The finite element method

In FEM I we derived finite element equations from

8NE = 8NE

and obtained:

$$K_{ij}^e U_j^e = R_i^e$$
 $i_{ij} = 1,...,n$

where:

n: number of element nodal points UE: element nodal displacements

$$K_{ij}^{e} = \int_{x_{i}}^{x_{i}} E A \frac{d\phi_{i}^{e}}{dx} \frac{d\phi_{i}^{e}}{dx} dx$$
: element stiffness matrix

 $R_{i}^{e} = \int_{x_{i}}^{x_{i}^{e}} F(x) \phi_{i}^{e} dx + P_{i}^{e}$: element stiffness matrix

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vector

Exercise: derive K_{ij}^e , R_i^e for linear and quadratic interpolation for the case of uniform cross section (A), Young's modulus (E) and distributed load ($q_i(x) = q_0$).

Finite element assembly

- Each finite element is connected to its neighbors at its end nodes.
- · As before define a global numbering (Identification) for all the nodes

For linear dements:

$$U_1^1 = U_1$$
, $U_2^1 = U_2 = U_1^2$, $U_2^2 = U_3 = U_1^3$

. Concept question: Expression for the local-global nodal mapping for the quadratic dement mesh.

The assembly of the element equations is based on the satisfaction of the variational principle for the whole system:

where IT is the sum of the element values Te over the mesh elements.

Example. Mesh with two linear elements

We had obtained Ke as:

Replacing local with global numbering:

$$\frac{U^{1} = \frac{1}{2} \left\{ U_{1}^{1} \ U_{2}^{1} \right\} \left[\begin{array}{cc} K_{11}^{1} & K_{12}^{1} \\ K_{21}^{1} & K_{22}^{1} \end{array} \right] \left\{ \begin{array}{cc} U_{1}^{1} \\ U_{2}^{1} \end{array} \right\}$$

$$= \frac{1}{2} \left\{ \begin{array}{cccc} U_1 & U_2 & U_3 \end{array} \right\} \left[\begin{array}{ccccc} K_{11}^1 & K_{12}^1 & 0 \\ K_{21}^1 & K_{22}^1 & 0 \end{array} \right] \left[\begin{array}{ccccc} U_1 \\ U_2 \\ 0 & 0 \end{array} \right]$$

$$U^{2} = \frac{1}{2} \left\{ U_{1}^{2} \quad U_{2}^{2} \right\} \left[K_{11}^{2} \quad K_{12}^{2} \right] \left\{ U_{1}^{2} \right\} \left[K_{21}^{2} \quad K_{22}^{2} \right] \left\{ U_{2}^{2} \right\}$$

$$= \frac{1}{2} \left\{ \begin{array}{cccc} U_1 & U_2 & U_3 \end{array} \right\} \left[\begin{array}{ccccc} 0 & 0 & 0 & 0 \\ 0 & K_{11}^2 & K_{12}^2 & V_2 \\ 0 & K_{21}^2 & K_{13}^2 \end{array} \right] \left\{ \begin{array}{ccccc} U_4 & V_2 & V_3 \\ V_2 & V_3 & V_3 \end{array} \right\}$$

$$= \underbrace{1 \left\{ U_{1} \ U_{2} \ U_{3} \right\} \left[\begin{array}{ccc} K_{11} & K_{12}^{1} & O \\ \hline 2 & & \\ \end{array} \right] \left\{ \begin{array}{ccc} K_{11} & K_{12}^{1} & O \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & K_{12}^{1} & V_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & K_{12}^{2} & V_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & K_{12}^{2} & V_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & K_{12}^{2} & V_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{ccc} W_{1} & W_{12} & W_{12} \\ \hline 4 & & \\ \end{array} \right\} \left\{ \begin{array}{$$

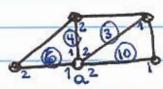
but here the "sum"

Sign has a special meaning: "assembly" which involves proper placement of the element stiffness matrix coefficials in the global matrix.

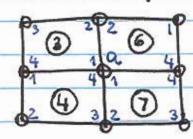
Remarks on assembly of global matrix

. Diagonal element corresponding to global node "i" gets contributions from all the elements writing to it.

Trusses, beams:



Plane elasticity

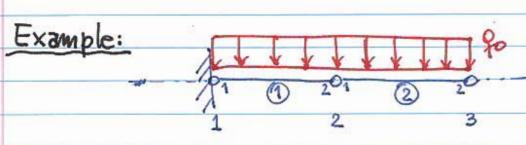




- . Kij = o if node "i" and "j" are in different elements
- . Kij preserves the symmetry of the element Kij

Assembly of global force vector R:

Find:
$$R_4 = \sum_{e=1}^{5} R_e^e$$



$$R^e = \frac{L^e q_0}{2} \left\{ \frac{1}{1} \right\}$$

$$R = R^{1} + R^{2} = \begin{cases} 1 \\ 1 \end{cases} \frac{L^{1}q_{0}}{2} + \begin{cases} 0 \\ 1 \end{cases} \frac{L^{2}q_{0}}{2}$$

$$R = \frac{90}{2} \left\{ \frac{L^{4} + L^{2}}{L^{2}} \right\}$$