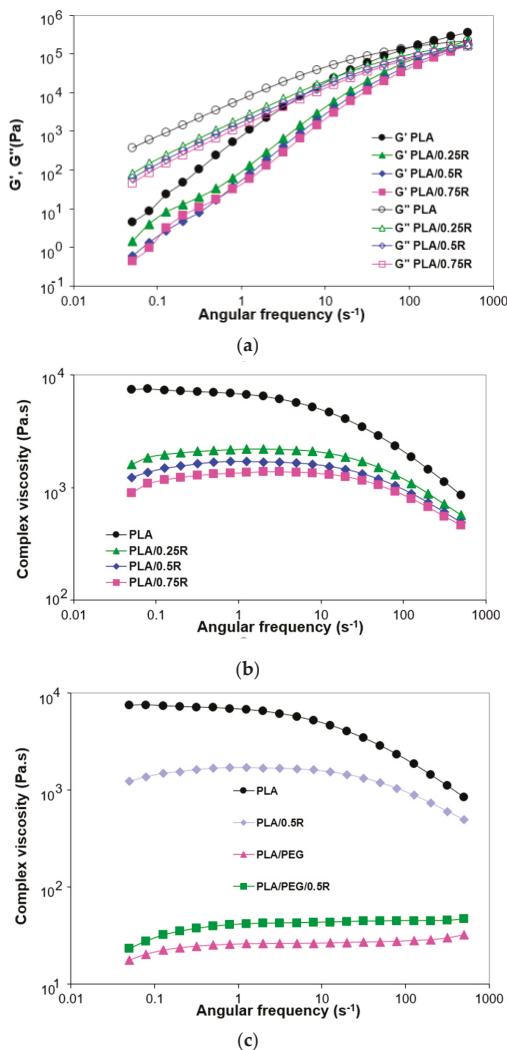


Figure 6. Angular frequency dependence of the storage modulus and loss modulus (a) and complex viscosity (b,c) for PLA, PLA/R and PLA/PEG/R systems.

The incorporated R amount maintains the decreasing order of moduli and viscosity, the highest content (0.75%) causes a drastic decrease of complex viscosity in the melt state as was also observed from the torque-time curves recorded during melt processing.

The lowest value is obtained for plasticized PLA, see Figure 6c, while the addition of R to plasticized PLA resulted in a small increase of the complex viscosity.

As shown in Table 4, the crossover frequency (ω_i) and the crossover modulus (corresponding to $G'' = G'$) were obtained at higher oscillation frequencies for the blends with an increasing R content incorporated. The relaxation time (θ)—calculated as $\theta = 1/\omega_i$ and the crossover modulus values obtained for PLA and its blends are plotted in Figure 7. For the PLA/0.75R blend, the relaxation time decreased by more than 23% compared with neat PLA, showing that less time was required for

reorientation of the entangled chains in these cases, as the rosemary powder induced relaxation and thus flexibility of the chains.

Table 4. Crossover frequency and crossover moduli values for PLA, and PLA/Rosemary blends.

Crossover Characteristic	PLA	PLA/0.25R	PLA/0.5R	PLA/0.75R
ω (s^{-1})	96.37	273.3	363.3	411.4
t (s)	10.38	3.66	2.75	2.43
$G' = G''$ (MPa)	144.5	146.9	145.2	145.4

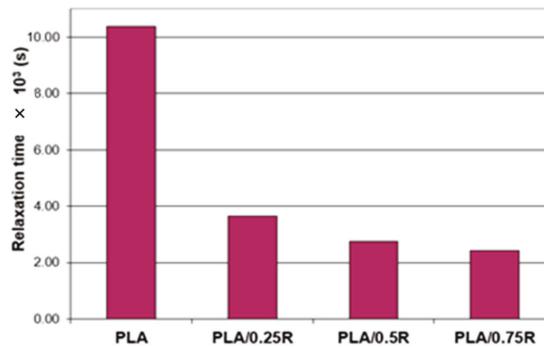


Figure 7. Relaxation time vs. sample composition.

3.6. DSC Results

The DSC curves of the PLA/R and PLA/PEG/R systems recorded both in run I and II are shown in Figure 8 and values of the thermal properties are summarized in Table 5. In the DSC curves, all particular transitions of PLA, namely, glass transition temperature (T_g), cold crystallization temperature (T_{cc}), and melting temperature (T_m) are evidenced, which show some differences between the studied systems.

Table 5. Thermal characteristics of the PLA/R and plasticized PLA/R systems determined by DSC method.

Sample	T_g ($^{\circ}$ C)	T_{cc} ($^{\circ}$ C)	ΔH_{cc} (J/g)	T_m ($^{\circ}$ C)	ΔH_m (J/g)	T_{cr} ($^{\circ}$ C)	X_{cr}
Run I							
PLA	60.64	125.89	17.69	151.63	23.12	55.80	24.6
PLA/0.25R	62.95	124.56	18.23	155.96	19.66	55.96	21.1
PLA/0.5R	64.07	124.82	10.40	154.51	10.78	56.26	11.5
PLA/0.75R	64.82	118.28	16.54	156.35	19.05	55.86	20.33
PLA/PEG	49.30	-	-	157.74	23.95	70.03	25.56
PLA/PEG/0.5R	59.59	90.23	2.6	157.07	26.06	66.70	28.39
Run II							
PLA	61.58	132.03	9.69	152.75	12.05	-	13.34
PLA/0.25R	60.96	128.95	17.14	154.01	16.4	-	17.50
PLA/0.5R	61.15	133.87	6.24	153.90	6.37	-	6.79
PLA/0.75R	60.40	133.48	7.18	154.04	7.9	-	8.43
PLA/PEG	-	91.37	0.36	154.66	25.32	-	27.02
PLA/PEG/0.5R	-	80.93	8.003	153.72	27.28	-	29.11

T_g —glass transition temperature; T_{cc} —cold crystallization temperature; T_m —melting temperature; T_{cr} —crystallization temperature; ΔH_{cc} —cold crystallization enthalpy; ΔH_m —melting enthalpy; X_{cr} —crystallinity index.

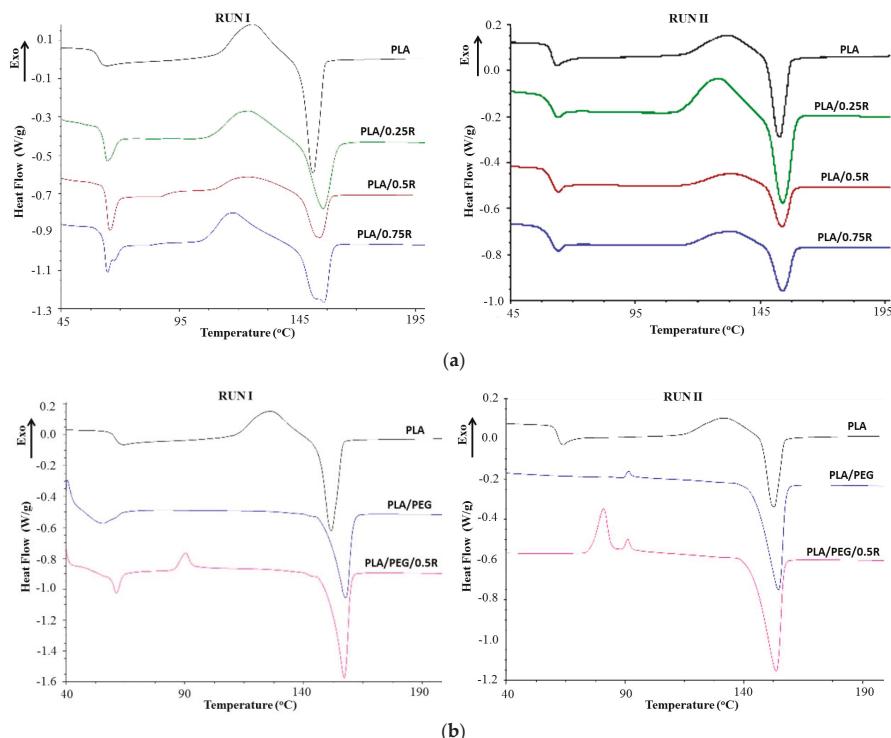


Figure 8. Differential scanning calorimetry (DSC) curves of the PLA and PLA/R (a) and plasticized PLA/R systems (b).

There is a strong dependence of the thermal properties of the powdered rosemary ethanolic extract containing samples on their particle distribution into the PLA matrix. In the binary systems, because of the agglomeration of particles, the majority of the properties decrease or remain unchanged while in the binary and ternary blend containing plasticizer the thermal characteristics are changed, eventually resulting in an increased degree of crystallization. The thermal characteristics recorded in the first run are a little different from those recorded in the second run, but the variation with sample composition is almost similar. T_g increases with R content and decreases as is expected when plasticizer is incorporated, and increases again for the ternary system PLA/PEG/0.5R. The T_{cc} recorded in both runs decreases for all studied systems, especially for PLA/PEG/0.5R. The decrease is less significant for values corresponding to the second run. The melting temperature T_m , increases in all cases; the most important increase was observed for plasticized PLA systems. As the plasticized systems are highly ordered the melting peak is very pronounced, especially in the second run because the plasticizer favors arrangement of the chains during cooling and pre-melting processes, increasing the degree of crystallinity. The results are in accordance with those found in other papers [16,17]. The enthalpy of the cold crystallization (ΔH_{cc}) is approximately constant for binary PLA/R systems and is very small for plasticized PLA systems, while the enthalpy of melting process (ΔH_m) decreases by R incorporation and increases in the cases of systems containing plasticizers because of the good distribution of particles and better mobility of the chains which favors the three-dimensional arrangements. As a result, the crystallization degree (X_{cr}) decreases by R incorporation and increases for plasticized PLA systems.

3.7. TG-FTIR/MS Data

As can be seen from the TG/DTG curves in Figure 9, the PLA and PLA/R samples decompose in a single step observed from 310–380 °C, evolving more than 98% as volatile products, see Table 6. Under an inert atmosphere, a lower thermal stability of the samples containing R was found. The plasticized PLA systems decomposed in two steps, the first one as the main step occurring in the temperature range of 280–370 °C with a mass loss of 82–83%, indicating a significant influence of the plasticizer on the thermal decomposition. The second step was assigned to the decomposition of the residue formed in the first step. It takes place in the temperature region of 365–430 °C with a mass loss of 15–16%. Comparing the onset and T_{10} decomposition temperature of the PLA/PEG and PLA/PEG/0.5R, results indicated that the incorporation of R led to an increased thermal stability of the system.

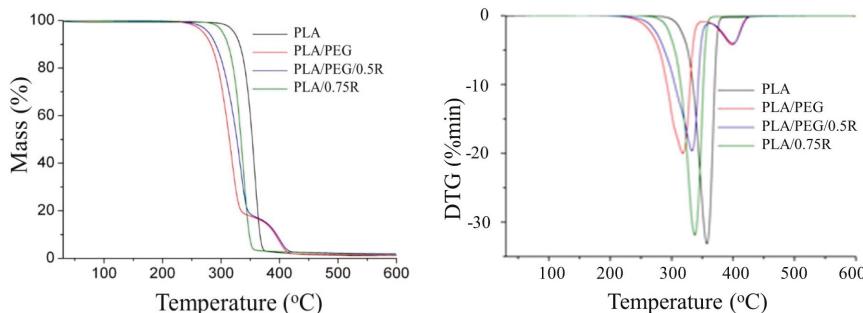


Figure 9. TG/DTG curves of the PLA, PLA/R, and PLA/PEG/R systems.

Table 6. TG data for PLA containing powdered rosemary ethanolic extract.

Sample	Degradation Stage	T_{onset} (°C)	T_{peak} (°C)	ΔW (%)	T_{10} (°C)	T_{20} (°C)
PLA	I residue	339	358	98.72 1.28	332.5	341.5
PLA/0.75R	I residue	310	338	98.50 1.50	312.5	321.5
PLA/PEG	I residue	280	322	82.51 16.31 1.18	285.5	298
PLA/PEG/0.5R	II residue	373	402	83.03 15.04 1.93	294	207.5

T_{onset} —the temperature at which the thermal degradation start; T_{peak} —the temperature at which the degradation rate is maximum; T_{10} , T_{20} —the temperatures corresponding to 10 wt % and 20 wt % mass losses; ΔW —residual mass at 600 °C.

As it concerns the type of decomposition products, some information has been obtained by coupling TG with FTIR/MS spectroscopies. Looking at the results from the data in Figure 10 showing the 3D FTIR spectra, the change in the thermal decomposition products after incorporation of R is evident.

The FTIR spectra show differences both in the intensity of the bands and also in the PLA/0.75R system. The number of bands is increased or important shifts in the PLA bands are observed due to the possible interaction between components of the system.

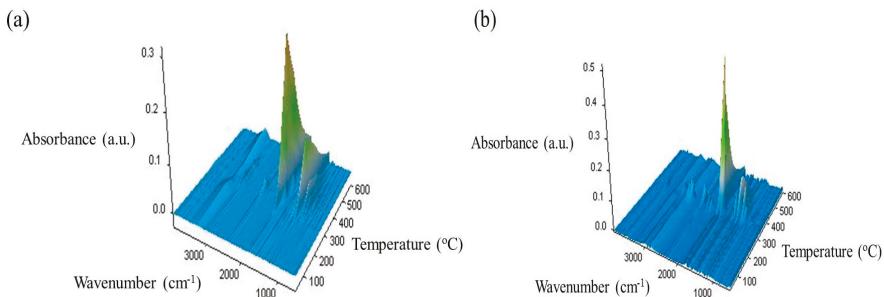


Figure 10. 3D-FTIR spectra of the volatile decomposition products resulting from the thermal degradation of PLA (a) and PLA/0.75R (b) samples.

The new bands in the 2D spectra of the thermal degradation products resulting from PLA/0.75R residue, see Figure 11, have been identified as: 2949.8 cm^{-1} (C–H stretching of CH_2 and CH_3); 2313.7 cm^{-1} (C=O , C–N and COO^- stretching); 1631.9 cm^{-1} (C=O , C–N and COO^- stretching); 1490.4 cm^{-1} (aromatic domain and N–H bending, C–O stretching vibration (amide), and C–C stretching from phenyl groups, COO^- stretching, CH_2 bending; 861 ; 747.9 and 602.5 cm^{-1} (C–H out-of-plane bending vibration from isoprenoids, etc.) [65].

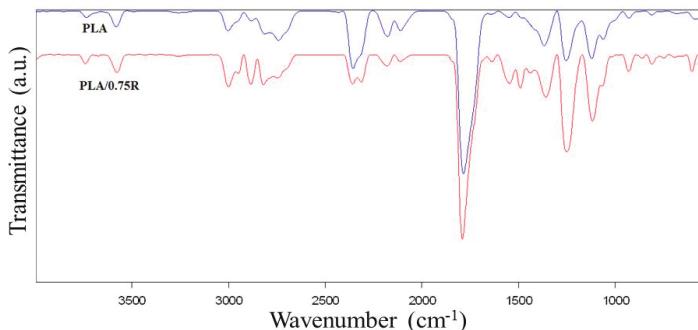


Figure 11. 2D FTIR spectra of the thermal degradation products resulting from PLA and PLA/0.75R.

The important shifts of the following bands are found from 2812 cm^{-1} in PLA to 2820 cm^{-1} in PLA/0.75R; 2841 cm^{-1} to 2845 cm^{-1} ; 1785 cm^{-1} to 1791 cm^{-1} ; 1367.7 cm^{-1} to 1359 cm^{-1} ; 1122 to 1117.2 cm^{-1} and 680.6 to 691.6 cm^{-1} . In the FTIR spectrum of degradation products, the following new bands and shifts of the bands appeared at approximately: 1736 , 1673 , 1366 , 1243 , 862 , and 750 cm^{-1} are found. These bands probably correspond to the fragments resulting from α –pinene and 1,8-cineole products which may evolve from rosemary ethanolic extract. These products appear together with those resulting from the PLA matrix.

At $T > 420\text{ }^{\circ}\text{C}$ all samples are almost totally degraded according to results from the TG/DTG curves, with a residual amount of $\sim 2\%$. Therefore, by FTIR/MS some of the thermal degradation products from the resulting mixtures at the final temperature are identified. Comparing these results with those obtained from the MS in Figure 12 indicated different products resulted by thermal degradation of PLA and its blends containing alcoholic extract of rosemary.

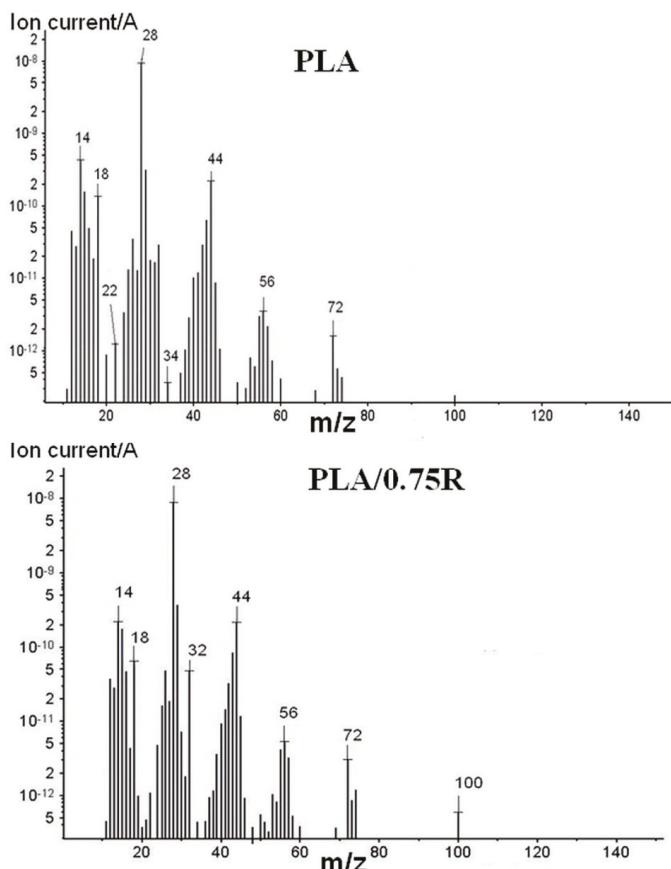


Figure 12. MS spectra of the thermal degradation products resulted from PLA and PLA/0.75R.

The pyrolysis of neat PLA results in the production of a large number of cyclic oligomers through the random degradation process. In accordance with the literature data, the main fragments of lactide meso-form or DL-form [66,67] are identified for $m/z = 32, 43, 45$ and 56. PLA, in general, shows a dominant series of signals with $m/z = 56 + (n \times 72)$ in which n assumed values of 1, 2, 3, and 4. Acetaldehyde (m/z 15, 26 and 43), 2,3-pentadione, and acrylic acid were also identified. Further decomposition products were H_2O , CO_2 , and hydrocarbons (m/z of 18, 44, 12–17, etc., respectively) [68]. The presence of the plasticizer led to very complex spectra.

3.8. Chemiluminescence

The stability of PLA is related to the formation of lactide structures [69]. Under gamma irradiation poly(L-lactic acid), the random scission of molecular chains takes place, which results in the sharp decrease in the numerical average molecular weight [70]. Moreover, due to the exposure to gamma radiation, several free radicals centered on carbon atoms are formed which release volatile products or restore polymeric configurations. The radiochemical behavior is the mirror of radiation processing during sterilization and grafting, when the weaker sites, α -methyl positions and branching places, become the main sources of degradation initiators [71].

The addition of natural phenolic antioxidants like powdered rosemary ethanolic extract increases the thermooxidative and radiation stabilities by scavenging degradation precursors. The contribution revealed by the components of this natural stabilizing mixture is observed by means of the differences between the CL intensities recorded for stabilized systems. The sharp progress in the radiation-stimulated degradation of PLA, see Figure 13a, is the result of the fast energy transfer from incidental radiation onto macromolecules followed by a high radiochemical yield of scission. In Figure 13b, the blocking action of oxidation is demonstrated by the diminution in the evolution of emission intensities, which drops as a parabolic decrease in the non-irradiated sample and the sudden hindrance of oxidation in the irradiated PLA/rosemary specimens.

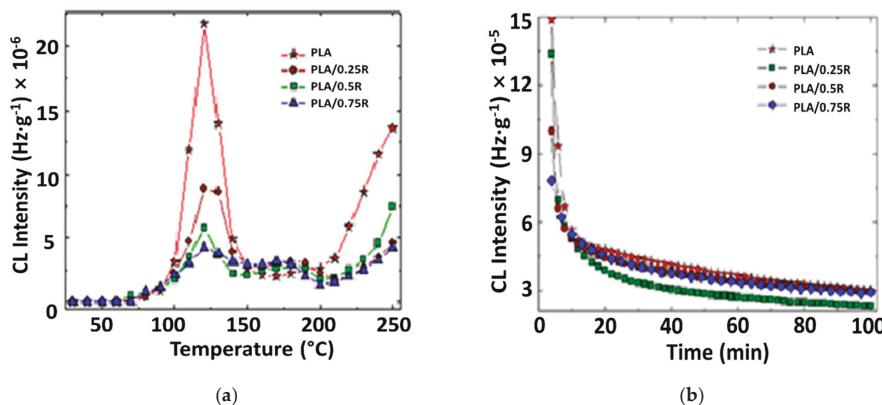


Figure 13. Chemiluminescence (CL) spectra recorded on PLA-based samples irradiated at 20 kGy: (a) nonisothermal measurements, heating rate: $3.7\text{ }^{\circ}\text{C min}^{-1}$; (b) isothermal measurements: testing temperature $180\text{ }^{\circ}\text{C}$

The comparison between progress in the oxidation of irradiated neat and stabilized PLA emphasizes that the scavenging action of free radicals is selective because the deceleration of oxidation does not happen similarly. The chemiluminescence intensity is gradually diminished over time in protected polymer samples, while the radicals are suddenly oxidized in pristine PLA.

The improvement in the thermal resistance of PLA in the presence of R is revealed in Figure 14. The linear modification of this parameter sustains the proportionality between the increase in the protection activity and material loading with rosemary ethanolic extract.

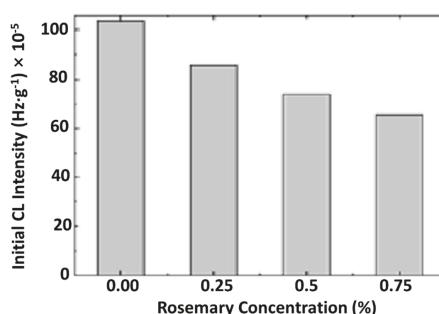


Figure 14. The dependence of the CL intensity on the concentration of powdered rosemary ethanolic extract.

The modification in the rosemary loading can provide a remarkable effect on stabilization. If the concentrations of 0.25% and 0.50% bring small contributions at medium oxidation temperatures, the degradation is effectively delayed at temperatures exceeding 170 °C. The concentration of 0.75% R, delivers a significant effect toward the preservation of the oxidation state in PLA samples. The low CL intensities recorded for these last-mentioned samples in comparison with the low-loaded material is evidence for the involvement of the powder component in the breaking action on the oxidation chain process.

The stabilization profiles for PLA mixed with PEG in the presence of rosemary are different if the concentrations of radicals are changed. As the literature data mentioned, “the components of rosemary extracts are very efficient stabilizers against oxidation by blocking free radicals towards reaction with oxygen according to the mechanism proposed by Pospišil” [72]. Thus, a cascade mechanism is responsible for the oxidation of carnosic acid, forming other intermediates with active antioxidant structures showing a high level in stabilization activity. The stabilization effectiveness depends on the active phenolic structures and the flavonoid components contained in rosemary extract [27,73].

The initial intensity of CL emission is related to the concentration of peroxy species [74]. A value of 1.63×10^{-3} Hz/g was found for the neat PLA/PEG system, while that of PLA/PEG/0.5R was 0.18×10^{-3} Hz/g, about nine times lower than that of the system without R, indicating a good oxidative stabilization of the system is achieved through this additive.

It can be concluded, that the non-isothermal oxidation starts at high temperatures, decreasing with R content. The isothermal CL determinations point out an evident contribution of powdered rosemary ethanolic extract to the polymer stability and the retardation of oxidation to long exposure times.

3.9. Antioxidant Activity Evaluation

The radical scavenging activity of the powdered rosemary ethanolic extract was determined by ABTS^{•+} method, and an IC₅₀ (the concentration of the sample required to inhibit 50% of radicals) of 26 µg/mL was obtained, which proved that the powdered rosemary ethanolic extract has very good antioxidant activity.

In Figure 15, the ABTS^{•+} radical scavenging activity of PLA blends with different contents of powdered rosemary ethanolic extract is presented. The free radical scavenging activity in polymeric systems is directly proportional with the content of powdered rosemary ethanolic extract of the blend and is again higher for the plasticized PLA. The antioxidant activity of plasticized PLA/R samples is comparable to other systems based on plasticized PLA. For example, Lopusiewicz et al. [75] found an antioxidant activity value of 23% for PLA/melanin composites, and Byun et al. [76] determined an antioxidant activity of 90% and 14% for PLA-based blends with α-tocopherol or butylated hydroxytoluene (BHT), respectively.

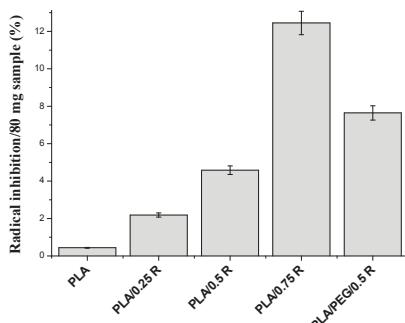


Figure 15. ABTS^{•+} radical inhibition activity of the polymeric blends containing powdered rosemary ethanolic extract.

The obtained results are in accordance with those obtained by the chemiluminescence method.

3.10. Antibacterial Activity

Escherichia coli and *Salmonella typhimurium* are Gram-negative bacteria while *Bacillus cereus* or *B. cereus* is a Gram-positive, rod-shaped, aerobic, facultative anaerobic, motile, beta hemolytic bacterium commonly found in soil and food that produces toxins. These toxins can cause two types of illness: One type is characterized by diarrhea and the other, called emetic toxin, by nausea and vomiting. These bacteria can multiply quickly at room temperature [77]. Both Gram-negative bacteria and Gram-positive bacteria are susceptible to the antibacterial activity of powdered rosemary ethanolic extract, and their sensitivity is highly variable, see Table 7. The antimicrobial activity at 24 h increases with an increasing concentration of the powdered rosemary ethanolic extract, reaching values of about 100% for a concentration of 0.75%, and is higher in the case of the plasticized PLA systems because of better distribution of the powder into the matrix, as the SEM results demonstrated. It is worthwhile to mention the promising results obtained against *B. cereus*, as it is known that very serious problems are caused by this bacterium in association with food poisoning. Also, this bacterium has been associated with a multitude of other clinical conditions such as anthrax-like progressive pneumonia, severe eye infections, and devastating central nervous system infections, etc. Its role in nosocomial acquired bacteremia and wound infections in postsurgical patients has also been demonstrated, especially when intravascular devices such as catheters are inserted. *B. cereus* produces a potent β -lactamase conferring a marked resistance to β -lactam antibiotics [78].

Table 7. Antibacterial activity of the alcoholic extract from rosemary incorporated into PLA-based materials against *Bacillus cereus*, *Salmonella typhimurium*, and *Escherichia coli*.

Sample	ATCC <i>Bacillus cereus</i> 14579		ATCC <i>Salmonella typhimurium</i> 14028		ATCC <i>Escherichia coli</i> 25922	
	Inhibition %/24 h	Inhibition %/48 h	Inhibition %/24 h	Inhibition %/48 h	Inhibition %/24 h	Inhibition %/48 h
PLA	5	59	32	61	53	71
PLA/0.25 R	59	100	52	87	61	86
PLA/0.5 R	91	100	52	84	71	100
PLA/0.75 R	100	100	55	87	94	100
PLA/PEG	45	91	29	77	69	94
PLA/PEG/0.5R	86	100	48	100	76	100

The activity is lower in the case of *Salmonella typhimurium*. These results are in accordance with those found by other authors. Golshani and Sharifzadeh tested the rosemary alcoholic extract against *Staphylococcus aureus*, *Escherichia coli*, *Bacillus cereus*, and *Pseudomonas aeruginosa*, and proved its inhibitory effect for all these strains [79]. Some inhibitory effect for bacteria growth of PLA could be explained by the acidic pH imparted by it to the culture medium (pH 2), which is not favorable to bacteria growth and is due to the residual content of lactic acid.

3.11. Gas Permeability

It is well-known that the properties of PLA are compared to other commodity plastics, and the PLA permeation is shown to closely resemble that of polystyrene. Crystallinity was found to dominate permeation properties in a biaxially-oriented film [80]. The permeability depends on the film thickness and polymer morphology. Improvement of the gas permeability of the PLA-based films of approximately the same thickness in the presence of natural additive R is evident by comparing the data of Table 8.

Table 8. Permeability of tested films to CO₂ (~4 h to equilibrium) and O₂ (~7 h to equilibrium).

Sample	Thickness (mm)	CO ₂ (mL/m ² /day)	O ₂ (mL/m ² /day)
PLA	0.151	873	1308
PLA/0.25R	0.120	588	487
PLA/0.5R	0.122	535	273
PLA/0.75R	0.130	412	201
PLA/PEG	0.128	524	455
PLA/PEG/0.5R	0.126	489	278
Food freezing bag	0.020	64,601	50,266
Food packaging foil (LDPE/PP)	0.009	128,374	35,629

The gas barrier improvement depends on the amount of R in the film's composition both in PLA/R and plasticized PLA/R blends. The oxygen barrier properties are better than those of CO₂. The results are in accordance with those obtained by Yuniarto et al. [81]. They found that the plasticized PLA by PEG enhanced the permeability value by about 20%, while the largest fraction PEG400 reduced the ability to prevent oxygen from passing through the film. In this case, the barrier properties were significantly affected by the degree of crystallinity in the film with a correlation number of 0.85. The gas permeability of two commercial food packages (a foil and a freezing bag) was also measured for comparative purposes. An unexpectedly high permeability for CO₂ and for O₂ was found for both packages. However, taking into consideration the difference in film thickness between our samples and the commercial ones, we do consider that PLA-based composites could be suitable for use as packages for food applications.

3.12. Overall Migration of Active Components from PLA/R Formulations into 50% Ethanol Solution as a Food Simulant Medium

As mentioned in the experimental section, the overall migration of active components from PLA/R-based formulations into the simulant medium was determined according to EU regulations, and the results are summarized in Figure 16 and Table 9.

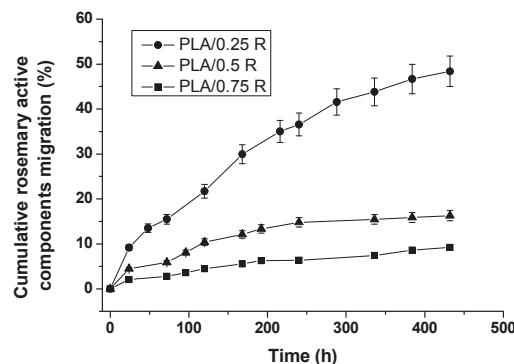


Figure 16. Migration profiles for the active ingredients of the powdered rosemary ethanolic extract (R) from PLA-based samples into 50% ethanol solution as a food simulant medium.

Table 9. Migration kinetic parameters for the active ingredients of the powdered rosemary ethanol extract from PLA-based materials into 50% ethanol solution as a food simulant medium.

Sample	Korsmeyer-Peppas Model			Higuchi Model		
	n	R ²	K × 10 ⁻³ (h) ⁻ⁿ	R ²	k _H × 10 ⁻³ (h) ⁻ⁿ	R ²
PLA/0.25R	0.61	0.99	14.1	0.989	27.57	0.98
PLA/0.5R	0.42	0.98	12.82	0.988	8.28	0.98
PLA/0.75R	0.54	0.985	3.52	0.993	4.48	0.99

The migration profiles from PLA/R films with three different R compositions show a quite similar release behavior of the rosemary ethanolic extract active ingredients, but it is quantitatively influenced by the amount of R incorporated in the film samples. Thus, in the 18-day interval investigated, the active ingredients of R were released faster and in the highest amount from the PLA/0.25R sample—reaching 48.4% release, followed by the PLA/0.5R sample with 16.3% released, and the PLA/0.75R sample with only 9.2% released. The increase of the R content leads to a slower release of the active components.

The calculated kinetic parameters and the corresponding correlation coefficient values (R^2) are summarized in Table 9.

The release exponent, n values, obtained by fitting the data to the Korsmeyer-Peppas equation, see Equation (2) [36], are 0.61 for PLA/0.25R, 0.42 for PLA/0.5R, and 0.55 for PLA/0.75R, all these values are situated around 0.5, indicating a behavior closer to Fickian diffusion, thus, in general, a diffusion-controlled mechanism characterizes the migration process of the bioactive components from the polymeric films. A decrease of the release rate constant values with an increasing amount of R incorporated (the lowest $k = 3.52 \times 10^{-3}$ for PLA/0.75R sample) was observed, which corresponds to a slower release, as shown by the migration profiles.

A good fit was obtained for the Higuchi model, see Equation (3) [37], as the R^2 values suggest, indicating diffusion as the preferred mechanism for migration, with the same trend of decreasing k_H values: $k_{PLA/0.25R} > k_{PLA/0.5R} > k_{PLA/0.75R}$ was found through the application of both models.

These results indicate that the migration rate of some components of the rosemary ethanolic extract from PLA/R films directly depends on their permeability and degree of crystallization. For films of approximately the same thickness, the gas permeability decreased by two or six times, indicating difficult diffusion of components through the materials. Also, the interaction between the PLA/R blends components can slow the migration into the food simulant.

3.13. Biocompatibility Evaluation

3.13.1. In Vitro Biocompatibility Evaluation Based on Surface Properties

The contact angles decrease for all systems with respect to that of PLA, see Table 10, indicating that an increased hydrophilicity was achieved through R incorporation. This increase is also proved by variations recorded in the surface tension and its components. The total surface tension γ_{sv}^{TOT} increases with R incorporation, and, as was the case for other properties, the highest values were registered for the PLA/PEG/0.5R system.

The most important change was found in the γ_{sv}^- electron donor (Lewis base) component which is 0.19 mN/m for PLA and increases to 38.05 mN/m for PLA/PEG/0.5R while γ_{sv}^{AB} , polar Lewis acid-base interaction varied from 0.86 mN/m to 13.99 mN/m. This phenomenon is related by the cohesion between molecules at the surface of the liquid. It is known that the stronger the intermolecular interactions, the greater the surface tension [82]; therefore, rosemary extract improved the interactions of the liquids with surfaces, obtaining composites with better water wettability. The presence of PEG as a plasticizer into the polymeric system enhances the surface hydrophilicity; the lowest CA was recorded for PLA/PEG (50°) compared with that of PLA (84.7°), see Table 10. The decrease of CA is

directly correlated with the content of rosemary ethanolic extract, indicating that by increasing the content of rosemary extract, more hydrophilic groups are accessible at the top surface, obtaining a material with a moderate surface wettability (64.4° for 0.75% content rosemary extract).

Table 10. The contact angle values (θ) between liquids (water, formamide, or diiodomethane) and surfaces of the sample of different compositions.

Samples	Contact Angles Values (degrees)		
	Water	Formamide	Diiodomethane
PLA	84.7	70.9	65.0
PLA/0.25R	81.9	62.7	60.1
PLA/0.5R	78.8	59.0	56.7
PLA/0.75R	64.4	42.8	38.7
PLA/PEG	50.0	46.4	40.7
PLA/PEG/0.5R	63.7	71.0	51.0

In Table 11, the values of the surface tension components (determined by acid/base method) and work of spreading for red blood cells and platelets are presented, indicating that with the addition of rosemary ethanolic extract and PEG into the PLA, the total SFE increases. This change of the surface free energy may lead to the improvement of the bio-adhesive ability of the material. In the interaction of biomaterials with tissues, their polar character has an important role, which is reflected in the SFE's polar component (γ_{sv}^{AB}), see Table 11. At the surface of PLA, Lifshitz-van der Waals interactions prevail over acid-base interactions, by comparison with the surfaces of its composites. Blending PLA with rosemary ethanolic extract and PEG determines an increase in the contribution of the polar components to the total surface energy, having a more pronounced polar character than PLA, which is indicated by the higher value of γ_{sv}^{AB} component. The basic component (γ_{sv}^-) of the surface free energy is much higher than the acidic component (γ_{sv}^+), suggesting that the surface of the composites is mainly monopolar with a Lewis base character, due to the surface being enriched with electron donor functional groups ($-OH$, $O-C=O$) from rosemary ethanolic extract. If polymeric materials are used as implant biomaterials, strong cell adhesion and rapid cell growth on the polymer surface will generally be beneficial for the incorporation of the device into the body. Van der Valk et al. [83] have shown that cell (fibroblast) spreading appeared to be dependent on the polar surface free energy. Cell spreading is low when the SFE's polar part of the material is lower than 5 mN/m , and marked spreading occurs when γ_{sv}^{AB} is higher than 15 mN/m [43]. Based on the values of the SFE polar part determined for the PLA/R composites, it can be assumed that the sample incorporating all the components (PLA/PEG/0.5R) will give better spreading and division of the fibroblasts because their γ_{sv}^{AB} takes an intermediary value.

Table 11. Surface tension parameters (mN/m) and work of spreading for red blood cells and platelets of composites samples.

Samples	γ_{sv}^{LW}	γ_{sv}^{AB}	γ_{sv}^+	γ_{sv}^-	γ_{sv}^{TOT}	W_{slrbc}	W_{slp}
PLA	25.65	1.75	0.06	12.45	27.40	-8.95	-109.56
PLA/0.25R	28.46	3.31	0.62	7.22	32.69	1.43	-107.13
PLA/0.5R	30.41	4.23	0.11	24.01	33.72	-2.11	-90.51
PLA/0.75R	40.17	5.41	0.33	22.22	45.58	10.83	-74.12
PLA/PEG	39.17	1.92	0.03	34.91	41.09	4.54	-69.58
PLA/PEG/0.5R	33.64	13.95	1.27	38.25	47.59	12.27	-71.51

θ = contact angle; γ_{sv}^{TOT} = liquid's total surface tension; γ_{lv}^{LW} and γ_{sv}^{LW} = apolar Lifshitz—van der Waals components of the liquid and the solid $\gamma_{sv}^+ \gamma_{lv}^- \gamma_{lv}^+$ and $\gamma_{sv}^- \gamma_{sv}^+$ = Lewis acid-base contributions of either the solid or the liquid phase; γ_{sv}^+ = electron donor (Lewis base) and γ_{sv}^- = electron acceptor (Lewis acid) components; “ lv ” and “ sv ” = denote the interfacial liquid-vapor and surface-vapor tensions; “ p ” and “ d ” = denote the polar and disperse components of total surface tension, γ_{lv}^{TOT} ; γ_{sv}^{AB} = polar Lewis acid-base interaction.

When blood comes into contact with a biomaterial, the surface properties, especially its wettability, play a crucial role. The response of platelets towards the hydrophobic or hydrophilic materials is different [84]. In the presence of a biomaterial, platelets' adherence to the foreign material and activation, usually results in the initiation of platelet aggregation, further initiating thrombosis by secreting prothrombotic factors that lead to clotting [85]. Under normal conditions, thrombosis and complement activation are favorable responses which prevent blood loss. However, in the presence of a foreign material such as a blood-contacting device, thrombosis, and complement activation are unfavorable, leading to blood clots and hence a low biocompatibility [84]. Thus, a blood-contacting device that does not elicit thrombosis would be considered biocompatible [86]. As revealed in Table 11, the work of spreading of the red blood cells, $W_{s/rbc}$, has positive values (except for the PLA and PLA/0.5R samples) and the work of the spreading of platelets, $W_{s/p}$, has negative values, which suggests that the work of adhesion is higher than that of cohesion for the red blood cells, but, comparatively, a smaller work of adhesion than that of cohesion for platelets. These findings denote that the contact of blood with PLA/R-based composites causes an increase in the work of cohesion for platelets; hence the platelets will not adhere easily onto the biomaterial's surface, thus avoiding the appearance of thrombosis [87].

3.13.2. In Vivo Biocompatibility Evaluation

No significant modifications between the percentage values of blood leucocyte formula elements were discovered in rats with PLA/0.25R, PLA/0.5R, PLA/0.75R, PLA/PEG, and PLA/PEG/0.5R implants and those of control group, PLA, and R, respectively, at 24 h and 7 days in the experiment, see Table 12.

Table 12. The effects of the PLA-based materials containing rosemary ethanolic extract on the differential white cell count. Values were expressed as mean \pm S.D. for six rats in a group.

Group		Leucocyte Formula				
		% Values				
		PMN	Ly	E	M	B
Control	24 h	29.5 \pm 0.83	66.3 \pm 2.11	0.6 \pm 0.08	3.4 \pm 0.10	0.2 \pm 0.10
	7 days	29.7 \pm 0.47	65.9 \pm 1.93	0.7 \pm 0.10	3.5 \pm 0.10	0.2 \pm 0.05
R	24 h	29.5 \pm 0.69	66.1 \pm 1.75	0.8 \pm 0.06	3.4 \pm 0.06	0.2 \pm 0.10
	7 days	29.6 \pm 0.73	66.2 \pm 1.89	0.6 \pm 0.08	3.4 \pm 0.10	0.2 \pm 0.05
PLA	24 h	29.6 \pm 0.89	66.1 \pm 2.13	0.6 \pm 0.05	3.5 \pm 0.05	0.2 \pm 0.05
	7 days	29.7 \pm 1.13	65.9 \pm 1.55	0.7 \pm 0.05	3.5 \pm 0.05	0.2 \pm 0.04
PLA/0.25R	24 h	29.6 \pm 0.21	66.0 \pm 1.73	0.7 \pm 0.12	3.5 \pm 0.08	0.2 \pm 0.04
	7 days	29.8 \pm 1.13	65.7 \pm 1.29	0.7 \pm 0.05	3.6 \pm 0.10	0.2 \pm 0.05
PLA/0.5R	24 h	29.7 \pm 0.29	65.9 \pm 2.14	0.6 \pm 0.10	3.6 \pm 0.08	0.2 \pm 0.10
	7 days	29.7 \pm 1.17	65.7 \pm 1.33	0.8 \pm 0.06	3.6 \pm 0.05	0.2 \pm 0.05
PLA/0.75R	24 h	29.6 \pm 0.98	65.8 \pm 1.67	0.8 \pm 0.12	3.6 \pm 0.10	0.2 \pm 0.10
	7 days	29.8 \pm 0.73	65.8 \pm 1.75	0.6 \pm 0.05	3.6 \pm 0.08	0.2 \pm 0.05
PLA/PEG	24 h	29.8 \pm 0.89	65.7 \pm 1.39	0.7 \pm 0.10	3.6 \pm 0.05	0.2 \pm 0.04
	7 days	29.9 \pm 0.55	65.5 \pm 1.63	0.7 \pm 0.05	3.7 \pm 0.12	0.2 \pm 0.05
PLA/PEG/0.5R	24 h	29.8 \pm 0.27	65.7 \pm 1.98	0.6 \pm 0.10	3.7 \pm 0.10	0.2 \pm 0.05
	7 days	29.9 \pm 1.63	65.4 \pm 1.47	0.8 \pm 0.13	3.7 \pm 0.05	0.2 \pm 0.05

PMN—polymorphonuclear leukocytes; Ly—lymphocytes; E—eosinophils; M—monocytes; B—basophils.

Laboratory investigations did not reveal substantial variations of AST, ALT, and LDH activity between groups with the PLA-based materials containing rosemary ethanolic extract pellets and the control, PLA, and R groups, respectively, 24 h and 7 days after the implantation, see Table 13.

Table 13. The effects of PLA-based materials containing rosemary ethanolic extract on the activity of AST, ALT, and LDH. Values were expressed as mean \pm S.D. for six rats in a group.

Group		AST (U/mL)	ALT (U/mL)	LDH (U/mL)
Control	24 h	41.7 \pm 2.72	95.3 \pm 4.14	342.29 \pm 44.55
	7 days	42.5 \pm 3.07	96.5 \pm 3.89	344.33 \pm 41.37
PLA	24 h	42.3 \pm 3.14	95.8 \pm 4.46	342.17 \pm 39.64
	7 days	42.9 \pm 2.33	97.6 \pm 3.55	345.25 \pm 40.89
R	24 h	41.6 \pm 1.89	96.2 \pm 3.37	343.42 \pm 42.14
	7 days	42.7 \pm 2.64	98.7 \pm 5.07	346.67 \pm 38.33
PLA/0.25R	24 h	42.1 \pm 3.14	97.5 \pm 4.27	343.54 \pm 43.46
	7 days	43.9 \pm 3.46	97.9 \pm 3.64	346.81 \pm 41.37
PLA/0.5R	24 h	43.2 \pm 3.33	97.6 \pm 3.37	344.55 \pm 39.89
	7 days	44.1 \pm 3.27	98.8 \pm 5.14	347.19 \pm 44.14
PLA/0.75R	24 h	43.4 \pm 2.37	98.3 \pm 5.55	344.29 \pm 43.72
	7 days	44.6 \pm 2.55	98.7 \pm 6.07	348.46 \pm 45.07
PLA/PEG	24 h	43.7 \pm 3.37	98.5 \pm 5.46	345.72 \pm 44.37
	7 days	44.8 \pm 3.89	98.8 \pm 4.33	349.15 \pm 40.46
PLA/PEG/0.5R	24 h	43.5 \pm 3.14	97.2 \pm 3.89	345.45 \pm 39.89
	7 days	44.6 \pm 3.64	98.6 \pm 5.72	347.83 \pm 42.27

AST—aspartate transaminase, ALT—alanine aminotransferase and LDH—lactic dehydrogenase.

The implantation of pellets with PLA/0.25R, PLA/0.5R, PLA/0.75R, PLA/PEG and PLA/PEG/0.5R, did not induce significant differences in the serum levels of urea and creatinine compared with the groups receiving PLA, R, and the control, see Table 14.

Table 14. The effects of PLA-based materials containing rosemary ethanolic extract on the serum urea and creatinine concentration. Values were expressed as mean \pm S.D. for six rats in a group.

Group		Urea (mg/dL)	Creatinine (mg/dL)
Control	24 h	37.2 \pm 3.37	<0.1
	7 days	37.9 \pm 4.55	<0.1
PLA	24 h	37.7 \pm 3.89	<0.2
	7 days	38.1 \pm 3.64	<0.2
R	24 h	37.9 \pm 5.07	<0.1
	7 days	38.5 \pm 3.46	<0.1
PLA/0.25R	24 h	38.6 \pm 4.37	<0.1
	7 days	38.9 \pm 4.33	<0.2
PLA/0.5R	24 h	38.8 \pm 3.64	<0.2
	7 days	39.3 \pm 3.72	<0.2
PLA/0.75R	24 h	39.1 \pm 5.14	<0.2
	7 days	39.4 \pm 4.46	<0.2
PLA/PEG	24 h	38.8 \pm 3.55	<0.2
	7 days	39.6 \pm 3.27	<0.2
PLA/PEG/0.5R	24 h	39.2 \pm 4.64	<0.2
	7 days	39.5 \pm 3.37	<0.2

No major dissimilarities were observed in the values of serum complement and the phagocytic capacity of peripheral neutrophils between the groups with PLA-based materials containing rosemary ethanolic extract implants, and PLA, R, and the control group, respectively, at 24 h and 7 days after the implantation see Table 15.

Table 15. The effects of PLA-based materials containing rosemary ethanolic extract on the serum complement activity and the NBT test. Values were expressed as mean \pm S.D. for six rats in a group.

Group		Complement	NBT Test
Control	24 h	16.33 \pm 1.55	53.73 \pm 3.46
	7 days	16.48 \pm 1.37	53.65 \pm 3.55
PLA	24 h	16.41 \pm 1.46	53.85 \pm 4.14
	7 days	16.65 \pm 1.14	53.49 \pm 3.72
R	24 h	16.39 \pm 1.55	52.63 \pm 3.50
	7 days	16.47 \pm 1.33	52.45 \pm 3.14
PLA/0.25R	24 h	16.43 \pm 1.64	52.77 \pm 3.67
	7 days	16.85 \pm 0.89	52.39 \pm 3.25
PLA/0.5R	24 h	16.56 \pm 1.72	53.68 \pm 3.46
	7 days	16.89 \pm 1.37	52.55 \pm 3.83
PLA/0.75R	24 h	16.77 \pm 1.64	53.73 \pm 3.46
	7 days	17.11 \pm 0.72	52.61 \pm 3.37
PLA/PEG	24 h	17.07 \pm 0.89	53.85 \pm 4.05
	7 days	16.63 \pm 1.55	53.37 \pm 3.64
PLA/PEG/0.5R	24 h	17.03 \pm 0.83	54.19 \pm 4.17
	7 days	17.13 \pm 1.46	53.49 \pm 3.55

All these results indicate a good and increased biocompatibility of the PLA/R which recommends them as biomaterials for various applications because rosemary ethanolic extract offers both an improved biocompatibility of PLA-based materials and it also confers the different biological activities mentioned above.

4. Conclusions

New multifunctional materials based on PLA-containing additives derived from natural resources were obtained by melt mixing.

Incorporation of powdered rosemary ethanolic extract into PLA improved the elongation at break, rheological and thermal properties, and antibacterial and antioxidant activities. Additionally, the novel materials showed a good compatibility and in vitro and in vivo biocompatibility. The contribution of additive to the protection of PLA against oxidative degradation is discussed with respect to the phenolic compounds contained in rosemary powder.

A good agreement between results was found, such as between those of chemiluminescence and radicals' scavenging activity determination via a chemical method that evidenced the increased thermoxidative stability of the PLA biocomposites containing powdered rosemary ethanolic extract which acts as an antioxidant. These biocomposites show low migration rates of the bioactive compounds from matrices and permeability to gases, and, therefore, can be considered as high-performance materials for food packaging.

In vitro biocompatibility based on the determination of surface properties demonstrated a good hydrophilicity, better spreading and division of fibroblasts, and an increase of platelets' cohesion. Therefore, they will not adhere easily on the biomaterial's surface thus avoiding the appearance of thrombosis.

It was demonstrated that implantation of PLA-based materials containing rosemary ethanolic extract resulted in similar blood parameter changes and biochemical responses with the control group, the group treated with pellets impregnated with R solution, and with PLA pellets, respectively.

The subcutaneous application of PLA-based materials containing rosemary ethanolic extract pellets did not significantly influence the immune reactivity of rats, compared with PLA, R, and the control group.

It can be concluded that, in our laboratory conditions, the implantation of PLA/0.25R, PLA/0.5R, PLA/0.75R, PLA/PEG, and PLA/PEG/0.5R pellets, proved a good in vivo biocompatibility, suggesting that these PLA-based materials containing rosemary ethanolic extract show very good

properties as potential biomaterials, which could be further used for evaluating their possible pharmacodynamics effects in different experimental models in animals.

The PLA/R-based materials show promising properties for application both in biodegradable food packaging and as biomaterials with bioactive activities.

Author Contributions: In this study, the concepts and designs for the experiment were supervised by C.V. and E.S. Manuscript text and results analysis were performed by C.V., R.N.D.-N. and E.S. Mechanical and rheological experiments and data processing were conducted by R.N.D.-N. The experimental results were examined by C.V., E.S., R.N.D.-N., D.P., R.P.D., L.T., T.Z., M.A.B., N.T., G.M.P., K.L. All authors read and approved the final manuscript.

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Article

Formulation and Characterization of New Polymeric Systems Based on Chitosan and Xanthine Derivatives with Thiazolidin-4-One Scaffold

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Abstract: In the past many research studies have focused on the thiazolidine-4-one scaffold, due to the important biological effects associated with its heterocycle. This scaffold is present in the structure of many synthetic compounds, which showed significant biological effects such as antimicrobial, antifungal, antioxidant, anti-inflammatory, analgesic, antidiabetic effects. It was also identified in natural compounds, such as actithiazic acid, isolated from *Streptomyces* strains. Starting from this scaffold new xanthine derivatives have been synthetized and evaluated for their antibacterial and antifungal effects. The antibacterial action was investigated against Gram positive (*Staphylococcus aureus* ATCC 25923, *Sarcina lutea* ATCC 9341) and Gram negative (*Escherichia coli* ATCC 25922) bacterial strains. The antifungal potential was investigated against *Candida* spp. (*Candida albicans* ATCC 10231, *Candida glabrata* ATCC MYA 2950, *Candida parapsilosis* ATCC 22019). In order to improve the antimicrobial activity, the most active xanthine derivatives with thiazolidine-4-one scaffold (XTDs: 6c, 6e, 6f, 6k) were included in a chitosan based polymeric matrix (CS). The developed polymeric systems (CS-XTDs) were characterized in terms of morphological (aspect, particle size), physic-chemical properties (swelling degree), antibacterial and antifungal activities, toxicity, and biological functions (bioactive compounds loading, entrapment efficiency). The presence of xanthine-thiazolidine-4-one derivatives into the chitosan matrix was confirmed using Fourier transform infrared (FT-IR) analysis. The size of developed polymeric systems, CS-XTDs, ranged between 614 μm and 855 μm , in a dry state. The XTDs were encapsulated into the chitosan matrix with very good loading efficiency, the highest entrapment efficiency being recorded for CS-6k, which ranged between $87.86 \pm 1.25\%$ and $93.91 \pm 1.41\%$, depending of the concentration of 6k. The CS-XTDs systems showed an improved antimicrobial effect with respect to the corresponding XTDs. Good results were obtained for CS-6f, for which the effects on *Staphylococcus aureus* ATCC 25923 (21.2 ± 0.43 mm) and *Sarcina lutea* ATCC 9341 (25.1 ± 0.28 mm) were comparable with those of ciprofloxacin (25.1 ± 0.08 mm/ 25.0 ± 0.1 mm), which were used as the control. The CS-6f showed a notable antifungal effect, especially on *Candida parapsilosis* ATCC 22019 (18.4 ± 0.42 mm), the effect being comparable to those of nystatin (20.1 ± 0.09 mm), used as the control. Based on the obtained results these polymeric systems, consisting of thiazolidine-4-one derivatives loaded with chitosan microparticles, could

have important applications in the food field as multifunctional (antimicrobial, antifungal, antioxidant) packaging materials.

Keywords: thiazolidine-4-one scaffold; chitosan; polymeric systems; antibacterial activity

1. Introduction

In the last time the xanthine scaffold was widely investigated based on its high biological potential. Some of the most important derivatives are caffeine, theophylline, theobromine, and paraxanthine [1]. These compounds are known for important biological effects such as bronchodilator, diuretic, anti-inflammatory and lipolytic [2,3]. New biological active molecules with a xanthine structure have been developed and evaluated for potential applications in asthma [4], diabetes mellitus [5], cancer [6], microbial infections [7] and neurodegenerative diseases such as Parkinson [8] and Alzheimer [2].

In the medicinal chemistry the thiazolidine heterocycle is also known as an important scaffold that is used to modulate the classical structures in order to improve their biological effects and to induce other new ones. For the first time this structure was identified as an actithiazic acid, a natural compound isolated from *Streptomyces spp.*, which showed high and specific action against *Mycobacterium tuberculosis* [9]. Later, many thiazolidine derivatives were synthesized and evaluated for their antimicrobial effect [10–12]. It was shown that the antimicrobial effects are in close correlation with the nature and position of substituents on the heterocycle. For example, the presence of arylazo, phenylhydrazono or sulfamoylphenylazo on the heterocycle was associated with improved antimicrobial effects [13].

In a previous study the researchers focused their studies on micro and nanotechnology as new strategies for increasing solubility, improving the biological properties, and decreasing the toxicity of the drugs. Some of the most important applications are in the regenerative medicine or tissue engineering area, as biosensors or as controlled drug release systems. The polymeric systems such as nano and microparticles are largely used as drug delivery systems due to their small particle size and large surface area [14]. Lately, chitosan, a natural polymer derived from chitin, has attracted the interest of many researchers due to its important and specific properties, such as biocompatibility, biodegradability, and reduced toxicity [15]. This biopolymer is considered the largest biomaterial after cellulose, having important applications in both the pharmaceutical and the food industry [16,17]. It is a linear polycationic polysaccharide, copolymer of D-glucosamine and N-acetyl-D-glucosamine linked in 1-4 positions [16]. The amino groups on chitosan allow it to react with varied types of reagents to introduce different functional groups to chitosan. This polymer has important biological effects such as antimicrobial [18,19], antidiabetic [20–22], antitumor [23], antioxidant [24,25], anti-inflammatory [24], antiulcerous [26], and not least, hypocholesterolemic [27]. The antimicrobial effect is the result of the interaction between the negatively charged bacterial cell membranes and the positively charged amino groups of chitosan, being directly proportional to the molecular weight and inversely proportional to the pH value. The studies showed also that *Gram-positive* bacterial strains are more susceptible to chitosan than *Gram-negative* ones [28].

Referring to the food industry, it is known that the packaging components have an important role for preservation of food as well as for environment protection, in a previous study the researchers focused on the use of renewable material and on the development of active packaging in order to increase the quality and safety of food [29]. The embedded food technology based on antimicrobial agents represents nowadays a challenge for researchers being strengthened also by the few marked products [30]. To obtain active packaging the antimicrobial agents could be included in the polymer matrix or the polymer surface could be covered with different antimicrobial agents [31,32]. Knowing that the microbial growth occurs mainly on the food surface, this new strategy involves slow diffusion of the antimicrobial agent from the package material, such as polymer films [33]. The controlled release packaging is a new approach for the food industry. The literature reported various packaging systems

based on chitosan or embedded chitosan with different antimicrobial agents [34–37]. The studies highlight the important role chitosan plays as a plasticizer and it is frequently used in different composite systems with potential application in the food industry in order to increase the mechanical strength of the developed structure [37].

In this study we report the preparation, physico-chemical characterization, and biological evaluation of new polymeric systems based on chitosan, which have been loaded with new xanthine derivatives with a thiazolidine-4-one scaffold. Based on the unique properties of chitosan (biodegradability, biocompatibility) and of the biological effects of xanthine derivatives with a thiazolidine-4-one scaffold, the developed polymeric systems could have important applications in the food industry as active packaging materials and also in the medical field.

2. Materials and Methods

2.1. Materials

Chitosan (CS, molecular weight 190–310 kDa, 75–85% deacetylation degree), pentasodium tripolyphosphate (TPP), disodium hydrogen phosphate, sodium dihydrogen phosphate, hydrochloric acid 37%, acetic acid (min. 99.8%, p.a. ACS reagent), dimethyl sulfoxide (DMSO, p.a., ACS reagent), Mueller–Hinton agar medium (Oxoid), Sabouraud agar medium were purchased from Sigma Aldrich. Xanthine derivatives with thiazolidine-4-one scaffold (XTDs: 6c, 6e, 6f, 6k) have been synthesized by our research group and were reported in a previous paper [38]. Bacterial strains (*Staphylococcus aureus* ATCC 25923, *Sarcina lutea* ATCC 9341, *Escherichia coli* ATCC 25922) and yeast strains (*Candida albicans* ATCC 10231, *Candida glabrata* ATCC MYA 2950, *Candida parapsilosis* ATCC 22019) were obtained from the Department of Microbiology, “Grigore T. Popa” University of Medicine and Pharmacy, Iasi, Romania. Ampicillin (30 µg/disc), ciprofloxacin (25 µg/disc) and nystatin (100 µg/disc) were used as positive controls for antibacterial and antifungal activity respectively. Swiss mice were purchased from the Biobase of “Grigore T. Popa” University of Medicine and Pharmacy, Iasi, Romania.

2.2. Development of New Polymeric Systems Based on Chitosan

2.2.1. Preparation of Chitosan Microparticles

Chitosan microparticles were prepared by the ionic gelation method. Briefly, chitosan (CS, 1.2–1.7 g) was dispersed in 100 mL of acetic acid 1% (v/v) and the mixture was left under stirring overnight. 3 mL of chitosan solution were dropped, using a syringe needle (26 G; 0.45 mm × 16 mm), into 20 mL of TPP (2%–3%), under light stirring and the mixture was left at room temperature, under stirring for 4–8 h in order to achieve an efficient reticulation. After 24 h the formed chitosan beads were separated from the TPP solution, washed three times with distilled water, and air-dried at room temperature.

2.2.2. Preparation of Chitosan Microparticles Loaded with Xanthine Derivatives with Thiazolidine-4-One Scaffold (CS-XTDs)

The xanthine derivatives with thiazolidine-4-one scaffold (XTDs: 6c, 6e, 6f, 6k) were loaded into chitosan microparticles by the ionic gelation method [5]. Briefly, different amounts of XTD (9 mg, 12 mg, 15 mg) were dissolved in 0.3 mL of DMSO and mixed with 3 mL of chitosan solution (1.2%–1.7%, v/v) in order to obtain three different concentrations (3 mg/mL; 4 mg/mL, 5 mg/mL) for each derivative (6c, 6e, 6f, 6k). The resulted mixtures were dropped, using a syringe needle (26 G; 0.45 mm × 16 mm), into 20 mL of TPP (2%–3%), under light stirring and the mixture was left at room temperature, under stirring for 4–8 h to achieve an efficient reticulation. After 24 h the formed chitosan loaded beads (CS-XTDs) were separated from TPP solution, washed with distilled water three times, and air-dried at room temperature.

2.3. Characterization of Chitosan Microparticles Loaded with Xanthine Derivatives with Thiazolidine-4-one Scaffold (CS-XTDs)

2.3.1. Particle Size and Morphology

The CS-XTDs microparticle size (in wet and dry state) was measured using a Leica DM750 microscope (Wetzlar, Germany) equipped with a video model ICC50 W0366. The values were recorded with 10 \times objective by LAS EZ program. The morphology of the microparticles was studied using a scanning electronic microscope (SEM), Vega II SBH model, produced by the Tescan Company (Brno, Czech Republic). All measurements were performed in triplicate and the results are expressed as mean size \pm standard deviation.

2.3.2. Swelling Degree (SD)

The swelling studies were carried out using distilled water and simulated gastric fluid (SGF, pH 2.2) at 37 °C (in a thermostated water bath) according to the literature references [5,39]. Briefly, an exact amount of CS-XTDs microparticles was immersed into the media. At different times microparticles were removed from media (water and SGF respectively), dried quickly with filter paper, and weighted (W_1). At the end of the study the microparticles were dried again and weighted (W_2). All tests were carried out in triplicate and the results are expressed as mean SD \pm standard deviation. The analysis of Variance (ANOVA) was used to analyze the experimental data. Statistical significance was set to p value ≤ 0.05 .

The swelling degree (SD) at different times was calculated using the following formula:

$$\text{SD} (\%) = W_1 - W_2 / W_2 \times 100 \quad (1)$$

where: W_1 —the weight of the swollen CS-XTDs microparticles; W_2 —the weight of the dried CS-XTDs microparticles.

2.3.3. Drug Loading and Entrapment Efficiency

The loading efficiency of XTDs (6c, 6e, 6f, 6k) into the chitosan matrix was analyzed using a GBC Cintra 2010 UV-VIS spectrophotometer (Madrid, Spain) equipped with Cintral Software, according to the literature references [40] with slight modifications. The content of the XTDs into TPP solution was evaluated spectrophotometrically at different wavelengths, corresponding to each derivative, as follows: $\lambda = 276$ nm for 6k, $\lambda = 277$ nm for 6c and 6e, $\lambda = 280$ nm for 6f. The recorded values were used to calculate the non-loaded and loaded amount of each XTD. A standard curve for each XTD with a specific correlation coefficient ($y = 21.23x - 0.0112$; $R^2 = 1$ for 6c, $y = 27.606x - 0.0151$; $R^2 = 1$ for 6e, $y = 28.89x + 0.0219$; $R^2 = 0.9996$ for 6f, $y = 20.914x + 0.0406$; $R^2 = 1$ for 6k) was used.

The drug loading (DL) was calculated using the following formula [40]:

$$\text{DL} (\%) = \frac{W_3}{W_1} \times 100\% \quad (2)$$

where: W_1 = the amount of CS-XTD microparticles, after drying (mg); W_3 = the amount of XTD loaded into the chitosan matrix (mg).

The entrapment efficiency (EE) was calculated using the following formula [41]:

$$\text{EE} (\%) = \frac{W_3}{W_2} \times 100\% \quad (3)$$

where: W_2 = the mount of XTD used in study (mg); W_3 = the amount of XTD loaded into chitosan matrix(mg).

All tests were performed in triplicate and the results are expressed as mean DL/EE \pm standard deviation.

2.3.4. In Vitro Release

In vitro release of XTDs from polymeric system based chitosan (CS-XTDs: CS-6c, CS-6e, CS-6f, CS-6k) was performed using simulated gastric fluid (SGF, pH 1.2) and simulated intestinal fluid (SIF, pH 6.8), according to the literature references, with slight modifications [42–44]. The polymeric systems (CS-XTDs) were firstly placed in SGF for two hand then were moved to SIF. Briefly, a weighed amount of CS-XTDs microparticles was placed in a flask with 2 mL of media and incubated at 37 ± 0.1 °C under stirring (100 rpm). Every 30 min, a sample of 1.8 mL was collected from the media and replaced with an equal volume (1.8 mL) of fresh media. The concentration of the XTDs in the solution was evaluated spectrophotometrically at the specific wavelengths, corresponding to each derivative, using the standard curve previously obtained.

The Drug release (DR) was calculated using the following formula [42]:

$$\text{DR}(\%) = \frac{C_1}{C_0} \times 100\% \quad (4)$$

where: C_1 = concentration of the XTD (mg/mL) in the release media at different times; C_0 = concentration of the XTD (mg/mL) in the CS-XTD microparticles.

All tests were performed in triplicate and the results are expressed as mean DR \pm standard deviation.

2.3.5. Fourier Transform Infrared (FTIR) Spectroscopy

FT-IR spectra of chitosan, XTDs (6c, 6e, 6f, 6k) and of CS-XTDs (CS-6c, CS-6e, CS-6f, CS-6k) were recorded using ABB-MB3000 FT-IR MIRacleTM Single Bounce ATR (Zürich, Switzerland) at a resolution of 4 cm^{-1} , after 16 scans, in the $4000\text{--}650 \text{ cm}^{-1}$ range and processed with the Horizon MBTM FT-IR Software (Horizon MB 3.1.29.5, LabCognition GmbH & Co. KG, Cologne, Germany).

2.4. Biological Evaluation

2.4.1. Acute Toxicity Assay

The acute toxicity of the XTDs (6c, 6e, 6f, 6k) was evaluated by determining the lethal dose of 50 (LD_{50}). The Swiss mice (22–35 g) were housed in polyethylene cages, at constant conditions: temperature of 24 ± 2 °C, humidity of 40–70%, and cycle of 12 h light and 12 h dark. The acclimatization of the animals to laboratory conditions was performed 7 days before the experiment, receiving standard food and water ad libitum. The animals were kept fasting for 24 h before starting the experiment. Each group (six mice/group) received XTDs, orally (p.o.), as suspensions in Tween 80 in doses ranging between 1500–6500 mg/kg b.w. The survival rate was determined at 1 day, 2 days, 3 days, 7 days, and 14 days after administration.

The lethal dose 50 (LD_{50}) was determined by the Karber method using the following formula [45,46]:

$$LD_{50} = LD_{100} - \frac{\Sigma(a \times b)}{n} \quad (5)$$

where: a = the difference between two successive doses of the XTDs; b = the arithmetic average of the mice died from two successive series; n = the number of animals from each group; LD_{100} = the 100% lethal dose.

This study was performed according to the ethics guidelines on laboratory animal studies (Law no. 206/May 27, 2004, EU/2010/63-CE86/609/EEC) and with agreement (no 17826/2016) of the Ethics Committee for Animal Research of “Grigore T. Popa” University of Medicine and Pharmacy Iasi.

2.4.2. Antibacterial/Antifungal Tests

The antibacterial and antifungal activity of XTDs and CS-XTDs³ (5 mg/mL) were evaluated using the agar disc diffusion and broth micro-dilution methods.

The Agar Disc Diffusion Method.

Antibacterial and antifungal activity of XTDs and CS-XTDs, expressed as the diameter of inhibition area, were evaluated using the standard disk diffusion assay according to literature reference [47] with slight modifications. Prior to the test, the bacterial and yeast strains were diluted in NaCl (0.9 %) in order to achieve a turbidity equivalent of 10^6 CFU/mL (McFarland standard no 5). The suspensions were diluted 1:10 in Mueller Hinton agar (bacteria) and Sabouraud agar (yeasts) and then spread on sterile Petri plates (25 mL/Petri plate). Sterile stainless steel cylinders (10 mm height and 5 mm internal diameter) were placed on the agar surface in Petri dishes. In each cylinder 200 μ L of XTDs, solutions in DMSO (20 mg/mL) and an equivalent concentration of CS-XTDs were added. Commercial discs containing ampicillin (25 μ g/disc), ciprofloxacin (30 μ g/disc), and nystatin (100 μ g/disc) were used as a positive control. DMSO was used as a negative control. The plates were incubated for 24 h at 37 °C (bacteria) and for 48 h at 24 °C (yeasts). After incubation the diameters of inhibition were measured. All tests were performed in triplicate and the results are expressed as mean diameter \pm standard deviation.

The Broth Micro-Dilution Method.

The minimum inhibitory concentration (MIC) and the minimum bactericidal/fungicidal concentration (MBC/MFC) of XTD were determined using the standard two-fold dilution method standardized by [47], with slight modifications. The strains were inoculated in the specific agar medium and incubated at 37 °C for 24 h for bacteria, respectively 48 h at 24 °C for *Candida* strains. After the incubation, the culture media were diluted in order to obtain a final concentration of 10^6 CFU/mL. In a 96-well microplate, different dilutions were prepared from the stock solution of the XTDs (20 mg/mL), in order to obtain a volume of 100 μ L in each well with final concentrations in the range of 10 mg/mL, 5 mg/mL, 2.5 mg/mL, 1.25 mg/mL, 0.625 mg/mL, 0.312 mg/mL, 0.156 mg/mL, 0.078 mg/mL, 0.039 mg/mL, 0.0195 mg/mL, 0.009 mg/mL, and 0.0048 mg/mL. A volume of 100 μ L strain suspension was inoculated onto the wells and the microplates were incubated for 24 h at 37 °C (bacterial strains) and at 24 °C for (fungal strains). The MIC value was established as the lowest concentration, which determined the visual inhibition of the strain's growth. For MBC/MFC determination, 1 μ L from each visually complete inhibition was transferred onto a plate with solid media and incubated for 24 h at 37 °C (bacterial strains) and at 24 °C for (fungal strains). The MBC/MFC values were considered the lowest concentration, which killed 99.9% of the tested strains. All tests were performed in triplicate.

3. Results and Discussions

The synthesis of new xanthine derivatives with thiazolidine-4-one scaffold (6a–k) (Figure 1) were presented in our previous paper [38]. Some of these compounds showed good antioxidant effects in terms of the antiradical scavenging effect (DPPH, ABTS) and phosphomolybdenum reducing antioxidant power [38]. In this study the compounds were evaluated for antibacterial and antifungal effects and the most active of them were formulated as new polymeric systems based on chitosan in order to increase their biological effects.

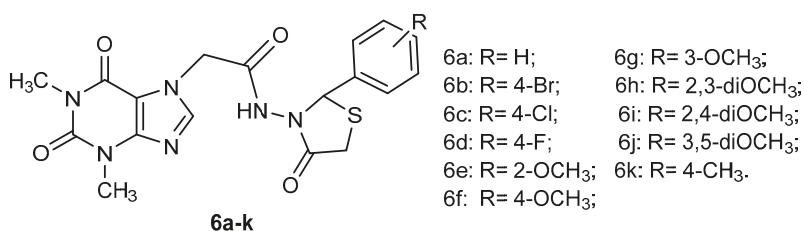


Figure 1. The structure of the xanthine derivatives with thiazolidine-4-one scaffold (XTDs: 6a–k).

3.1. New Polymeric Systems Based on Chitosan

The chitosan microparticles could be prepared using chemical and physical methods. The chemical method is based on the covalent bond formation between the functional groups of chitosan while the physical process involves electrostatic hydrophobic interactions or hydrogen bonds formation in the polymer matrix [48,49]. It is considered that the last type of polymeric system seems to have increased biocompatibility and are more tolerated than the chemical ones [50,51]. The most used physical method is ionic gelation, which is based on the ionic complexes formation between positively charged amino groups and anions such as sulphate, citrate, and phosphate. The most used cross-linking agent is pentasodiumtripolyphosphate, which interacts with the amino groups of chitosan by electrostatic forces [52].

Four XTDs (6c, 6e, 6f, 6k) were selected based on their biological effects and were inglobated into a polymeric matrix based on chitosan using the ionic gelation method. In order to optimize the preparation procedure of chitosan microparticles loaded with xanthine derivatives with thiazolidine-4-one scaffold (CS-XTDs) different parameters were applied: chitosan concentration (1.2%–1.7%), TPP concentration (2%–3%), and reticulation time (4–8 h). The most stable CS-XTDs systems were obtained using the following parameters: CS concentration of 1.7%, TPP concentration of 2%, and reticulation for 8 h. Using three concentrations (3 mg/mL, 4 mg/mL, 5 mg/mL) for each XTD, twelve CS-XTD systems were developed and characterized. The mass ration between CS, TPP, and XTD, based on the concentration of used XTD (9 mg, 12 mg, 15 mg) was as follows: 5.7:44:1, 4.25:33:1 and 3.4:27:1.

3.1.1. Particle Size and Morphology

The size of the CS-XTDs ranged between 858–953 µm (wet state) and 611–855 µm (dry state) and it was higher than CS (825 µm—wet state; 611 µm—dry state), thus confirming the loading process (Table 1). The data showed that the size increases with the concentration of the compounds and are in good agreement with similar data presented in the literature [53].

Table 1. Microparticles size of CS and CS-XTDs (CS-6c, CS-6e, CS-6f, CS-6k) at different concentrations.

CS/CS-XTDs	Size in Wet State (µm)	Size in Dry State (µm)	CS-XTDs	Size in Wet State (µm)	Size in Dry State (µm)
CS-6c ¹	904 ± 4.2	638 ± 3.1	CS-6f ¹	887 ± 2.1	614 ± 3.1
CS-6c ²	897 ± 7.2	762 ± 2.5	CS-6f ²	921 ± 4.0	675 ± 5.0
CS-6c ³	951 ± 3.1	855 ± 2.1	CS-6f ³	947 ± 3.2	751 ± 6.4
CS-6e ¹	858 ± 3.1	632 ± 3.5	CS-6k ¹	929 ± 6.0	639 ± 7.0
CS-6e ²	923 ± 3.5	634 ± 4.7	CS-6k ²	912 ± 5.0	688 ± 4.0
CS-6e ³	953 ± 2.9	646 ± 4.0	CS-6k ³	918 ± 2.1	728 ± 4.7
CS	825 ± 3.5	611 ± 3.1	-	-	-

¹ = 3 mg/mL, ² = 4 mg/mL, ³ = 5 mg/mL.

The SEM showed that chitosan microparticles (CS) have a spherical and regular shape, regular outline and a slightly rough surface. Upon loading of XTD, a deformation of microparticles was observed, which is intensified by the increasing concentration described in other studies [5]. The most intense deformation was observed in the case of CS-6c³ (5 mg/mL), for which the spherical shape is lost and pronounced flattening was recorded (Figure 2).

The results showed that a higher concentration of the cross-linking agent was associated with decreased stability of microparticles during the gelation process. Also, it was highlighted that the deformation of CS-XTDs microparticles during the air-drying process was directly proportional to the concentration of the TPP solution, which resulted in strongly flattened microparticles being obtained for a value of 3% TPP. The reticulation time is also an important parameter for the stability

of microparticles; increasing the time was associated with the increased stability of the developed polymeric systems [54,55].

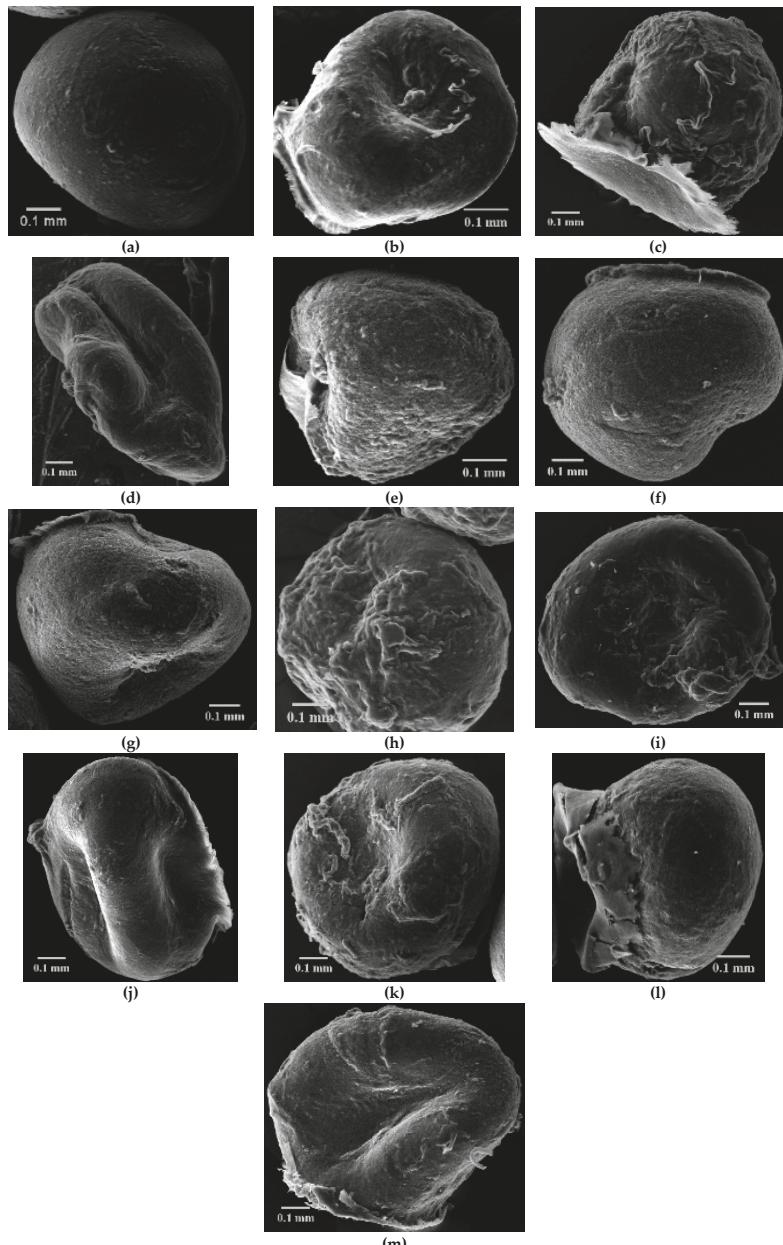


Figure 2. Scanning electron microscope (SEM) images for CS and CS-XTDs microparticles (**a**: CS, **b**: CS-6c¹, **c**: CS-6c², **d**: CS-6c³, **e**: CS-6e¹, **f**: CS-6e², **g**: CS-6e³, **h**: CS-6f¹, **i**: CS-6f², **j**: CS-6f³, **k**: CS-6k¹, **l**: CS-6k², **m**: CS-6k³); ¹ = 3 mg/mL, ² = 4 mg/mL, ³ = 5 mg/mL.

3.1.2. Swelling Degree (SD)

The swelling degree is an important parameter in the release of the drug from the polymer matrix, having an important influence on the drug's bioavailability. The results for CS-XTDs systems recorded in distilled water and simulated gastric fluid (SGF, pH 2.2) are presented in Figures 3–6. For distilled water, the swelling degree values of CS-XTDs was comparable with that of CS. The CS-XTDs absorbed the highest amount of water in the first 10 mins of the experiment, with the SD (%) value ranging around 150% (Figures 3 and 4). This phenomenon could be explained by the cross-linking agent which, by dissolution in aqueous medium, released the amino groups of chitosan, increasing the hydrophilic character of the polymer matrix.

The thermodynamic equilibrium state was reached after different times depending on the structure of XTDs loaded into the polymer matrix. At the end of the experiment the swelling degree values ranged between 190 ± 2.6 (CS- $6e^3$) and 206 ± 2.9 (CS- $6k^1$). In similar conditions the recorded value for CS was 209 ± 3.5 (Table 2).

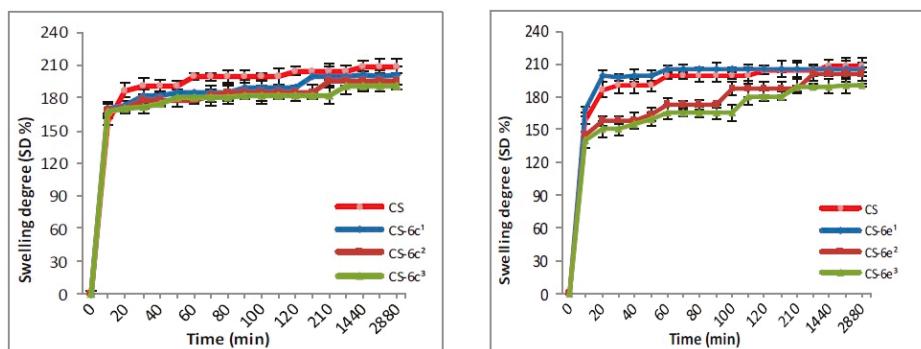


Figure 3. Swelling degree of CS and CS-XTDs (CS-6c; CS-6e) in distilled water at different concentrations ($^1 = 3 \text{ mg/mL}$, $^2 = 4 \text{ mg/mL}$, $^3 = 5 \text{ mg/mL}$).

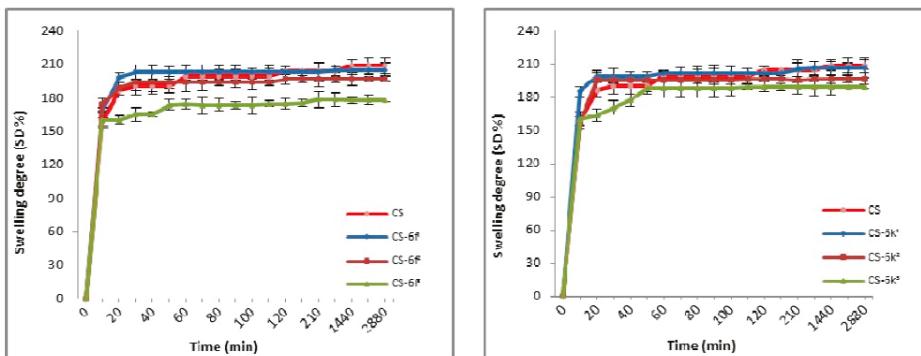


Figure 4. Swelling degree of CS and CS-XTDs (CS-6f; CS-6k) in distilled water at different concentrations ($^1 = 3 \text{ mg/mL}$, $^2 = 4 \text{ mg/mL}$, $^3 = 5 \text{ mg/mL}$).

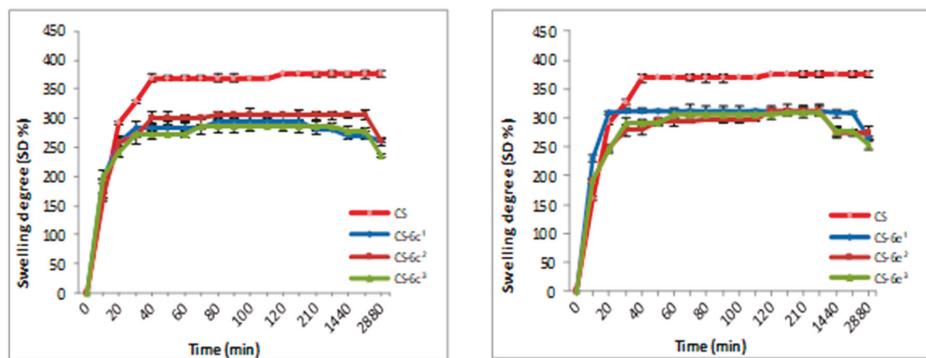


Figure 5. Swelling degree of CS and CS-XTDs (CS-6c; CS-6e) in SGF at different concentrations (¹ = 3 mg/mL, ² = 4 mg/mL, ³ = 5 mg/mL).

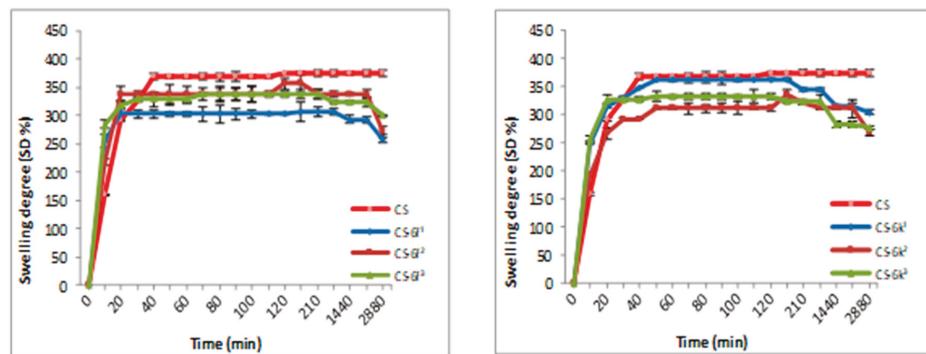


Figure 6. Swelling degree of CS and CS-XTDs (CS-6f; CS-6k) in SGF at different concentrations (¹ = 3 mg/mL, ² = 4 mg/mL, ³ = 5 mg/mL).

Table 2. Swelling degree of CS and CS-XTD at thermodynamic equilibrium state.

CS-XTDs	SD (%)						
CS-6c ¹	200 ± 2.7 *	CS-6e ¹	205 ± 3.6	CS-6f ¹	205 ± 4.5	CS-6k ¹	206 ± 2.9
CS-6c ²	195 ± 2.2 *	CS-6e ²	201 ± 1.7 *	CS-6f ²	197 ± 3.6 *	CS-6k ²	196 ± 5.2 *
CS-6c ³	190 ± 4.1 *	CS-6e ³	190 ± 2.6 *	CS-6f ³	178 ± 3.1 *	CS-6k ³	189 ± 3.1 *
CS	209 ± 3.5	-	-	-	-	-	-

* significant different ($p < 0.05$) in reference with CS; ¹ = 3 mg/mL, ² = 4 mg/mL, ³ = 5 mg/mL.

The analysis of the SD results recorded in SGF highlighted that the SD of CS-XTDs was lower than of CS (375%) (Figures 5 and 6); the results could be explained based on the hydrophobic character of the XTD loaded into the polymer matrix, a character which results in decreasing the chitosan matrix permeability and thus the swelling degree. The presence of functional groups such as halogen (6c) or methyl (6k), attached to the aromatic ring of the thiazolidine-4-one scaffold increases the hydrophobic character of the XTD. Our observation is in agreement with other literature data [56]. A high absorption degree (over 300%) at the beginning of the experiment was observed, after which it decreased in intensity. For CS the thermodynamic equilibrium state was reached after 2 h and

maintained until the end of the experiment. In similar conditions, for CS-XTDs the thermodynamic equilibrium state was reached after 40 min–2 h, depending on the kind of XTD loaded into the polymer matrix, which could result in a shorter period.

3.1.3. Drug Loading and Entrapment Efficiency

The results obtained for drug loading (DL) and entrapment efficiency (EE) parameters are presented in Figure 7 (CS-6c, CS-6e) and Figure 8 (CS-6f, CD-6k). The study highlighted that the entrapment efficiency ranged between 63.71% (CS-6e¹) and 93.91% (CS-6k³) and is directly proportional to the concentration. The highest entrapment efficiency, at all three concentrations (3 mg/mL, 4 mg/mL, 5 mg/mL), was recorded for CS-6k, the values being: 87.86 ± 1.25% (3 mg/mL), 91.58 ± 0.55% (4 mg/mL) and 93.91 ± 1.41% (5 mg/mL). These results could be explained based on the structure of the XTD (6k), which has hydrophobic *methyl* group at *para* position of the aromatic ring. The XTD with hydrophilic *methoxy* group attached at the *ortho* (6e) and *para* (6f) position on the aromatic ring have showed lower values of entrapment efficiency.

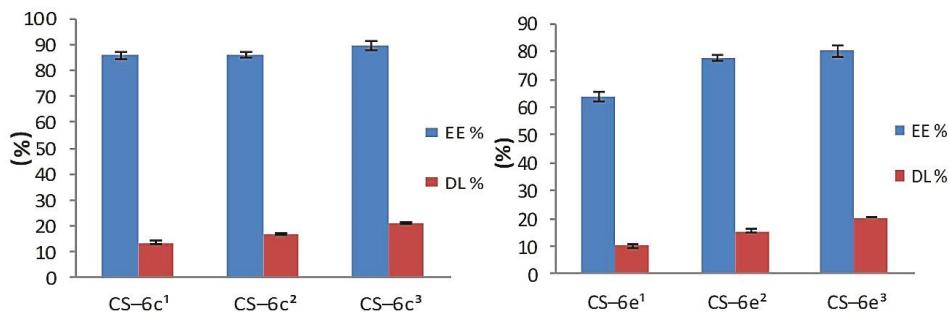


Figure 7. The Entrapment efficiency (EE%) and Drug loading (DL%) for CS-6c and CS-6e (¹ = 3 mg/mL, ² = 4 mg/mL, ³ = 5 mg/mL).

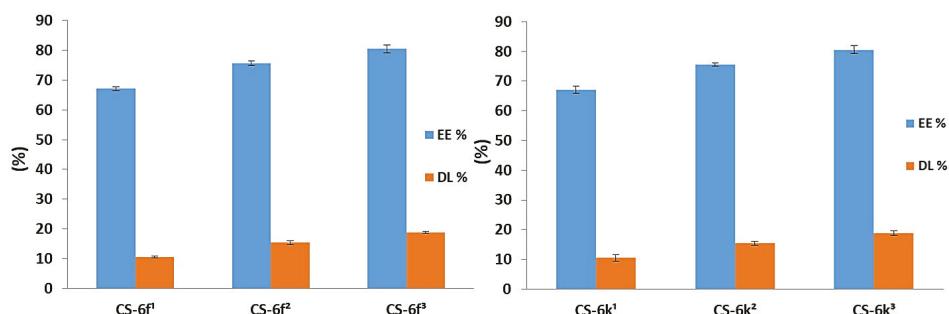


Figure 8. The Entrapment efficiency (EE%) and Drug loading (DL%) for CS-6f and CS-6k (¹ = 3 mg/mL, ² = 4 mg/mL, ³ = 5 mg/mL).

Concerning the DL of XTDs into the polymeric matrix, it was noted that this parameter increases with the concentration. The obtained values ranged between 10.04 ± 0.49% (CS-6e¹) and 22.02 ± 0.74% (CS-6k³). As a previous parameter, the highest values were obtained for derivative 6k, which has a *methyl* group at the *para* position of the aromatic ring as follows: 14.32 ± 1.12% (CS-6k¹), 18.90 ± 0.67% (CS-6k²), and 22.02 ± 0.74% (CS-6k³). A good correlation was also observed between DL and EE values, which proves the accuracy of the study. Thus, it has been demonstrated that the optimal CS-XTD formulation was obtained for 5 mg/mL of XTD.

3.1.4. In Vitro Drug Release

The literature describes two methods for releasing the drugs from the polymer matrix: by direct and indirect diffusion, the last one being based on the dissolution of the drug into the matrix, followed by the release through membrane pores. In turn, the membrane permeability is influenced by the method used to prepare the polymeric systems, by the morphology of microparticles, and not least by the chemistry structure of the drug. The oral route is the most used for drug administration. After the absorption of drugs through gastric or intestinal mucosa, it will pass to the blood system and then will arrive at the site of action. Normally, the gastric pH ranges between 1 and 1.5 and will contain 99% water and only 1% different organic or inorganic substances, while the small intestine has a pH, which ranges between 4.8 to 8.2.

In the SGF, the drug release from CS-XTD was ranging between 51.34% and 98.42%, while the drug release in SIF was lower, being around 5%, excepting the CS-6k for which the drug release in SIF was 17% (Figures 9 and 10). The lowest cumulative release was observed for CS-6f (CS-6f¹ = 58.10%, CS-6f² = 51.34%, CS-6f³ = 54.52%), while the highest values were recorded for CS-6c (CS-6c¹ = 98.42%, CS-6c² = 89.92%, CS-6c³ = 97.44%).

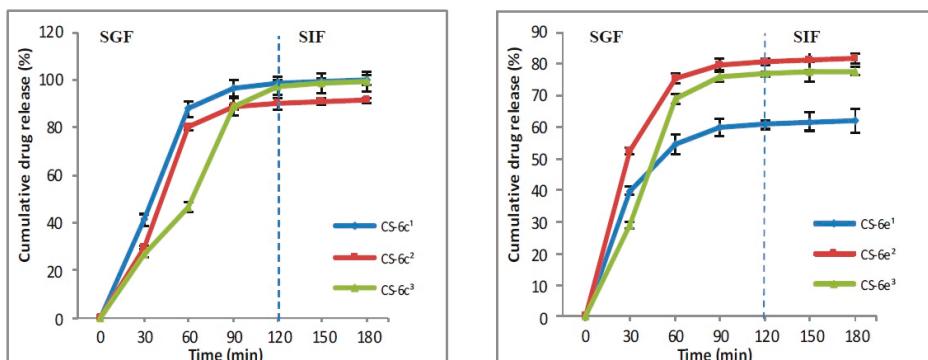


Figure 9. The release profile of compound 6c and 6e from CS-6c and CS-6e respectively (¹ = 3 mg/mL, ² = 4 mg/mL, ³ = 5 mg/mL).

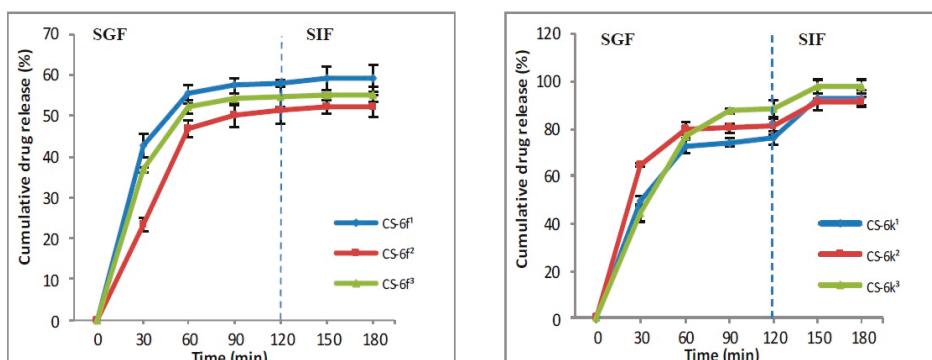


Figure 10. The release profile of compound 6f and 6k from CS-6f and CS-6k respectively (¹ = 3 mg/mL, ² = 4 mg/mL, ³ = 5 mg/mL).

3.1.5. FTIR Analysis

The confirmation of the loading process was performed by highlighting in FTIR spectra the CS-XTDs of the specific functional groups of the components of the polymeric matrix: CS, XTDs, and TPP. The FTIR spectra of CS-XTDs (CS-6c, CS-6e, CS-6f and CS-6k) at different concentrations in reference with the FTIR spectra of CS and XTDs (6c, 6e, 6f and 6k) are presented in Figure 11.

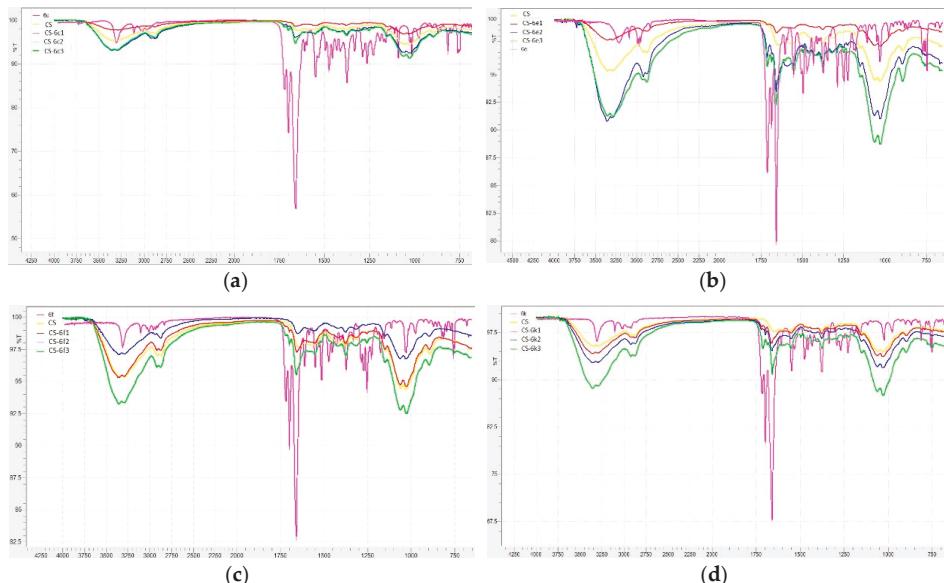


Figure 11. The Fourier transform infrared (FTIR) spectra of CS, XTDs (6c, 6e, 6f, 6k) and CS-XTDs (CS-6c, CS-6e, CS-6f, CS-6k) (¹ = 3 mg/mL, ² = 4 mg/mL, ³ = 5 mg/mL).

In acetic acid solution, chitosan has a pKa of 6.3 and a polycationic structure with positively charged amino groups. In water, TPP dissociates to form both hydroxyl and phosphoric ions. In the crosslinking process the cationic amino groups of chitosan react with negatively charged TPP to form ionic complexes by electrostatic bonds. A secondary mechanism based on hydrogen-hydrogen bonds between the hydroxyl groups of CS and of TPP is also possible [50]. The XTDs are physically and uniformly dispersed into the polymer matrix. The concentration of CS and XTDs are very important parameters, because they influence the physic-chemical properties of the CS-XTD systems [49].

The specific vibrations of functional groups of CS have been identified in the following regions: 3362–3285 cm⁻¹ (OH, NH), 2981–2872 cm⁻¹, 1431–1414 cm⁻¹ and 1377–1375 cm⁻¹ (-CH₂-CH₃), 1661–1647 cm⁻¹ (C=O), 1267–1250 cm⁻¹ (C-N), 1034–1026 cm⁻¹ (C-O-C). The presence of XTDs (6c, 6e, 6f and 6k) into the polymer matrix was confirmed by identification of the specific absorption bands: NH bond (3362–3285 cm⁻¹), thiazolidine-4-one ring: 2981–2872 cm⁻¹ (-CH₂-), 1724–1711 cm⁻¹ (C=O) and 671–660 cm⁻¹ (C-S), aromatic ring: 3362–3285 cm⁻¹, 810–746 cm⁻¹ (=C-H), 1558–1549 cm⁻¹ and 1494–1452 cm⁻¹ (C=C), amide group, which are overlapping with valence vibrations of the same group in the chitosan structure, and not the substituents on the aromatic ring at 1063–1059 cm⁻¹ (C-O from -OCH₃ in case of 6e and 6f), 822–818 cm⁻¹ (-Cl in case of 6c) and 1377–1375 cm⁻¹ (-CH₃ in case of 6e, 6f and 6k). The reticulation agent, TPP, was identified by specific absorption bands in the 1151–1149 cm⁻¹ region (P=O) and the 895–893 cm⁻¹ region (P—O—P).

3.2. Biological Evaluation

3.2.1. Toxicity Degree

The toxicological screening highlighted that all tested XTDs (6c, 6e, 6f, 6k) have a low toxicity, with the following LD₅₀ values: 2125 mg/kg bw (6c), 1687.5 mg/kg bw (6e), 1937.5 mg/kg bw (6f) and 1312.5 mg/kg bw (6k). These compounds proved to be less toxic than theophylline, which is used as a starting reagent in their synthesis (LD₅₀ = 332 mg/kg bw) [57] and supports the favorable influence of thiazolidine-4-one scaffold upon the chemical modulation of xanthine structure.

3.2.2. Antibacterial/Antifungal Study

The data presented in Table 3 showed that XTDs (6a–k) and CS-XTDs³ (CS-6c³, CS-6e³, CS-6f³, CS-6k³) are active on both bacterial and fungal strains, the diameter of the inhibition area being in correlation with structure of the XTD and also with bacterial and yeasts strains, respectively.

Table 3. Antibacterial/antifungal inhibition area (mm) of XTDs (6a–k) and CS-XTDs.

Sample	Diameter of Inhibition Area*(mm)					
	Bacterial Strains			Yeasts Strains		
	SA	SL	EC	CA	CG	CP
6a	15.2 ± 0.23	20.1 ± 0.17	12.2 ± 0.35	11.1 ± 0.36	12.2 ± 0.22	12.2 ± 0.24
6b	15.3 ± 0.40	19.1 ± 0.28	11.1 ± 0.23	10.1 ± 0.21	10.8 ± 0.37	10.3 ± 0.31
6c	14.9 ± 0.21	19.0 ± 0.13	10.4 ± 0.15	15.2 ± 0.21	12.1 ± 0.42	11.2 ± 0.24
6d	17.1 ± 0.24	18.1 ± 0.42	11.2 ± 0.47	10.0 ± 0.11	11.0 ± 0.46	11.3 ± 0.32
6e	14.0 ± 0.38	18.8 ± 0.29	11.1 ± 0.14	10.1 ± 0.28	10.9 ± 0.26	14.2 ± 0.12
6f	15.0 ± 0.50	20.1 ± 0.43	11.2 ± 0.35	12.1 ± 0.07	10.0 ± 0.06	15.2 ± 0.11
6g	15.5 ± 0.27	20.0 ± 0.31	12.1 ± 0.26	11.3 ± 0.23	16.1 ± 0.28	15.4 ± 0.31
6h	15.4 ± 0.34	19.2 ± 0.09	12.0 ± 0.06	15.2 ± 0.26	19.1 ± 0.17	12.0 ± 0.14
6i	15.4 ± 0.25	19.1 ± 0.11	12.1 ± 0.04	12.5 ± 0.10	15.0 ± 0.24	12.1 ± 0.23
6j	15.2 ± 0.14	19.1 ± 0.17	12.2 ± 0.26	12.2 ± 0.26	15.3 ± 0.09	12.1 ± 0.24
6k	14.3 ± 0.19	17.8 ± 0.23	11.0 ± 0.31	10.3 ± 0.23	13.2 ± 0.11	11.0 ± 0.13
CS-6c ³	16.4 ± 0.41	21.0 ± 0.23	12.3 ± 0.21	17.4 ± 0.29	14.3 ± 0.38	13.2 ± 0.31
CS-6e ³	15.2 ± 0.23	20.4 ± 0.21	13.4 ± 0.25	12.5 ± 0.21	12.6 ± 0.21	15.4 ± 0.26
CS-6f ³	21.2 ± 0.43	25.1 ± 0.28	14.7 ± 0.38	16.7 ± 0.42	12.3 ± 0.51	18.4 ± 0.42
CS-6k ³	17.1 ± 0.32	22.4 ± 0.18	15.2 ± 0.18	14.6 ± 0.21	16.3 ± 0.38	17.2 ± 0.35
CS	12 ± 0.35	11 ± 0.26	9 ± 0.41	-	-	-
C ^a	25.1 ± 0.08	25.0 ± 0.1	28.9 ± 0.18	-	-	-
A ^b	27.1 ± 0.12	31.8 ± 0.15	21.0 ± 0.21	-	-	-
N ^c	-	-	-	20.1 ± 0.11	21.0 ± 0.14	20.1 ± 0.09

* mean values (n = 3) ± standard deviation. SA = *Staphylococcus aureus* ATCC 25923; SL = *Sarcina lutea* ATCC 9341; EC = *Escherichia coli* ATCC 25922; CA = *Candida albicans* ATCC 10231; CG = *Candida glabrata* ATCC MYA 2950; ³ = 5 mg/mL; CP = *Candida parapsilosis* ATCC 22019; C^a = Ciprofloxacin (30 µg/disc); A^b = Ampicillin (25 µg/disc); N^c = Nystatin (100 µg/disc).

Referring to the XTDs it was noted the most active compound on *Staphylococcus aureus* ATCC 25923 was 6d, for which the diameter of the inhibition area was 17.1 ± 0.24 mm. The compounds 6a, 6f and 6g showed improved antibacterial effects on *Sarcina lutea* ATCC 9341, their effect (6a: 20.1 ± 0.17 mm, 6f: 20.1 ± 0.43 mm, 6g: 20.0 ± 0.31 mm) being higher than the effect of CS and comparable with ciprofloxacin (25.0 ± 0.1 mm). The effect of XTDs on Gram negative bacterial strain *Escherichia coli* ATCC 25922 was reduced in reference to Gram positive bacterial strains (*Staphylococcus aureus*, *Sarcina lutea*), the diameter of the inhibition area ranging between 10.4 mm and 12.2 mm.

Appreciable antifungal effects were noted for compounds 6c and 6h on *Candida albicans* ATCC 10231 (15.2 ± 0.21 mm and 15.2 ± 0.26 mm respectively), for 6h and 6g on *Candida glabrata* ATCC MYA 2950 (19.1 ± 0.17 mm and 16.1 ± 0.28 mm respectively) and for 6f and 6g on *Candida parapsilosis* ATCC 22019 (15.2 ± 0.11 mm and 15.4 ± 0.31 mm respectively).

As we expected, the loading of the XTDs into the polymer matrix based on chitosan was associated with increasing the antimicrobial effects, all CS-XTD systems (CS-6c, CS-e, CS-6f, CS-6k) show improved antibacterial and antifungal effects in reference to corresponding XTD (6c, 6e, 6f, 6k) (Table 3).

The antibacterial effect of 6d was confirmed by the broth micro-dilution assay, for which the minimum inhibitory concentration (MIC) and minimum bactericidal concentration (MBC) were 0.3125 mg/mL and 10 mg/mL, respectively (Table 4). The similar results were obtained also for 6a. It was also noted that, in most cases, the value of MBC was 10 mg/mL, higher than the value of MIC, which means that the compounds act, especially, by the inhibition of microbial growth that can then act as bactericidal agents.

Table 4. Antimicrobial activity expressed as MIC and MBC values (mg/mL) of XTDs (6a–k).

Sample	<i>Staphylococcus Aureus</i> ATCC 25923		<i>Escherichia Coli</i> ATCC 25922		<i>Candida Albicans</i> ATCC 90028	
	MIC *	MBC *	MIC *	MBC *	MIC *	MBC *
6a	0.625	10	1.25	1.25	1.25	1.25
6b	2.5	10	2.5	2.5	1.25	1.25
6c	2.5	10	1.25	1.25	1.25	2.5
6d	0.3125	10	1.25	2.5	2.5	2.5
6e	1.25	10	1.25	1.25	1.25	2.5
6f	0.625	10	1.25	2.5	2.5	2.5
6g	0.625	10	1.25	2.5	2.5	2.5
6h	1.25	5	2.5	2.5	2.5	2.5
6i	0.625	10	2.5	2.5	2.5	2.5
6j	0.625	10	1.25	2.5	2.5	2.5
6k	1.25	10	0.625	2.5	0.625	1.25
A	1 ¹	2 ¹	2 ¹	4 ¹	-	-
N	-	-	-	-	8 ¹	16 ¹

* mean values (n = 3) ± standard deviation; ¹ µg/mL.

4. Conclusions

In this study new polymeric systems based on chitosan (CS) loaded with new xanthine derivatives with thiazolidine-4-one scaffold (XTDs) were developed and characterized. The success of the loading process was proved by highlighting in FTIR spectra of the CS-XTDs of the specific functional groups of XTD. The optimized polymeric systems were evaluated in terms of particle size, morphology, swelling degree, drug loading and entrapment efficiency. The results demonstrated a good swelling degree for CS-XTDs and the entrapment efficiency of the XTD into polymer matrix was between 63% and 94%. In the simulated biological fluids (SGF, SIF), an increased cumulative release, between 54.52% and 97.44% was observed. The data supports also improved antimicrobial effects for CS-XTDs in reference with XTDs. Based on the obtained results the developed polymeric systems could have important applications in the food field as active multifunctional (antimicrobial, antifungal) packaging materials and in medical and pharmaceutical fields.

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Abbreviations

ABTS	2,2'-Azino-bis(3-ethylbenzthiazoline-6-sulfonic acid)
bw	Body weight
CFU	Colony Forming Unit
CS	Chitosan
CS-XTDs	Chitosan microparticles loaded with xanthine derivatives with thiazolidine-4-one scaffold
DL	Drug loading
DMSO	Dimethyl sulfoxide
DPPH	2,2-diphenyl-1-picryl-hydrazyl-hydrate
DR	Drug release
EE	Entrapment efficiency
FT-IR	Fourier transform infrared
LD ₅₀	Lethal dose 50
MBC	Minimum bactericidal concentration
MFC	Minimum fungicidal concentration
MIC	Minimum inhibitory concentration
SD	Swelling degree
SEM	Scanning electron microscopy
SGF	Simulated gastric fluid
SIF	Simulated intestinal fluid
TPP	Pentasodium tripolyphosphate
XTDs	Xanthine derivatives with thiazolidine-4-one scaffold

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Article

Antioxidant/Antibacterial Electrospun Nanocoatings Applied onto PLA Films

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Abstract: Polylactic acid (PLA) films were coated by coaxial electrospinning with essential and vegetable oils (clove and argan oils) and encapsulated into chitosan, in order to combine the biodegradability and mechanical properties of PLA substrates with the antimicrobial and antioxidant properties of the chitosan–oil nanocoatings. It has been established that the morphology of the electrospun nanocoatings mainly depend on the average molecular weight (MW) of chitosan. Oil beads, encapsulated into the main chitosan nanofibers, were obtained using high-MW chitosan (Chit-H). Oil encapsulated in chitosan nanoparticles resulted when low-MW chitosan (Chit-L) was used. The coating layer, with a thickness of 100 ± 20 nm, had greater roughness for the samples containing Chit-H compared with the samples containing Chit-L. The coated PLA films had higher antibacterial activity when the nanocoating contained clove oil rather than when argan oil was used, for both types of chitosan. Nanocoatings containing Chit-H had higher antibacterial activity compared with those containing Chit-L, for both types of oil tested, due to the larger surface area of the rougher nanoscaled morphology of the coating layer that contained Chit-L. The chitosan–clove oil combination had higher antioxidant activity compared to the simple chitosan nanocoating, which confirmed their synergistic activities. The low activity of systems containing argan oil was explained by big differences between their chemical composition and viscosity.

Keywords: electrospinning; nanocoating; chitosan; vegetable oil; essential oil; cold-press oil; antimicrobial; antioxidant

1. Introduction

Due to increased demand for food packaging, efforts are being made to increase the storage- and shelf-life of food products by developing active antimicrobial packaging that does not require the use of synthetic additives [1]. The antibacterial agent may be incorporated into the packaging material [2] or coated onto it [3,4].

Various natural antibacterial agents have been encapsulated into different matrices to create coatings onto base packaging materials, such as cinnamaldehyde and carvacrol encapsulated in soy protein isolates [5]; nisin and natamycin in polyvinylchloride lacquer [6]; sorbic acid in polyvinyl

acetate [7]; essential and vegetable oils, such as garlic oil and rosemary oleoresin, in soy protein isolate [8]; and oregano essential oil in ethylene-vinyl alcohol copolymer film [9].

Due to its well-known antibacterial activity against various pathogens such as *Klebsiella pneumoniae*, *Escherichia coli*, *Staphylococcus aureus*, and *Pseudomonas aeruginosa* [10], chitosan has been extensively studied to obtain antibacterial coatings [11]. Chitosan was also used to encapsulate another antibacterial agent, nisin [12], which, in combination with chitosan, could improve the antimicrobial activity of the coatings [13]. The biodegradable chitosan is non-toxic and confers antibiofilm, antioxidant, and antifungal properties to the coated layer [14].

Various procedures have been proposed for preparation of the antimicrobial coating: Spreading with a thin-layer chromatography applicator [5] or a lab bench coater [7]; using a bar coater [15] or a brush [16]; spraying (nebulization) [17]; lamination [18]; gravure printing [9]; dip-coating [19]; and translated, at industrial scale, by coupling with a wet-coating station and roll-to-roll system [20].

In this work, electrospinning/electrospraying is used as the coating technique. The properties of the coatings, containing the essential and cold-pressed oils, depend on the way they are distributed onto the base polymer (substrate) and also on the way they make contact with the food. In this respect, the nanoscale dimensions and high area-to-volume ratio of the electrospun/electrosprayed nanostructures (nanofibers and nanoparticles), help to improve the contact between the coatings and the packed food, while the encapsulation of the essential and vegetable oils, into the polymeric nanostructures, helps to maintain their antibacterial and antioxidant activities over a longer time period. Therefore, electrospinning/electrospraying is an effective and convenient method to obtain nanocoatings [21] due to several advantages offered by this technique, such as:

(a) By electrospinning, very thin nanofibers with a high porosity and area-to-volume ratio can be obtained.

(b) The thickness of the coated (deposited) layer can be easily controlled by changing the deposition time or the flow rate of the electrospinning solutions. Thus, it is possible to obtain a very thin coating (nanocoating) with a very small quantity of materials, which in many cases is enough to obtain the desired antibacterial and antioxidant [4] or antifungal activity [22]. In comparison, with the coating thickness obtained by other methods, such as solvent casting or dip-coating with special film applicators (3 µm [23], 2 ÷ 9 µm [6], 2 ÷ 3 µm [24]), the very thin layer (100 nm or even less) has the added advantage of requiring a low amount of the coating material.

(c) Plasticizers are often added to the chitosan coating layer [12] to overcome the brittleness exhibited during the package deformation, and to improve the flexibility and processability. As a coating layer, the nanofibers can exhibit better ductility than the corresponding bulk material [25] due to low-nanofiber crystallinity, which resulted from rapid solidification of the ultrafine electrospun jets [26]. Thus, it is expected that the nanosized electrospun coating layers will exhibit the needed flexibility, either in the form of nanofibers or nanoparticles, without the plasticizer addition.

In the present work, the polylactic acid (PLA) films were coated by electrospinning with bio-formulations containing chitosan and one of the two vegetable oils (i.e., clove and argan oils), which were chosen due to their different compositions. According to the literature data, acylglycerols constitute 99% of the argan oil composition, while the unsaponifiable matter contains tocopherols, squalene, sterols, and phenols as the main antioxidant compounds [27,28]. Eugenol (~80%) is the main volatile component of clove oil, which is responsible for its strong antioxidant and antimicrobial activities [29]. The different compositions of the two types of oils are expected to result in different antimicrobial and antioxidant activities of the coated PLA films, and also in different rheological properties, which, in turn, will determine differences in the morphologies of the electrospun coated layers at nanoscale level.

PLA films were coated with active bio-formulations with the intention to combine the biodegradability and mechanical properties of PLA substrate polymer with the antimicrobial and antioxidant activities and biological functions of clove and argan oils, in combination with the chitosan. The oils were encapsulated in chitosan by coaxial electrospinning so as to prolong their functions as

antimicrobial and antioxidant agents over a long time, to prevent their degradation and loss during the processing conditions, and also to prevent their rapid diffusion and migration into the packaged food.

2. Materials and Methods

2.1. Materials

Chitosan with two different average molecular weights (MW) was purchased from Sigma-Aldrich (Schnelldorf, Germany): Highly viscous chitosan (Chit-H), MW = 310,000–375,000 g/mol, deacetylation degree DD ≈ 77% [21], with a dynamic viscosity in 1% acetic acid (20 °C) > 400 mPa·s; and low viscous chitosan (Chit-L), MW = 50,000–190,000, DD ≈ 87% [21], with viscosity in 1% acetic acid of 20–300 cP. The range values for MW (average molecular weight) were taken from producer specifications.

Glacial acetic acid (analytical purity) and chloroform were obtained from Chemical Company (Iasi, Romania).

Vegetable oils (argan and clove oils) with antioxidant and antimicrobial activities were chosen and were purchased from the Fares SA (Orastie, Romania) and Herbavit SA (Oradea, Romania) companies, respectively. The phenol content of the oils were 1.16 mg GAE/g DW (gallic acid equivalents/dry weight) for the clove oil and 0.02 mg GAE/g DW for the argan oil.

Two types of PLA films were coated: (a) Hot-pressed films obtained from PLA 2002D pellets (from NatureWorks LLC, Minnetonka, MN, USA), and (b) commercial NATIVIA® NTSS 40 µm PLA foils (from Taghleef Industries, Newark, DE, USA). The hot-pressed PLA substrates with a thickness of 0.30 ± 0.05 mm were obtained using a Carver press at 175 °C (2 min pre-melting and 2 min pressing at 240 bar). The NATIVIA® commercial PLA foils (Taghleef Industries, Newark, DE, USA) were used in order to test the applicability of this coating method for commercial products that currently exist in the market.

2.2. Preparation of the Nanostructured Coatings

The electrospinning system, used for coating the PLA foils (Figure 1), consisted of a high voltage supply (HV), a rotating metallic-plate collector, and two syringes with a coaxial needle oriented perpendicular to the metal plate. The PLA substrate film was placed on the metallic collector. The high direct voltage (0 to 30 kV) was applied between the metal plate and the metallic needle.

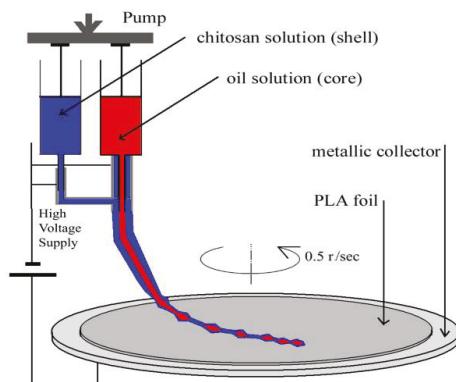


Figure 1. The coaxial electrospinning set-up used for coating the poly(lactic acid) (PLA) foils. The PLA foil is placed directly onto the metallic collector.

The low surface energy of polymeric substrates often leads to poor adhesion of the coatings to the substrates. To improve the adhesion, the surface is usually activated or functionalized by corona [9] or plasma [30] treatment. Before getting coated with the chitosan–oil formulations by electrospinning,

the PLA substrates were treated by exposure to cold plasma (nitrogen gas discharge atmosphere, 1.3 MHz frequency, 100 W power, 0.4 mbar pressure). Plasma treatment, and the consequent air exposure, leads to the implementation of some functionalities on the surface, such as groups and free radicals containing nitrogen and oxygen, which are able to interact with functional groups of the components of the nanocoating that were deposited by electrospinning [31].

After plasma treatment, the coaxial electrospinning was applied to obtain oil-loaded nanostructures, by encapsulating the clove or argan oil into the chitosan nanostructures, simultaneous with being coated onto the plasma-treated PLA substrates. The coaxial system consisted of chitosan supplied to the outer nozzle and oil solutions supplied to the inner nozzle.

For the hot-pressed PLA film substrates, the samples were designated the codes HC, HA, LC, and LA where H and L signifies high- and low-viscous chitosan, respectively, and C and A signifies clove and argan oil, respectively.

Correspondingly, for the commercial NATIVIA® NTSS substrate, the samples were labelled as HC-NATIVIA and HA-NATIVIA. Additionally, H-NATIVIA was designated the commercial NATIVIA® NTSS 40 µm, coated only with Chit-H, and PLA-NATIVIA was designated the uncoated PLA commercial foil (Table 1).

Table 1. PLA samples uncoated and coated with chitosan and clove oil or argan oil, using the electrospinning technique.

Code	Sample Description
Uncoated Samples	
PLA Hot-Pressed	Hot-pressed PLA films obtained from PLA 2002D pellets (NatureWorks LLC)
PLA-NATIVIA	Commercial NATIVIA® NTSS 40 µm PLA foils (from Taghleef Industries)
Coated Samples: PLA Hot-Pressed Substrate	
PLA-H	PLA hot-pressed film coated with Chit-H
HC	PLA hot-pressed film coated with Chit-H/clove oil
HA	PLA hot-pressed film coated with Chit-H/argan oil
LC	PLA hot-pressed film coated with Chit-L/clove oil
LA	PLA hot-pressed film coated with Chit-L/argan oil
Coated Samples: PLA-NATIVIA Substrate	
HC-NATIVIA	Commercial PLA-NATIVIA® NTSS 40 µm coated with Chit-H/clove oil
HA-NATIVIA	Commercial PLA-NATIVIA® NTSS 40 µm coated with Chit-H/argan oil
H-NATIVIA	Commercial PLA-NATIVIA® NTSS 40 µm coated with Chit-H

Both of the chitosan and oil solutions had the same concentration of 1.5 wt%. Chitosan was dissolved in 9:1 glacial acetic acid and water, respectively, argan oil was dissolved in chloroform, and clove oil was dissolved in glacial acetic acid. Electrospinning parameters (for all samples) were 1 kV/cm electrical field strength, 1.2 µL/min feed rate (for both the inner and outer needle), and 30 min deposition time. To be sure of complete solvent removal, the electrospun nanostructures were placed for two days in a vacuum desiccator (Binder GmbH, Tuttlingen, Germany). The absence of the acetic acid in the deposited mesh in was confirmed by IR spectroscopy (using a Bruker VERTEX 70 spectrometer, Ettlingen, Germany).

2.3. Investigation Methods

Scanning electron microscopy (SEM/EDX) analyses were carried out using a QUANTA 200 scanning electronic microscope (Thermo Fisher Scientific, Waltham, MA, USA) with an integrated EDX system, (Thermo Fisher Scientific Waltham, Waltham, MA, USA), and a GENESIS XM 2i EDAX with SUTW detector (FEI Company, Eindhoven, The Netherlands).

Atomic force microscopy (AFM) investigations were done with a Solver-Pro-M type instrument (Solver Inc., Moscow, Russia) under ambient conditions, using standard tips of Si₃N₄ (10 nm curvature

radius). The root mean square roughness was calculated from the total image sample after a second-order flatness treatment of the raw data. NT-MDT Nova v.1.26.0.1443 software (NT-MDT Spectrum Instruments, Moscow, Russia) was used for the acquisition and analysis of the images.

Transmission electron microscope (TEM) investigations were conducted with a Hitachi High-Tech HT7700 microscope (Hitachi High-Tech GLOBAL, Tokyo, Japan) high contrast mode at 100 kV accelerating voltage) on electrospun grids (300 mesh holey carbon coated copper grids). The grids were placed onto the PLA substrate during the electrospinning process.

Antimicrobial activity was determined, using two kinds of tests, in order to verify the differences between the antimicrobial activities of the clove and argan oils.

In the first test the suspension and culture medium were prepared as is described in the ISO 22196 (ISO 22196: Plastics—measurement of antibacterial activity on plastics and other non-porous surfaces (2011)). The test strains were incubated for 24 h at 37 °C. The antimicrobial testing method consisted of placing a drop of a suspension, of either *Escherichia coli* (ATCC 8739) or *Staphylococcus aureus* (ATCC 6538), onto the surface of the tested material (with a surface area of 5 cm × 5 cm). Each tested sample was prepared in a separate sterile vessel, with the test surface facing upwards. Then 0.4 mL of the test inoculum was dropped onto the tested surface. The test inoculum was covered with a piece of film (with a surface area 4 cm × 4 cm), which did not have anti-bacterial properties (neutral film), and was pressed mildly onto the film so that the test inoculum spread to the periphery. Half of the untreated specimens were processed instantly after inoculation, by adding 10 mL of Soybean Casein Lecithin Polysorbate Medium (SCDLP) broth (ISO 22196) to the vessel containing the test specimen. After this, the sum of viable bacterial cells was assessed. This obtained amount was used to evaluate the recovery rate of the bacteria from the investigated test specimens. After the inoculation of the specimen and the application of the cover film, the lid of the vessel was changed. After a 24 h incubation period, at 35 °C, the bacterial suspension was released from the coverslip-test sample and the sum of the viable bacterial cells that had survived was determined. The log values were the mean of 3 parallel samples (for each film type). The log reduction was the difference between the growth obtained with a neutral film (Stomacher bag) and the growth obtained with an active treated film. Sometimes a reduction, rather than growth, was observed with the neutral film, because of the low pH of the free lactic acid containing the PLA.

The second test was performed as it is described in the ISO 16649-2/2007: Microbiology of alimentary and animal products. There are several phases in the procedure for testing antimicrobial activity against *Escherichia coli*, *Salmonella typhimurium*, and *Listeria monocytogenes*: Sterilization of samples; inoculation with ATCC culture bacteria; 24 and 48 h (at 44 °C) inoculation and incubation, respectively; and the identification of target germs. Sterilization of the samples was performed for 20 min at 0.5 bar and at 110 °C, in an autoclave. Formation of the ATCC cultures was performed by seeding the average pre-enrichment, followed by incubation for 24 h at 37 °C; counting the number of colonies in the 0.1 mL culture after the culture medium separation; and then seeding 0.1 mL of bacterial culture ATCC, using sterile swab samples taken from the surface. The following standardized bacteriological procedures were employed in order to identify the target germs: For *Escherichia coli*, the SR ISO 16649, horizontal method for beta-glucuronidase-positive *Escherichia coli* quantification, was used. Then colonies were counted at 44 °C using 5-bromo-4-chloro-3-indolyl beta-D-glucuronide according to Minerals Modified Glutamate Broth (Cat. 1365), which produce blue or green-blue colonies on agar glucuronide; for *Listeria monocytogenes*, SR EN ISO 11290 was used; and for *Salmonella* sp., SR EN ISO 6579/2003/AC/2004/AC/2006, Amd.1:2007 was used.

The antioxidant activity of PLA (NATIVIA) coated films was measured by DPPH (1,1-diphenyl-2-picryl-hydrazyl) free radical assay [32]. The samples (coated films) were immersed in the DPPH solution and the decrease of the absorbance at 517 nm, which reflected the amount of DPPH radicals in the solution, was measured by means of a Cary 60-UV-Vis Spectrophotometer (Mettler Toledo, Columbus, OH, USA). The measurements were done at different immersion times (after 0, 15, 40 and 60 h immersion time). The DPPH solution (in the absence of the coated films) was used as a

control. The radical scavenging activity (RSA) of the samples was expressed by the relative decrease in DPPH absorbance at 517 nm ($RSA = 1 - A_{\text{SAMPLE}}(t)/A_{\text{DPPH}}(t)$ where $A_{\text{DPPH}}(t)$ and $A_{\text{SAMPLE}}(t)$ are the absorbance of the control and sample at the time of measurement). For testing, a 4 cm^2 area of the coated film was cut into pieces and immersed in 1.5 mL of DPPH solution in methanol with a concentration of 8 micrograms/mL. Before immersion and testing, the samples were stored for seven days at room temperature. Between measurements the solutions were stored in the dark at 24°C .

3. Results and Discussion

3.1. Transmission Electron Microscope (TEM) Results

The TEM images show a hybrid fiber and particle morphology for the HA and HC samples (Figure 2a,b), and particle morphology for the LA and LC samples (Figure 2c,d).

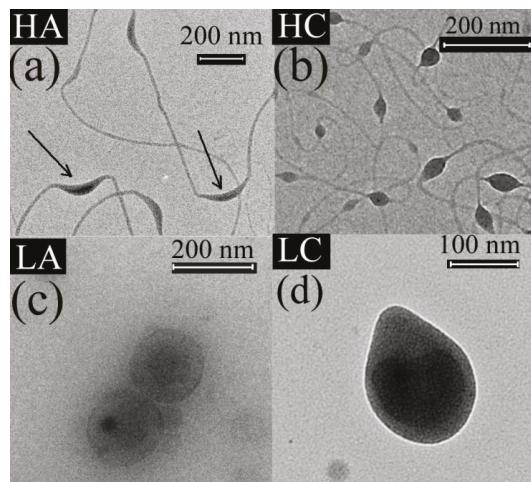


Figure 2. Transmission electron microscope (TEM) images of the studied samples: (a) HA; (b) HC; (c) LA; and (d) LC samples.

It is well known that sufficient chain entanglements should occur in the electrospun solution [33] in order to obtain nanofibers by electrospinning. Thus, the presence of fibers for the HA and HC samples could be explained by the high MW of chitosan, which resulted in better macromolecular entanglements in the electrospun solution. Due to the low MW, the chain entanglements in LA and LC samples were not enough [34] to sustain the fiber formation, which resulted in the spraying of beads (which ultimately may form a rather compact film). Thus, the only spinnable (nanofiber mesh forming) samples are those containing Chit-H.

The TEM images also show two different encapsulation types, of the vegetable oils into the chitosan, depending on the MW of the chitosan used for the shell solution: The LA and LC samples (Figure 2c,d), with low-MW chitosan, had a particle morphology whereby isolated oil beads were encapsulated by chitosan; whereas the HA and HC samples (Figure 2a,b), with high-MW chitosan, had oil encapsulated as scattered beads along the main chitosan fiber.

The beads-into-fiber structure of the HA and HC samples can be explained by the different molecular structure and viscosities of the shell and core solutions used in the coaxial system, that is, a highly viscous ($>400 \text{ mPa}\cdot\text{s}$) electrospinnable macromolecular (Chit-H) shell solution and a sprayable oil core solution with very low viscosity ($1\text{--}2 \text{ mPa}\cdot\text{s}$). It is known that the similarity between the rheological properties of the core and shell solutions control the viscous dragging exerted by the

shell solution on the core solution [35]. If the viscosity of the core solution is too low, compared with the shell solution, the viscous drag exerted by the shell solution is unable to overcome the cohesive forces of the core solution [36]. This was the case for the solutions used for the HA and HC samples. The entanglements provided by the highly viscous shell Chit-H solution were enough to prevent fiber rupture, which can be caused by low viscosity of the core oil solution, but, due to the low viscosity, the core oil solution was unable to follow the stretching of the macromolecular shell solution [37], thus taking the form of beads into the chitosan fibers [38]. It can also be observed that the HA and HC samples had a similar fiber diameter (10–20 nm), which supports the assertion that the HA and HC fibers were mostly made of Chit-H and the oil was encapsulated into the beads along the fibers. Similar morphologies, with beads-into-fiber structures, were obtained by other authors for proteins [39] or dexamethasone [40] encapsulated along the polymeric nanofibers as beads, which can act as depots for sustained drug release [40]. Other authors reported that coaxial electrospinning employed to encapsulate sunflower oil into PEO produced beaded fibers, with the oil encapsulated into the beads [36]. The authors also reported that the oil was confined or encapsulated solely inside these beads [36]. This is in good agreement with our findings, that is, the fibers contained mainly chitosan and the oil was distributed as beads along the main chitosan fiber.

From the TEM images, another observation can be made regarding the morphology of the HA and HC samples: The beads distributed along the Chit-H fibers were much more elongated for the HA sample (Figure 2a) compared with the HC sample (Figure 2b). Because a higher viscosity of the core fluid increases the viscous drag, exerted by the shell solution onto the low molecular core fluid [36], the more elongated argan oil beads can be explained by the higher viscosity of the argan oil compared with the clove oil. Considering the rapid evaporation of the solvent during the jet stretching [41], it is more relevant to compare the viscosities of pure oils instead of the oil solutions. In our case, argan oil was ten times more viscous (~0.6 poise [42]) than the clove oil (~0.06 poise [43]), which explains the more elongated argan oil beads.

3.2. Atomic Force Microscopy (AFM) Results

The particle and fiber diameters evaluated from AFM images (Figure 3) are all in the nanometer scale with similar values as those revealed by TEM images (Table 2).

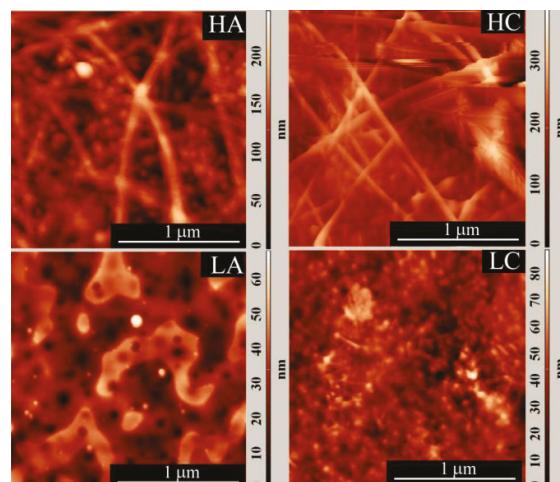


Figure 3. Atomic force microscopy (AFM) images of the studied samples: (a) HA; (b) HC; (c) LA; and (d) LC samples.

Table 2. Low and high values (range) of the particle and fiber diameter and height distributions evaluated from AFM images.

Sample	Range of the Particle Diameter Distribution (nm)	Range of the Fiber Diameter Distribution (nm)	Range of the AFM Height Distribution (nm)
HA	20–140	20–140	150–500
HC	10–80	30–140	150–600
LA	10–60	-	10–55
LC	20–80	-	10–80

It is interesting to compare the width (range) of the particle and fiber diameter distributions, determined from the AFM images, with the width of the AFM height distribution (Table 2, Figures 4 and 5). The width of the AFM height distribution was similar to the width of the particle AFM diameter distributions for the LA and LC samples, but was much wider than the particle and fiber diameter distributions for the HA and HC samples.

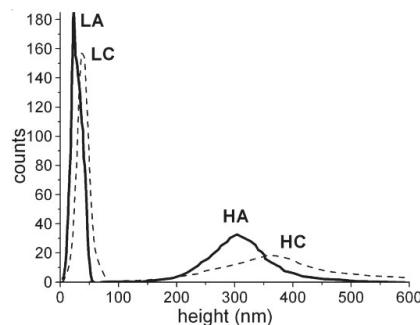


Figure 4. AFM height distributions for the studied samples: (a) HA; (b) HC; (c) LA; and (d) LC samples.

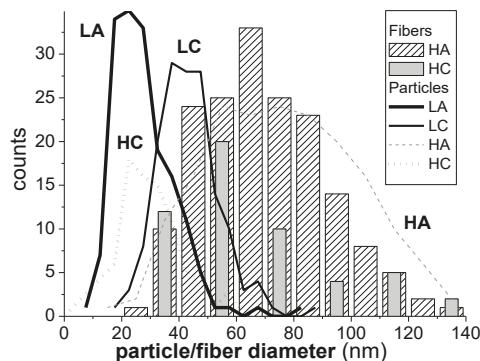


Figure 5. Distributions of the particle (lines) and fiber (bars) diameters, in the coated layers, determined from AFM.

This is because, compared with the HA and HC samples, the LA and LC samples had a more compact particle arrangement, with smaller voids between them, which narrowed the height distribution. This was also shown by other authors [44,45], who correlated the roughness (or the width of the height distribution) of nanoparticle layers with the experimentally measured nanoparticle

sizes, and also with the way the particles are packed [44]. For a closely (or orderly) packed spherical structure, with spheres tangent to one another (particle-near-particle), the roughness is low and the AFM height distribution approaches the particle diameter distribution (roughness approaches the average diameter of the particles). But when the same particles are randomly packed in a more porous arrangement, the roughness increases [45]. Thus, it can be concluded that, for the LA and LC samples, the structures were more compact with lower porosity (smaller voids between particles) and, consequently, with narrower height distribution than the HA and HC samples.

3.3. Scanning Electron Microscopy (SEM) Results

The SEM images for the HC-NATIVIA coated sample show the presence of nanofibers with diameters around 60–70 nm (Figure 6a). In contrast with the NATIVIA® PLA commercial foils, the hot-pressed PLA films experienced sample damage due to high electron acceleration during the SEM analysis, which lowered the resolution of the SEM images. Based on the presence of nitrogen, the SEM-EDX analysis was used to investigate the presence of chitosan on the PLA substrate. The mapping of nitrogen distribution, with an average nitrogen content of 5–6%, revealed a uniform coating on the surface at a micrometric scale.

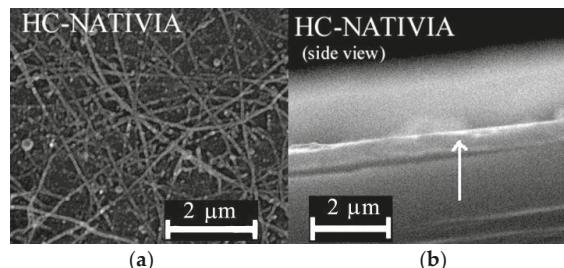


Figure 6. Scanning electron microscopy (SEM) images of the HC-NATIVIA sample: (a) Morphology of the coated surface; and (b) side view showing the coated layer.

Because of their smooth and glossy finish, the PLA-NATIVIA® films were used to evidence the coated layer. The side view of the coated PLA-NATIVIA® foil (Figure 6b) shows the coating layer with a thickness of 100 ± 20 nm. Considering that the entire output of the electrospinning syringe was deposited onto the PLA-NATIVIA® foil ($10 \mu\text{g}/\text{cm}^2$), based on chitosan and oil density, we would need to have the coated layer at a thickness of around 250 nm for maximum compactness of the chitosan (with no porosity of the coated layer). These results, therefore, show that only a part of the syringe output was deposited onto the PLA substrate (about $4 \mu\text{g}/\text{cm}^2$ assuming no porosity of the chitosan mesh). Considering porosity (void percent) of ~80% for the chitosan mesh [46], results suggest that the amount of the antimicrobial oil deposited onto the PLA substrate was at least $0.4 \mu\text{g}/\text{cm}^2$. For meat packaging applications, the contact between the antibacterial coated layer and the meat packaged is realized by means of the moist layer, which exists between the packaging foil and the meat. If we consider a moist layer with a thickness of approximately 1 mm is in contact with the meat, the oil concentration throughout the moist layer would be ~ $4 \mu\text{g}/\text{mL}$, which is well above the minimum inhibitory concentration of clove oil against *E. coli* (0.1 mg/mL) [47].

Therefore, nanostructured chitosan morphologies were obtained by electrospinning, with clove and argan oils encapsulated as beads into the chitosan nanofibers or nanoparticles. The nanofibres were predominant in the samples obtained from the electro-spinnable Chit-H. Nanoparticles were obtained when Chit-L was used.

3.4. Antibacterial Tests

The results of the antibacterial tests are presented in Table 3 (ISO 22196) and the Table 4 (ISO 16649-2/2007).

Table 3. Results of the antibacterial tests performed according to ISO 22196:2007 (E) (only the upper face was treated).

Sample	Log Reduction of the Number of Viable Bacterial Cells	
	<i>E. coli</i>	<i>S. aureus</i>
PLA Hot-Pressed		
PLA (uncoated)	invalid	-0.8
HC	invalid	0.8
HA	invalid	0.7
PLA-NATIVIA® NTSS 40 μm		
NATIVIA (uncoated)	1.1	-0.7
H-NATIVIA	1.8	0.8
HC-NATIVIA	2.2	1.2
HA-NATIVIA	0.8	0

Table 4. Results of the antibacterial tests performed according to ISO 16649-2/2007.

Sample	<i>Escherichia Coli</i>		<i>Listeria Monocytogenes</i>		<i>Salmonella Typhimurium</i>	
	24 h	48 h	24 h	48 h	24 h	48 h
Inhibition (%)						
PLA Hot-Pressed						
PLA -H	26	42	29	32	22	29
LA	43	70	49	54	37	49
LC	68	80	37	63	100	100
HA	50	77	60	100	51	78
HC	80	91	77	100	100	100
PLA NATIVIA® NTSS 40 μm¹						
H-NATIVIA	10	53	16	58	35	71
HA- NATIVIA	49	82	47	100	55	94
HC- NATIVIA	53	78	53	100	65	90

¹ As the antibacterial tests for the PLA hot-pressed samples evidenced the highest antimicrobial efficiency for the samples containing Chit-H, the commercial NATIVIA® foils were coated only with formulations containing Chit-H.

The results of the two antibacterial tests are presented as log reduction of the viable cells (first test—Table 3) and as inhibition percent (second test—Table 4). Regarding the efficiency of the coating procedure, it can be noted that there was higher antibacterial activity in the coated versus uncoated samples (Table 3), and also higher antibacterial activity on the chitosan–oil coatings versus chitosan coatings (Tables 3 and 4). Regarding the two types of chitosan and oils used for the coatings, the second antibacterial tests also showed higher antibacterial effect for Chit-H versus Chit-L, and for clove oil versus argan oil (Table 4).

More specifically, for both Chit-H–argan oil and Chit-H–clove oil combinations, the results obtained by the first test (Table 3) evidenced improved antibacterial activity of the coated PLA films compared with the uncoated films (for both NATIVIA and hot-pressed PLA films). Even the HA-NATIVIA sample (with 0 log reduction) had higher antibacterial activity against *S. aureus* (Table 3) compared with the uncoated NATIVIA film (with negative log reduction, i.e., cell proliferation). In the

case of *E. coli* bacteria, antibacterial effect was observed even for the uncoated NATIVIA films because of the decreased pH by the free lactic acid, which was present in the film (Table 3).

Also, both tests showed that the combination Chit-H–oil had higher antibacterial effect than Chit-H coated alone (Table 3 and 4) and, therefore, indicates that improved antibacterial activity could be obtained by coating the PLA films with chitosan. In addition, the coaxial encapsulation of the clove and argan oils, electrospun together with the chitosan, led to enhanced antimicrobial activity for both NATIVIA and hot-pressed PLA films.

The second antibacterial test also showed higher antibacterial effect for Chit-H versus Chit-L, and for clove oil versus argan oil (Table 4).

The different antibacterial activities of the two types of oils can be explained by the different amounts of the compounds responsible for the antimicrobial activity in the two oils (primarily phenolic compounds [48–50]). Eugenol, which increases antimicrobial and antifungal activity, is the main component (~80%) of clove oil. On the contrary, the phenolic compounds in argan oil are found in much lower amount (<1%), which explains the lower antibacterial and antifungal activity of argan oil compared with clove oil [51,52].

The higher antibacterial activity of Chit-H compared with Chit-L cannot be explained by its higher MW or by its lower deacetylation degree (DD) because many authors reported an opposite result (i.e., lower antibacterial activity for higher MW and lower DD), as it is shown further on.

Indeed, it is reported in literature that chitosan had lower antibacterial activity for higher MWs [53,54], for both gram-positive bacteria (GP-b) [55] and gram-negative bacteria (GN-b) [56]. This effect is reported to take place for MWs higher than 100 kDa [57], and some authors even report low activity for MWs > 30 kDa [58]. As the MW of the chitosan types used in this work was higher than this threshold (50–200 kDa for Chit-L and 300–370 kDa for Chit-H) [57,58], we conclude that the higher antibacterial activity of Chit-H (for the same type of oil) cannot be attributed to its higher MW.

Moreover, the different DD for the two types of chitosan cannot explain the higher antibacterial activity for the Chit-H (for the same type of oil). There are many papers reporting higher antibacterial activity for higher DD of chitosan [59–64], due to the disruption of the cell wall which is caused by the higher number of free amino groups present in chitosan with higher DD [65]. Our results, showing lower antibacterial activity for the chitosan with higher DD (DD ≈ 87% for Chit-L compared to DD ≈ 77% for Chit-H) are opposed to the reports presented above, and also to another report which showed higher antibacterial activity for chitosan with higher DD and lower MW [66].

The higher antibacterial activity of Chit-H compared with Chit-L can be explained by the larger surface area of the rougher nanoscaled morphology of the coating layer for Chit-H samples compared with the Chit-L samples (according to SEM, TEM and AFM results).

In other papers it was reported that the chitosan nanoparticles (MW of 680 kDa) exhibit higher antibacterial activity against *E. coli* than the corresponding microparticles obtained from the same chitosan [56], because of the higher surface charge [67] and the larger surface area of the nanosized chitosan nanoparticles, which probably tightly adsorbed onto the bacteria cells surface, disrupting the normal functions of the membrane [56].

There are also studies showing that the bacterial attachment decreases when the exposed substrate surfaces (such as polydopamine [68]) have higher roughness [69,70], for both gram-positive bacteria (GP-b) and gram-negative bacteria (GN-b) [71]. Some authors have found that GP-b (which has a more rigid membrane than GN-b) are more sensitive to roughness than GN-b, due to the surface nano-irregularities, which limit the number of anchoring points for GP-b bacteria. In this way, the surface area in contact with the membrane is reduced, which in turn reduces the adhesion of GP-b to the rougher surface [72,73]. Additionally, it was hypothesized that air entrapped by the topographical features inhibited contact between *S. aureus* and the substrate [74]. Our results agree with these reports. Furthermore, among Chit-H samples, the GP-b *L. monocytogenes* (for the samples HA, HA-NATIVIA, and HC-NATIVIA after 48 h) had maximum inhibition. This confirms the above-mentioned results,

which state that the GP-b are more sensitive to roughness, and make us conclude that the higher antibacterial activity of the Chit-H samples was attributed to the higher roughness of the coating.

3.5. Antioxidant Activity

It is known that it is advisable to perform the antioxidant tests with fresh DPPH solutions. However, if prolonged experiments are required (as are further presented in this section), the DPPH test can also be performed with solutions prepared tens of hours before testing without a substantial reduction in the activity of DPPH [75]. In order to test the stability of our DPPH solution, the absorbance of the DPPH (control) solution was measured over time. After 70 h (solution stored in the dark) the absorbance of the DPPH solution was about 80% of the initial value (with an almost linear decrease). This result is in line with other experimental results of other authors, which show that, after 24 h post preparation, the free radical activity of 0.1 mM DPPH methanolic solution was still very similar to that of the fresh preparation (about 20% activity was lost after about 120 h) [75].

It has been previously shown that it is possible to evaluate the antioxidant capacity of various compounds without preliminary solvent extraction. The reaction between the radical and the antioxidant occurs at the interface, when they come into contact, or by liquid diffusing into the interior of the reacting solid [76,77]. Using this method, it was possible to measure the antioxidant activity of solid matrices containing polyphenols [78], which are known to be found in argan [79] and clove oils [80]. In our study a similar approach was used: A small area of the coated films was cut into pieces and immersed into the methanolic DPPH radical solution. The antioxidant activity of the coated films was expressed by the relative decrease in DPPH absorbance at 517 nm:

$$\text{Relative Scavenging Activity (RSA)} = 1 - A_{\text{SAMPLE}(t)} / A_{\text{DPPH}(t)} \quad (1)$$

In order to eliminate the effect of decreasing DPPH absorption over time, the control was considered the absorbance of the control DPPH solution at the time of spectrophotometric analysis ($A_{\text{DPPH}(t)}$).

In the first test, a 1 cm^2 area, from the HC-NATIVIA and HA-NATIVIA freshly coated films, was cut into pieces and immersed for 24 h in 1.5 mL of DPPH solution in methanol (8 $\mu\text{g/mL}$). This first test evidenced the higher antioxidant activity of the samples containing clove oil. The RSA values were 0.29 for the HC-NATIVIA sample and 0.17 for the HA-NATIVIA sample. These results were in good agreement with the higher phenolic content in clove essential oil compared with argan oil. Due to high eugenol content, the concentration required to scavenge 50% of 2,2'-azino-bis 3-ethylbenzthiazoline-6-sulfonic acid (ABTS) free radicals (half inhibitory concentration) was much higher for argan oil (~5800 $\mu\text{g/mL}$) compared with clove oil (~8 $\mu\text{g/mL}$) [81]. At the same time, taking into consideration the low volatility and diffusivity of the components of argan oil (fatty acids), a very low antioxidant and antimicrobial activity of argan oil was expected.

In a second test, the sample with higher antioxidant activity (HC-NATIVIA) was chosen to measure the antioxidant activity over the immersion time. Before testing, the samples were stored for seven days at room temperature, in order to check the encapsulation and persistency of the volatile clove oil in the samples. The results were compared with the corresponding uncoated (NATIVIA) and chitosan coated film (H-NATIVIA). In this second test, a higher film area (4 cm^2) was cut and immersed into the same amount of radical solution with the same concentration. It can be observed that all the three samples had antioxidant activity (Figure 7) that was maintained over a fairly long time (tens of immersion hours) as a result of the clove oil encapsulation into the chitosan fibers. The concentration of biphenyl radicals continued to decrease (RSA increased) in the solution containing the immersed film relative to the control sample, even after 70 h of immersion. The antioxidant activity of the uncoated NATIVIA, which was lowest among the tested samples, was due to the residual lactic acid in the films.

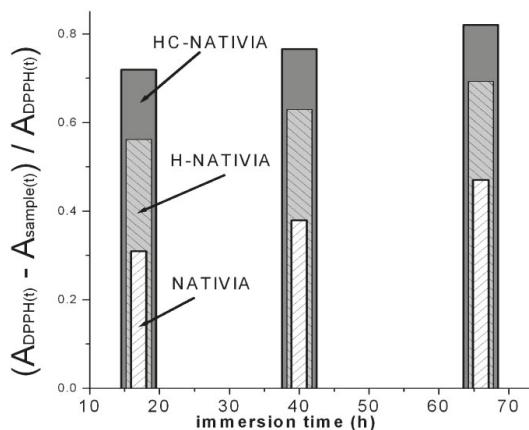


Figure 7. Antioxidant activity versus immersion time for the NATIVIA® films coated with Chit-H–clove oil (HC-NATIVIA), Chit-H (H-NATIVIA), and the uncoated film (NATIVIA).

Of these three samples, PLA-NATIVIA® films (HC-NATIVIA) coated with chitosan–clove oil had the highest antioxidant activity. In spite of the high volatility of the clove oil [81,82], the antioxidant activity of the HC-NATIVIA was maintained even after seven days of shelf storage. This shows that clove oil can be efficiently immobilized into the coating layer by encapsulation in chitosan. Therefore, the antioxidant tests confirmed the TEM results and the presence of the encapsulated clove oil into the chitosan fibers, which results in a combined effect obtained by simultaneous use of chitosan and clove oil.

4. Conclusions

The novelty of this study lies in providing a new and effective approach of nanocoating polymeric films with chitosan by coaxial electrospinning, with the advantage of simultaneous encapsulation of active vegetable and/or essential oils into the chitosan.

Polylactic acid (PLA) films were coated by coaxial electrospinning with formulations containing essential or vegetable oils (clove and argan oils, respectively) and encapsulated into chitosan in order to obtain biodegradable packaging materials with antimicrobial and antioxidant properties. When chitosan with high MW (Chit-H) was used, the coaxial electrospinning produced beaded chitosan nanofibers, with the oil distributed and encapsulated along the main chitosan fiber. Chitosan nanoparticles encapsulating the oil were obtained with low-MW chitosan (Chit-L). The roughness of the coating layer was higher for the samples prepared with Chit-H compared with samples prepared with Chit-L. The PLA films coated with chitosan–oil formulations had higher antibacterial activity than the films coated only with chitosan. The clove oil had higher antibacterial activity than the argan oil, for both types of chitosan, because of its higher phenolic content. Chit-H samples had higher antibacterial activity compared with Chit-L, for both types of oil, due to the higher specific surface area of the rougher nanofibrous morphology of the coating layer. As was expected, due to the phenolic content of clove oil, the chitosan–clove oil combination had higher antioxidant activity compared to the simple chitosan coating. Considering the volatility of the clove oil, its immobilization into the coating layer can be realized by encapsulation in chitosan. The TEM results and the antioxidant tests also confirm the encapsulation of the oil into the chitosan.

Author Contributions: In this study, the concepts and designs of the experiments were supervised by B.S.M. The manuscript text and the analysis of results were performed by C.V., B.S.M., and J.T.R. The experimental results were examined by B.S.M., L.S., A.-L.V., G.E.H., C.V., G.M.P., M.S., and J.T.R. All authors read and approved the final manuscript.

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Article

Characterization of Active Edible Films based on Citral Essential Oil, Alginate and Pectin

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Abstract: Thermal, structural and physico-chemical properties of different composite edible films based on alginate and pectin with the addition of citral essential oil (citral EO) as an agent to improve barrier properties, were investigated. The obtained films were clear and transparent, with a yellow hue that increased with citral EO addition. All the films displayed good thermal stability up to 160 °C, with a slight improvement observed by increasing the amount of citral EO in the composites. Gas transmission rate (GTR) strongly depended on the polymer structure, gas type and temperature, with improvement in barrier performance for composite samples. Also, citral EO did not exert any weakening action on the tensile behavior. On the contrary, an increase of the elastic modulus and of the tensile strength was observed. Lastly, water contact angle measurements demonstrated the dependence of the film wettability on the content of citral EO.

Keywords: edible film; alginate film; pectin film; essential oil; barrier properties; mechanical properties

1. Introduction

Edible coatings and films belong to an environmental-friendly technology aimed at enhancing food safety, quality and handling properties by creating a biodegradable semi-permeable barrier protection to water vapor, oxygen and carbon dioxide coming from the external environment. Edible coating is a thin edible substance layer, applied in a liquid form directly on the surface of different food products, mainly fruits and vegetables [1–5]. Edible films are a thin layer obtained as a solid sheet, which can be applied as a wrapping on the food product. For fresh fruit and vegetables, the creation of a wrong moisture and gas atmosphere may lead to weight loss and respiration rate reductions, with a consequent acceleration of the senescence process and a worsening of the visual gloss of coated commodities. Several studies have identified the necessity to evaluate mechanical (flexibility, tension), thermal, optical (brightness, opacity), wettability and morphological properties of edible films, as it creates a modified atmosphere that influences the gas transfer and further becomes a barrier for aromatic compound transferring [6,7]. The above-mentioned characteristics depend on several parameters related to the coating and film composition, such as preparation conditions (solvent, pH, components concentration, temperature) and type of added additives (cross-linking agents, antimicrobials, plasticizers, emulsifiers).

Recently, further potential applications were studied in order to formulate edible coatings and films with special functionalities [8]. They could be used as carriers of antioxidants, flavoring and/or coloring agents and antimicrobials to improve food safety and quality [9,10].

Edible coating and film formulations require several components. At least one of them needs to have structural properties. Between the different compounds that could be used in the formulation, alginate and pectin have been widely investigated [1]. They are hydrocolloid compounds coming from respectively seaweed extracts (brown algae) and plant tissue. Both belong to the polyuranoates group and are natural ionic polysaccharides giving rise to a chain–chain association and forming hydrogels. In order to design new films with improved and selective mechanical and barrier properties, it is important to understand their compatibility [1,11,12]. Further, essential oils represent a very interesting ingredient for edible film formulation with the purpose of realizing active and natural packaging materials [13,14]. Due to their natural origin and special functionality (antioxidant/antimicrobial) they could be selected to extend food shelf-life and add value to the product. However, the introduction of edible films for food packaging application may affect several properties such as optical, tensile, permeability and so on [15]. This, in turn, could influence the consumer acceptability. Citral EO was selected since it has been proved to have a positive effect against food spoilage microorganisms, as described by Guerreiro et al. [16].

The objective of this study was to investigate the final properties of edible films based on sodium alginate (SA) and pectin (Pe), with the addition of citral essential oil (citral EO).

The optimization of an edible film composition is one of the most important steps [17,18], as it must be formulated in order to maintain or increase the quality of fruit and vegetables. In this framework, physico-chemical and structural analyses have been performed on the prepared formulations to evaluate the properties of interest for the in-use application.

2. Materials and Methods

2.1. Materials

Citral essential oil, sodium alginate, glycerol ($\geq 99.5\%$), Tween®20 and Pectin from citrus peel (Galacturonic acid $\geq 74.0\%$) were purchased all from Sigma-Aldrich (Darmstadt, Germany, Europe) and used as received.

2.2. Film Preparation

Edible films were prepared using the solution casting method. Three different compositions were tested: 2% (w/w) of SA, 2% (w/w) of Pe and a combination of 1% (w/w) sodium alginate and 1% (w/w) pectin (SA + Pe). 1.5% (w/w) of glycerol and 0.2% (w/w) of Tween® 20 were added to each solution, which was subsequently dissolved in distilled water. Moreover, different amounts (0, 0.15, 0.3% w/w) of citral essential oil (citral EO) as antimicrobial agent were introduced in the formulation and homogeneously dispersed. In total, nine different films were obtained, as reported in Table 1.

Table 1. Concentration (w/w %) of the components in the film forming solutions.

Sample	Sodium Alginate	Pectin	Glycerol	Tween® 20	Citral EO
SA	2	-	1.5	0.2	-
SA _{0.15}	2	-	1.5	0.2	0.15
SA _{0.3}	2	-	1.5	0.2	0.3
Pe	-	2	1.5	0.2	-
Pe _{0.15}	-	2	1.5	0.2	0.15
Pe _{0.3}	-	2	1.5	0.2	0.3
SA + Pe	1	1	1.5	0.2	-
SA + Pe _{0.15}	1	1	1.5	0.2	0.15
SA + Pe _{0.3}	1	1	1.5	0.2	0.3

All solutions were heated at 70 °C for 30 min under conditions of stirring (until complete dissolution) and homogenized at 5000 rpm for 2 min. Afterwards, about 27 g of solution was used to obtain 1 g of soluble solids in petri dishes (\varnothing 90 mm). Air bubbles were removed by placing the film forming solution under vacuum (60 mbar, 15 min). Films were dried at 40 °C for 5 h to ensure a complete solvent removal, and then stored at room temperature in a desiccator before characterization.

2.3. Film Thickness and Gas Barrier Properties

Film thickness was measured by using a Sample Thickness Tester DM-G, consisting of a digital indicator (MarCator 1086 type, Mahr GmbH, Esslingen, Germany) connected to a PC. The reading was made twice per second measuring a minimum, a maximum and an average value, with a resolution of 0.001 mm. The reported results represent the mean thickness value of three experimental tests run in 10 different positions of each film at room temperature.

The determination of the gas barrier properties was performed by a manometric method using a Permeance Testing Device, type GDP-C (Brugger Feinmechanik GmbH, Munchen, Germany), in accordance with the ASTM 1434, DIN 53536, ISO 15105-1 and with the Gas Permeability Testing Manual-2008. The equipment consisted of an upper and a lower chamber, as previously described [19]. The film sample, of approximately 3 cm \times 3 cm in size, was placed between the two chambers. A film mask was used to cover the remaining section of the permeation chamber. The top chamber was filled with the dry test gases at ambient pressure. The gas permeation was determined by evaluating the pressure increase in the bottom chamber, which had been previously evacuated. Ambient temperature fluctuations during the test were controlled by an automatic temperature compensation software, which minimizes gas transmission rate (GTR) temperature deviations. The following conditions were adopted: gas stream of 100 cm³/min, pure food grade gases with 0% RH, active sample area of 0.785 cm². *Method A* (with evacuation of top and bottom permeation chamber) was employed in the analysis, as reported in the Gas Permeability Testing Manual (2008).

In order to determine the activation energies of the permeation process, the films were tested at three different temperatures (8, 15 and 23 °C), in the same operating conditions as reported above. Chamber and sample temperature were kept constant by an external thermostat HAAKE-Circulator DC10-K15 type (Thermo Fischer Scientific, Waltham, MA, USA). All experiments were done in triplicate and the results are presented as mean values.

2.4. Mechanical Properties

Tensile testing was performed by using a Zwick Roell Texture machine mod. Z2.5 (Ulm, Germany), equipped with a rubber grip and a 500 N load cell. A pre-load of 1MPa with a pre-load speed of 5 mm/min was applied. Stress-strain measurements were performed on rectangular films (5 mm width and 50 mm length) with an initial grip separation of 23 mm and a crosshead speed of 5 mm/min. Five different specimens were analyzed for each film and the results are provided as the average value \pm standard deviation. All measurements have been carried out in accordance with ASTM D882-09.

2.5. Thermo-Gravimetric Analysis (TGA)

Thermo-Gravimetric Analysis (TGA) was carried out under nitrogen atmosphere by means of a Perkin Elmer TGA7 apparatus (Perkin Elmer, Waltham, MA, USA). Gas flow of 30 mL/min and heating scan of 10 °C/min, over a temperature range 40–800 °C, were used for the analyses. Samples mass of 10 mg were used for the experiments.

2.6. Attenuated Total Reflectance Infrared Spectroscopy (ATR-IR) Analysis

Experimental ATR modified absorbance spectra were collected on a Perkin Elmer FTIR (Perkin Elmer 1725 \times Spectrophotometer, Labexchange Gropu, Burlandingen, Germany) over the range 650–4000 cm⁻¹, with a resolution of 4.0 cm⁻¹. The results are presented as an average of 10 experimental

tests, run on 10 different samples point. 64 scans were recorded on each sample. The experiments were performed at room temperature, without any preliminary samples' treatments.

2.7. Water Contact Angle Determination (WCA)

Static contact angle measurements were performed on edible films using a KSV CAM101 (KSV Instrument, Elsinki, Finland) instrument at ambient conditions, by recording the side profiles of deionized water drops ($4 \mu\text{L}$) deposited on the film surface. The measurement was taken 2 s after the drop deposition to ensure its stabilization, yet to minimize water absorption and evaporation. At least five drops were observed on different areas for each film (both on the top and on the bottom side), and contact angles were reported as the average value \pm standard deviation.

2.8. Color

The color of film samples was measured using a HunterLab ColorFlex EZ 45/0° color spectro-photometer (Hunterlab, Reston, VA, USA), with D65 illuminant, 10° observer, according to ASTM E308. The measurements were made using CIE Lab scale. The instrument was calibrated with a black and white tile ($L^* 93.47$, $a^* 0.83$, $b^* 1.33$) before the measurements. Results are expressed as L^* (luminosity), a^* (red/green) and b^* (yellow/blue) parameters.

The total color difference (ΔE) was calculated using the following equation:

$$\Delta E = [(L^* - L')^2 + (a^* - a')^2 + (b^* - b')^2]^{1/2} \quad (1)$$

where L^* , a^* and b^* are the color parameter values of the sample and L' , a' and b' are the color parameter values of the standard white plate used as the film background ($L' = 66.39$, $a' = -0.74$, $b' = 1.25$). The analyses were conducted in five repetitions. A mean value recorded for the top side and bottom side is reported.

2.9. Morphology Evaluation

The films' morphology was determined by using a Nikon upright microscope (Eclipse Ti-U, Nikon Co, Shanghai, Japan) with a standard light. Samples were observed in black and white and the images were recorded at a $20\times$ magnification.

2.10. Statistical Analysis

Significance of the different edible films effects was evaluated by means of one-way analysis of variance (ANOVA, 95% significance level) using the software STATISTICA 6.0 (Statsoft Inc., Tulsa, OK, USA).

3. Results and Discussions

In general, all films appeared homogeneous and transparent, without evident pores and crakes. It can be noticed that SA-based films were visually more transparent than Pe-based ones. Similar observations were made by Galus and Lenart [11] in their study on edible films based on sodium alginate and pectin. Visually, the addition of citral essential oil added a bright yellow color to the prepared films.

3.1. Thickness and Gas Barrier Properties

3.1.1. Thickness

Films thickness ranged from 94 to 127 μm as reported in Table 2, showing a slight variation of thickness within the different formulations, associated to the film casting technique. This is a crucial parameter for the calculation of mechanical and barrier properties. It depends on the film preparation method, on the flatness of the dish surface and on the film formation during the drying process. Despite the same volume of film forming solutions were used for the film casting, the drying

time for complete solvent evaporation increased with the citral EO concentration (anyway remaining in all cases within 5 h). The homogeneity of the films increased with the solvent evaporation time. Consequently, as reported in literature, the thickness tends to be lower in a well-organized and dense network [20]. Differences in the film structure may be attributed to the effect on the drying kinetics of the liquid film-forming dispersion thickness [21]. Several authors reported the effects of thickness on the permeability of edible matrix [22,23].

The thickness values have been used to calculate gas permeability and tensile properties.

3.1.2. Gas Barrier Properties

As it is well known, oxygen might cause food oxidation, which in turn influences various food properties such as odour, colour, flavour and nutrient content [24,25]. The film ability to retard oxidation or degradation of the product is an important characteristic that affects the final product quality and food shelf-life. Therefore, gas barrier properties should be taken into due account. Furthermore, the incorporation of other compounds, such as essential oils, into the polymer matrix could contribute to the modification of their barrier behavior.

Gas transmission rate (GTR) strongly depends on the polymer structure, gas type and temperature. Edible films barrier properties were examined at three different temperatures [26,27]: 8 °C (home and supermarket refrigerated storage temperature), 15 °C (abusing temperature) and 23 °C (room temperature). As reported by Marklinder and Eriksson [27], a typical recommended storage temperature for perishable food items should not exceed 8 °C, with the exception for minced meat that should be stored at 4 °C maximum. Further, in almost all the refrigerators the temperature ranges between 5–8 °C, but it is not uncommon that in certain zones of the refrigerators the temperature increases to values higher than 12 °C.

Data recorded with 100% pure food grade O₂ and CO₂ are reported in Table 2.

The matrix composition influenced the diffusion of the gas molecules through the polymer, resulting in a substantial variation of the gas transmission. Citral EO caused a modification of the barrier performances, correlated to the compatibility between alginate and pectin, ultimately resulting in effective gas molecule permeation through the films. The impact of lipid addition on the microstructure of the coating films is a determining factor in barrier efficiency. The microstructure of the films is affected by the physical state of the essential oil and its distribution in the polymer matrix. The liquid state of citral EO could favor molecular mobility, promoting the transport of gas molecules through the films. In turn, its distribution is another important factor. The more homogeneous is the distribution, the lower is the GTR. Antarés and Chiralt [28] reported that the addition of essential oil causes an increase of the oxygen permeability due to its hydrophobic character. However, a different trend can be described for the materials object of the present study. Indeed, a GTR decrease, particularly evident at lower temperatures, has been observed. The data here presented are well in accordance with the results reported by Rojas-Graü and coworkers [8]. They observed that the introduction of antimicrobials agents (oregano, carvacrol and lemongrass oil) did not affect the oxygen permeability of the films, while a slight decrease was observed by adding citral EO to alginate-based edible films.

It must be considered that the film barrier behavior at 8 °C is the most crucial for food packaging applications, as it corresponds to home and commercial (supermarket) storage conditions. At this temperature the gas transmission rate of O₂ and CO₂ is very similar: CO₂ permeates maximum 1.4 times faster than O₂, as it can be seen from the perm-selectivity ratio reported in Table 2.

Table 2. Film thickness, O₂ and CO₂ gas transmission rate (GTR) at 8, 15 and 23 °C, with the corresponding perm-selectivity ratio and GTR Activation Energy.

Sample	Thickness (μm)	O ₂ -GTR (cm ³ /m ² d bar)			CO ₂ -GTR (cm ³ /m ² d bar)			CO ₂ /O ₂			CO ₂ E _{GTR} (J/mol K)		O ₂ E _{GTR} (J/mol K)	
		8 °C	15 °C	23 °C	8 °C	15 °C	23 °C	8 °C	15 °C	23 °C	a	b	c	
SA	127 ± 13 ^a	102 ± 1 ^a	118 ± 1 ^b	148 ± 2 ^c	110 ± 0 ^c	111 ± 1 ^d	222 ± 1 ^a	1.1	0.9	1.5	33 (0.8)	17 (1)		
SA_{0.15}	111 ± 6	94 ± 1 ^c	112 ± 2 ^{de}	134 ± 1 ^d	99 ± 2 ^d	96 ± 1 ^f	105 ± 1 ⁱ	1.1	0.7	0.8	3 (0.4)	16 (1)		
SA_{0.30}	110 ± 4 ^b	70 ± 1 ^f	92 ± 1 ^f	110 ± 0 ^g	99 ± 1 ^d	129 ± 1 ^b	124 ± 2 ^h	1.4	1.4	1.1	10 (0.6)	21 (1)		
Pe	110 ± 5 ^b	102 ± 1 ^a	123 ± 1 ^a	159 ± 1 ^b	134 ± 2 ^a	144 ± 2 ^a	195 ± 1 ^b	1.3	1.2	1.2	-16 (0.6)	20 (1)		
Pe_{0.15}	107 ± 1 ^{bc}	99 ± 2 ^{ab}	109 ± 1 ^e	119 ± 1 ^f	97 ± 1 ^d	101 ± 1 ^e	176 ± 1 ^d	1.0	0.9	1.6	28 (0.8)	8 (1)		
Pe_{0.30}	94 ± 9 ^c	84 ± 2 ^d	117 ± 1 ^{bc}	127 ± 0 ^e	66 ± 2 ^g	110 ± 1 ^d	180 ± 1 ^c	0.8	0.9	1.4	46 (1)	19 (1)		
SA + Pe	101 ± 3 ^{bc}	98 ± 1 ^b	117 ± 1 ^{bc}	166 ± 1 ^a	131 ± 1 ^b	117 ± 1 ^c	173 ± 1 ^e	1.3	1.0	1.0	13 (0.5)	24 (1)		
SA + Pe_{0.15}	104 ± 1 ^{bc}	75 ± 1 ^e	114 ± 4 ^{cd}	136 ± 1 ^d	94 ± 1 ^e	116 ± 2 ^c	165 ± 1 ^f	1.3	1.0	1.2	26 (1)	27 (0.9)		
SA + Pe_{0.30}	104 ± 5 ^{bc}	84 ± 1 ^d	117 ± 1 ^e	94 ± 3 ^f	92 ± 1 ^f	116 ± 1 ^c	150 ± 1 ^g	1.1	1.2	1.3	23 (1)	44 (0.9)		

Values with different letters within the same column differ significantly at $p < 0.05$ levels. Values in brackets indicate the R² parameter of the fitting curve. Samples with *a* present the highest value, while samples with *d* the lowest.

As reported in the literature [29], for non-condensable gases the perm-selectivity ratio is relatively constant and is not correlated to the polymer chemical structure. Moreover, CO_2 transmission across the matrix is in general about six times faster than O_2 ones.

Furthermore, the perm-selectivity ratio changes with the temperature, i.e., it usually increases as the temperature decreases. On the contrary, our study evidenced a different trend, as the permselectivity remained almost constant in all cases.

The Arrhenius model was used to describe the permeation dependence on the temperature and to calculate the activation energy of the gas transmission (E_{GTR}) process. In Figure 1, natural logarithm (\ln) of GTR has been plotted as a function of the reciprocal of the absolute temperature ($1/T$).

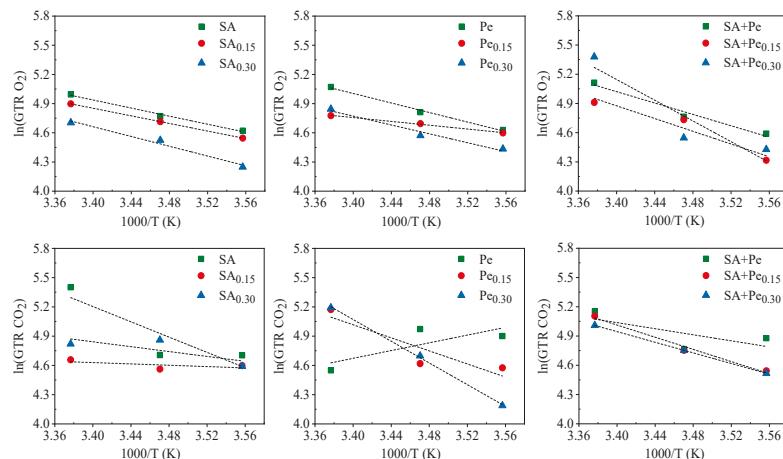


Figure 1. Arrhenius plot of O_2 and CO_2 GTR coefficient for SA, Pe and SA + Pe films.

Data reported in Table 2 well fit the theoretical relation (high R^2 value) in most cases, indicating a good correlation between permeability and temperature for both CO_2 and O_2 . As expected, the higher the temperature, the higher the permeability. In addition, E_{GTR} reflected the dependence of the barrier behavior from the temperature for each polymer matrix. The low activation energy demonstrated a low dependence of the gas transmission process on the temperature.

In conclusion, the GTR data here reported confirm the antioxidant action of citral EO, which is due to the promotion of oxygen barrier capacity, as already reported by Rojas-Graü et al. and Shahbazi [8–30]. The samples containing citral EO showed an interesting improvement of the gas barrier behavior, making them suitable as edible films for food more susceptible to oxidative degradation. As can be evicted from the data reported, the GTR value decreased when citral EO was added. The barrier properties improvement is responsible of the feasibility of formed films to meet the desired functionality for the product to be packed, as was reported also by Avila-Sosa et al. [31] in their study of chitosan and oregano essential oil, as well as their combination, for antimicrobial food packaging application.

3.2. Mechanical Properties

The tensile behavior of the films under study is reported in Table 3. Films were analyzed in terms of their elastic modulus (E), stress at yield (σ_y) and at break (σ_b), and elongation at yield (ϵ_y) and at break (ϵ_b). Generally speaking, the tensile properties of edible films and coatings are dependent on film constituents, relative proportion and preparation conditions [28].

Neat SA and Pe films showed very comparable tensile properties, although the elongation at break of SA was higher, while SA + Pe films displayed the lowest elastic modulus and stress at break and the highest elongation at break among the studied samples. The addition of citral EO caused

a significant change of the mechanical properties of all the formulations. A general increase of E, σ_y and σ_b can be observed, while no significant differences can be noticed for ε_b (Table 3). Also, the introduction of different amounts of citral EO did not influence the tensile behavior of the samples. In all the investigated samples, the yield phenomenon is visible.

Table 3. Mechanical data of SA, Pe and SA + Pe films.

Sample	E (MPa)	σ_y (MPa)	ε_y (%)	σ_b (MPa)	ε_b (%)
SA	526 ± 52 c	14 ± 1 d	4 ± 1 b	25 ± 3 cd	30 ± 1 b
SA _{0.15}	1102 ± 68 ab	24 ± 2 b	3 ± 1 b	44 ± 7 ab	24 ± 5 cd
SA _{0.30}	955 ± 74 b	17 ± 5 c	5 ± 2 b	31 ± 11 c	30 ± 3 b
Pe	492 ± 51 c	13 ± 1 de	4 ± 1 b	21 ± 2 cd	18 ± 2 e
Pe _{0.15}	1120 ± 112 ab	21 ± 2 bc	3 ± 1 b	42 ± 5 b	20 ± 1 de
Pe _{0.30}	1338 ± 115 a	32 ± 5 a	4 ± 1 b	54 ± 7 a	20 ± 2 de
Pe + SA	173 ± 17 d	11 ± 1 e	12 ± 1 a	18 ± 1 d	50 ± 1 a
Pe + SA _{0.15}	915 ± 109 b	19 ± 3 c	4 ± 1 b	31 ± 4 c	18 ± 2 e
PE + SA _{0.30}	1171 ± 98 ab	28 ± 3 a	4 ± 1 b	50 ± 6 ab	26 ± 2 bc

Values with different letters within the same column differ significantly at $p < 0.05$ levels. Samples with a present the highest value, while samples with d the lowest.

The effect of the essential oil addition on the mechanical properties of edible films is quite complex and conflicting results have been reported in the literature, since both enhancement and weakening of the tensile characteristics have been observed [28]. Specific interactions between the film constituents and the oil, such as crosslinks, different structural arrangements of the components or the formation of heterogeneous biphasic structures, must be taken into consideration [28].

Our study demonstrates that citral EO does not have any detrimental effect on the tensile properties of SA and Pe based formulations. On the contrary, an enhancement of the tensile strength and of the film rigidity has been obtained. The results indicate that not only the film microstructure was preserved, yet citral EO played a reinforcement role. Also, the introduction of a hydrophobic compound may have caused a reduction of the film water absorption, this latter acting as plasticizer and causing a decrease of E and σ_b in the neat films as compared to the composites.

In conclusion, the composite films, in particular those containing a higher amount of citral EO, displayed improved mechanical resistance with respect to the neat films, thus making them more suitable for food wrapping applications.

3.3. Thermogravimetric Analysis

Table 4 reports the thermogravimetric data of the materials under study, i.e., T_{onset} (the temperature at which the degradation starts), T_{max} (the temperature of the maximum degradation rate), and $m_{\text{res},600\text{ }^{\circ}\text{C}}$ (the residual mass at 600 °C).

Table 4. Thermogravimetric and wettability data of Sa, Pe and SA + Pe films.

Sample	T _{onset} (°C)	T _{max} (°C)	m _{res,600 °C} (%)	WCA (°)
SA	163 ± 1 e	220 ± 1 b	20 ± 1 de	44 ± 3 b
SA _{0.15}	172 ± 1 c	221 ± 1 ab	23 ± 0 b	45 ± 3 ab
SA _{0.30}	178 ± 1 ab	221 ± 0 ab	24 ± 0 a	49 ± 4 a
Pe	171 ± 1 c	218 ± 1 c	17 ± 1 f	35 ± 4 d
Pe _{0.15}	176 ± 3 b	222 ± 2 ab	21 ± 1 cd	38 ± 4 cd
Pe _{0.30}	179 ± 2 a	222 ± 1 a	20 ± 1 e	42 ± 2 bc
SA + Pe	163 ± 1 e	210 ± 1 d	18 ± 1 f	43 ± 3 bc
SA + Pe _{0.15}	166 ± 2 d	207 ± 1 e	22 ± 0 bc	46 ± 2 ab
SA + Pe _{0.30}	173 ± 2 c	213 ± 2 c	20 ± 1 de	48 ± 1 ab

Values with different letters within the same column differ significantly at $p < 0.05$ levels. Samples with a present the highest value, while samples with d the lowest.

The degradation patterns of the different films are very similar, although a slight improvement of the stability can be seen by increasing the amount of citral EO in the composites (Table 4).

Figure 2 reports the thermogravimetric curves of SA_{0.15}, Pe_{0.15} and SA + Pe_{0.15}, together with their derivative.

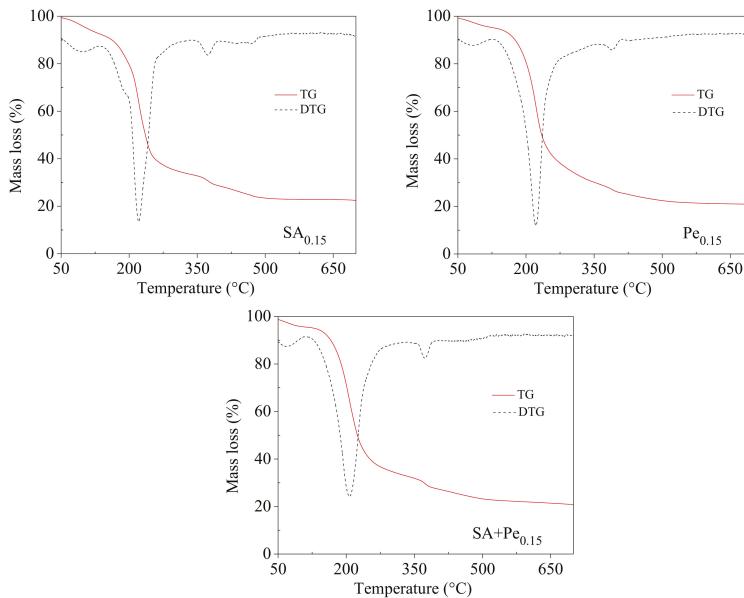


Figure 2. Thermogravimetric curves of SA_{0.15}, Pe_{0.15} and SA + Pe_{0.15} under N₂ flow.

Two main degradation steps can be outlined (Figure 2). The first one, which takes place below 160 °C, is due to film dehydration. The second step, which comprises two distinct peaks (as evidenced by the DTG curves), is related to the decomposition of the film components. In particular, the most evident mass loss (which reached the maximum in the range 210–220 °C), can be ascribed to the degradation of the polymer backbone.

3.4. Water Contact Angle (WCA) Measurements

Surface hydrophobicity is an important parameter to control the sensitivity of the films to water or moisture and it is usually evaluated by measuring the contact angle that forms between the film

surface and a water droplet [20,32]. Generally, higher contact angle values correspond to higher surface hydrophobicity, with higher surface water repellent ability. Figure 3 collects, as an example, the images of the water drops deposited on the film surface of SA_{0.15}, Pe_{0.15} and SA + Pe_{0.15}. Water contact angle measurements (Table 4) demonstrated the high wettability of the prepared films, due to the presence of a high amount of ether bonds and free hydroxyl-groups. In fact, WCAs were in all cases below 50°. The addition of citral EO caused a rise of the contact angle. In particular, the higher the content of citral EO, the higher the WCA, because of the hydrophobic nature of this latter. Therefore, the presence of citral EO plays a beneficial role in decreasing the wettability of the edible film, thus improving its protective action towards the wrapped food.

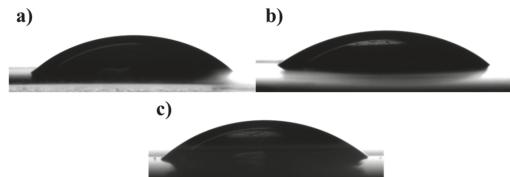


Figure 3. Water drops deposited on the film surface of: (a) SA_{0.15}; (b) Pe_{0.15}; (c) SA + Pe_{0.15}.

3.5. ATR-IR Analysis

The IR pattern of SA and Pe, as well as those of the composites, displayed some common and characteristic peaks (Figure S1). In particular, a broad and intense peak in the range 3270–3300 cm⁻¹ due to the stretching of the OH groups, a smaller peak of the CH stretching at 2920–2930 cm⁻¹, and an intense and sharp peak at 1015–1025 cm⁻¹ due to the C-O-C stretching of the glycosidic bonds linking two galacturonic sugar units were observed [33–35].

Some differences between the SA and Pe profile can also be highlighted. Indeed, the SA spectrum reveals the presence of two intense peaks at 1602 cm⁻¹ and 1408 cm⁻¹, respectively due to the COO-asymmetric and symmetric stretching vibration, and with a weak shoulder at 1298 due to the CO stretching. On the contrary, Pe showed its characteristic band at 1743 cm⁻¹, assigned to the stretching of the methyl esterified carboxyl groups [36]. The peak at 1607 cm⁻¹ (due to the COO- asymmetric stretching) was also clearly visible. The IR pattern of the composites presented the peaks of both SA and Pe.

The identification of the characteristics peaks allowed to confirm for all films the expected structure.

3.6. Color

In Table 5, L*, a*, b*, and total color difference (ΔE) values were reported for each sample.

Table 5. L*, a*, b* and total color difference (ΔE) of SA, Pe and SA + Pe films.

Sample	L*	a*	b*	ΔE
SA	86 ± 2 ^b	-1.56 ± 0.06 ^{de}	5.1 ± 0.4 ^e	9 ± 2 ^c
SA _{0.15}	87.4 ± 0.7 ^a	-1.69 ± 0.02 ^{efg}	6 ± 1 ^{de}	8 ± 1 ^c
SA _{0.30}	87.1 ± 0.3 ^a	-1.75 ± 0.02 ^{fg}	6.9 ± 0.6 ^d	8.5 ± 0.6 ^c
Pe	83.7 ± 0.7 ^c	-0.17 ± 0.03 ^a	10 ± 1 ^b	13 ± 1 ^{ab}
Pe _{0.15}	84.3 ± 1.3 ^c	-1.2 ± 0.2 ^b	13 ± 1 ^a	15 ± 2 ^a
Pe _{0.30}	87.9 ± 0.4 ^a	-1.62 ± 0.08 ^{def}	8 ± 2 ^{cd}	8 ± 2 ^c
SA + Pe	83.7 ± 0.8 ^c	-1.40 ± 0.04 ^c	7.9 ± 0.6 ^{cd}	11.8 ± 0.7 ^b
SA + Pe _{0.15}	85 ± 2 ^{bc}	-1.5 ± 0.2 ^{cd}	11 ± 2 ^a	13 ± 3 ^{ab}
SA + Pe _{0.30}	87.5 ± 0.8 ^a	-1.80 ± 0.03 ^g	8.9 ± 0.9 ^{bc}	10 ± 1 ^c

Values with different letters within the same column differ significantly at $p < 0.05$ levels. Samples with *a* present the highest value, while samples with *d* the lowest. L* (luminosity), a* (red/green index) and b* (yellow/blue index).

All the films were transparent. Since the color of edible films may affect the consumer acceptance, it is of primary importance that its transparency is preserved or that at least they display a color as close as possible to the natural pigment of foods on which the film is going to be applied [37]. SA based films showed slightly higher values of L* (luminosity) as compared with those composed of Pe and SA + Pe, in agreement with Galus and Lenart [11]. The addition of citral EO led to a general enhancement of L*. In particular, the increment was of the same entity in the SA samples containing different amounts of citral EO, while for Pe and SA + Pe films the L* values gradually increased with the increment of citral EO content. In terms of a* (red/green index) and b* (yellow/blue index) parameters, the samples containing Pe (both pure or in combination with SA) tended to a more yellowish color. In this case, 0.15 w/w of citral EO significantly enhanced ($p < 0.05$) the b* values. The obtained ΔE data ranged from 8 to 15. Pe-based samples showed the highest value, indicating a greater color variation, in agreement with the results reported by Galus and Lenart [11]. Samples displaying higher ΔE values (Pe, Pe_{0.15}, SA + Pe and SA + Pe_{0.15}) appeared also less transparent.

By citral EO addition, only a slight yellowish hue was recorded, making all those films suitable for food application.

3.7. Microstructure

As reported by Antarés and Chiralt [28], while conventional plastics are non-polar materials, edible films are usually hydrophilic. The incorporation of essential oil in the film forming dispersion is usually carried out by emulsification or homogenization of the aqueous solution containing the polymer. When the film is dried, droplets of lipid remain embedded into the polymer matrix, as observed by microscopy. The drying time plays an important role in determining the arrangement of the components during the film-forming step, thus the final microstructure of the edible films.

Morphological analysis of the films under study was carried out by optical microscopy (20× magnification), to evaluate the homogeneity and the structure of the prepared films. Figure 4 shows the surface micrographs of SA (a), Pe (c) and SA + Pe (e) films and of SA_{0.30}, Pe_{0.30} and SA + Pe_{0.30} (respectively (b), (d) and (f)).

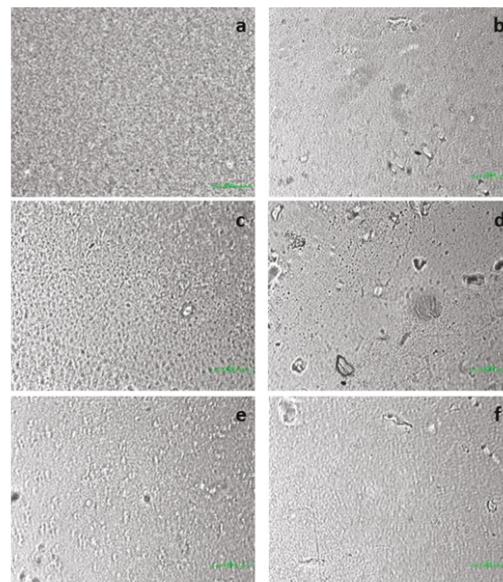


Figure 4. Surface micrographs of: (a) SA; (b) SA_{0.30}; (c) Pe; (d) Pe_{0.30}; (e) SA + Pe and (f) SA + Pe_{0.30} films.

SA films presented a more homogenous and uniform structure than Pe ones, in accordance with Bierhalz et al. [38], who performed the microstructural analysis on alginate and pectin based films with the addition of natamycin as antimicrobial agent. The addition of citral EO caused a mild change in the structure of all films. Furthermore, some agglomerates can be noticed, possibly indicating a non-uniform distribution of citral EO. The most irregular structure was observed in Pe-based films. The morphology of the films supported the tensile results, evidencing that a different structural arrangement of the components in the film forming dispersion significantly influences both mechanical and gas barrier properties.

4. Conclusions

Citral EO has been incorporated into edible films through emulsification. Film structural, physical, mechanical and barrier properties were evaluated. The combination of citral EO with SA and/or Pe gives continuous and transparent edible films. Samples with citral EO addition showed improved performances with respect to the neat ones. As compared to neat films, no substantial differences were observed in the visual appearance of the composite samples, with the exception of a slight yellowish hue. On the other hand, citral EO addition caused a different microstructure arrangement and some agglomerates. However, the film structure was not weakened as testified by the gas barrier and mechanical tests, rather a reinforcement role was exerted. Furthermore, by increasing the amount of citral EO, a slight increase of the thermal stability as well as of the surface hydrophobicity was recorded.

With the aim to extend the shelf-life of food, the addition of essential oils can provide edible films with antimicrobial properties, depending both on their nature and interaction with the polymer matrix. Further studies are necessary to optimize and verify the suitability of these natural films on food products. The oil type and its interaction with the matrix determine the effectiveness of the edible films as food packaging material. In order to understand the feasibility of edible films to improve the shelf-life of food products susceptible to oxidation or to microbial spoilage, a real food systems needs to be investigated, together with specific tests on antioxidant activity [39,40].

Supplementary Materials: The following are available online at <http://www.mdpi.com/1996-1944/11/10/1980/s1>, Figure S1: ATR-IR spectra of SA 0.15, Pe 0.15 and SA + Pe 0.15.

Author Contributions: V.S., S.R. and N.L. conceived of and designed the experiments; C.M., J.P.C. and U.T. prepared the edible films and performed microscopic examination and statistical analysis; V.S. performed the thickness determination, permeation analyses, mechanical analyses and color evaluation; M.G. and N.L. performed thermogravimetric analyses, infrared spectroscopy and water contact angle determination; all authors analyzed the data; V.S., S.R. and N.L. contributed to reagents/materials/analysis tools; V.S. wrote the paper with the fundamental contribution of all authors for the final revision, especially M.G.

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Article

Chitosan-Based Bionanocomposite Films Prepared by Emulsion Technique for Food Preservation

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Abstract: Biopolymer nanocomposite films were prepared by casting film-forming emulsions based on chitosan/Tween 80/rosehip seed oil and dispersed montmorillonite nanoclay C30B. The effect of composition on structural, morphological characteristics and, mechanical, barrier, antimicrobial and antioxidant properties was studied. The presence of rosehip seed oil in chitosan films led to the formation of flexible films with improved mechanical, gas and water vapour barrier properties and antioxidant activity. The *in vitro* antibacterial tests against *Escherichia coli*, *Salmonella typhimurium*, and *Bacillus cereus* showed that the chitosan/rosehip seed oil/montmorillonite nanoclay composites effectively inhibited all the three microorganisms.

Keywords: chitosan; rosehip seed oil; montmorillonite nanoclay; antibacterial; antioxidant

1. Introduction

The global food market has strict demands regarding food safety and quality. Nowadays, society lives in a continuously changing environment, which sometimes has an important impact on the food industry. Currently, consumers prefer foods with natural food additives because these are correlated with various health benefits. This phenomenon has increased interest in searching for natural compounds with bioactive properties to preserve the quality of different types of foods. Biopolymer films could be a viable solution for some of the problems arising from the use of traditional food plastic packaging materials (e.g., originating from fossil resources, limited ability for bioactive behavior, very low biodegradability). Biopolymers with film forming properties [1,2] are suitable materials for adding different additives, such as antioxidants [3], antifungal [4] or antimicrobial agents [5], etc. Specifically, several biopolymer materials such as cellulose, starch, alginate, chitosan or pectin have good film forming capacity. Additionally, using natural polymers as coatings can prolong the shelf life of foods by controlling water loss, oxidation, or color changes, but these natural polymers have poor water vapor barriers due to their high hydrophilic nature [6]. Many studies have been conducted on edible bio-based films to demonstrate their capacity to avoid oxygen penetration to the food material or water absorption by the food matrix, loss of flavor, and solute transports [7]. One of the most promising edible active films is the one based on chitosan because of its particular physicochemical properties. Chitosan is a modified, cationic, non-toxic carbohydrate polymer, obtained through chitin deacetylation and has a complex chemical structure formed by β -(1,4) glucosamine units as its main component (>80%) and N-acetyl glucosamine units (<20%), randomly distributed along the chain. It presents some important advantages over other matrices used as edible films packaging materials such as excellent biocompatibility and biodegradability, non-toxicity, good antimicrobial activity (against bacteria and fungi), oxygen impermeability and film forming properties [8–11]. Chitosan has been approved as a

food additive in some countries from Asia, like Japan (1983), Korea (1995) or China (2007). In Europe, chitosan is still not permitted as food contact material; although the European Food Safety Authority decided that chitosan is sufficiently well characterized [12]. There is a good opportunity of using chitosan-based materials as films and coatings since new regulation dealing with active and intelligent packaging was issued by the European Food Safety Authority (EFSA) [13]. The antimicrobial activity of chitosan is determined by its cationic nature. Therefore, the positively charged amino groups (NH_3^+) can interact with negatively charged microbial cell membranes of microorganisms. However, the antimicrobial effect against Gram-positive or Gram-negative bacteria was found to be questionable in many studies. In some reports it was found that chitosan generally has stronger effects on Gram-positive bacteria (*Listeria monocytogenes*, *Bacillus megaterium*, *Bacillus cereus*, *Staphylococcus aureus*) than on Gram-negative bacteria (*Escherichia coli*, *Salmonella typhimurium*, etc.) [14,15]. Due to the higher hydrophilicity in Gram-negative bacteria, it was demonstrated that this type of bacteria were most sensitive to chitosan [16]. Even though chitosan has good film forming properties, a selective permeability to gasses (CO_2 and O_2) and acceptable mechanical properties, the highly permeability to water vapor limits its use in contact with food. Accordingly, different methods have been used to improve the physical properties of biopolymer based films. For example, good results in increasing the hydrophobicity have been obtained by addition of neutral lipids, fatty acids, waxes, or clay [8].

Vegetable oils have received great attention from food scientists due to their antioxidant and antimicrobial activity. Rosehip seed oil can be obtained from wild roses (*Rosa moschata* L., *Rosa rubiginosa* L. or *Rosa canina* Herrm.) from Rosaceae family, bushes, which grow in various areas around the world. Rosehip seed oil has a subtle woody scent and color that can range from golden yellow to light orange. It has been found that rosehip seed oil is an important and inexpensive source of unsaturated fatty acids, the most abundant being linoleic (54.41–48.64%), followed by linolenic (17.14–18.41%) and oleic acid (14.71–18.42%) [17]. Rosehip seed oil also contains a variety of chemical compounds (mainly carotenoids, tocopherols, squalenes, phytosterols, phenolic compounds, fatty acids) which provide its antioxidant and antimicrobial activity [18]. Rosehip seed oil is becoming popular in cosmetic and other high valuable applications such as in the pharmaceutical industry, due to its antioxidant properties [19]. However, there are very few examples of the use of rosehip seed oil in the agro-food industry [19,20] or food packaging [21]. To confer superior antibacterial and antioxidant activities, barrier and mechanical properties to chitosan films various bioactive compounds and other additives have been incorporated in chitosan matrix by emulsion/casting method [22–26].

Hydrophilic (D-glucosamine) and hydrophobic parts (N-acetylated residues) in chitosan molecules offer to it the ability to form emulsion systems; therefore, it is used as emulsifier in the food industry, to uniformly stabilize oil droplets [22]. The emulsifying property of chitosan can be influenced by chitosan characteristics (e.g., molecular weight, degree of deacetylation) or by the type of oil used and concentration. It was found that chitosan with lower molecular weight was adsorbed more easily on the surface of the oil droplets than chitosan with higher molecular weight [23]. Rodriguez et al. [24] have studied the emulsification of sunflower oil by chitosan solution and found that the chitosan emulsifying capacity was proportional to chitosan concentration. Li and Xia also tried to understand the effects of molecular weight and degree of deacetylation on emulsifying properties of chitosan [25]. The conclusions of their study were that chitosan showed superior emulsifying activity and emulsifying stability within the range of 60.5–86.1% degree of deacetylation and that the chitosan with low molecular weight exhibited better emulsifying activity than that with high molecular weight. In the present study, a medium molecular weight chitosan with a deacetylation degree (DD) of 83.2% was selected. The vegetable oil will also act as a plasticizer for chitosan, increasing the flexibility of the final product, which is important when applying as wrapping on a food product [26]. However, the mechanical and water vapor barrier properties of polysaccharides-based films are, in general, poor. An alternative to improve these properties is the addition of layered silicates nanoparticles (e.g., sodium montmorillonite). Several studies found improvement in mechanical [26] and barrier properties [27] of chitosan films containing 1–5 wt% nanoclay.

Starting from these considerations, the objective of this research was to analyze the beneficial effect of the addition of rosehip oil to chitosan film properties intended to be used as food packages or edible films. With this aim, new bionanocomposites films based on chitosan, rosehip seed oil and montmorillonite nanoclay are obtained using a simple and original casting emulsion method. The bionanocomposites as films were investigated for their structural, morphological characteristics and, mechanical, barrier, antibacterial and antioxidant properties. All determined characteristics proved that these bionanocomposites are good potential materials for food industry.

2. Experimental

2.1. Materials

Chitosan medium molecular weight (CH) with 200–800 cP viscosity in 1% acetic acid, 75–85% deacetylation degree and $M_w = 190,000\text{--}300,000 \text{ g/mol}$, was provided and used as received from Sigma-Aldrich (Darmstadt, Germany).

Cold-pressed rosehip seed oil (RSO), was purchased from S.C Herbavit S.R.L, Oradea, Romania. It was obtained as a cold-pressed (high-pressure) oil of rosehip seeds in small batches. The fruits were collected from wild rose bushes of the common dog-rose (*Rosa canina* L., species belonging to the Rosa genus in the Rosaceae family) growing in Romania. According to the producer's specifications it has a high content of monounsaturated fatty acids: oleic (10–20%); essential polyunsaturated fatty acids: linoleic (35–50%) and linolenic (25–50%) and also palmitic and stearic acids. In this study, the rosehip seed oil was incorporated into chitosan film in a proportion of 0.75:1 (mL/g) RSO/chitosan. IC₅₀ of RSO was determined by DPPH (2,2-diphenyl-1-picrylhydrazyl) method (as described below) measuring the percentage radical inhibition vs. different oil concentrations in the range of 0.5–3.5 mg/mL. IC₅₀ represents the concentration of sample required to obtain a 50% radical inhibition. RSO shows a good antioxidant activity with an IC₅₀ as low as 2.3 mg/mL.

Polyoxyethylene sorbitan monooleate (Tween 80, T80), also known as Polysorbate 80 is a nonionic surfactant and emulsifier often used in foods and cosmetics, which is a viscous and water-soluble yellow liquid. Tween 80 with Mw of 1310 g/mol and more than 58% oleic acid content, obtained from Sigma-Aldrich, was added (0.125 g Tween 80/1 g chitosan) as an emulsifying agent to stabilize the hydrophobic oil droplets into aqueous chitosan solution—the resulting sample was noted as CHM.

MMT-MTEtOH Cloisite C30B (C30B) is an organoclay derived from montmorillonite by modification with methyl, tallow (~65% C18; ~30% C16; ~5% C14), bis-2-hydroxyethyl and quaternary ammonium and was selected to improve the mechanical properties of chitosan-based films. It was obtained from Southern Clay Products (Gonzales, TX, USA) and it has 75% clay content, a moisture content of <2%, density of 1.98 g/cm³, average particle size of 6 μm, basal spacing d₀₀₁ = 18.5 Å, and modifier concentration 90 meq/100g clay. It has two functional groups (hydroxyl groups and long alkyl chains linked with quaternary ammonium groups) [28] and it has been approved by the Food and Drug Administration (FDA) for use in contact with food.

2.2. Emulsion Preparation

Chitosan solutions (3%, w/v) were prepared by dispersing chitosan powder in acetic acid solution (5%, v/v) under magnetic stirring, at room temperature (23 ± 2 °C) for 72 h. To obtain the chitosan/rosehip seed oil (CHM/RSO) emulsion, 2 mL of rosehip seed oil and 0.375 g Tween 80 were added to the 85 mL chitosan solution (3%, w/v). The chitosan/rosehip seed oil/C30B (CHM/RSO/C30B) system was obtained by adding 0.09 g C30B to chitosan/rosehip seed oil/T80 mixture as described above. The obtained solutions were homogenized for 2 min with an ultrasonic processor UP50H (Hielscher—Ultrasound Technology, Teltow, Germany) using a power of 50 W at 30 kHz.

2.3. Film Preparation by Solvent Casting Method

The films were obtained by casting 50 mL of binary or ternary mixtures in glass Petri dishes (153 cm^2), drying first at $25\text{ }^\circ\text{C}$ in a forced-air oven for 24 h and then at $40\text{ }^\circ\text{C}$ in a vacuum oven. In all cases, films with relatively uniform thickness of $0.148\text{--}0.193\text{ mm}$ were obtained. Prior to analyses, the films were conditioned in desiccators for 2 days at $22\text{ }^\circ\text{C}$, over a saturated solution of NaBr (58% relative humidity). The schematic representation of the encapsulation of rosehip seed oil and C30B into the chitosan matrix by the emulsion/solvent casting method is presented in Figure 1. All the films were easily removed from the cast Petri dishes and showed smooth surfaces. As a reference sample, film obtained by casting the chitosan solution containing only Tween 80 (CHM) was used.

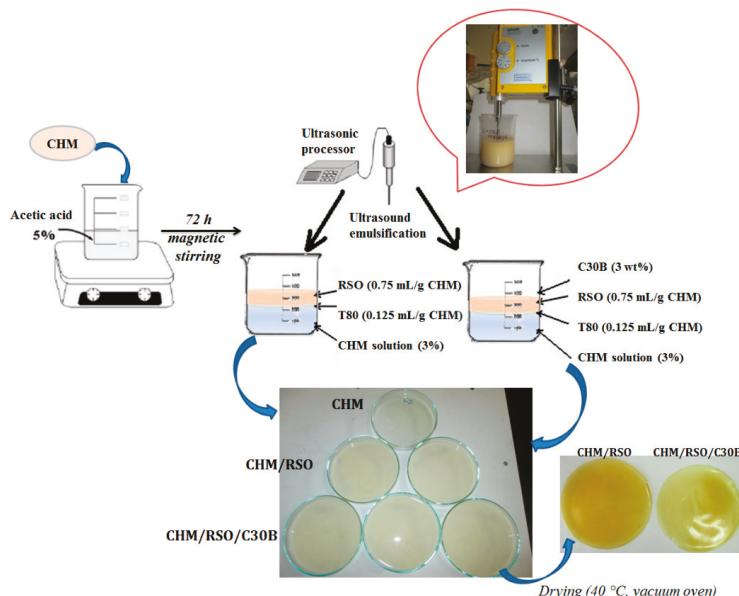


Figure 1. Schematic representation of the rosehip seed oil/C30B encapsulation into chitosan matrix by emulsion/solvent casting method.

2.4. Investigation Methods

2.4.1. Droplet Size Measurement and Zeta Potential Analysis

Using dynamic light scattering (DLS) technique the samples hydrodynamic radius was determined by a Zetasizer instrument (Nano ZS model, Malvern Instruments, UK), equipped with a red laser 633 nm He/Ne . The device uses technology that reduces the multiple scattering effects, which is based on a non-invasive back scatter (NIBS). The technology used is a non-invasive one, with the optics not being in contact with the sample, and backscattered light being detected. The Mie method was used during measurements over the whole recording range and comprised between 0.6 nm and $6\text{ }\mu\text{m}$. Samples were diluted in double distilled water, each analysis consisting of three replicates and each determination was analyzed twice. The apparent hydrodynamic diameter (D_H) of samples was determined using Equation (1):

$$D_H = \frac{kT}{3\pi\eta D}, \quad (1)$$

where D_H is the hydrodynamic diameter (nm), k —Boltzmann constant ($\text{J}\cdot\text{K}^{-1}$), T —temperature (K), η —viscosity ($\text{Pa}\cdot\text{s}$), D —the diffusion coefficient (m^2/s). The hydrodynamic diameter is related on the intensity means, and not a mass or number mean, being calculated from the signal intensity.

Zeta Potential (ξ) (in mV or V) was determined by using the Smoluchowski relationship:

$\xi = \eta\mu/\epsilon$, and $k\alpha >> 1$, where η —the medium viscosity ($\text{Pa}\cdot\text{s}$), μ —electrophoretic mobility (m^2/SV), ϵ —dielectric constant, k and α —Debye–Hückel parameter and particle radius.

2.4.2. ATR-FTIR Spectroscopy

The attenuated total reflection-Fourier transform infrared spectroscopy (ATR-FTIR) technique was used to determine the samples molecular structure. Using a Bruker VERTEX 70 spectrometer the background and samples spectra were recorded in absorbance mode in the 600 to 4000 cm^{-1} wavenumber range, at a 4 cm^{-1} resolution, by performing 64 scans and the ATR module being equipped with a 45° ZnSe crystal (penetration thickness is around 100 μm). The processing of spectra was achieved using OPUS and ORIGIN programs. For each sample, the evaluations were made on the average spectrum obtained from three recordings.

2.4.3. Scanning Electron Microscopy (SEM)

Scanning electron micrographs were obtained with a QUANTA 200 scanning electronic microscope (FEI Company, Hillsboro, OR, USA), at an accelerating voltage of 20 kV, which has an integrated EDX system, GENESIS XM 2i EDAX (FEI Company, Hillsboro, OR, USA) with a SUTW detector. The film surfaces were examined as such (without the metal coating), being recorded at different magnifications that are shown on the SEM images.

2.4.4. Mechanical Testing

Tensile tests were carried out by means of an Instron testing machine (model 3345) with a loading cell of 5 kN, according to EN ISO 527-2/2012. The tested samples of 1 mm thickness were conditioned at 23 °C and relative humidity of 50%. A loading speed of 10 mm/min and a 40 mm gauge length were used for mechanical testing. The following tensile properties were assessed: Young's modulus, tensile strength at the break and strain at break. For each measurement, five replicates were used and the average data are presented further.

2.4.5. Gas Permeability Tests

Oxygen and carbon dioxide permeability measurements were performed on triplicate samples using a manometric gas permeation tester (Lyssy L100-5000, Systech Illinois, Johnsburg, Illinois, USA), which uses the dynamic measuring principle based on pressure change due to gas transmission through films. The experimental tests were conducted at 23 °C, after the samples were conditioned for minimum 4 h. The area of tested film was 10 cm^2 . Oxygen and carbon dioxide permeability was obtained in $\text{mL}/(\text{m}^2 \cdot \text{day})$. The film separates the two compartments of the measuring chamber, the lower one being evacuated down to defined pressure while a continuous flow of gas (O_2 or CO_2) passes through the upper compartment. Closing the valve on the line to the vacuum pump, the pressure in the lower compartment increases due to migration through the film of the gas from the upper compartment. The instrument measures the time required for the increase of pressure within two pre-defined limits and, comparing with the values measured for a standard film, calculates the permeability of the tested film.

2.4.6. Dynamic Moisture Sorption

Dynamic water vapors sorption capacity for the samples was established using a fully mechanized instrument, named IGAsorp, a gravimetric analyzer manufactured by Hiden Analytical, (Warrington, UK). This device has a very sensitive microbalance able to determine the weight change as the relative

humidity is varied in the sample compartment, at a constant temperature. The measurements are totally adjusted by a special software. Initially, the samples were dried at 25 °C, in a nitrogen flow (250 mL/min) till their masses were kept constant at relative humidity (RH) <1%. After that, the RH was gradually raised from 0% to 90%, in 10% humidity periods, each one having a pre-determined equilibrium time between 40 and 60 min and the sorption equilibrium was realized for each step. Then, the RH was diminished, and sorption/desorption curves were recorded. Equilibrium moisture content (EMC) values represent the average of three different determinations.

2.4.7. Antibacterial Tests

For testing the bactericidal activity of chitosan emulsion films, three different food pathogenic bacteria including *Salmonella typhimurium* ATCC-14028, *Bacillus cereus* ATCC-14579 and *Escherichia coli* ATCC-25922 were used. ATCC cultures were presented in lyophilized form and were reconstituted following the rules set out specific standards: SR EN ISO 11133/2014—Microbiology of food, animal feed and water—Preparation, production, storage and performance testing of culture; ILAC G9/2005—Guidelines on the selection and use of reference materials; SR EN ISO 7218—A1/2014—Microbiology of food and animal feeding stuffs—General requirements and guidance for microbiological examinations—Amendment 1.

The reconstituted cultures were subcultured to obtain replicate reference stock cultures and the reference stock culture was further subcultured to obtain the working stock culture. From this working stock culture bacterial suspensions of 0.5 McF (McFarland units measured with a densitometer) were obtained, which were serially diluted in order to achieve concentrations of about 10^2 – 10^3 CFU/0.1 mL. These suspensions were used for testing antibacterial activity of the surface of the chitosan films obtained by emulsion method. Sterilization of the polymeric samples was made in an autoclave at 110 °C and 0.5 bars for 20 min. After sterilization, a certain volume of bacteria suspensions was added dropwise to the surface of each 1 × 1 cm² chitosan-based films placed on Petri dishes and thermostated at 37 °C. After 24 h and 48 h, using sterile tampons moistened in peptone water, the specimens from the test surfaces were collected and were seeded on the surface of specific culture media for each food pathogenic bacteria as: XLD (Xylose Lysine Desoxycholate agar) for *Salmonella typhimurium*; BACARA®(chromogenic media and method for the enumeration of *Bacillus cereus* in food products, *B. cereus* colonies turn pink-orange with an opaque halo); and VRBG (Violet Red Bile Glucose Agar) for *E. coli*. The Petri dishes with inoculated culture media were incubated at 37 °C, and after 24 h the specific colonies of each bacterial species were counted. Antibacterial inhibition was determined by the colonies counting method. Reduction in the number of CFU represented the antibacterial activity by comparison with sterile inert film used as control sample. Each experiment was realized in triplicate.

The following standardized methods of bacteriology procedures were used, according to standards in force:

- SR EN ISO 21528-2/2007, Microbiology of food and animal feeding stuffs—Horizontal methods for the detection and enumeration of Enterobacteriaceae—Part 2: Colony-count method—*E. coli*;
- SR EN ISO 7932/2005, Horizontal method for the enumeration of presumptive *B. cereus*—Colony-count technique at 30 °C;
- SR EN ISO 6579/2003/AC/2004/AC/2006, 2007, Horizontal method for detection of bacteria of the genus *Salmonella* spp;

2.4.8. DPPH Radical Scavenging Assay

The radical scavenging activity (RSA) of CHM/RSO and CHM/RSO/C30B films was measured using the 2,2-diphenyl-1-picrylhydrazyl (DPPH) radical. Free radical scavenging method is the simplest, inexpensive and widely used method to measure the ability of compounds to act as free radical scavengers or hydrogen donors, and to evaluate antioxidant activity of foods [29]. The DPPH is a stable free radical, which shows a strong absorption band at 517 nm. When the stable DPPH radical

accepts an electron from the antioxidant compound, the violet color of the DPPH radical is reduced to yellow colored diphenylpicrylhydrazine radical [30].

A total of 300 mg of each sample was used to perform the assay. This was placed in a vessel containing 10 mL of chloroform under continuous stirring for 24 h. From each mixture a 1.5 mL volume was extracted, which was mixed with 3 mL of ethanolic DPPH solution (1.5×10^{-4} mol/L). The control sample was obtained by mixing the same volume of chloroform with 3 mL of DPPH. The reaction mixtures were left to stand for 30 min at room temperature in the dark. Afterwards, the scavenging activity of samples was estimated by measuring the absorption of the mixture at 520 nm, using a UV-Vis spectrometer (Cary 60-UV-Vis Spectrophotometer, USA) which reflected the amount of DPPH radicals remaining in the solution.

The radical scavenging activity was calculated according to the following equation:

$$\%RSA = 100 \times \left(\frac{A_{control} - A_{sample}}{A_{control}} \right), \quad (2)$$

where A_{sample} represents the absorbance of the sample solution in the presence of DPPH, and $A_{control}$ is the absorbance of the standard DPPH solution. RSA values for film samples depend on film properties.

Statistical analysis was carried out using OriginPro 8 (OriginLab Corporation, Northampton, MA, USA). All data are presented as mean value with their standard deviation indicated (mean \pm SD).

3. Results and Discussion

3.1. Droplet/Particle SIZE and Emulsion Stabilization

DLS results (mean droplet diameter of the o/w nano/micro sized emulsion and Zeta potential) are compiled in Table 1. Emulsions without C30B nanoclay (CHM/RSO) had bimodal droplet size distributions. The main population of droplets (that scatter around 81% of the total scattered intensity) presented diameters of 737–1250 nm and the second population had a drop average diameter of 136 nm (around 19% of the total scattered intensity). Differently, emulsions containing C30B nanoclay had trimodal droplet size distributions. The averages diameters of the detected droplet populations were 385 nm (85%), 98 nm (7%), and 63 nm (8%), respectively. C30B nanoclay added to the continuous phase of the emulsion conferred its distinct droplet size distribution, the average size diameter of the main population of droplet decrease almost threefold.

Table 1. Zeta potential (ζ) and average diameters (d) of the emulsions' droplets.

Sample	ζ -Potential (mV)	Droplet Sizes	
		Type of Distribution	d (nm)
CHM/RSO	24.35 ± 1.17	Bimodal	993.5 ± 256 136.1 ± 35
CHM/RSO_C30B	30.7 ± 1.31	Trimodal	385.7 ± 84 98.17 ± 16 63.11 ± 11

ζ —Zeta potential; d—average diameter.

The zeta potential of the obtained emulsions presented positive values due to the presence of cationic polysaccharide (chitosan), as expected. By comparing the positive zeta potential with mean particle diameter at nanoscale level, it could be deduced that chitosan molecules are localized at the oil–water interface and intercalated between the nonionic surfactant (T80) molecules. Therefore, the combination of steric (by nonionic surfactant) and electrostatic (by cationic chitosan) repulsions was responsible for the stabilization of dispersed rosehip seed oil droplets in the o/w nano/micro-sized emulsions. The same behavior was noticed also for other o/w chitosan-based emulsions as mentioned by Tamilvanan et al. for castor oil-based chitosan emulsion [31]. The addition of C30B nanoclay

determines and increases of the positive values of ζ -potential, indicating that nanoclay is located at the oil–water interface forming a Pickering interfacial layer [32]. Additionally, the addition of C30B nanoclay into o/w emulsion decreased the particles size.

3.2. Structural Characterization of Chitosan Emulsion Films by ATR-FTIR

FTIR spectrum of rosehip seed oil reveals vibrations bands at 3010 cm^{-1} assigned to =CH vibration from lipids (methyl-oleate group), and bands at 2925 and 2855 cm^{-1} , which are characteristic of asymmetrical and symmetrical vibrations $\nu(\text{C}-\text{H})$ of the CH_2 and CH_3 aliphatic groups from the alkyl rest of the triglycerides (found in large quantities in vegetable oils)—Figure 2. The absorption band at 1743 cm^{-1} is assigned to $\nu(\text{C}=\text{O})$ ester carbonyl, which is a chemical group specific to oils with a high content in saturated fatty acids and short hydrocarbonated chains. The vibration band near 1654 cm^{-1} corresponds to the double $\text{C}=\text{C}$ bond and may be correlated with the content of polyunsaturated fatty acids in the oil [33]. The band at 1461 cm^{-1} is associated the $\delta(\text{C}-\text{H})$ deformation. Other bands are observed at 1375 cm^{-1} (deformation vibration in the phase of methylene group from lipids), 1316 cm^{-1} ($\delta(\text{C}-\text{H})$ from resins impurities) [34], and 1237 cm^{-1} (in plane deformation vibration of =CH groups from the unconjugated cis double bonds [33].

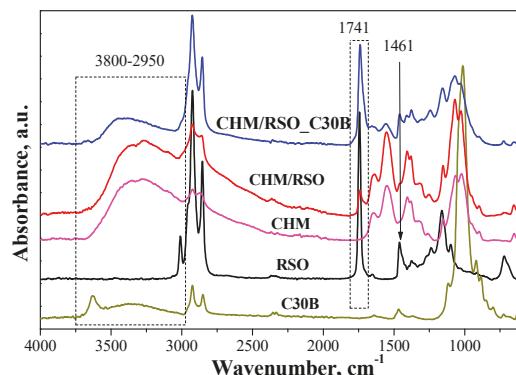


Figure 2. Attenuated total reflection-Fourier transform infrared spectroscopy (ATR-FTIR) spectra of rosehip seed oil (RSO), medium molecular chitosan (CHM), C30B and films obtained from emulsions.

The FTIR spectrum of chitosan presents a broad band between 3680 and 2980 cm^{-1} , with two highlighted peaks at 3355 and 3271 cm^{-1} attributed to amine N–H stretch and O–H stretch, respectively. The band between 2980 and 2750 cm^{-1} , with maximum at 2923 and 2873 cm^{-1} , is assigned to aliphatic C–H stretching [35]. The band at 1647 cm^{-1} is assigned to amide C=O stretching from acetylated amino groups in chitosan. Another major absorption band with a maximum at 1549 cm^{-1} belongs to free primary amino group bending (νNH_2) at C_2 position of glucosamine, which is one main group present in chitosan. The bands found in the spectrum at 1405 and 1380 cm^{-1} are attributed to the CH_2 and CH_3 bend. The band at 1323 cm^{-1} is due to $-\text{O}-\text{H}$ in plane vibration of primary alcohol groups ($-\text{CH}_2-\text{OH}$). The absorption bands at 1152 cm^{-1} (anti-symmetric stretching of the C–O–C bridge), 1064 and 1023 cm^{-1} (skeletal vibration involving the C–O stretching overlapped with C–N stretching vibration) are characteristics of the saccharide units of the chitosan structure [35,36].

FTIR spectrum of C30B clay reveals typical vibration bands responsible for stretching vibrations of the Si–O bond at 1116 cm^{-1} , bending vibrations of AlAlOH at 919 cm^{-1} and AlMgOH bonds at 885 – 849 cm^{-1} . Other absorptions bands are found at 1012 cm^{-1} , assigned to stretching vibrations of Si–O–Si, and at 3631 and 3538 cm^{-1} , ascribed to the free –OH stretching and the hydrogen-bonded –OH stretching, respectively. The band located at 1643 cm^{-1} for C30B organoclay is caused by the hydrogen free carbonyl, and the bands at 1467 and 1369 cm^{-1} are associated with the $-\text{CH}_3$ group.

Bands characteristic to $-\text{CH}_2$ stretching of methylene group are found in the region located at 2924 and 2850 cm^{-1} [37].

The FTIR spectra of CHM/RSO and CHM/RSO/C30B sample reveals some characteristic bands of rosehip seeds oil incorporated into chitosan-based film, namely at 3006, 2858, 1741, and 1450 cm^{-1} that are assigned to $\nu (= \text{CH})$, symmetrical $\nu (\text{C}-\text{H})$ from methyl group, $\nu (\text{C}=\text{O})$ from $\text{RC}=\text{OOR}$ structure and to $\delta (\text{C}-\text{H})$ deformation. Significant modifications are observed in FTIR spectra of chitosan by rosehip seed oil incorporation into emulsion-based films. The vibration absorption band given by the free O-H bond valence occurs in the region of $3590\text{--}3650\text{ cm}^{-1}$, and the association through polymer hydrogen bonds leads to wide bands in the region $3200\text{--}3600\text{ cm}^{-1}$. By rosehip seed oil addition into chitosan-based films. the band associated with free bonded O-H group of chitosan is shifted to a lower wavenumber, from 3355 to 3343 cm^{-1} , indicating interaction by hydrogen bonds between chitosan and rosehip seed oil. The band ascribed to primary amino group bending (νNH_2) of chitosan is shifted to higher wavenumbers by RSO incorporation (from 1549 to 1554 cm^{-1}). Most vibration bands of chitosan are shifted to higher wavenumbers by RSO incorporation and this may be due to the fact that the added components can inhibit the inter/intra molecular hydrogen bonding which existed in the neat chitosan film [38].

The obtained hybrid emulsion-based films exhibit characteristic bands associated with the isolated $\text{MgO}-\text{H}$ stretching at 3690 cm^{-1} , stretching of structural $-\text{OH}$ at 3661 cm^{-1} . Between 3650 and 3050 cm^{-1} a broad band is present, due to the fact that many specific bands of the components are overlapping, which can be associated with the stretching vibrations of $-\text{OH}$ groups of interlayer water from C30B, N-H stretching and hydroxyl $-\text{OH}$ stretching [36,39,40].

The FTIR spectroscopy has demonstrated the RSO and C30B clay successful incorporation into chitosan-based film. The formation of hydrogen bonds and van der Waals interactions that appear on the phase boundaries, indicated by the band shift in FTIR spectra, influences the mechanical properties of the materials. Addition of the C30B nano-filler to the liquid system of chitosan dissolved in acetic acid solution facilitated formation of hydrogen bonds between functional groups of the chitosan matrix, mainly with amine and hydroxyl groups, and the Si-O bonds existing within the silicate layers of the nanoclay. Moreover, both hydroxyl and amine groups of chitosan may bond with Si-O-Si groups of the silicate layer of C30B clay [37].

3.3. Morphological Analysis

Scanning electron microscopy examination reveals the morphology of the films surface obtained by the incorporation of rosehip seeds oil and nanoclay C30B into chitosan films (Figure 3). Analysis of the CHM sample reveals a smooth and continuous film structure surface (Figure 3a,d). Inspection of CHM/RSO/T80 film surface showed the presence of large spherical cavities, attributed to RSO oil droplets, that are relatively homogenously dispersed into the CHM matrix (Figure 3b,e), as revealed by SEM images. Similar surface microstructure, namely discontinuities associated with the formation of two phases, was found for quinoa protein-chitosan-sunflower oil film by Valenzuela et al. [41]. The average particle size of the RSO globules is $4.7 \pm 1.6\text{ }\mu\text{m}$, with the size of oil droplets varying from 2.1 to $7.2\text{ }\mu\text{m}$. The good homogeneity of the films and the encapsulation of the oil are assured by the presence of the nonionic surfactant and T80 emulsifier. By C30B nanoclay addition into the emulsion system, the average particle size of the RSO droplets decrease at about $2.6 \pm 0.7\text{ }\mu\text{m}$, the oil droplets being better distributed into the emulsion-cast film (Figure 3c,f). The C30B organoclay is also well distributed into the emulsion-cast films with an average particle size of $0.44 \pm 0.1\text{ }\mu\text{m}$.

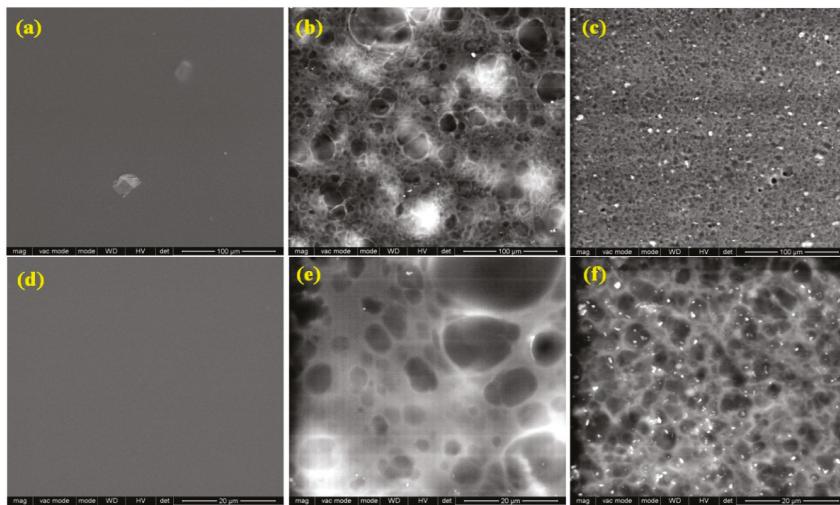


Figure 3. Scanning electron microscopy (SEM) images of CHM, CHM/RSO and CHM/RSO/C30B films; (a–c) scale bar: 100 μm and (d–f) scale bar: 20 μm .

3.4. Mechanical Properties

Mechanical properties are important when referring to materials proposed for applications in the packaging industry, because strength at break and flexibility ensure the integrity of films intended for food packaging. The strength at break indicates the maximum tensile stress that the film can resist while being pulled before breaking [42].

The effect of incorporating RSO and nanoclay C30B on the mechanical properties of chitosan-based films are shown in Figure 4.

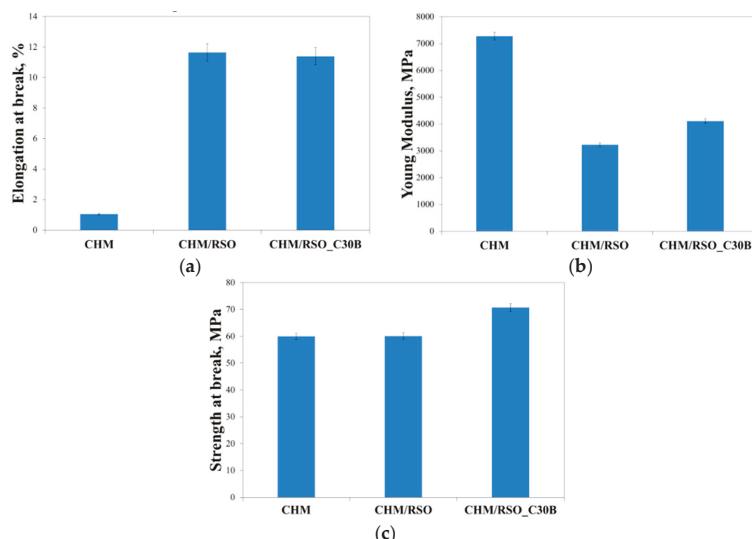


Figure 4. Elongation at break (a), Young modulus (b), and strength at break (c) of CHM, CHM/RSO and CHM/RSO/C30B emulsion-cast films.

Chitosan control film (containing T80) had the strength at break of 59.9 MPa, Young Modulus value of 7282.0 MPa and 1.05% elongation at break. Incorporation of rosehip seed oil and C30B nanoclay into chitosan films significantly increased elongation at break from 1.05% to 11.7% in case of RSO incorporation and 11.40% for RSO/C30B. The nanofiller does not change elongation at break. A high value of Young modulus was registered for the reference chitosan film, which means that it is a rigid material. On the other hand, an increase of tensile strength and a decrease of elastic modulus after the incorporation of the rosehip seed oil and C30B nanoclay can be observed in Figure 4. The strength at break values for the chitosan based-films containing RSO and C30B nanoclay, are 60.1 and 70.7 MPa, respectively and Young modulus values determined for the same samples were 3232.3 and 4110.9 MPa, respectively. This behavior could be attributed to the oil components, which act like plasticizers for the chitosan film. The role of plasticizers is to weaken the inter/intra molecular forces between polymer chains, and thereby increasing the flexibility of the films [6]. A different behavior was noticed for chitosan films formulated with clove essential oil (CEO) and halloysite nanotube (HNT), the films with CEO presented lower elongation values than the film without CEO [43]. There are also other reports indicating a reduction of the tensile parameters when a bioactive compound is incorporated in chitosan films [44,45]. The authors attributed this behavior to the presence of structural discontinuities in the chitosan matrix caused by the oil-dispersed phase. The C30B further improved the strength at break of the films. According to Krochta and De-Mulder-Johnston's [46] film classification, values of tensile strength below 10 MPa indicate poor mechanical properties. Therefore, chitosan based-films containing RSO and C30B nanoclay show good and satisfactory mechanical properties; and the strength at break values can be considered acceptable for materials proposed for applications in bioactive food packaging.

3.5. O_2 and CO_2 Permeability

A barrier polymeric material is most commonly used in the packaging industry to stop the passage of small molecules of gases, moisture or flavors. The barrier properties of a polymeric film are important because it is necessary to preserve the quality of food and to estimate its shelf-life [47]. Generally, gas permeability depends on film microstructure (holes or discontinuities in the polymer structure), thickness, the solubility of gases in the corresponding material, and the level of arrangement of the polymer chains [42]. Oxygen and carbon dioxide are the most common permeates studied in food packaging applications. The oxygen diffusion from air into the package should be avoided because the product quality can be modified during prolonged storage due to the oxidation, which leads to changes in organoleptic properties and decreased nutritional value. The oxygen permeation through a material is calculated as the weight or volume of oxygen which is able to pass through a known area of a packaging material in a given time [48]. Like oxygen, the barrier property to carbon dioxide is also important in food packaging applications, since carbon dioxide can initiate deterioration reactions and should be removed to ensure freshness of food products.

Table 2 summarizes the results from O_2 and CO_2 permeability tests of the chitosan emulsion films. The values of O_2 permeability for reference chitosan film was of 67 mL/m^2 per day and after incorporation of rosehip seed oil and C30B nanoclay, the O_2 permeability was higher with values of 212 and 134 mL/m^2 ·per day, respectively. These kind of gas barrier features were observed also by other authors, the values of O_2 permeability of chitosan films being comparable [41,49]. The increased values of O_2 could be attributed to the plasticization effect of the amorphous biopolymer backbone by the water molecules [50]. The plasticizing effect tends to increase the mobility of the oxygen molecules due to the disruption of hydrogen-bonding, creating additional sites for the dissolution of oxygen [51]. The presence of C30B nanoclay leads to the improvement of CO_2 barrier properties reaching half lower CO_2 values for films with C30B compared to neat chitosan.

Even if the samples obtained by RSO and C30B addition into chitosan matrix presents higher oxygen permeability, the obtained values indicate that chitosan emulsion films show a superior oxygen

barrier compared to a synthetic biodegradable polymer-based packaging material, polylactic acid (PLA), of similar thickness (Table 2).

Table 2. Permeability to O₂ and CO₂ of chitosan emulsion-cast films.

Sample	Thickness (mm)	CO ₂ (mL/m ² per day)	O ₂ (mL/m ² per day)
PLA	0.151 ± 0.012	873 ± 26.1	1308 ± 39.4
CHM	0.148 ± 0.008	45 ± 1.8	67 ± 3.35
CHM/RSO	0.237 ± 0.019	37 ± 1.1	212 ± 10.6
CHM/RSO_C30B	0.193 ± 26.19	18 ± 0.9	134 ± 6.7

3.6. Dynamic Moisture Sorption

The relationship between the equilibrium moisture content (EMC) against the relative humidity (RH) at constant temperature (25 °C) for chitosan-based films is presented in Figure 5.

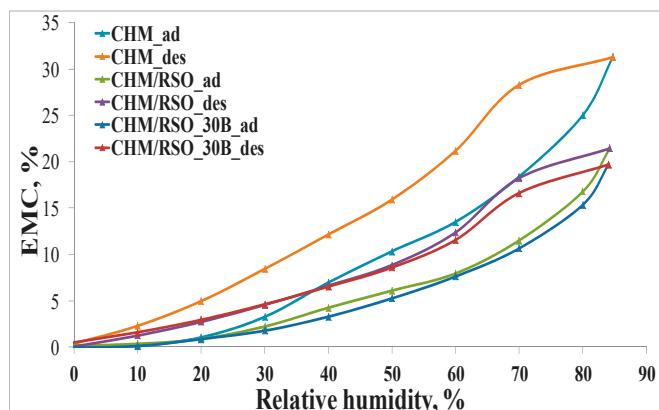


Figure 5. Moisture sorption isotherms (adsorption/desorption) for chitosan-based samples.

According to the IUPAC classification [52–54], the adsorption/desorption isotherms can be associated to type V curves describing adsorption on hydrophobic/low hydrophilic materials with weak sorbent–water interactions. The values of water vapor sorption capacities for all the samples are presented in the Table 3. The isotherms show hysteresis between sorption and desorption. In Figure 5, it can be seen that the final mass is the same as the initial one. The chitosan-based films showed an improvement of the water vapor barrier property by incorporation of rosehip seed oil and C30B nanoclay in the film matrix (Table 3). The EMC of rosehip seed oil–chitosan films is significantly lower than that corresponding to the reference chitosan film. This may be due to the diminished availability of amino groups of chitosan, determined by the electrostatic neutralization with the carboxylate groups of rosehip seed oil that contributes to the compactness of the film network and may cause limited access of water molecules to the hydrophilic sites of chitosan. Pereda et al. [6] observed the same behavior of EMC for olive oil–chitosan films.

Addition of C30B nanoclay into the chitosan-RSO emulsion film leads to a further slight decrease in equilibrium moisture content. This result indicates that nanoclay affects the water vapor barrier property of biopolymer films, which may be due to the fulfilling of interspaces in the chitosan matrix by nanoclay particles [55] or due to the hydrophobic nature of the C30B nanoclay [40].

Table 3. Equilibrium moisture content (EMC) assessed at 90% relative humidity (RH) of chitosan-based films containing RSO and C30B.

Sample	EMC (%)
CHM	31.29 ± 1.1
CHM/RSO	21.44 ± 0.8
CHM/RSO/C30B	19.70 ± 1.2

EMC—equilibrium moisture content.

3.7. Antibacterial Inhibition

Two Gram-negative bacteria, namely *E. coli* and *S. typhimurium*, and one Gram-positive bacterium, *B. cereus* were used as test bacteria to examine the bactericidal properties of chitosan film and the effect of RSO, as well as C30B nanoclay addition on the antibacterial action of chitosan. These bacteria were selected because they are the common foodborne pathogens, which are responsible for most of the foodborne diseases [56]. The results of antibacterial tests are shown in Figure 6.

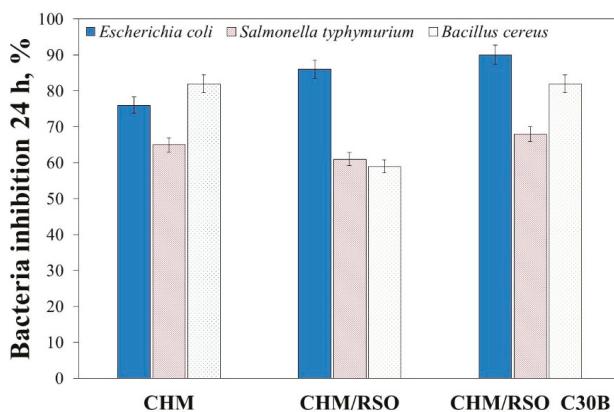


Figure 6. The antibacterial activity of chitosan-based bionanocomposites against *Escherichia coli*, *Salmonella typhimurium* and *Bacillus cereus*.

From the results shown in Figure 6, it can be observed that chitosan film is an effective antimicrobial agent against the tested bacteria. The results showed bacteria inhibition at 24 h, with 65% reduction for *S. typhimurium*, 73% reduction for *E. coli*, and 82% reduction for *B. cereus*. Addition of rosehip seed oil resulted in the decrease of the antibacterial action against *S. typhimurium* and *B. cereus*. On the other hand, all tested chitosan emulsion films showed pronounced antibacterial activity against *E. coli*. Addition of rosehip seed oil and C30B nanoclay resulted in the increase of antibacterial activity of the chitosan film against *E. coli*. These results are in accordance with those reported by Kamarasamy et al. [57], where a weak antibacterial effect of rosehip seed oil was demonstrated, and only against *E. coli*. Additionally, is important to mention that addition of C30B nanoclay resulted in an increase of antibacterial activity of the chitosan emulsion films against all tested bacteria (Figure 6). Similar results regarding the antibacterial property of C30B nanoclay were also reported by various authors [40,58,59]. The results shown in Figure 6 indicates a synergism between chitosan, rosehip seed oil and C30B nanoclay, and that by mixing them a material with strong antibacterial property resulted.

3.8. Antioxidant Activity

Antioxidant properties, especially radical scavenging activity, are important because free radicals have a negative effect both on foods and the human body, leading to oxidative stress, which is involved in the development of many human diseases [60,61]. As demonstrated by other authors, chitosan itself holds some antioxidant activity, mainly attributed to the capacity of residual free amino groups of chitosan to react with free radicals, forming stable macromolecular radicals and ammonium groups, but its activity is negligible compared to other bioactive compounds [49,62–65]. When rosehip seed oil was added to the chitosan film, the radical scavenging activity (RSA, %) increased up to three-fold (determined after 30 min). The addition of C30B nanoclay into the chitosan/rosehip seed oil films did not significantly affect the antioxidant activity of the samples (Figure 7).

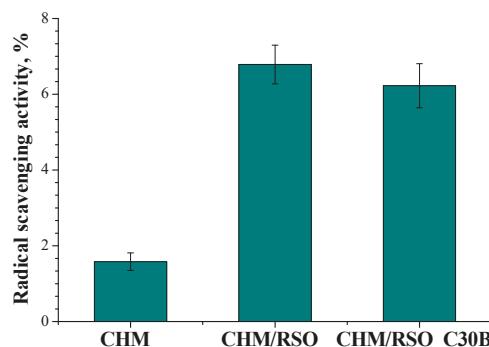


Figure 7. Radical scavenging activity (RSA) of chitosan-based films obtained by emulsion cast technique, determined after 30 min.

4. Conclusions

Films based on chitosan, rosehip seed oil and C30B montmorillonite were successfully prepared and characterized by the encapsulation emulsion method. The addition of rosehip seed oil, which acts also as antioxidant, antibacterial and plasticizer, was found also responsible for improving the flexibility of chitosan-based films, whereas addition of the C30B nanoclay improved the strength at break of the biocomposites. The inter/intra molecular hydrogen bonding between components, confirmed by FTIR analysis, assures the excellent integrity of the films and, as a consequence, superior gas (oxygen and carbon dioxide) and water vapor barrier properties. The results of the present study show that the chitosan emulsion films exhibited potent antibacterial and antioxidant activity, and can be considered acceptable for materials proposed for applications in bioactive food packaging.

Author Contributions: In this study, the concepts and designs for the experiment were supervised by E.S. and C.V. Manuscript text and results analysis were performed by E.B., E.S. and C.V. The experimental results were obtained and examined by E.B., E.S., C.V., R.N.D.-N., M.A.B. and A.B. All authors read and approved the final manuscript.

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Article

Release of Graphene and Carbon Nanotubes from Biodegradable Poly(Lactic Acid) Films during Degradation and Combustion: Risk Associated with the End-of-Life of Nanocomposite Food Packaging Materials

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Abstract: Nanoparticles of graphene and carbon nanotubes are attractive materials for the improvement of mechanical and barrier properties and for the functionality of biodegradable polymers for packaging applications. However, the increase of the manufacture and consumption increases the probability of exposure of humans and the environment to such nanomaterials; this brings up questions about the risks of nanomaterials, since they can be toxic. For a risk assessment, it is crucial to know whether airborne nanoparticles of graphene and carbon nanotubes can be released from nanocomposites into the environment at their end-life, or whether they remain embedded in the matrix. In this work, the release of graphene and carbon nanotubes from the poly(lactic) acid nanocomposite films were studied for the scenarios of: (i) biodegradation of the matrix polymer at the disposal of wastes; and (ii) combustion and fire of nanocomposite wastes. Thermogravimetric analysis in air atmosphere, transmission electron microscopy (TEM), atomic force microscopy (AFM) and scanning electron microscope (SEM) were used to verify the release of nanoparticles from nanocomposite films. The three factors model was applied for the quantitative and qualitative risk assessment of the release of graphene and carbon nanotubes from nanocomposite wastes for these scenarios. Safety concern is discussed in respect to the existing regulations for nanowaste stream.

Keywords: graphene; carbon nanotubes; poly(lactic) acid; degradation; combustion; fire; risk analysis

1. Introduction

Manufactured nanomaterials are applied in various consumer goods in order to enhance their properties or to supplement novel functionalities. The industry has already utilized nanoclays, metal nanoparticles and carbon nanotubes and has managed to use them in products for a variety of applications, e.g., semiconductors, automotive, aerospace, electronics, energy, defense, sporting goods, and packaging [1]. Nanotechnology allows scientists to alter the structure of packaged materials on a molecular scale in order to give the materials the desired properties [2,3]. Nowadays, different types of carbon nanotubes and graphene in polymer nanocomposites are widely investigated for the development of smart, active and intelligent packaging that can improve the quality and safety of food, to solve the food storage problem and to inform the consumer about the quality of packaged food [2–4]. Graphene and multiwall carbon nanotubes (MWCNTs) in biodegradable polymers are the most continuous and potentially valuable nanoscale materials to have emerged in recent years, and

are increasingly studied to enhance the thermal, mechanical, barrier properties and functionality of food packaging materials [1–3,5]. Among the many different biopolymers available, polylactic acid (PLA) is a promising alternative, especially for food packaging and biomedical packaging applications. However, a key challenge is to enhance the barrier properties of the PLA packaging. Graphene and its derivatives are identified as powerful candidates for gas-barrier materials because perfect graphene does not allow the diffusion of small gases through its plane [6–8]. Incorporation of graphene and carbon nanotubes into polymer matrices are also a promising nanotechnology approach to increase mechanical strength and improve thermal properties when properly dispersed in a polymer matrix [9,10].

At the same time, regulators at national, European and international level are still struggling to agree upon a unified and mutually accepted definition of a “nanomaterial”. As the market of nanomaterial-based products is expected to triple by the year 2020 in more industrial sectors, the application of nanomaterials and nanoparticles is expected to grow proportionally [2,3,11]. As a result, environmental exposure to nanoparticles in air, water and soils is also expected to increase [11]. Therefore, more research efforts in nanoscience are needed to focus exclusively on the potential risk of nanomaterials graphene and carbon nanotubes with the increasing exposition of consumers and the environment to nanoparticle-containing packaging. The specific nanoscale size and shape of graphene and carbon nanotubes with a large aspect ratio and large surface area, airborne, non-soluble in water and absorptive in soil, will enhance the risk of their mobility in the environment [12,13].

Currently, very little is known about the release of the nanomaterials graphene and carbon nanotubes (CNT) incorporated into polymer nanocomposites. Although they are typically tightly bound in the matrix polymer, their release through the lifecycle of nanocomposites is possible [11]. Therefore, greater information is needed on the potential hazard associated with specific exposure scenarios. Few scenarios were identified and published in the literature [11,14,15] where CNTs might be released into the environment during the life cycle of polymer nanocomposites in the production, service life and disposal stages. Release during service the life of CNT-based composites is projected to be quite low and composed of polydisperse fragments with only a small fraction of free single nanotubes [15–17]. The general conclusion is that the CNTs form a network and are not easily detachable from the samples, but the CNT layer on the surface of the degraded composites could be a source of a high quantity of released free standing CNTs and thus, may pose a health risk [16,17]. Researchers [16,17] reviewed the potential release of CNTs into the environment during the service life where untrained humans are in contact with oil-based polymer nanocomposites. They considered three possible pathways for the release of CNTs: due to exploitation and use, degradation of the matrix due to weathering processes, and fire events. Duncan and Pillai [18] assumed the nanoparticle release paradigms to be: (i) via passive diffusion, desorption and dissolution into external liquid media; and (ii) by matrix degradation. However, currently there are no standard methods to measure what is released from use of products containing nanomaterials.

Studies on the release of graphene through the lifecycle of nanocomposites are very scarce. Arvidsson, et al. [12] reported that the potential environmental and health risk of graphene at the production stage could be great, depending on the type of synthesis methods [12]. For most materials, degradation of the polymer matrix during the service life is associated with the greatest potential for release, with rates dependent on the specific characteristics of the polymer, carbon nanofiller, and environment [15,16]. In our previous studies [19–21], we have reported on the release of graphene nanoplatelets from food packaging materials into food simulants, due to the migration processes and the partial degradation of the biodegradable polymer matrix. Therefore, the released graphene nanoplatelets and their aggregates from the nanocomposite wastes during their degradation may pose a health risk [16,17]. The fate of graphene in polymer nanocomposite exposed to UV radiation was discussed and researchers concluded that graphene nanoparticles would be able to pass into the air or engage in the soil and groundwaters [22].

End-of-life aspects of nanomaterials have received far less attention than their preparation or application [23]. The two main strategies used for the end-of-life of thermoplastics products are recycling and burning to produce energy (thermal valorization). As the release of nanoparticles during grinding of nanocomposite wastes presents a potential risk, the incineration of nanocomposites has recently been accepted as a prospective waste management strategy, for which nanoparticle emission during burning must be addressed as a premise. So far, no detailed study has been published that investigates the release of graphene from nanocomposites due to accident fire or burning. Few publications have discussed the incineration and burning of CNT-based nanocomposites [24,25]. In contrast to incineration, where under high temperatures CNTs can be destroyed [24], a fire or burning of CNT nanocomposites in open air may not degrade all CNTs particles in composites, since the decomposition temperature of CNTs is much higher than that of the polymer matrix. A network of CNTs is formed in the char (residue ash), but measurements are still missing if CNTs can be released from the residue ash into the air. Bouillard, et al. [25] reported on the release of free CNTs and agglomerates of CNTs from acrylonitrile–butadiene–styrene (ABS) nanocomposites into the air during nanowastes combustion at quite low temperatures (about 400 °C). This information was found to be important to assess the environmental risks and the inhalation risks to people engaged in those practices.

In the present study, we investigate the release of graphene nanoplates and multi-walled carbon nanotubes from biodegradable poly(lactic) acid nanocomposite films at various temperatures, due to polymer degradation and burning. We analyze the risk from the release of graphene nanoplatelets and multi-walled carbon nanotubes at the end-of-life of the nanocomposite wastes, due to biodegradation at composting, combustion and accident fire. The thermogravimetric analysis (TGA), transmission electron microscopy (TEM), atomic force microscopy (AFM) and scanning electron microscope (SEM) were used to verify the release of nanoparticles from nanocomposite films. The three-factors model (C.E.L.) was applied for the quantitative and qualitative risk assessment of the release of graphene and carbon nanotubes from nanocomposite wastes for these scenarios' materials. Safety concerns are discussed in respect to the application of nanomaterials in food packaging, bio-medical packaging and others.

2. Materials and Methods

Nanocomposite of poly(lactic) acid polymer (PLA) filled with graphene nanoplatelets (GNP) and multiwall carbon nanotubes (MWCNTs) was supplied from Graphene 3D Lab, (Ronkonkoma, NY, USA) in the form of filament for 3D printing (FDM). Commercial neat PLA filament was also supplied. The matrix polylactic acid is CAS# 26100-51-6, Sigma-Aldrich, (St. Louis, MO, USA) with Mw~60,000 and 1.8% crystallinity. Disk samples having sandwich structure of 10 alternative layers of the nanocomposite and the PLA were 3D prepared with the dual extruder X400 Rep Rap printer (Feldkirchen, Germany). The printed samples were hot pressed to thin films with a thickness of 30 microns. The amount of nanocarbon filler in the final film samples is 3 wt. %.

The film samples were emerged in two aqueous-based solvents of 10 vol. % ethanol and 50 vol. % ethanol. Ultra-strong migration test was performed with heating at 90 °C for 4 h, followed by storage for 10 days at 40 °C and dynamic treatment for 1 min daily. The migration test regime was applied to simulate the conditions of high temperature treatment of nanocomposite packaging during their end-of-life as waste disposal.

Different visualization techniques were applied in order to identify migrants in the simulant media and to verify the film integrity after the migration test. TEM (EOL JEM 2100, Preabody, MA, USA) at accelerating voltage 200 kV and AFM (Bruker, Billerica, MA, USA) were used for the analysis of the dried colloids of migrated substances into the surrounding solvents. For preparation of the test samples, a micro-quantity of colloid after migration test was dropped on a copper TEM grid covered by a membrane from amorphous carbon (or on glass plate for AFM scan), and after that dried in a dust-free atmosphere at ambient conditions. The morphology of the film surface before and after the

migration test was studied by scanning electron microscope (Philips 515, Eindhoven, Netherlands) with accelerating voltage 25 kV and 5 kV. Before the examination in the microscope, the samples were covered with metal coating for better conductivity of the surface and to avoid discharge effects.

Thermal stability and degradation of nanocomposite films were studied by TGA (Q50, TA Instruments, New Castle, DE, USA), in air atmosphere, at a heating rate of 10 °C/min in three different temperature ranges, from 30 °C to 500, 650 and 850 °C. The mass loss during heating and the amount of residue ash were analyzed. TEM was performed for analysis of the residue ash after burning at the three temperatures.

Risk assessment analysis was performed using the three factors method, 3F or C.E.L., i.e., grading the three risk analysis factors: Consequences (C), Exposure (E), and Probability/Likelihood (L).

3. Results and Discussions

3.1. Release of Graphene and Carbon Nanotubes Due to Degradation of PLA Polymer

The use of biodegradable packaging materials, such as PLA will contribute to sustainability and reduction of wastes via degradation [26,27]. Composting, for example, has the potential to transfer biodegradable waste, including biodegradable plastics, into useful soil amendment products by an accelerated degradation using a mixed microbial population in a moist, warm, aerobic environment under controlled conditions. Song, et al [26] found that biodegradable packaging materials are most suitable for single-use disposable applications where the post-consumer waste can be locally composted. However, special care should then be taken while handling local composting of biodegradable nanowastes to limit potential environmental risks due to the release of nanoparticles in the soil from the compost.

We discuss herewith if the GNP and MWCNTs release as single nanoparticles or large aggregates from the nanocomposite packaging films via degradation of the PLA matrix. The characterization of such release provides critical information for environmental nano-object exposure from biodegradable nanocomposites. In our previous studies [19–21], we have investigated the release of GNP and MWCNTs from the composite film GNP/MWCNT/PLA in alcoholic and acid food simulants, at high temperature migration conditions, such as: (i) strong static migration test (heating at 90 °C for 4 h); and (ii) ultra-strong dynamic migration test (heating at 90 °C for 4 h followed by subsequent storage for 10 days at 40 °C, including dynamic treatment for 1 min daily). The migration conditions were set accordingly with the prescription in EU Regulation 10/2011 (EU 2011) [28] and literature sources [29,30].

We have observed that large graphene nanoplatelets (GNP) of about 100–1000 nm in length and a few nanometers in thickness indeed migrate from the GNP/MWCNT/PLA film into the food simulants, due to the diffusion processes [19,20]. During the strong static migration test, the total amount of released substances (nanoparticles and organic matter) from the composite GNP/MWCNT/PLA films was estimated around 0.028–0.053 mg/cm², where the nanoparticle migrants are of 0.006–0.011 mg/cm², depending on the food simulants [20]. Therefore, the released substances after this test remain below the overall migration limit (OEL = 0.10 mg/cm²) for food contact material accepted by the EU regulatory documents [28,31].

By contrast, during the ultra-strong dynamic migration test [20], the release of nanoscale size particles (100–1000 nm) from the GNP/MWCNT/PLA composite film is higher (0.5–0.7 number %) compared to (0.1–0.2 number %) nanoparticle migrants that were observed during the strong static migration test in the three food simulants, 3% acidic acid, and 10% and 50% ethanol. The larger size nanoparticle migrants (1–10 microns) were found also in higher amounts (3–5 number %) during the ultra-strong migration test, compared to 1–2 number % for the strong static test. Laser diffraction analysis was used in our previous studies [19,20] to detect the number and size distribution of the released nanoparticles from GNP/MWCNT/PLA films into the food simulants. In general, a threefold higher number of nanoparticles are observed to release during the ultra-strong dynamic migration test (heating at 90 °C for 4 h followed by storage for 10 days at 40 °C and dynamic treatment for 1 min daily) compared to the strong static test above. The detected nanoscale particles (100–1000 nm) in the food simulants are 0.5–0.7% while the micron scale agglomerates (1–10 µm) are 3–5%, compared to 0.1–0.2% nanoparticles and 1–2% agglomerates released after the strong static conditions [20]. This was associated with partial degradation of the PLA polymer matrix, which supports the diffusion of GNPs together with dissolved organic substances out of the film. However, the MWCNTs form the entangled network in the polymer film, which prevents their migration into food simulants if the polymer partially degrades.

Based on upper results, we discuss herein the scenario of nanoparticle release due to degradation of GNP/MWCNT/PLA composite films at the end-of-life stage of disposal or composting the wastes. Figure 1 presents the TEM micrographs (Figure 1a,b) and AFM scans (Figure 1c,d) of the dried migrants in 10% and 50% ethanol after an ultra-strong dynamic migration test. In Figure 2, the SEM micrographs of the film surfaces before and after such treatment are compared.

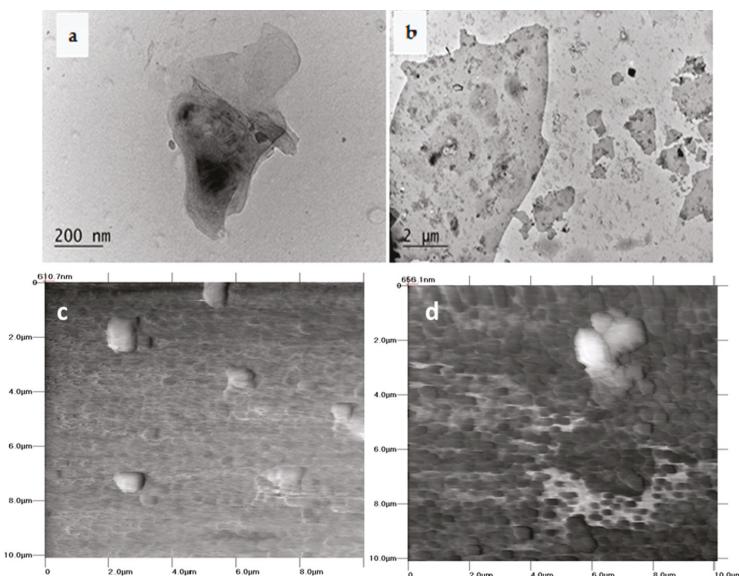


Figure 1. (a,b) transmission electron microscopy (TEM) micrographs and (c,d) atomic force microscopy (AFM) scan of dried migrants from GNP/MWCNT/PLA film after the ultra-strong dynamic test in 10% ethanol (first column) and 50% ethanol (second column).

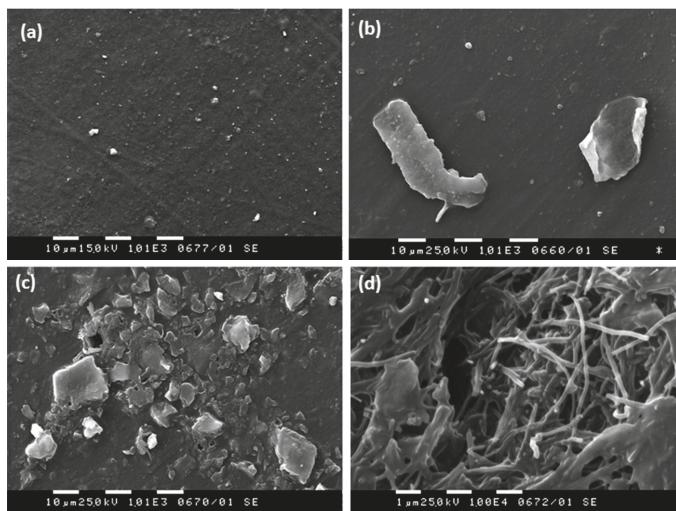


Figure 2. Scanning electron microscope (SEM) micrographs of the film surfaces: (a) reference GNP/MWCNT/PLA film before the test; (b) after the ultra-strong dynamic test in 10% ethanol, (c,d) after the ultra-strong dynamic test in 50% ethanol (in different places).

As seen from the TEM micrographs in Figure 1a,b, mainly small aggregates of GNPs below 500 nm are observed in a low amount in 10% ethanol (Figure 1a). While in a more aggressive media of 50% ethanol (Figure 1b), the amount of released GNPs increases apparently, and most of the platelets are in nanoscale size, 100–1000 nm; only a few aggregates of size 1–10 μm are visible. The AFM scans of dried colloids in 10% ethanol (Figure 1c) visualize the presence of a small amount of particles in a size of about 1 μm . However, in 50% ethanol (Figure 1d), the migrants are many small objects with a nanoscale size below 500 nm and a large aggregate of $\sim 2 \mu\text{m}$ length and thickness of ~ 500 nm. Importantly, MWCNTs are not visible to release from the GNP/MWCNT/PLA nanocomposite films, as observed by TEM and AFM analysis. Following the release mechanisms of nanoparticles proposed by Duncan and Pillai [18], we assume that the physical changes of biodegradable PLA polymer due to polymer hydrolysis provokes the diffusion of the graphene nanoplatelets and the dissolved organic substances out of the film into the food simulant.

SEM analysis was performed in order to examine the GNP/MWCNT/PLA film integrity before and after the ultra-strong dynamic migration test in the two alcohol-based simulants. The film surface before the treatment (Figure 2a) is smooth and free from ingredients. For the film immersed in 10% ethanol (Figure 2b), a few graphene nanoplates of a size of above 10 μm are extracted on the film surface. By contrast, in 50% ethanol (Figure 2c,d), the integrity of the GNP/MWCNT/PLA composite film is destroyed due to the partial degradation of the PLA polymer and much extraction of substances on the film surface. It is visible that the fibrous MWCNTs formed an entangled network as the PLA polymer matrix dissolved, which prevented their release into the food simulant.

It may be concluded based on the above results, that if the biodegradable nanocomposite wastes containing GNPs and MWCNTs are disposed in landfills, nanoscale graphene platelets can certainly be released into the environment due to partial degradation and weathering. If such nanowastes are subjected to composting, the biodegradation process provides compost that is very likely to contain large amounts of nanoscale GNPs, as well as graphene aggregates and bundles of carbon nanotubes of micron size. Since the compost is intended to be used for soil improvement, those nanoparticles would penetrate into soil and groundwater, and there is a potential risk of falling into the food chain of different organisms.

3.2. Release of Graphene and Carbon Nanotubes Due to Burning of Nanowastes

Burning of nanocomposite wastes to produce energy (thermal valorization) has been recently discussed as a nanowaste management strategy, and thus the risks for nanoparticle emission during incineration of thermoplastic nanocomposites must be addressed and investigated [25]. Moreover, the treatment of such waste by accidental fire or burning in landfills (a common practice in underdeveloped regions) may pose questions associated with environmental and human risks due to the potential release of large amounts of nanoparticles into the environment. In principle, graphene and CNTs are combustible materials above 600 °C, and they can be easily transformed into CO/CO₂ during degradation [25]. The published results on this subject are very scarce, but a few papers [32–34] have reported that the combustion of polymer composites with CNTs could form residues (ashes) containing unburned CNTs. Moreover, the CNTs also may release in the combustion gas phase [25]. Therefore, in the present work, we classify burning of nanowastes as a scenario that may have a greater possibility to release airborne nanoparticles. The characterization of such a release may provide critical information for environmental and human accidental nanoparticle exposures.

TGA was performed to simulate the nanowaste combustion in three heating regimes: 30–500 °C, 30–650 °C and 30–850 °C, at a heating rate 10 °C/min in air atmosphere. The graphene nanoplatelets used in this study are one of the possible forms of graphene-related materials. In general, the obtained thermal stability and the release results will depend strongly on the particular graphene material used in the nanocomposite. The thermal decomposition of the neat PLA and the nanocomposite films (GNP/MWCNT/PLA) were analyzed by the thermal gravity analysis (TG) and Differential thermal gravity (DTG) curves, which present the weight loss (%) and its first derivative versus temperature (°C), as shown in Figure 3a,b, respectively. The initial decomposition temperature (T_{onset}), the decomposition peak temperature (T_p) and the residue ash (%) were evaluated from the TG/DTG curves and data are presented in Table 1. The T_{onset} of the nanocomposite is observed around 230 °C, while T_p appears at 361 °C, which are higher than 10 °C and 5 °C, respectively, compared to the neat PLA. This indicates that the thermal stability of PLA is improved by the addition of 3 wt. % mixed nanofillers, GNP and MWCNT. As might be expected, the weight loss increases with increasing the heating temperature (T_{max}) from 500 to 850 °C. The combustion of the neat PLA at 500 °C results in 0.3% residue from the initial weigh of the polymer sample and the ash consists of amorphous carbon (CB). In contrast, the combustion of GNP/MWCNT/PLA forms residue ash of 3.3% at 500 °C, 1.5% at 650 °C and 0.07% at 850 °C, containing mostly unburned nanoparticles, GNP and MWCNT. Therefore, further potential environmental problems may arise with handling such residue ash. Our study advances the observations in References [25,32–34] by showing that the amount of GNP and MWCNTs in the residue ash decreases by increasing the burning temperature, this indicating increased decomposition of carbon nanoparticles by controlled incineration/combustion temperatures.

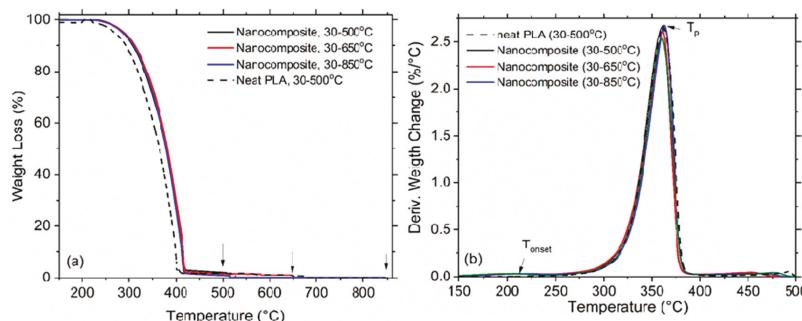


Figure 3. TGA (a) and DTG (b) curves of the neat PLA and GNP/MWCNT/PLA nanocomposite film compared to the neat PLA at three temperature regimes, 500, 650 and 850 °C, in an air atmosphere.

Table 1. Thermal characteristics of PLA and GNP/MWCNT/PLA nanocomposite by TG analysis.

Sample	Temperature of Burning T_{max}	T_{onset} , °C	T_p , °C	Weight Loss, % at T_{max}	Residue Ash, %
Neat PLA	500 °C	219.8	356.5	99.63	0.30
Nanocomposite	500 °C	230.7	360.2	96.70	3.30
Nanocomposite	650 °C	230.1	361.3	98.50	1.05
Nanocomposite	850 °C	230.3	362.8	99.98	0.07

TEM micrographs in Figure 4 visualize the content of the residue ash after combustion at the three temperatures in air atmosphere. As seen in the first column (Figure 4a), at 500 °C, the residue ash (3.3%) is completely composed of unburned single MWCNTs and GNPs, or their loose agglomerates. At 650 °C (Figure 4b), the residue decreases to 1.5% and consists mostly of single airborne particles, MWCNTs and GNP, and some soot CB nanoparticles of primary sizes of 10–30 nm. The nanotubes are about 30 nm in diameter and a few microns in length and are very similar to the original MWCNT size. Similar findings are observed for the GNP particles. While at 850 °C (Figure 4c), the amount of the residue ash strongly decreases to 0.07%, confirming that the carbonaceous fillers are mostly degraded. Indeed, the MWCNTs are missing in the residue ash, but unexpected content of GNP particles is observed and they are mainly displayed as fractal aggregates mixed with some soot nanoparticles.

The observations in Figure 4 reveal that large amounts of single isolated airborne MWCNTs (<50 nm diameter and >1 μm length) and GNPs (>100 nm), as well as their loose fractals (1–2 μm) can be released during burning in air atmosphere, addressing, therefore, a new kind of safety issue with regards to the combustion/incineration of nanowastes or accidental fires. The airborne particles of GNPs and MWCNTs may either stay in the char residues, or may be released in the gas phase during incineration or fire. Their fate depends on the local operating conditions of the burning process.

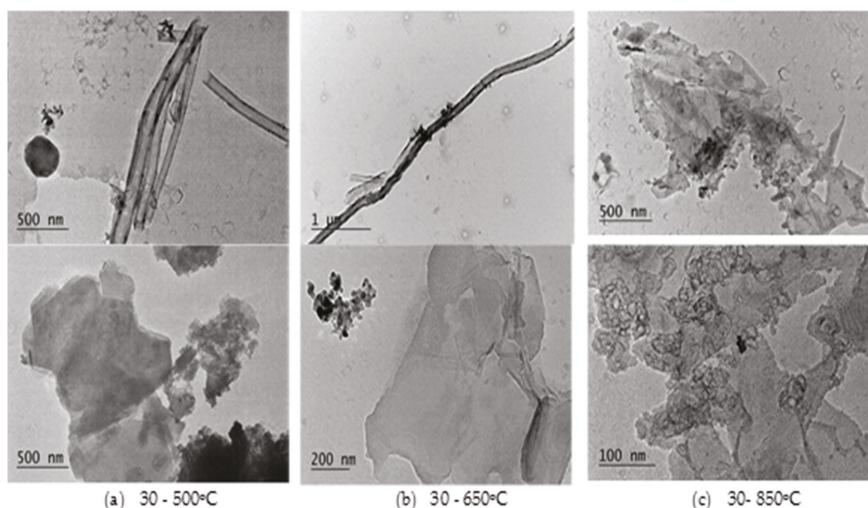


Figure 4. TEM micrographs of MWCNTs (first line) and GNPs (second line) observed in the residue ash at the three decomposition temperatures: (a) 500 °C, (b) 650 °C and (c) 850 °C in air atmosphere.

3.3. Risk Assessment Associated with End-of Life of Nanocomposite Food Packaging Materials

Risk could be defined as a combination of the probability of occurrence of an event and its consequences, establishing a negative outcome. The methodology we applied to analyze and quantify

the risk is borrowed from the standards and guidelines presented in several regulatory documents, such as: Risk Management Standard ISO 31000:2009 [35], British Standard BSI 2007 on safe handling and disposal of manufactured nanomaterials [36], USEPA Guidelines for Ecological Risk Assessment [37], and the British CSIRO Safe Handling and Use of Carbon Nanotubes [38]. In this study, the risk is mainly defined according to standard ISO 31000:2009 [35] as a comprehensive process of analysis and categorization, where the risk could be assessed quantitatively or qualitatively, depending on the probability of occurrence of the possible consequences.

To quantify the risk (R) of the release of MWCNTs and GNP from 3 wt. % GNP/MWCNT/PLA film at the end-of-life, as food packaging wastes, we have adopted the three factors method (C.E.L.), i.e., grading the three risk analysis factors: Consequences (C), Exposure (E), and Probability/Likelihood (L). The C.E.L. model is a widely recognized method of analysis and quantitative risk assessment [39,40]. Therefore, we have applied it for risk assessment in the four most popular scenarios for treatment of the food packaging wastes: biodegradation, combustion, burning in open air and accidental fire. The risk analysis factors are defined according to the C.E.L. model [39].

Consequences (C) represent the undesired results of an event or series of events. In this work, consequences are determined from the amount of the released MWCNTs and GNPs, as graded according to the recommended exposure limit of Carbon Nanotubes and Nanofibers (μg) in air (1 m^3), $\text{REL} = 1 \mu\text{g}/\text{m}^3$, proposed by NIOSH [41]. The NIOSH REL is expected to reduce the risk for pulmonary inflammation and fibrosis. Thus, six grades from 1 to 100 [39] are used for the quantification of consequences ($x\text{REL} = 1$ to $>1,000,000$), as shown in Table 2.

Exposure (E) shows how often a certain danger can occur and how much the system is often threatened by accidents. The exposure estimates are based on the E-classification method [39], with six steps in the range from 0.5 to 1 (Table 2).

Likelihood (L) shows how likely it is to have consequences. The following six steps of grades from 0.5–10 are used to quantify this factor, as shown in Table 2.

The risk (R) is defined as the quantity comprised of the product of the three parameters: consequences (C), exposure (E) and probability (L): $R = C \times E \times L$. The eligibility of risk to health and environment is classified in the following five risk areas presented in Table 2, namely: minimal, acceptable, high, very high and unacceptable (hazard), depending on the calculated values of risk (R) varying from <20 to >400 [39]. The end-results of the risk assessment determine the eligibility of the identified risk and the need to apply measures to prevent or limit it.

Table 2. The grades for Consequences (C), Exposure (E), Likelihood (L) and Risk (R) used in this study.

Consequences (C)	Exposure (E)	Likelihood (L)	Risk (R)
1 = minimal ($\leq 100 \text{ REL}$)	0.5 = very rare (less than once a year)	0.2 = not imagine et al	$<20 = \text{minimal}$
3 = significant ($100\text{--}1000 \text{ REL}$)	1 = rarely (once a year)	0.5 = almost impossible	$20\text{--}70 = \text{acceptable}$
7 = serious ($1000\text{--}10,000 \text{ REL}$)	2 = sometimes (once a month)	1 = unbelievable, but long-term still possible	$70\text{--}200 = \text{high}$
15 = very serious ($10,000\text{--}100,000 \text{ REL}$)	3 = happening (once a week)	3 = not be normal, but possible	$200\text{--}400 = \text{very high}$
40 = major damage ($100,000\text{--}1,000,000 \text{ REL}$)	6 = regular (daily)	6 = completely possible	$>400 = \text{unacceptable (hazard)}$
100 = crash ($>1,000,000 \text{ REL}$)	10 = continuous	10 = almost certain	

Quantitative and Qualitative Risk Assessment for the Release of GNP and MWCNTs

For the quantitative risk assessment, we used the data obtained above for the release of GNP and MWCNTs from 3 wt. % GNP/MWCNT/PLA film, during the degradation in ultra-strong dynamic test, as well as the burning at three heating temperatures 500, 650 and 850 °C in air atmosphere. Importantly, for the biodegradation (i.e., composting, weathering), we assumed that the total amount of 3 wt. % GNPs/MWCNTs nanofiller may release from the GNP/MWCNT/PLA nanocomposite film in the form of agglomerates and single nanoparticles due to the full degradation (hydrolysis) of the PLA polymer.

While for the burning processes like: combustion, burning in open air and accidental fire, the released GNPs and MWCNTs will depend on the heating temperature. The results from thermogravimetric analysis in Table 1 are used to simulate the combustion at the three temperatures in air atmosphere. For analysis of risk to humans and the environment, the released GNPs and MWCNTs are estimated for 100 kg wastes. Moreover, we have assumed that the single airborne nanoparticles of GNPs and MWCNTs (≤ 100 nm) and CB nanoparticles, that may release in 1 m³ air or soil are only 1% of the total amount of released nanoparticle agglomerates during the four scenarios studied.

The admissibility of the human and environmental risk is presented as a multiplication of the three factors ($R = C \times E \times L$). Table 3 presents the three risk analysis factors and the quantitative risk assessment for the four scenarios: biodegradation; combustion at 500, 650 and 850 °C; burning in open air (at 500 °C); and accidental fire (at 500 °C). As seen, the risk of GNPs and MWCNTs from the biodegradation is $R = 270$, while the risk from combustion varies within $R = 100\text{--}1500$ depending on the heating temperature (500–850 °C). However, the risk from the burning of wastes in open air (in landfills) is quite high ($R = 180$), while that from accident fire is low of $R = 22.5$, due to the very rare exposure.

Table 3. Risk assessment by CEL model for the release of GNPs, MWCNTs and CB from 3% GNP/MWCNT/PLA film during biodegradation, combustion, burning and accidental fire.

Scenario	Amount of Nano Wastes (kg)	Released Total Amount GNP/MWCNT/CB (kg)	Released GNP/MWCNT/CB Nanoparticles in 1 m ³ Air ($\mu\text{g}/\text{m}^3$)	Consequences (C) (\times REL)	Exposure (E)	Likelihood (L)	Risk, (R) = C \times E \times L
Biodegradation	100	3	30,000	15	3	6	270 very high
Combustion 850–650–500 °C	100	0.07–1.05–3.3	70–10,500–33,000	1–15	10	10	100–1500 high-to-hazard
Burning of wastes at 500 °C	100	3.3	33,000	15	2	6	180 high
Accident fire 500 °C	100	3.3	33,000	15	0.5	3	22.5 acceptable

For qualitative risk assessment, we used the approach described by Aven [40], which represents the dependence of the “consequences” in a function on the “frequency” of occurrence, the last being a derivative of “exposure” and “likelihood”. This dependence is shown in Figure 4, for the purpose of classification of the risk of MWCNTs and GNP release from 100 kg of 3 wt. % PLA/MWCNT/GNP nanocomposite wastes, under the scenarios of biodegradation, combustion (500–850 °C), burning in open air (at 500 °C) and accidental fire (at 500 °C).

The lines represent the “constant risk” at the following levels of risk: $R = 20$, $R = 70$, $R = 200$ and $R = 400$, and outline the five risk zones: minimum ($R < 20$); acceptable ($20 < R < 70$); high ($70 < R < 200$); very high ($200 < R < 400$) and hazard ($R > 400$). The experimental points represent the risk of exposure to MWCNTs and GNPs from the PLA nanocomposite film throughout the four scenarios of the waste treatment, listed in Table 3.

As shown in Figure 5, the scenario of total biodegradation of GNP/MWCNT/PLA nanowastes leads to a “very high” risk for release of GNPs and MWCNTs nanoparticles to the environment. This may pose questions associated with environmental and human risks due to local composting of post-consumer wastes, when those nanoparticles enter the soil. Combustion of nanowastes at heating temperatures of 500 °C may result in “unacceptable risk/hazard” from airborne GNPs and MWCNTs; however, by increasing the heating temperature to 850 °C, the risk decreases to “high”. Particularly, burning of nanowastes in open air (e.g., in landfills), which is a regular practice in underdeveloped regions, results in “high” risk. Therefore, such practices must be addressed and limited by the regulators, as it may affect more people and cause significant damage to the environment in those regions. The scenario of accident fire lead to “acceptable” risk, but it will have a local negative effect; therefore, preventive measures for safety have to be taken into account.

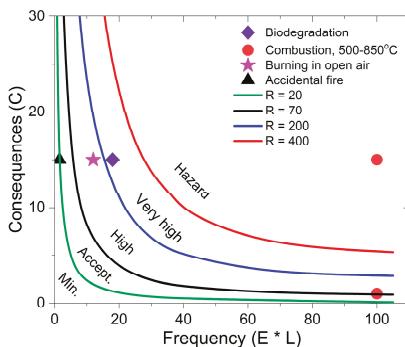


Figure 5. Qualitative risk assessment: consequences vs. frequency of occurrence of GNP and MWCNT exposure, related to four scenarios at the end-of-life of 3 wt. % GNP/MWCNT/PLA packaging films: biodegradation, combustion, burning and accident fire. Risk is estimated for 100 kg nanocomposite wastes.

3.4. Safety Concerns

Bioplastic packaging is widely used these days for wrapping products from food to electronics to protect them from dust, bacteria and water vapor, and to maximize the lifetime of packaged products. Among the many different biopolymers used, poly(lactic acid) (PLA) possesses good mechanical property and cost-effectiveness necessary of biodegradable food packaging. However, PLA packaging suffers from poor water vapor and oxygen barrier properties compared to many petroleum-derived ones. A key challenge is, therefore, to simultaneously enhance both the water vapor and oxygen barrier properties by incorporation or encapsulation of graphene and carbon nanotubes into the PLA packaging [42,43]. Studies comparing the graphene nanoplates, GNPs and carbon nanotubes, shows CNTs are very rare, making it difficult to analyze their overall safety and risk [44,45]. In general, authors agree, that despite their common carbon structure, CNTs and GNPs are two very different nanomaterials, due to their different physical and chemical characteristics. Dimensions, surface chemistry and impurities are equally important for determining the aggregation, degradation and toxicological effects of CNTs and GNPs. Their shape (tubular vs. plane) and their dimensions (2D vs. 1D) are key structural differences. The CNTs tend to form entangled aggregates, and GNPs tend to stack in several layers. GNPs are characterized by a lower aspect ratio (length/width), greater surface area and better dispersion in most solvents, compared to CNTs. The colloidal dispersions of graphene can be obtained without metallic impurities, with high stability and less aggregation. All those characteristics could theoretically offer significant advantages of GNPs over CNTs, in terms of risk management and safety.

Our current study expands the upper safety concerns comparing GNPs and CNTs, by finding that large graphene nanosheets indeed release from PLA-based nanocomposite films at temperatures above the glass transition, during ultra-strong dynamic migration test. However, MWCNTs remain embedded in the polymer matrix if the PLA matrix is partly degraded. Moreover, GNPs and MWCNTs are found to remain unburned in the residue after combustion up to 650 °C, while at 850 °C only GNPs and carbon soot are found, but not MWCNTs.

In this research, we stress the safety concerns at the end-of-life of nanocomposite food packaging, related to different waste treatments, such as: biodegradation, combustion, burning in open air, and accident fire. Safety concerns may arise due to biodegradation and composting of nanowastes based on biodegradable polymers. Composting has the potential to transfer biodegradable plastics into useful soil amendment products by accelerated degradation. However, special care should be taken

while handling local composting of biodegradable nanowastes to limit potential environmental risks due to the release of nanoparticles in the soil from the compost.

Combustion of nanocomposite wastes to produce energy has recently been discussed as a nanowastes management strategy, and thus the risks for nanoparticle emission during incineration of thermoplastic nanocomposites must be addressed and investigated. Our current study confirms that the combustion of PLA-based nanocomposites could form residue ashes containing unburned GNPs and MWCNTs; this is associated with “hazard” to “high risk”, depending on the temperature. The amount of unburned nanoparticles may be controlled by increasing the heating temperature above 500–850 °C; however, single GNPs and MWCNTs may also release in the combustion gas phase. Such release can be a source of risk in accidental scenarios, like fire, uncontrolled incineration/combustion, or the absence of nano-filtration of the combustion gas phase. Safety concerns arise about common practice in some regions for the burning of nanowastes in open air, e.g., in landfills or single-use disposable systems, due to the gradual increase of nanowastes from food packaging. As shown in this study, such regular practice leads to “high” risk for humans and the environment from airborne nanoparticles, such as GNPs and MWCNTs.

Based on the above study, we may propose a few safety measures for the prevention of risk from the packaging containing GNPs and MWCNTs at the end-life waste treatment: (i) Material safety data sheet (MSDS) should contain clear information if the nanomaterial is safe for composting; (ii) specific labeling for prevention from composting should be adopted and printed on the packaging; (iii) regulatory limitations imposing the control on the combustion processes and exhaust gases will contribute to safety and risk prevention; (iv) regulatory measures imposing the limitation of burning of nanowastes in open air in landfills are required.

4. Conclusions

The release of graphene nanoplatelets and multiwall carbon nanotubes from polylactic-based film at the end-of-life of wastes treatment was investigated during degradation and combustion/burning. The released airborne nanoparticles and the degradation of the nanocomposite film during an ultra-strong dynamic migration test were confirmed by different visualization methods (TEM, AFM, SEM). Thermogravimetric analysis in air atmosphere was used to simulate the combustion of nanocomposite wastes. It was found that single graphene nanoplatelets of nanosized thickness and length of 100–1000 nm, as well as their micron-size loose aggregates, indeed release in relatively large amounts from the PLA nanocomposite film at high temperature dynamic treatment due to partial degradation of the PLA polymer. However, the release of the entangled MWSNTs is possible only after full degradation (hydrolysis) of the PLA matrix polymer.

Combustion or burning at 500 and 650 °C result in residue ash, which contains mainly single airborne GNPs and MWCNTs, while at 850 °C, the small amount of residue ash (~0.07%) contains only GNPs and amorphous carbon soot. Therefore, the MWCNTs fully degrade at the heating temperature of 850 °C, while the GNPs still remain in the residue.

New concerns with the end-of-life nanostructured materials emerged by adopting the 3-factors, C.E.L. model for risk assessment. The consequences (C) were determined from the amount of the released MWCNTs and GNPs, and were graded according to the recommended exposure limit of carbon nanotubes, REL = 1 µg/m³, proposed by NIOSH. The exposure (E) and likelihood (L) were estimated based on the E-classification method. Four scenarios are discussed: biodegradation by composting, combustion, burning in open air and accidental fire, which may lead to “very high”, “hazard” and “high” risk, respectively. Such treatment of nanowastes may pose a potential release of GNPs and MWCNTs into the environment, with all their associated environmental and human risks presently not accounted for. Safety measures are proposed for the end-of-life phase of nanowastes in order to avoid or prevent the risks.

Author Contributions: In this study, the concept, analysis of results and writing of the manuscript were performed by S.K.; the A.F.M. visualization was conducted by E.I.; the methodology and manuscript text were examined by N.V. and E.I. All authors read and approved the final manuscript.

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Article

Evaluation of Reliefs' Properties on Design of Thermoformed Packaging Using Fused Deposition Modelling Moulds

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Abstract: The increased consumption of food requiring thermoformed packaging implies that the packaging industry demands customized solutions in terms of shapes and sizes to make each packaging unique. In particular, food industry increasingly requires more transparent packaging, with greater clarity and a better presentation of the product they contain. However, in turn, the differentiation of packaging is sought through its geometry and quality, as well as the arrangement of food inside the packaging. In addition, these types of packaging usually include ribs in the walls to improve their physical properties. However, these ribs also affect the final aesthetics of the product. In accordance with this, this research study analyses the mechanical properties of different relief geometries that can affect not only their aesthetics but also their strength. For this purpose, tensile and compression tests were carried out using thermoformed PET sheets. The results provide comparative data on the reliefs studied and show that there are differences in the mechanical properties according to shape, size and disposition in the package.

Keywords: packaging design; product design; mechanical properties; thermoforming; tensile test; 3D printing; simulation; technology

1. Introduction

Thermoformed food packaging, usually called rigid or semi-rigid containers, have as main functions protection, containment, preservation and distribution [1,2]. Different types of thermoformed packaging can be observed in the market according to the specific needs of the food. These include heat-sealable containers for processed or semi-processed products [3,4]. Packaging usually applied to fresh products, such as fruit or vegetables [5], all of which are therefore often used for products with a short life cycle and with the aim of protecting and making food more functional [6]. For this reason, during the development of these containers, the aim is to reduce the amount of material used to increase sustainability by reducing the large amount of waste generated [7]; and to optimise production costs while maintaining their functional properties [5].

Although distribution is one of their main functions [8,9], most of these packages reach the consumer, especially because of the new trend of food on the move [10]. For this reason, the design and finish of these packages must also be taken into consideration. Thus, the ergonomic and functional aspects of the packaging must be aimed at adapting the product to the consumer's needs for use and protection of the food it contains [2].

Throughout the short life cycle of freshly packaged food there are very different situations to which the packaging is exposed to external aggressions. This is linked to the sustainability of both the product inside and the cost of material involved. Thus, food packaging can delay and protect food from physical,

chemical and biological spoilage, that is, packaging can extend shelf life and ensure product quality [7] and therefore can be understood as a sustainability system for food. Light, humidity, microorganisms, shocks and other mechanical forces are examples of some of the external agents that can adversely affect food [2]. In general, both the handling of the package, its transport or its stacking on the supermarket shelf are considered external aggressions to the food contained inside before consumption [5]. Therefore, elastic deformation of the packaging may be required to preserve its content.

Specifically, the weight of the food generates tensile stresses in the walls. One of the situations where this occurs is when the container is suspended during transport or handling. Also, during transport the containers are normally stacked and this means that the container must also withstand the stacking weight. These mechanical forces cause a compressive stress on the container walls. Also, in situations where a user, whether a consumer or not, handles the packaging, a functional situation occurs where the packaging must protect the food [11].

According to these approaches, thermoformed containers usually incorporate patterns on their walls in the form of reliefs, which are used to give them some mechanical properties, without the need to increase the thickness of the plastic sheet used during the manufacturing of the packaging. In addition, reliefs can attribute a different geometric aspect by creating a semantic value on the product. However, the containers currently used in the market usually incorporate reliefs in the form of vertical ribs or columns, generally with square geometry.

A related point to consider is the package visual appearance, which influences the decision of consumption due to its symbiotic or simply aesthetic qualities [12,13]. In these circumstances, the container may be a key factor in the consumer decision-making, allowing inferences to be drawn about the product, like attributes or taste. Therefore, the package can influence subsequent experiences in the product so much so that researchers study its influence concerning materials, shapes and sizes [3,13–17], although only a few studies focus on the tactile sensation that a container causes. This is a new trend in packaging, such as in cosmetics or drinks [18]. As a designed texture or relief using differentiating factors can attract consumers as much as shape or colour, designing custom geometries is of utmost interest, although it may alter the functional properties of the package.

Given the above conditions, the influence of relief geometries on the mechanical properties of thermoformed sheet is studied and analysed in this work. By means of this method, the properties of the reliefs of the packaging can be evaluated in order to guarantee sustainability and also to reduce the expense of plastic material. Furthermore, the improvement of the mechanical properties of the containers also contributes to increase the useful life of the food. It should be also stressed that, conventionally, reliefs are not specifically evaluated until the physical package is tested. This means that design and development times can be increased by design modifications.

For this purpose, Fused Deposition Modelling (FDM), an Additive Manufacturing (AM) technology, is proposed for making economic moulds that allow the thermoforming of test specimens. AM refers as a general term to manufacturing technologies that build up a product layer by layer [19]. Since the 1980's, AM first started unsteadily and then moved from laboratory to industrial practice. New applications are constantly announced and they have been developed over time [20]. Thus, the applications of this technology have been increasing. Despite the fact that AM processes, such as Stereolithography (SLA), FDM or Selective Laser Sintering (SLS) were initially created for the purpose of generating rapid prototypes, it is currently sought to use them to create final products as well [21,22].

In the context of thermoformed products, moulds from additive manufacturing are being created nowadays [23]. Specifically, the applications focus on the study of this technology in the field of design and development processes, in order to create moulds for short series [24]. To do this, additive manufacturing is used to validate proposals as well as for research support, as it allows to generate moulds in a fast and economic way [25,26].

In the field of thermoforming, Laser Sintering is widely used. In this research, in contrast, the application of the FDM technology is considered since it is an affordable technology and accessible to any design team [27]. In effect, the use of FDM offers the possibility of creating moulds of high

quality, though it may also be slow and costly [28]. Thus, printers provide the possibility of generating moulds in order to create thermoforming prototypes in a rapid way, resulting in shortened deadlines and reduction of errors.

This work presents an experimental procedure that provides a novel scheme to evaluate the relief patterns designed on food packages with a double objective: to improve the mechanical resistance without increasing the quantity of raw material and to build more efficient products. Moreover, this evaluation technique, can be used with thermoplastic materials like Polyéthylène Terephthalate (PET), due to their predominance in disposable containers but can be extended to new biodegradable materials such as Bio Polyéthylène Terephthalate (Bio-PET) and Polylactic Acid (PLA). In addition, its application could be extended to other materials such as thin cardboard sheets.

In short, additive manufacturing allows new applications and procedures to emerge in the field of engineering, as is the case with the work proposed here.

2. Construction of Test Specimens

In this work, a study of the mechanical behaviour of reliefs has been carried out. Initially, the reliefs were evaluated as a unit, performing tensile tests with the aim of comparatively analyse the existing differences between geometries and relief sizes. After that, the influence of the position and number of the reliefs on the faces of a container, used as a test tube, was studied by performing compression tests.

The overall procedure for the manufacture and preparation of the specimens consists of several phases, as seen in Figure 1. Specifically, the generation of the specimen and mould in Computer Aided Design (CAD) was done by using the Solidworks® software (2016 version, Dassault Systèmes SE, Velizy-Villacoublay, France) and the 3D printing of the specimen was done with the Simplify3D® software (Cincinnati, OH, USA) for the generation of the G-code. For the manufacture of the mould of the specimen printed in FDM, a 3D printer machine Witbox® and PLA filament with a diameter of 1.75 mm have been used. The machine used for thermoforming of the sheet was the table-top thermoforming machine Formech 450DT. Finally, Minitab® software (18 version, Minitab Inc., State College, PA, USA) was used for the treatment of the statistical data.

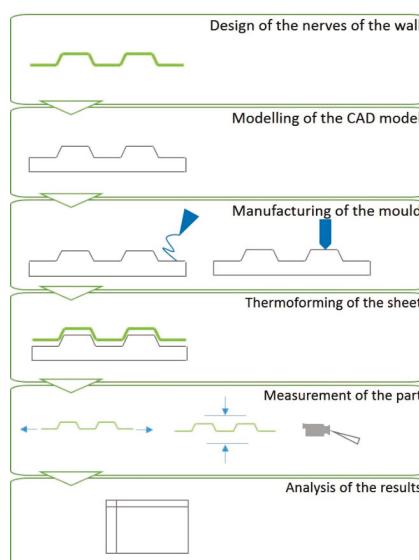


Figure 1. Methodological procedure.

2.1. Procedure for the Construction and Preparation of Tensile Specimens

In the case of the generation of tensile specimens, to ensure the flatness on the surface, a two parts hybrid mould was designed, Figure 2a. One part was common to all the specimens (labelled 1 in Figure 2a), consisting of a wooden profile with perforations along the perimeter to ensure that the sheet was fixed along the entire surface during the thermoforming. This profile also served as a cutting template to remove the excess of material to ensure repeatability during specimen creation. The second part corresponded to the mould of the specific specimen obtained by FDM (labelled 2 in Figure 2a) and it was fitted into the wooden profile to generate a mould with a flat surface, Figure 2b. This ensured that there were no roundings along the perimeter of the base of the specimen.

Then, Figure 2c shows the procedure for obtaining the final specimen. Once the specimen was thermoformed, the PET sheet was cut. The wooden profile was used to mark the cutting perimeter over the thermoformed sheet. To make the cut, a sheet shear has been used, according to [29].

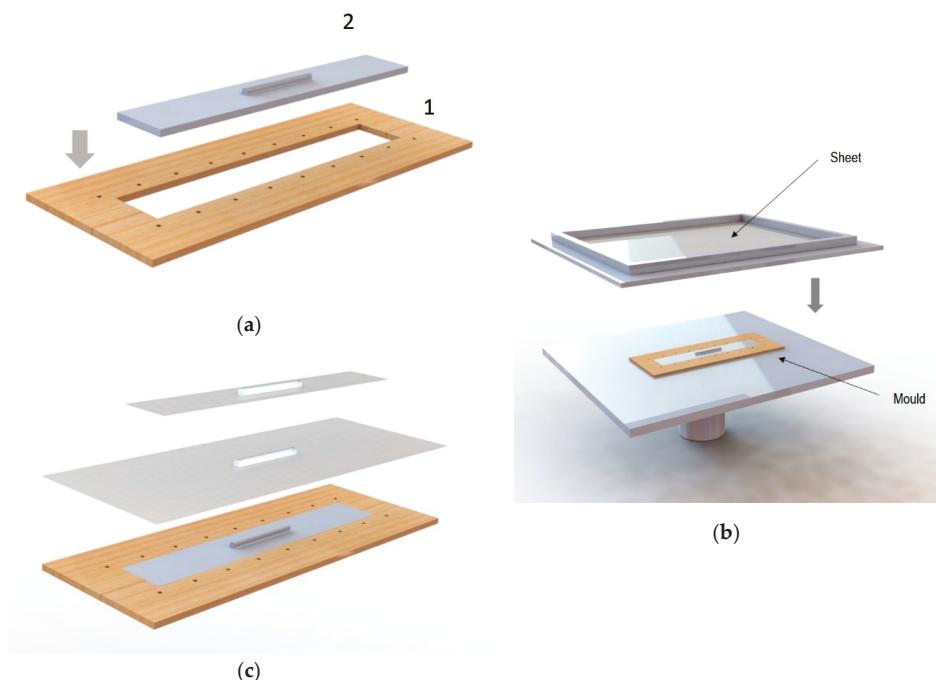


Figure 2. Thermoforming of specimens for tensile tests: (a) Hybrid mould; (b) Thermoforming of the sheet with hybrid mould to obtain the thermoformed sheet specimen; (c) Procedure for obtaining the thermoformed specimen.

2.2. Procedure for the Construction and Preparation of Specimens for Compression Tests

The specimens used for compression tests had a square shape. A mould made entirely of FDM, Figure 3, was used for their construction, as it had flat sides and this way it could be compared with the traction experiments.

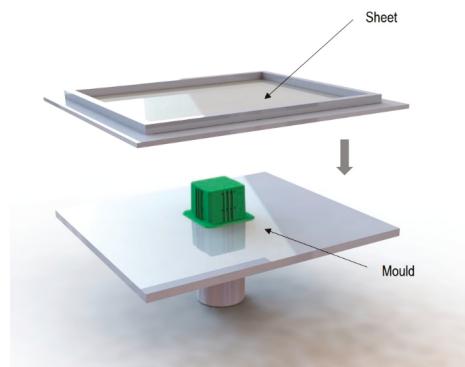


Figure 3. Thermoforming process of specimens for compression tests.

The generated mould, Figure 4a, contained a draft angle and a base with a 45° chamfer to avoid the appearance of defects on the thermoformed sheet, in accordance with [30]. It also contained vacuum channels to ensure proper attachment of the PET sheet to the mould. The channels have been made at three heights along the walls of the mould with an angle of 45° , Figure 4b.

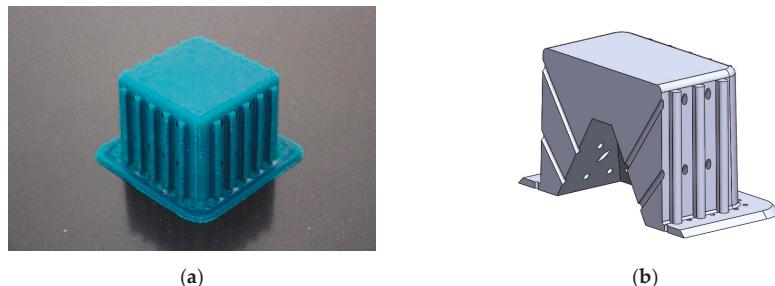


Figure 4. Example images of the mould used for thermoforming compression specimens: (a) image of the mould, (b) vacuum channels included inside the mould.

Once the thermoforming process had been carried out, Figure 3, the excess of material has been eliminated using the Iberolaser IL-1390 laser cutting machine. This cutting procedure was precise and left no relevant defects on the cutting surface.

3. Materials and Methods

3.1. Tested Material

The material used in this test was a three-layer PET laminate roll with a recycled PET sheet inside and the thickness used was 180 micrometres. This material is commonly used for food packaging in industrial applications. The material had undergone an extrusion manufacturing process. The properties provided by the supplier are detailed in Table 1, according to UNE-EN-ISO 527-3 [31] and DIN 53479-B [32].

Table 1. Properties of PET laminate.

Thickness	Surface Treatment	Tensile Strength	Ductility	Impact Resistance	Density
0.180 mm ± 3%	Silicone on both outer sides	>50 N/mm ²	220%	>3 KJ/m ²	1.33 gr/cm ²

3.2. Tensile Test Method

The main objective of these tensile tests was to deepen the knowledge of the behaviour of the different geometries in relation to the dimensions of the sheet protrusion. In addition, for the correct evaluation of the reliefs, a morphological study of the thermoformed geometries was performed. For this reason, the reliefs were included in a unitary way on each specimen.

3.2.1. Morphological Study

A total of 9 different types of test tubes, based on three different reliefs, were studied. On one hand, three basic geometries were analysed: semi-circular (A), square (B) and triangular (C). These geometries were transferred to the PET sheet in a straight line. On the other hand, three sizes or scale relationships were studied: a , $a/2$ and $2a$ where a was 3 mm in the designs, Figure 5. That particular value was chosen after analysing the reliefs of different commercial packages.

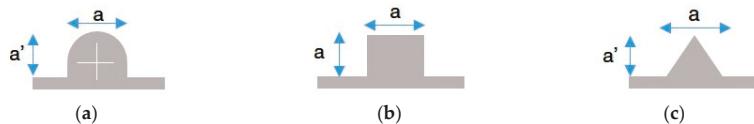


Figure 5. Geometries of the studied reliefs: (a) semi-circular, A; (b) square, B.; (c) triangular, C.

Obviously, the section, S , of these three geometries is different, directly affecting the mechanical properties, Equation (1).

$$\sigma = F_y/S, \quad (1)$$

where F_y corresponds to the axial force applied to the specimen, either in tensile or compression tests.

Sections were easily calculated as the chosen reliefs were simple geometrical shapes. Relief type A corresponded to a semicircle attached to a rectangle, Figure 6a. Relief B was chosen to be a square, Figure 6b, while relief C was designed as a triangle, Figure 6c. Their respective sections are:

$$S_A = \left(\pi * \frac{a^2}{8} \right) + a * \left(a' - \frac{a}{2} \right), \quad (2)$$

$$S_B = a^2, \quad (3)$$

$$S_C = (a * a') / 2 \quad (4)$$

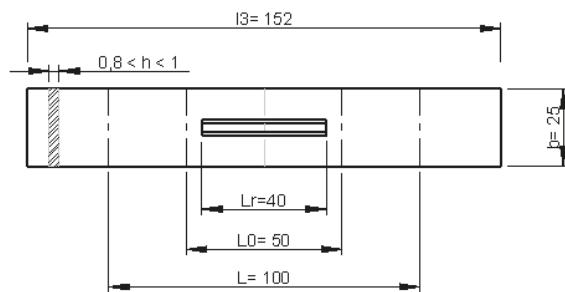


Figure 6. Dimensions of specimen according to standard [31].

3.2.2. Mechanical Characterization Study

In accordance with standard UNE-527-3 [31], Figure 6, the designed dimensions used for a' and l_3 in the test specimen corresponded to 25 mm and 152 mm, respectively. All the other relevant dimensions are depicted in Figure 7.

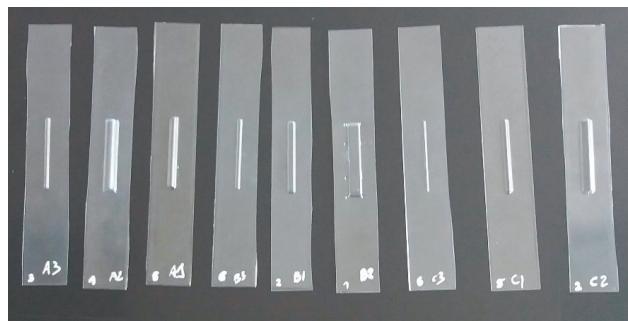


Figure 7. Thermoformed specimens.

The guidelines established in References [31] and [33] had been taken as a reference for carrying out the tensile tests. Thus, a total of 5 specimens per geometry were studied.

The machine used for mechanical testing was the equipment Shimadzu, model AG-X, with a load cell of 50 KN, Figure 8a. All test parameters were managed with the help of the universal test software Trapezium® for Windows®. For the development of the tests, plastic-specific jaws were used, Figure 8b.



Figure 8. Testing machine with clamps for tensile tests: (a) testing machine for the experimental (b) clamps with specimen in the middle.

After the laboratory tests, from which experimental data were extracted, simulations of the tensile tests using the Finite Elements Method (FEM) were carried out with the software Solidworks® and Hyperworks® Radios for geometric modelling and dynamic simulation, respectively.

Due to the fact that the range of displacement increases with the test time, the study time was defined at 6 s.

3.3. Method for Compression Tests

The objective of the compression tests, with a structure similar to that used for tensile tests, is to deepen the knowledge of the behaviour of the reliefs included on the walls of the packaging. The main idea of this study is to evaluate the influence of the number of reliefs on the packaging and the distance between them.

1, 3 and 5 reliefs had been inserted on each face in order to study their influence on the mechanical properties. In this case, the study was restricted to the study of type A geometry, Figure 5. All the reliefs were placed symmetrically from the centre of each face.

3.3.1. Macrogeometric Analysis

The moulds and the thermoformed packaging had been visually inspected to analyse the final result, Figure 9. Likewise, all the tests carried out had been recorded in order to study the behaviour of the specimens subjected to compression.

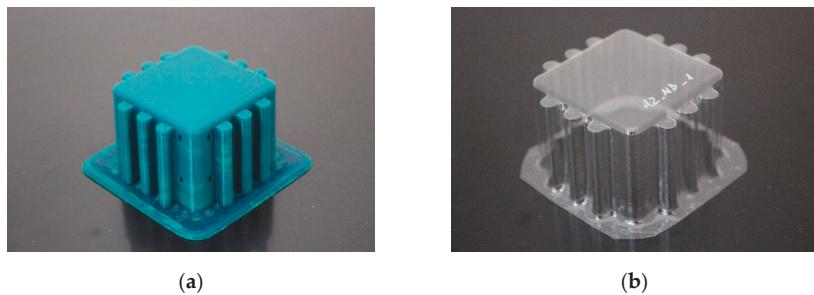


Figure 9. Example images of the results obtained: (a) mould A2_M3, (b) packaging created with mould A2_M3.

Two distances between reliefs had been studied: 3 mm and 6 mm. M1 being the test piece that included 1 relief, M2 and M3 corresponded to 3 reliefs, with a distance of 3 and 6 mm, respectively and M4 and M5 corresponded to the test pieces that had 5 reliefs, 3 and 6 mm, respectively. A2 geometry with 5 reliefs and 6 mm spacing was not evaluated because the size of the specimen face was too small to include these reliefs. Table 2 details the full nomenclature of the designed test specimens.

Table 2. Nomenclature of reliefs according to the type of relief, distance and dimensional correspondence.

Relief	Specimen	Nº Reliefs	Relief Dimensional Proportion	Relief Size (mm)	Distance between Reliefs (mm)
-	O2	0	-	-	-
A0	M1	1	$a/2 \times a/2$	1.5×1.5	-
A0	M2	3	$a/2 \times a/2$	1.5×1.5	3
A0	M3	3	$a/2 \times a/2$	1.5×1.5	6
A0	M4	5	$a/2 \times a/2$	1.5×1.5	3
A0	M5	5	$a/2 \times a/2$	1.5×1.5	6
A1	M1	1	$a \times a$	3×3	-
A1	M2	3	$a \times a$	3×3	3
A1	M3	3	$a \times a$	3×3	6
A1	M4	5	$a \times a$	3×3	3
A1	M5	5	$a \times a$	3×3	6
A2	M1	1	$2a \times 2a$	6×6	-
A2	M2	3	$2a \times 2a$	6×6	3
A2	M3	3	$2a \times 2a$	6×6	6
A2	M4	5	$2a \times 2a$	6×6	3

3.3.2. Mechanical Characterization

A total of 15 tests were performed, including the specimen test without reliefs. The specimens had a square base of dimensions 50×50 mm, according to [34]. Figure 10 shows an image with the dimensions of the specimen O2.

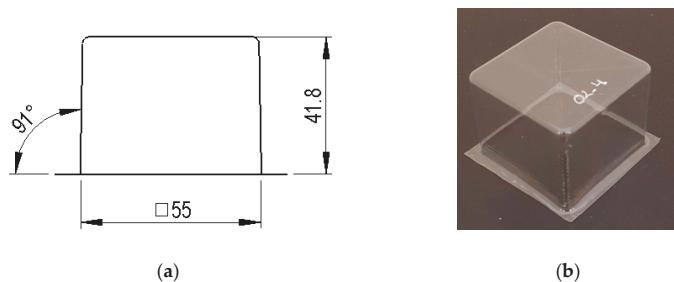


Figure 10. Images and dimensions of the plain test specimen, O2: (a) general dimensions; (b) test specimen.

The compression tests were carried out according to the guidelines established in Reference [34] and [35]. 4 tests were realized per test specimen typology.

The machine used to carry out the mechanical compression tests was the same used for the tensile ones, Figure 11. The load cell was set to 50 KN. As for the tensile tests, the test parameters were handled with Trapezium®. The compression speed of the tests was 10 mm/min, according to [35].

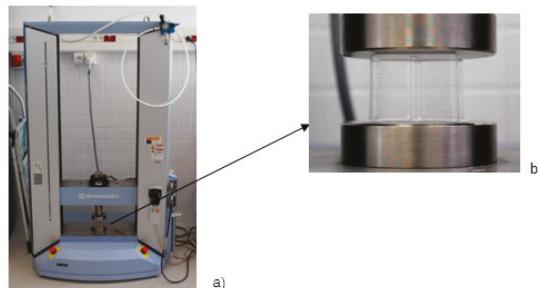


Figure 11. Compression tests: (a) general machine view; (b) specimen positioning.

The compression tests were recorded using a high-precision digital camera Canon EOS 650D. The recorded images of the compressed specimens were used to relate the real deformation to the measured stress-strain data. This is important, because the recorded axial force, F_y , could be overestimated if folding of the packaging occurs. Also, plastic deformation could be admitted if the packaged product was not affected by it.

The test procedure started with the placement of the specimens on the cylindrical platform of the testing machine, Figure 11b. The load cell approached the specimen and, once the machine had been calibrated, the compression test began. The control parameters set in the program were force in N, time in s and displacement in mm. After carrying out the laboratory tests, a case study was carried out using the same methodology as in the tensile tests, with one of the test pieces used to compare the simulation with the data obtained in the real tests. The simulation, as in the tensile tests, was carried out with Hyperworks Radioss® and Solidworks® where the base was established as fixed and constant speed was included in the upper side.

4. Results and Discussion

4.1. Tensile Strength

4.1.1. Mechanical Evaluation

Table 3 shows the measured section of geometries studied. A study of the thicknesses on the physical specimens was carried out to obtain the real section, bearing in mind that the material was stretched where the thermoforming process took place. According to this, the specimens presented a different tensile strength given by the type of area and volume generated.

Table 3. Results of the area of specimens and tensile strength.

Relief	Measured S (mm^2)	F_y (N)	Standard Deviation (N)
A0	4.60	187.24	15.87
A1	4.82	163.49	22.04
A2	5.31	109.75	15.02
B0	4.68	182.78	22.56
B1	4.73	128.53	17.74
B2	5.63	112.71	16.07
C0	4.56	184.06	30.90
C1	4.66	180.38	16.14
C2	4.93	112.84	10.09

As can be seen in Figure 12, geometries A0, B0 and C0 provided higher force values compared to A2, B2 and C2. This is related to the fact that a smaller section provides a greater wall thickness after thermoforming due to the lower stretching suffered by the specimen and generates greater rigidity to the relief.

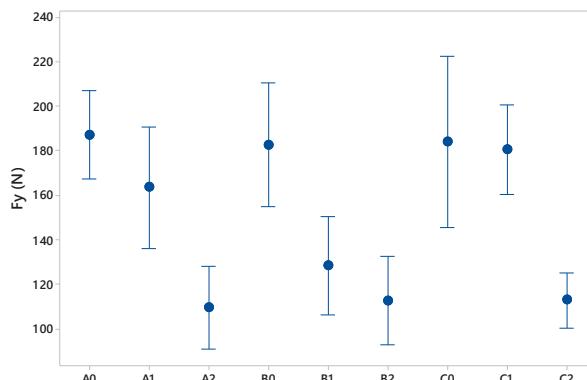


Figure 12. Dispersion of F_y in tensile tests.

Indeed, for the smallest packaging, the values reached forces around 185 N, although it is true that it is the A geometry that seems to maintain a lower dispersion in the repetitiveness of the tests. This phenomenon is especially visible in the results for the B0 and C0 reliefs, although it is in the latter geometry where the dispersion of the results is greater, with values of up to 35% lower than the established maximum. This could be due to the fact that the vertices of the square and the triangular geometry act as stress concentration points, which could lead to defects and micro-cracks that lead to premature failure.

Size 1 presented intermediate force values to those compared for size 2 and size 0 with greater variability in the averages obtained. Thus, C geometry presented values close to those reached for the smallest relief with an average of approximately 180 N. However, B geometry obtained values closer to those found in higher relief tests with an average of about 130 N. This seems to reinforce what was previously discussed with respect to the size of the section.

Size 2 presented mean values of about 110 N, about 40% lower than the other sizes. In a deeper analysis of the results, the geometry 2 tests showed values between 90 N and approximately 130 N with smaller dispersions than in previous cases.

Summarizing, the nominal stress analysis shows the trend followed by each A, B and C geometry as a function of their relief. In all three cases there is a tendency for the stress to decrease as the relief increases in size. However, as discussed, the C1 case shows a different trend because its section is proportionally smaller than in cases A1 and B1 and similar to the values obtained for size 0.

4.1.2. Dimensional Evaluation

Due to the fact that the base of the specimen influences the result of the tests, dimensional analysis has been carried out isolating the stress of the relief by means of the dimensional relation given by Equation (5):

$$\sigma_{y_relief} = (\sigma_y * S_{rel}) / S, \quad (5)$$

where S is the real section of area of the specimen and S_{rel} is the real section area of the relief.

Figure 13 details the results obtained according to the middle section, by calculating the stress from the force and area of the relief. It is observed that the geometries A1 and C1, which contain the smaller reliefs, supported a greater tension, especially C1, considering its size. This reinforces the results obtained previously for circular and triangular reliefs with less size. On the other hand, it can also be seen that the three largest geometries bore less stress, as seen in previous sections, thus highlighting the importance of the relationship between the area of the specimen and the relief.

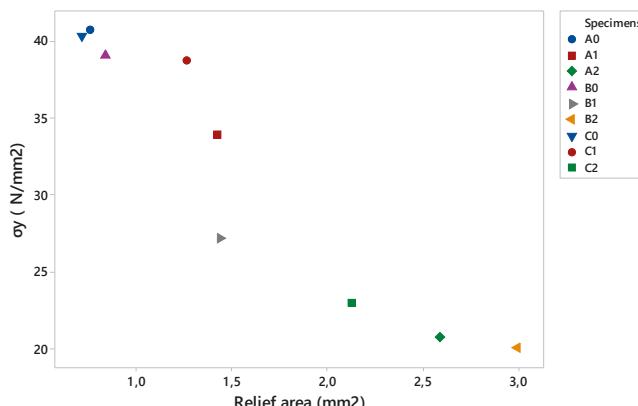


Figure 13. Data of the yield stress with respect to the section of the relief.

To try to have a detailed view of the results by taking into account only the geometry, the dispersion of the results obtained in Figure 14 is shown.

Regarding the results for size 0, Figure 14a, it is observed that the differences of F_y are minimal according to relief and size. This may be due to the fact that the area of the relief with respect to the specimen is minimal and therefore has less influence on the base geometry.

The results of the tests with the specimens with relief size 1, Figure 14b, evidence that there are differences with respect to the dimension of the relief. They also show that the C1 geometry withstands the highest stress and that B1 has the lowest tensile strength.

Finally, Figure 14c shows the results for size 2. The A2 and B2 reliefs present similar creep stress despite the dimensional differences between them, although the triangular geometry, C2, presents greater strength.

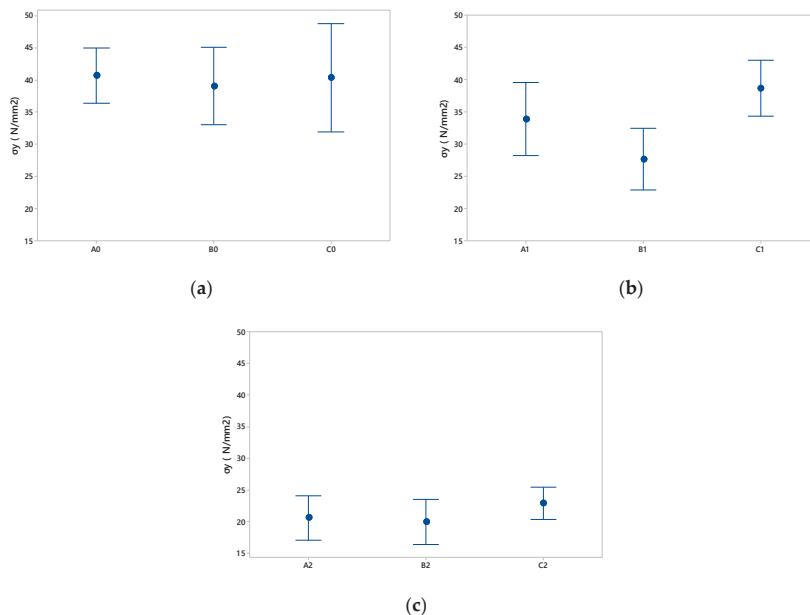


Figure 14. Comparative graph of the average results obtained for the yield stress of the three types of relief (A, B and C): (a) for the lower relief measure 0, 1.5×1.5 mm; (b) for the lower relief measure 1 of 3×3 mm; (c) for the relief measure 2 of 6×6 mm.

4.1.3. Simulation Validation

In general, the curve obtained in the different geometries is partially shifted to the left with respect to the experimental ones, probably due to the placement of the specimen in the testing machine, Figure 15. Another explanation can be given by the flexible characteristic of the specimens where the initial tension varies at the beginning of the test. In this way, it is observed that the specimen began to stress when the jaws move less than 1 mm, that is, there was a delay reflected by the described displacement.

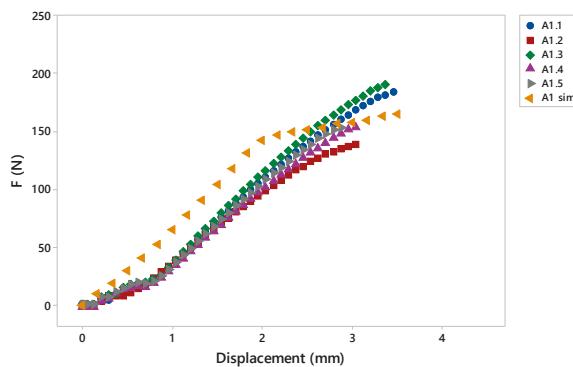


Figure 15. Example comparing the results obtained in the simulation test and the experimental studies.

On the other hand, the average values of σ_y obtained experimentally from the five tests and the values obtained in the simulation are detailed in Figure 16. Following [36], it is possible to relate the values obtained in the simulation with respect to the tests using the following equation:

$$Er = \frac{\text{Test value} - \text{simulation value}}{\text{test value}} \times 100, \quad (6)$$

where Er is the relative error.

In view of the results obtained, it can be considered that the simulation model adequately reproduces the mean specimen rupture with a relative error below 2% for circular and square geometries and slightly higher for triangular geometry specimens. This may be due to the concentration of stresses in the main corner of the triangular specimen as a consequence of the scale of the meshing and the simplification of the geometries, this being a singular point of study that shows a distorted behaviour in comparison to the rest of the reliefs.

The graph in Figure 16 shows that the C0 and C2 specimens, both with triangular geometry, are the ones with the greatest relative error for the reasons discussed above, although it is the C2 type specimen that lies outside the range of dispersion obtained experimentally, being the only set of tests under these conditions.

It should be noted that for general purposes the simulation results comply to a large extent with the experimental results validating the simulation methodology applied.

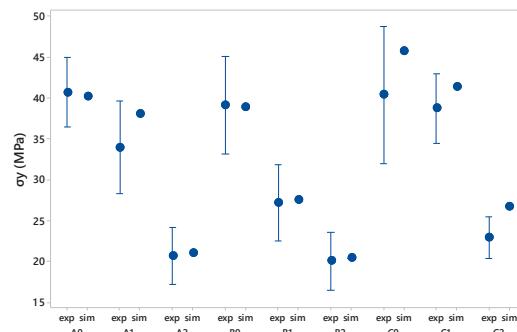


Figure 16. Comparative results of the experimental study (exp) and the simulation carried out (sim) for the yield stress.

4.2. Compression Tests

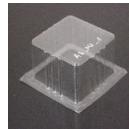
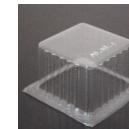
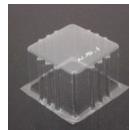
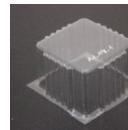
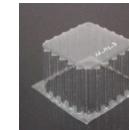
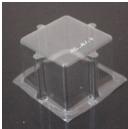
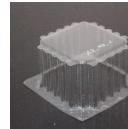
4.2.1. Visual Characterization

As shown in Table 4, in general, for the same size of relief, the film adapts better to the contour of the plastic mould for bigger separation of the reliefs. This is due to the stretching of the film. Thus, the lack of definition that occurs when the reliefs are located at a shorter distance can cause the compressive strength of the container to be reduced.

Similarly, the relief size also affects the type of adaptation of the film on the reliefs. Thus, the larger the relief size, the poorer the definition of the geometry obtained after thermoforming. According to [37] and [38], this is due to the fact that the machine has to exert a greater force to adapt the sheet to the geometry, also producing greater stretching. Thus, in the smaller geometries, A0 and A1, the sheet adapts to the relief, while in the A2 geometry, with a height of 6 mm, there is less definition in the intermediate spaces between reliefs.

It is observed that in the lateral walls the thickness of the sheet was reduced considerably being the part of the sheet where the greatest stretching took place. Therefore, the smaller the distance between reliefs, the less defined the relief geometry.

Table 4. Kinds of specimens made according to the number of reliefs and disposition.

	M1	M2	M3	M4	M5
A0					
A1					
A2					

4.2.2. Mechanical Evaluation

The force in the tests made on the thermoformed specimen without reliefs, O2, presented an average F_y of 5.13 N, Figure 17a. The standard deviation presented an interval amplitude range of 1.18 N. According to the images collected in the test video, this deviation in the results was due to the fact that the container began to deform on the walls and folds were produced that could result in a different F_y . Thus, it was observed that, when there was a displacement of 0.5 mm, the container was deformed but no folds were observed. At that moment, the average force collected was 3.10 N and its deviation was 0.43 N, Figure 17b. From the data collected, it can be seen that the 3 sizes, A0, A1 and A2, improved the $F-\epsilon$ properties with respect to the O2 container, although it is true that A2 shows higher values than the rest. Comparing the results obtained by separation and reliefs, the graph shows that slightly higher results are obtained when the reliefs were arranged with a separation of 6 mm (M3 and M5) conserving the same number of reliefs per face: M3 with respect to M2 and M5 with respect to M4. This phenomenon was in good agreement with the videos studied since the greater the relief, the less the deformation of the walls was, due to the fact that a greater distance between reliefs favoured the sheet adaptation to the mould during the thermoforming process.

On the other hand, it should be pointed out that, although A2 has the highest values of force with respect to A0 and A1, it stands out for reflecting higher deviations, especially in A2-M2 and A2-M3, indicating that the behaviour of these containers was more irregular when tested as a consequence of having a higher relief height.

In Figure 17b, it is observed that the recorded force data, for a 0.5 mm of displacement, have greater homogeneity when compared at the same point and not at the yield point, where each test shows different values. Thus, in this case, the results show a similar trend in terms of behaviour based on geometry, relief and separation.

In addition, the dispersion of the data is considerably reduced, which indicates that the tests carried out had a greater homogeneity in the first stages of the test, making possible to clearly distinguish the package that presented better properties. Also, it should be noted that, for deformities greater than 0.5 mm, the packaging could lose its functional properties, thus deteriorating the product contained inside.

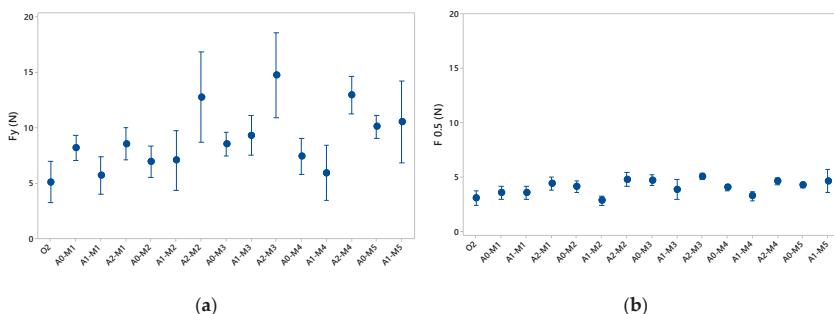


Figure 17. (a) Compression forces at stress yield; (b) Compression forces for a displacement of 0.5 mm.

4.2.3. Case Study of Validation by FEM

Figure 18 shows that the compression curve obtained by simulation for the A1-M1 specimen is within the range of the experimentally measured values. When a displacement of 0.5 mm occurred, the obtained force data was also homogeneous with respect to laboratory tests.

Thus, the relative error, according to Equation (6), is 0.14% with respect to the mean data. It is therefore within the dispersion value collected in the performance of the 4 experimental tests.

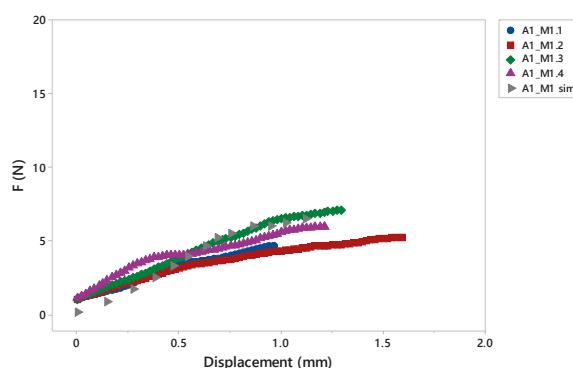


Figure 18. Comparative graph of the results obtained in the compression test by FE.

4.3. Relationship between Tensile and Compressive Tests

Figure 19 shows the area graphs that relate the force data obtained in the tensile tests, F_y-T , where the reliefs have been studied in a unitary way, with respect to the results of the compressive strength in two stages, $F_{0.5-C}$ and F_{y-C} , according to the number of reliefs included per face. Figure 19a relates the results of the F_y-T with respect to the force at the moment when the displacement has reached 0.5 mm. On the other hand, in Figure 19b the performance is made with respect to the force to compression at the creep point, F_{y-C} .

It is observed that the most favourable data of traction and compression, for the force at the moment of 0.5 mm of displacement, were collected with 3 and 5 reliefs per face, Figure 19a. In the case of the F_{y-C} , Figure 19b, data reflects that the results that obtain an equilibrium of compressive force between 8 and 10 N in addition to good traction results are the containers presenting 5 reliefs per face.

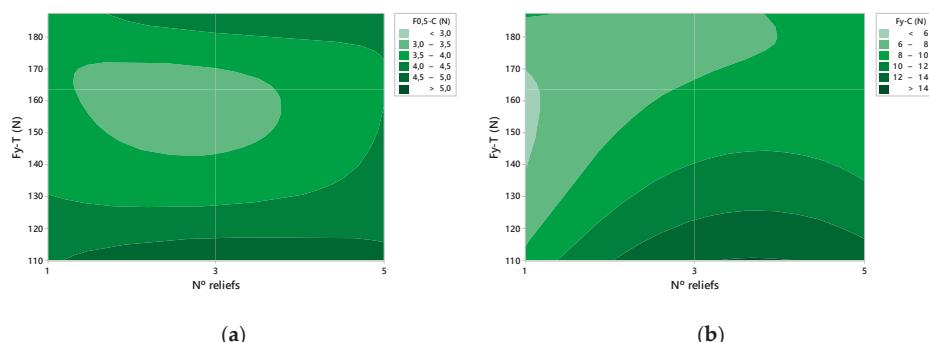


Figure 19. Graph of the compression force, $F-C$, in relation to the number of reliefs per face and the tensile force at the yield point, F_y-T , (a) at the moment of displacement of 0.5 mm, $F_{0.5-C}$ (b) at the yield point, F_{y-C} .

5. Conclusions

The physical tests carried out show that, the higher the relief, the lower the tensile strength compared to smaller sizes. This may be due to the stretching of the sheet on the side walls. However, it provides greater rigidity to the container by favouring compressive strength by introducing relief patterns on the surface of the thermoforming container.

From the geometries studied it can be observed that the semi-circular geometry, A and triangular, C, are the ones that present the best results. Also, the semi-circular geometry, A, adapts better to the shape of the mould since the shape of the relief has no edges.

The analysis carried out shows that the main structural factors are the relationship between the width of the relief and its height. In addition, the type of geometry performed affects the mechanical properties. Likewise, from the comparison of the physical tests and the simulation it is concluded that the correct positioning and tension of the specimen on the testing machine influences the displacement registered in the laboratory tests.

Thus, it can be stated that, by simulation tests, a virtual evaluation method can be established as a basis for the optimization of the design applied to thermoforming packaging. In addition, validation by means of FEM tests gives rise to the possibility of testing new reliefs with more complex geometries. Therefore, it is proposed that, by means of the individualized study of the behaviour of the reliefs, it is possible to compare their mechanical properties.

Moreover, it was also possible to develop a method that has allowed satisfactory results after the compression tests carried out. The results obtained show that the correct design of the reliefs, according to the number of reliefs used and their disposition, can favour the improvement of the

mechanical properties of the containers. Specifically, the reliefs with greater distance increase the resistance of the packaging.

In comparison with the conventional design process of thermoforming packaging, this new procedure, aimed at the study of reliefs using low-cost moulds of AM, facilitates the realization of more innovative and efficient designs through the study of geometries, number of reliefs and their positioning. In this sense, it is possible to design containers with lower material costs by improving the mechanical properties using materials of reduced thickness and increasing the protection of the food.

Along these lines, a field of study was opened on the inclusion of complex relief patterns on thermoformed surfaces. The realization of complex patterns can be possible by means of the application of FDM moulds. Also, these moulds could be used to make cut series and thus improve personalization and brand identity. In short, this work presents a tool for designers that facilitates customization, eco-design and allows them to optimize their mechanical properties.

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Article

Custom Design of Packaging through Advanced Technologies: A Case Study Applied to Apples

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Abstract: In the context of food packaging design, customization enhances the value of a product by meeting consumer needs. Personalization is also linked to adaptation, so the properties of the packaging can be improved from several points of view: functional, aesthetic, economic and ecological. Currently, functional and formal properties of packaging are not investigated in depth. However, the study of both properties is the basis for creating a new concept of personalized and sustainable product. In accordance with this approach, a conceptual design procedure of packaging with personalized and adapted geometries based on the digitization of fresh food is proposed in this work. This study is based on the application of advanced technologies for the design and development of food packaging, apples in this work, in order to improve the quality of the packaging. The results obtained show that it is possible to use advanced technologies in the early stages of product design in order to obtain competitive products adapted to new emerging needs.

Keywords: food packaging; customization; product design; personalized design; reverse engineering; computer aid design (CAD); fused deposition modelling (FDM)

1. Introduction

During the last decade, the demand for healthy and fresh food, especially fruits and vegetables, was gradually growing in a context where eating and consumption habits were constantly changing due to the society lifestyle. For this reason, the European Union raised new objectives for the food packaging industry: sustainability of raw materials, minimization of waste, reduction of energy consumption during the production process, minimization of environmental impact, recyclability of packaging and littering reduction [1–3].

Besides, consumers demand specific needs, mainly related to the design and adaptability of packaging [4]. Among others, providing more nutritional information on the packaging, greater food security and less risk to health are requested [5–7]. Thus, there are studies that place the packaging of fresh product as the second reason for choosing a product where factors such as comfort, appearance, transparency and texture should be considered [5].

Consequently, regarding the selection of material, thermoplastic polymers comply with all of these conditions, which is why they have been chosen by manufacturers of different products as materials for their packaging [8]. Polyethylene terephthalate (PET) is a polymer whose properties include its mechanical resistance to both impact and chemical products, its transparency, its lightness, the reduced demand for energy in its manufacture and transport, its mouldability and its recyclability [8]. In addition, it is the most recycled plastic in the world, and the European Food Safety Authority has corroborated that PET does not contain bisphenol-A (BPA), phthalates or dioxins [2].

However, PET has been identified as one of the main causes of global environmental degradation and this problem is expected to increase due to growing demand from developing or re-industrializing

countries around the world [9–11]. For example, China, which is one of the largest exporters as well as producers, accounted for 24% of the world's demand for PET plastic in 2016. For this reason, understanding the consumption needs of this type of market is critical when examining the prospects for global PET volume growth [12].

In fact, the clear trend towards the increase in consumption of food that needs packaging carries with it the constant development of materials and techniques that improve the performance of this service [13]. In short, several aspects can be highlighted [14]: the improvement of the production times, the reduction of the material and the improvement of its aesthetic and functional properties.

Thus, the fresh food packaging industry is interested in developing efficient and innovative solutions to ensure the quality of the products by taking into account their sustainability, especially at the environmental level [12]. For this reason, the design evaluation in the development of sustainable products should include aspects related to the design, manufacture and use of the packaging [15,16].

In this context, the packaging design process implies the consideration of aspects associated with its cost, appearance, usability, manufacturing, sustainability, standards or competitiveness [15]. Therefore, the selection of the manufacturing process of the food package is extremely important and, in this case, one of most commonly used is the thermoforming process [17]. Previous research on the packaging design process in thermoforming focused on the study of the moulds and the materials used in the process [10,18–20]. Also, recent research implements functions for intelligent packaging development through which sensitive labels control the condition of the food [21]. These initiatives are aimed at improving food health and freshness, achieving in this way its better preservation [4].

On the other hand, the packaging sector demands customized solutions in terms of shapes, sizes and colours, so that each packaging solution is unique [22]. In turn, it is intended to pursue product differentiation by means of sustainable products and new designs [23]. In such a way, it is also possible to respond to demographic changes and consumption habits [24–26]. Thus, packaging can be personalised in design, brand and/or size, among other characteristics. Also, it can be understood that an adapted packaging is the one that adapts itself to the inner shape and size of the product [27].

However, despite the needs that were determined in previous research and after having analysed the fresh food packaging which is currently commercialised on the market, it is observed that the majority of them are standard and just a few include customization in terms of forms [28]. In addition, there is no adaptation to specific sizes according to calibres in these cases.

For this reason, this work studies the personalization and adaptation in packaging design for the protection of the product in order to provide designers with a tool for the packaging 4.0 generation. This is linked to the sustainability of both the interior of the product and the material expense. A case study with apples is shown in order to validate the use of advanced technologies as part of the unconventional design of packaging, increasing the sustainability and functionality of these products. Thus, a technique that allows the design of personalized packaging to optimize the cost of packaging material, the technological resources and to improve the functionality of packaging is developed. The research also focuses on obtaining packaging that offers brands the possibility of differentiating themselves by means of personalization and in accordance with sales expectations and consumer perception.

2. Materials and Methods

2.1. Tools and Materials Used to Obtain the Customized Packaging

To carry out the experimental development, apples were used as the target product because their size facilitates the acquisition of measurements, studying the adaptation to packaging depending on two different calibres: category I and category II, according to [29].

For the development of the experimental procedure, 10 units of each calibre were used. To carry out the design-adapted concept from the computer-aided design (CAD), the apples were digitized by means of 3D techniques [30], Figure 1. To this end, 8 images were captured for each unit to create

a three-dimensional model, Figure 2. An SLS-1 David® 3D scanner (David Vision Systems GmbH, Koblenz, Germany) of Hewlett-Packard (HP inc.) was used, according to [31]. These scanned elements have, as their main purpose, the creation of adapted geometries through the generation of curves based on the scanned elements.

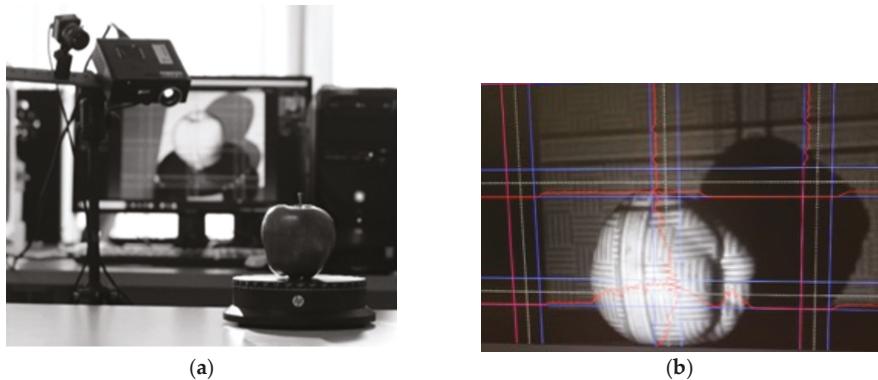


Figure 1. (a) Scanning procedure using the SLS-1 David® V5 scanner, (b) Visualization of the apple through the software (HP 3D Scan David®, version Pro V5, HP inc., Palo Alto, CA, US).

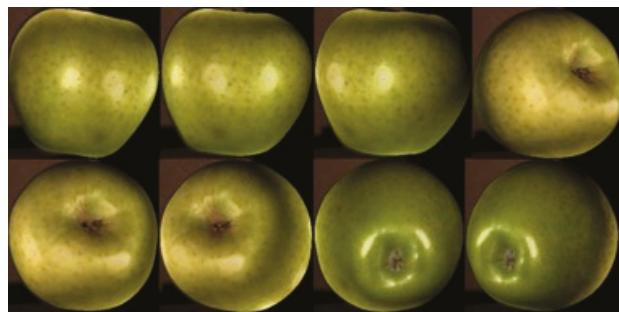


Figure 2. Example of image capture, which the 3D scanner performs, of an apple of calibre 1.

Thus, the concept development was carried out through CAD software, Solidworks® (2016 version, Dassault Systèmes SE, Velizy-Villacoublay, France). As a result, the development of packaging design has been simplified in time and has allowed us to generate more complex and personalized forms for the food.

The evaluation of the design proposals was validated through the generation of reliable prototypes. The mould design and The Standard Triangle Language (STL) file of the mould were generated by Solidworks® and were then parameterized using software for 3D printing, Simplify3D® (Cincinnati, OH, USA). A Gcode file was generated for printing in the FDM machine BQ Witbox (Mundo Reader S.L., Madrid, Spain), that uses a diameter filament of 1.75 mm. A PET sheet of 500 μm thick was thermoformed to generate the prototype with Formech 450DT using the FDM mould, Figure 3.

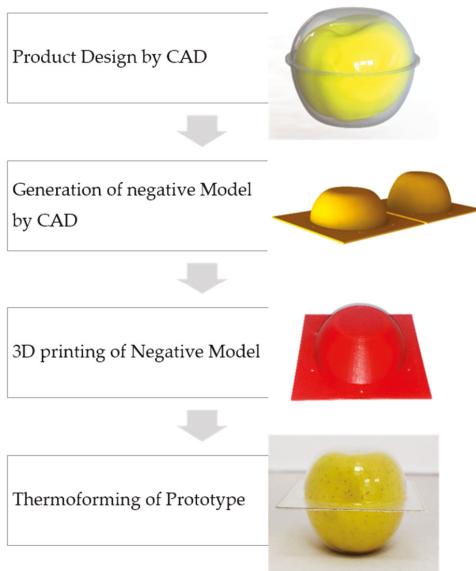


Figure 3. Generation of prototypes in thermoforming with moulds created by FDM.

2.2. Parameterization of the Packaging Design

Figure 4 details the procedure carried out for the design and development of customised and adapted packaging. Once the conceptual design of the package has been carried out for this case study, the properties of these products are studied through the application to scanned apples, in order to define the main parameters to be taken into account. These data were used for two purposes: packaging design using CAD tools and parameterization of the final geometry. Then, the parameterized package was validated by prototypes made with FDM moulds.

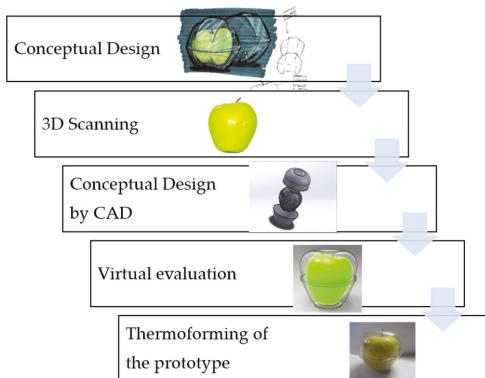


Figure 4. General procedure used to obtain the final package.

Also, several functional measures of each natural product were evaluated to analyse the differences between them, also using Solidworks® software. These dimensions were selected according to the parameters established for the calibres: the largest diameter, D_m , and the maximum height, H . According to this, two measurements were collected for each of the dimensions studied: L_{01} and

L02 for Dm and L03 and L04 for H, Figure 5. It should be noted that L01/L02 were made in the two directions of the maximum diameter of the fruit and L03/L04 for the two highest recorded heights. This allows the calculation of the variation of the measurement between pieces of fruit.

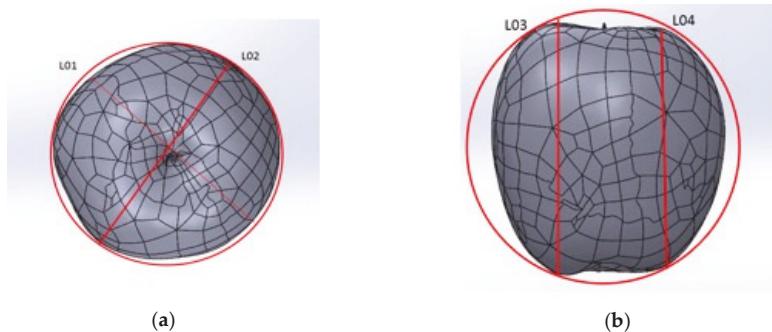


Figure 5. Measurements collected on the digitized products: (a) width measurements, (b) high measurements.

One of the objectives of digitizing these elements, because of the normal variations of a natural product, is to define the range of measures that present representative variations that must be taken into account for the design of the packaging. As a result, comparative tables were obtained and the dimensional range was defined, which will serve to obtain the adaptation parameters on the design of the packaging, which is the object of study.

Once the concept was generated, the design was developed in Solidworks® using the 10 scanned elements as a means of generating the construction curves. In accordance with this, the set of lines and tangent arcs, which together form the design of the idea previously conceptualized, were defined. Likewise, the numerical relations between the different container geometries were defined, using as relation parameters the maximum height, H and the maximum diameter, Dm, of the container.

Then, when the final design was developed in Solidworks®, the relationship equations, defined above, were introduced in order to evaluate the degree of adaptability through this type of digital tool. Then, the variable measures of the packaging were defined in order to carry out the adaptation to the two categories of size of apple studied according to [31].

Finally, the adaptability range of the design created for this practical case was established and, in addition, the degree of adaptation of the dimensions obtained with each of the digitalized units for the two calibres studied were evaluated. Figure 6 shows an example of the results obtained.

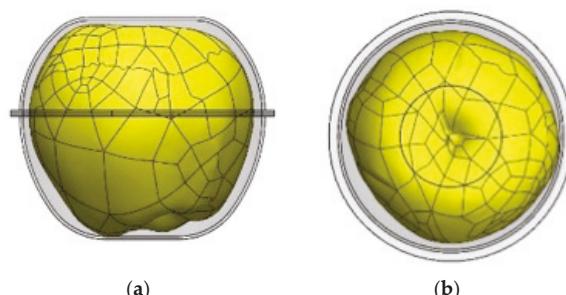


Figure 6. Example of the result of the adaptation parameters with respect to the digitized product: (a) evaluation of the high packaging designed, (b) evaluation of the width of the packaging designed.

The two calibres studied were evaluated through the creation of a reliable physical prototype using FDM moulds for thermoforming of the sheet. The developed prototypes were then used to validate the dimensions obtained by introducing real apples. In total, 20 apples were used for each calibre at this stage and the selection of each of them was made taking into account shapes and size variations. Also, different types of varieties were included.

3. Results

3.1. Virtual Evaluation of Digital Elements

As described above, the study was conducted for two types of calibres, according to [29]. As seen, the calibre refers to the predominant size within the packaging and is defined according to the maximum equatorial diameter [32]. Thus, the apple samples were scanned to generate a parametric model of each one to make the measurements according to the methodology. The data obtained from the samples studied are detailed in Figure 7.

From the results obtained from the study of the morphology of apples it is determined that the dominant geometry of the fruit is slightly oval. Therefore, a major axis, L01, and a minor axis, L02, can be defined in order to name the maximum dimensions of the digitized samples. It is worth mentioning again that L01 and L02 correspond to the average dimensions of the width of the apple.

On the other hand, L03 and L04 are the height measurements collected on the digitized elements. Figure 7 shows that, generally speaking, calibre 1 (category Extra) is larger than calibre 2 (category I). For calibre 1, parameter L01 lies between 83 mm and 85.5 mm, while L02 varies between 80.2 mm and 83.75 mm, Figure 8a. This shows the disparity of measurement for apples of the same calibre, intrinsically affecting their standardisation for subsequent parameterisation.

Regarding the height of the apple, for parameters L03 and L04, the aim is to find the maximum per calibre of the apples. In this case, L03 is the larger dimension with measures between 77.7 mm and 88.16 mm.

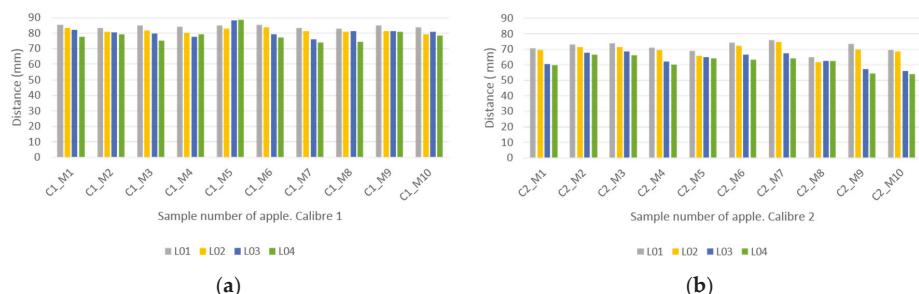


Figure 7. Measurements collected from scanned parametric models of apple samples: (a) calibre 1, (b) calibre 2.

As for calibre 2, in Figure 8b, the measurement intervals tend to increase according to standard (CE) N° 85/2004 [29]: 5% for calibre 1 and 10% for calibre 2. As for the measurement results and because parameter L01 is predominant from the point of view of packaging design, a measurement range between 69.4 mm and 75.9 mm is observed. Likewise, as far as the maximum height is concerned, parameter L03 also plays a part in the design and varies between 56 mm and 68.5 mm.

On the other hand, Figure 8 shows the mean data for the four parameters with their standard dispersion. In both cases, the measurements show a greater dispersion for the parameters L03 and L04, being slightly higher for the apples of calibre 2. L01, which has a greater influence in the design of the package, exhibit more homogeneity than the other dimensions.

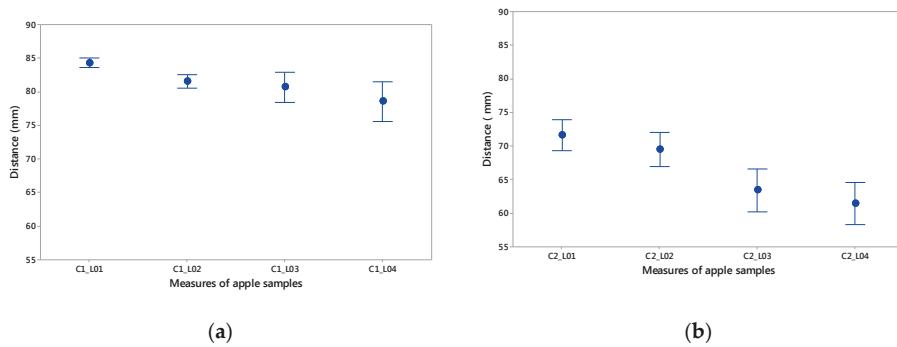


Figure 8. Mean data for parameters L01, L02, L03 and L04 with measurement dispersion: (a) calibre 1; (b) calibre 2.

Analysing the data presented so far, it can be deduced that the sizes of the packages of a certain calibre can be grouped in a dimension that encompasses all sizes of apple inside a category, including the difference between all the fruits of the same type and calibre. Therefore, the variations in the samples that affect the design of the packaging are the maximum width and height obtained from grouping the digital models.

For calibre 1, the maximum measurement within the calibre established according to the standard and with a tolerance of 5% [29] was 85 mm. For virtual measurements, a maximum diameter of 86.7 mm was obtained, Figure 9a. For calibre 2, with a maximum nominal size of 73 mm and a permitted tolerance of 10% according to [29], 78 mm was obtained as maximum diameter for the virtual measurements, Figure 9b. These dimensions served as starting points for the dimensional study of the container, although these dimensions could be reduced due to the irregular geometries.

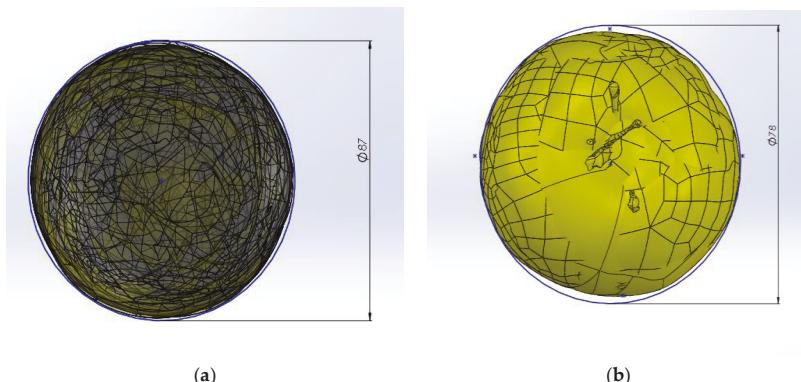


Figure 9. Overlap of the 10 apple units to establish a common diameter based on the sample: (a) larger size 1; (b) size 2 with dimensions between 63 and 73 mm.

Although all apples are included in the same diameter, the plant shape is slightly oval, as discussed previously. Thus, the linear dimension on the plant in one of the sides is lower with respect to its

perpendicular components, L02 and L01 respectively. According to this, a dimensional relationship, Dr, was established for the diameter, according to Equation (1):

$$Dr = \frac{L01}{L02}, \quad (1)$$

Thus, from the data obtained in the 20 case studies corresponding to calibres 1 and 2, a dimensional relationship was established between both distances of 0.97 and 0.98, respectively, Figure 10. This relationship was used for the design and parameterization of the packaging by CAD, giving rise to the final geometry of a non-cylindrical container.

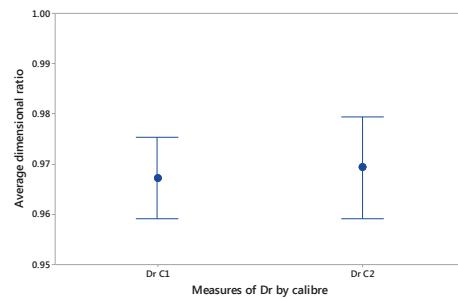


Figure 10. Average dimensional ratio between dimensions L01 and L02 for calibre 1 and 2.

It is important to bear in mind that these dimensions were studied at an experimental level. The aim is to propose a method in which, using scanned elements, designs can be generated. To this end, a clearance coefficient, that can be applied to the dimension of a given calibre, Cd, was proposed.

Analysing the dimensional results of the three-dimensional models of the scanned apples and the measurements according to the norm, a particular Cd can be defined for the design of a packaging. This coefficient was defined as the ratio between the observed maximum dimension per calibre according to the norm, and the virtual dimensions studied. Consequently, this definition makes it possible to ensure that the size of the containers is adapted to all geometries included within a calibre.

As an example, if, for calibre 1, the maximum diameter allowed is 89.25 mm including tolerance, and the maximum diameter that appears as a measure of nominal calibre is 85 mm, then Cd could lie between 1.05 and 1.06. However, because of the differences that naturally arise in fresh foods, 1.06 was considered for use to ensure proper functioning. Thus, the validation of this coefficient was carried out by implementing this coefficient in the development of the adaptation of calibre 2.

Therefore, the calculation of packaging dimensions can be done according to the following equation:

$$Dm = Cd \times Cm, \quad (2)$$

where Cm is the maximum nominal size of the calibre, Dm is the width of the packaging and Cd is the clearance coefficient.

Then, for designing the packaging for calibre 1, Dm is 90 mm; this size is obtained by multiplying 1.06 and 85 mm. In the case of calibre 2, Dm is 77.4 mm, obtained by the multiplication 1.06 and 73 mm. These data were validated during the parametric design, which is explained in the following section.

The norm does not specify apple heights by calibre. Therefore, from the measurements made on the scanned samples, a ratio, Rd, was established between the average dimensions of width (L02) and height (L03) of the apples, Equation (3).

$$Rd = L02/L03, \quad (3)$$

Therefore, the R_d for calibre 1 corresponds to 1.05 and 1.07 for calibre 2. This means that, compared to calibre 1, calibres 2 have lower height in relation to their diameter. Then, the total height H of the package in this case study is given by Equation (4).

$$H = D_m / R_d, \quad (4)$$

Thus, in the parametric design of the package, C_d is implicitly included in all the dimensions of the package from the D_m obtained in Equation (4). It should be stressed that this ratio, R_d , can be modified to obtain containers with different height in relation to the width.

3.2. Parameterization of the Conceptual Proposal

Once the design of the packaging was carried out, two variables, the maximum height of the container, H , and the maximum width, D_m , were used to define a series of parameters that characterise the package. Figure 11a shows a diagram of the variables that affect the sizing of the container.

From the initial geometry extracted from the concept design of the apple, the packaging was parameterized according to a series of equations described below. Figure 11b shows a diagram with the dimensions that affect the mould when thermoforming the designed package. Thus, the equations that affect the overall dimension of the packaging correspond to:

$$H_b = H \times 0.57, \quad (5)$$

$$H_t = H \times 0.43, \quad (6)$$

$$D_n = D_m \times 0.97, \quad (7)$$

where H_b is the height of the bottom half of the designed packaging and H_t is the height of the top half. In the same way, the projected dimensions of the container are given by the greater width, D_m , and the smaller width, D_n . In this case study, an oval geometry has been created.

As mentioned above, the design created in this study consists of a series of arches that are tangentially joined, in plan and profile, and a flat surface at the ends with a circular shape. The curves that define these geometries, Figure 11, could be related by means of equations from the initially created CAD design. Thus, the relationship between H and the slightly oval curved geometry that makes up the package design in the profile view is given by the equations:

$$R_b = H \times 0.27, \quad (8)$$

$$R_t = H \times 0.18, \quad (9)$$

$$d_b = D_m \times 0.3, \quad (10)$$

$$d_t = D_m \times 0.45, \quad (11)$$

$$R_p = (D_m + 10)/2, \quad (12)$$

These equations define the radius of curvature of the upper part, R_t , and lower, R_p . In addition, the adaptation of the dimension of the flat part, so that the packaging can be easily supported, is given by the diameter in both halves of the container, d_b and d_t , and was related to the parameter d_m . On the other hand, the radius R_p is the parameter that encompasses the overall geometry of the container in plant, and the shape was constructed by sweeping through the vertical curves given by R_b and R_t .

The rest of the tangent arcs that make up the packaging design are automatically adapted from the curves generated with the above equations.

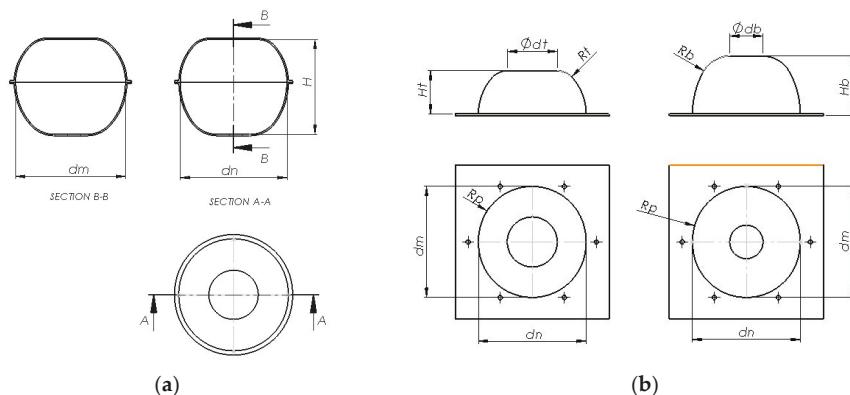


Figure 11. Dimensions of the container and the mould: (a) Plan of the variables that affect the container and therefore the upper and lower mould; (b) Dimensions of the moulds, on the left upper half and on the right lower half.

Then, the generated equations were introduced in the parametric design software, Solidworks®. The benefit of the parametric design of a packaging is the customization of the geometry according to the need of adaptation to the product to be contained. In addition, the design can be evaluated in real time by means of the digitized fruit samples. As a result, all construction operations such as roundings, tangent arcs, etc. were related. The number of operations obtained was a total of 12 for each part of the container. These equations and variables serve to quickly modify the geometry of an object.

For the lower part, according to the equations defined in the previous section, a relationship was defined between the curves that make up the container and, therefore, the mould. These equations were related to the sketches made in the parametric design program. In the same way, the equations of the upper part were parameterized.

In short, by modifying one of the measures, the packaging is automatically adapted. This is one of the first steps for the generation adapted to a specific packaging design in the context of industry 4.0.

Another result obtained in this case study is the maximum and minimum ratio (Rd) of measures between H and Dm , obtaining a range of adaptation measures. The maximum Rd is 1.32 and the minimum is 0.24. This range of measures means that the packaging created can also be used for other types of fresh food or measurements. Figure 12 shows an example of the variations in function of the maximum and minimum ratio.



Figure 12. Example of maximum and minimum ratio between Dm and H for H equal to 85 mm: (a) Maximum ratio for Dm = 137 mm; (b) Minimum ratio for Dm = 20 mm.

Also, if D_m is kept constant in the two parts, top and bottom, of the parametric packaging, H_t and H_b can be adapted independently, in the CAD file, to obtain intermediate H measurements by modifying the H value only in one of the parts. Also, with this modification, R_t and R_b also adapt automatically according to H_t and H_b , respectively. This parameter offers greater versatility if possible combinations for containers using fewer moulds are taken into account.

Once the packaging was parameterized, a series of configurations were established in Solidworks® software to evaluate the appropriate sizes for each of the samples studied and with which the theoretically established C_d was validated. The configurations allow the packaging to adapt automatically to the measures established, making it easier to adapt to calibres and measures according to specific needs.

3.3. Evaluation of Results

In order to analyse the viability of the coefficient obtained, C_d , using the 3D scanned fruit models, the correct arrangement of the apple was evaluated with respect to the dimensions of the packaging. Then, after analysing the dimensions with the configurations of the packaging, it was observed that the C_d corresponds adequately, although the optimum height for each sample varies, Appendix A.

Bearing this in mind, it can be concluded that, depending on the design needs for the same calibre, several containers with different H could be constructed. This may be possible thanks to new technologies such as additive manufacturing, which allows low-cost moulds to be made in order to optimise the maximum performance of the container. However, if the design requirements allow it, with this methodology it is possible to establish an optimal design that encompasses all food units of the same topology.

On the other hand, generating a custom packaging for a unit is also possible. This example could have multiple applications that could be extended to other types of products.

Thus, the final dimensions, which were adapted to the size obtained according to the C_d calculated in the measurement part, correspond to calibre 1 with the ratio R_d of 1.05, with D_m of 89.3 mm and H of 85 mm. Although, as it was mentioned, some of the samples studied could modify the H for the use of the dimensions having a range between 80 mm and 85 mm. Similarly, for calibre 2, the dimensions correspond to the ratio R_d of 1.07 with D_m and H being 75 mm and 70 mm, respectively, and, according to the samples studied, with a range of H between 67 mm and 70 mm. For more information see Appendix A.

Finally, the results obtained for the two calibres studied were validated by means of a physical prototype. The FDM moulds created for the two calibres are shown in Figure 13.



Figure 13. Parts, inferior and superior, of the mould to generate the physical prototypes: (a) Moulds for calibre 1; (b) moulds for calibre 2.

The design was validated using the physical prototypes and 20 apples for each calibre studied, Figure 14. These apples were selected taking into account shapes and size variations, and different varieties were included in the units studied. For more information see Appendix B.

Once the results were analysed, it can be said that the final solution obtained is positive as all the units of the same calibre correspond to the dimensions of the packaging. However, according to the

studies in the parametric software, it can be seen that, in several of the cases studied, the dimensions are not adjusted in their entirety, causing parts of the packaging to be empty. This is not a functional problem for the design because these variations are given by the wide range of measurements that are included within a calibre. Specifically, these dimensional deviations are accentuated in calibre 2, which is a smaller calibre and comprises a larger range of measurements. In the case of calibre 1, which belongs to category I according to [28], lower dimensional deviations are observed. However, the morphological inequalities between the different apple varieties are larger.

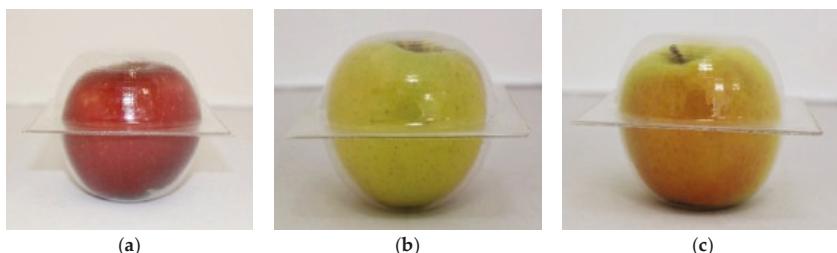


Figure 14. Images of the evaluation carried out with the prototype and commercial fruits: (a) Pacific rose apple, (b) Golden apple, (c) Jonagold apple.

In this situation, personalisation and adaptation could be increased by reducing the spectrum of fruit types that can be introduced in the same type of packaging. Therefore, depending on the type of product to be packed, adaptation and personalization can be considered with a greater degree of accuracy.

4. Discussion

The main idea of reverse engineering is to synthesize a fruit model so that it can be used and measured as part of the design process. The studies carried out show that it is possible to generate personalized designs and that they can also be adapted according to the specifications required by a specific product. Digitization and flexible designs make it easier to customize and test concepts in real time to help design teams make faster decisions and with greater reliability [33].

Then, the introduction of scanned elements in the design process facilitates the adaptation of the size and shape of the packaging to the type of fruit contained, allowing only the quantity of plastic material necessary for its sale and transport to be used. In this way, the product is optimised, which means a reduction in environmental and economic impact. This fact is relevant because, currently, thousands of tons of plastic and food are discarded daily [12], and great efforts are made to mitigate this impact, generating stricter and stricter regulations in the withdrawal and recycling of food packaging [34]. The huge quantity of packaging manufactured means that a small reduction in each container has a great influence on the environment. This working methodology promotes the reduction of material that is so necessary in a strategic sector such as the food industry. Thus, by adapting the packaging to the size and shape of the food, less raw material is wasted. In addition, the technique presented in this paper for designing efficient packaging also offers the possibility of creating packaging with less food, adapted to emerging consumption needs, which translates into less food waste and, therefore, in the protection of the environment. In addition, this tool can be used with any type of sustainable raw material, i.e., PLA (Polylactic Acid) sheet, although the material currently on the market has been used in this work.

As noted above, much of the food waste is produced by using containers with large amounts of food that end up deteriorating in homes [35]. Thus, the possibility offered by this methodology for the realization of custom packaging by type of fruit and category can lead to the reduction of food waste

due to the possibility of reducing the amount of product inside and by improving the preservation of specific properties of each food [36].

The application of digital elements in the design process was validated as part of the creation of a method that includes advanced technologies in its procedure, as was researched in other fields of engineering [37,38]. In the study, two main parameters related to the functional measures for the containers were selected, the maximum height and width, to adapt a packaging to a given calibre. However, the geometry of a fresh food is irregular so four measurements at the top and bottom were taken to calculate the height and width. It should be added that these measurements had been carried out to analyse the dimensions of the product studied at laboratory level. The main objective of this work was to evaluate the direct application of the scanned models for the generation of personalized packages for a range of measures established within a calibre.

This study proposed a 3D scanning scheme for fresh food to support custom packaging design [31]. Then, the three-dimensional model of the fruits approximates the real geometry. Thus, the application of 3D fruits facilitates the realization of personalized and adapted designs, as well as the evaluation in real time of design proposals. Moreover, the parametric design of the package according to the two parameters studied, gives rise to the possibility of generating packages adapted to the dimensions and needs of the food according to its established range of measures. In short, the result was the creation of a packaging, fully defined by equations, which is capable of adapting to the measurements in a given range.

Based on these results, computational design is aimed at the parameterization to favour customization by means of optimal configurations of the variables, favouring the adaptation of the design to specific needs [39,40]. Computer programs facilitate the realization of personalized and flexible designs to adapt to specific needs by means of the parameterization and digitalization of elements [41–43]. Product customization also serves as an engine to improve sustainability throughout the product life cycle [44]. Custom design enhances product design by meeting the specific needs of users [45].

Furthermore, according to new trends and competitiveness, the design and development of packaging need solutions that streamline the working procedure. In this context, based on the approaches made on the customization of packaging, there is also a latent need for quick and flexible solutions. Specifically, the process of manufacturing moulds by conventional methods usually delays the validation time of the final prototype of the product, so designers cannot make changes or explore quick and reliable options [46]. Facing this situation, the application of additive manufacturing techniques can provide design teams with a fast and economical tool that can thus be used from the early stages of product design.

Summarizing, it is possible to build reliable prototypes by additive manufacturing. The similarity of the prototypes generated thanks to 3D printing and thermoforming technologies shows the possibility of creating prototypes that provide greater reliability in a simple way. Then, the evaluation by means of these prototypes provides a trustful tool for the validation of the mentioned designs. In short, it was proven that it is possible to thermoform geometries with different shapes. Therefore, it is possible to obtain products with better performance and, consequently, competition. This can also affect the life cycle of the product as there is a significant improvement from the point of view of the social, economic and environmental impact.

Finally, this work presents several future lines of action, the most important of which is the advanced study of new packaging designs by means of topological optimisation and the extension of the study of virtual environments for early evaluation.

5. Conclusions

The following conclusions can be drawn from the research work carried out in this study:

It was possible to digitize fresh food by means of 3D scanning techniques, obtaining reliable digital elements that could be used in advanced technologies. In this sense, it was possible to define

a procedure for the reverse engineering of different types of food, detailing the specific parameters according to size and finish.

It was possible to use the digitized fruits during the conceptual phase in the packaging design process. Thus, custom designs were developed using these elements as a reference during computer-aided design, thus validating the proposed methodology. In addition, the evaluation of the ideas generated was also favoured by the possibility of checking dimensions in real time using these digital products. On the other hand, the adaptation according to the specifications required by a specific product was also improved. Therefore, the application of 3D fruits facilitated the development of customized and adapted designs.

It was possible to completely parameterize the geometry of the package to create custom and, in turn, automatically adaptable designs. In short, the creation of a packaging, fully defined by equations, was able to adapt to measurements in a given range. The parameterized design was made possible by means of the virtual evaluation of digitized fruits.

Finally, by adapting the containers to the size and shape of the food content, less raw material used for the container was wasted. Likewise, the technique presented in this work to design efficient containers also offered the possibility of creating containers with less food, adapted to emerging consumption needs, which lead to less food waste and therefore a better protection of the environment. In addition, this tool could be used with any type of sustainable raw material, although in this study the material currently on the market was used.

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Appendix

Table A1. Images of virtual evaluation for both calibres.

Sample	Calibre 1		Calibre 2	
	Front View	Top View	Front View	Top View
M1				
M2				
M3				

Table A1. Cont.

Sample	Calibre 1		Calibre 2	
	Front View	Top View	Front View	Top View
M4				
M5				
M6				
M7				
M8				
M9				
M10				

Appendix

Table A2. Images from the validation study with prototype of the custom packaging for Calibre 1.

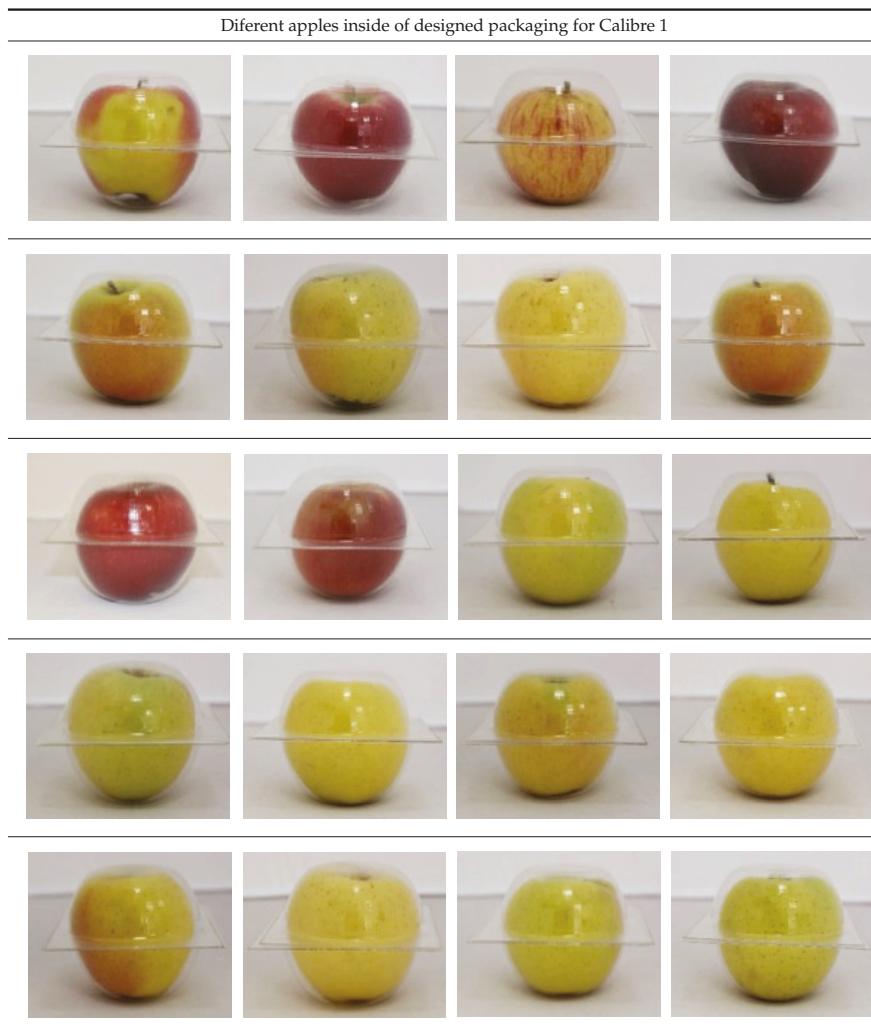
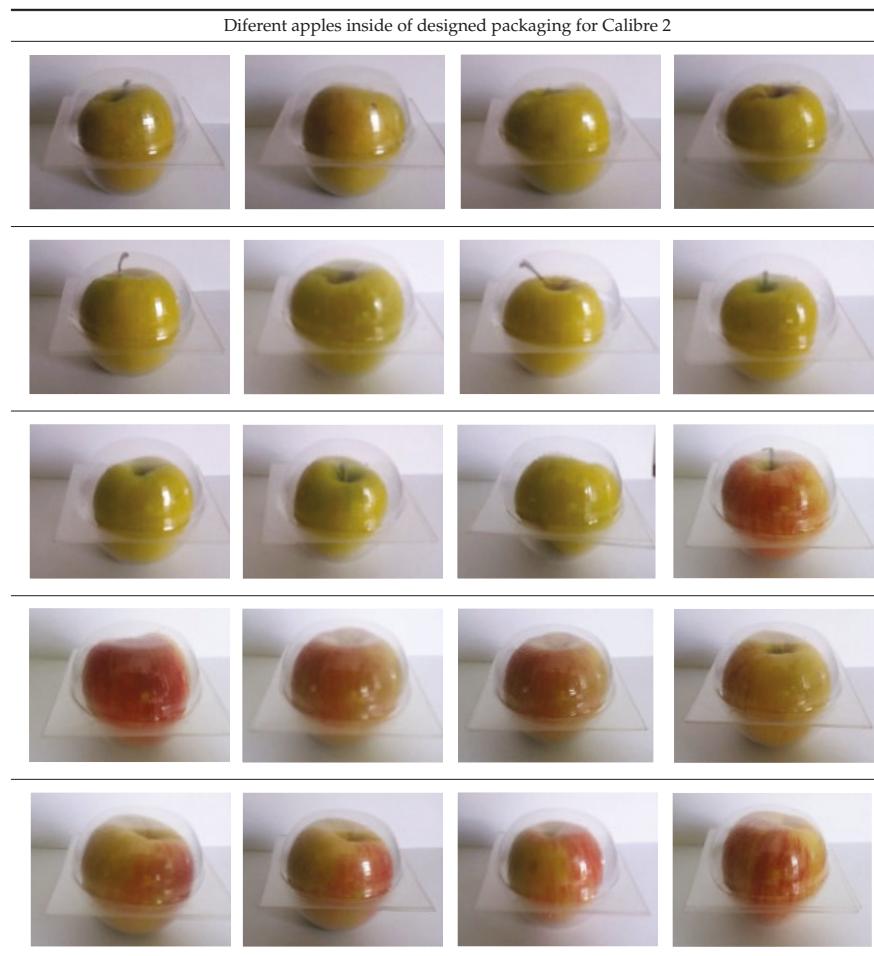


Table A3. Images from the validation study with prototype of the custom packaging for Calibre 2.

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