## **12.005 Lecture Notes 22**

## **Plates (continued)**

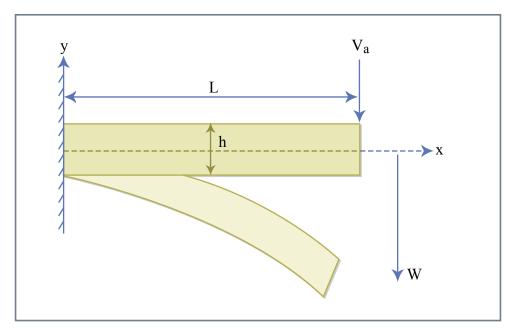


Figure 22.1 Figure by MIT OCW.

$$w = \frac{V_a}{2D}x^2(L - \frac{x}{3})$$

Assumption  $|\sigma_{xy}| = |\sigma_{xx}|$ 

$$\sigma_{xx} = \frac{E}{1 - v^2} \varepsilon_{xx}$$

$$\varepsilon_{xx} = -y \frac{d^2 w}{dx^2}$$

$$M = -D\frac{d^2w}{dx^2}$$

$$\varepsilon_{xx} = \frac{y}{D}M$$

$$\sigma_{xx}^{\text{max}} = \frac{E}{1 - v^2} \frac{h}{2} \frac{1}{D} V_a L = \frac{6V_a L}{h^2} = \frac{6V_a}{h} \left(\frac{L}{h}\right)$$

$$\langle \sigma_{xy} \rangle = \frac{V_a}{h} = \frac{1}{6} \frac{h}{L} \sigma_{xx}^{\text{max}}$$

Response to a line load (e.g. volcanic chain under water)

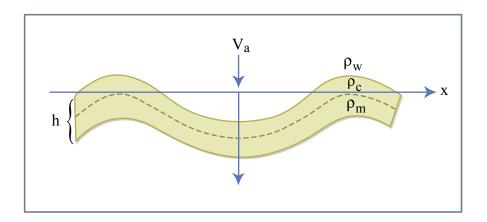


Figure 22.2 Figure by MIT OCW.

$$D\frac{d^{4}w}{dx^{4}} + (\rho_{m} - \rho_{w})gw = \begin{cases} 0 & \text{at } x \neq 0 \\ V_{0} & \text{at } x = 0 \end{cases}$$

Solution to homogeneous equation

$$w = e^{x/\alpha} \left( C_1 \cos \frac{x}{\alpha} + C_2 \sin \frac{x}{\alpha} \right) + e^{-x/\alpha} \left( C_3 \cos \frac{x}{\alpha} + C_4 \sin \frac{x}{\alpha} \right)$$

with 
$$\alpha = \left[\frac{4D}{(\rho_w - \rho_w)g}\right]^{1/4}$$
  $\alpha$  is flexural parameter.

Invoke symmetry, boundedness. Determine solution only for  $x \ge 0$ .

$$\frac{dw}{dx} = 0 \quad \text{at } x = 0 \quad C_3 = C_4$$

$$w \to 0$$
  $x \to \infty$   $C_1 = C_2 = 0$ 

$$w = C_3 e^{-x/\alpha} (\cos \frac{x}{\alpha} + \sin \frac{x}{\alpha})$$

Now to evaluate  $C_3$ , go back to the end load problem (or original definition)

$$\frac{dM}{dx} = V + P\frac{dw}{dx}$$

 $C_3$  depends on  $V_0$ .

$$\frac{d^3w}{dx^3} = -\frac{1}{2}\frac{V}{D}$$

$$\frac{1}{2}V_0 = D\frac{d^3w}{dx^3}\bigg|_{x=0} = \frac{4DC_3}{\alpha^3}$$

 $V_0$  is negative load, half supported by each side.

$$w = \frac{V_0 \alpha^3}{8D} e^{-x/\alpha} \left(\cos \frac{x}{\alpha} + \sin \frac{x}{\alpha}\right)$$

$$w_0 = \frac{V_0 \alpha^3}{8D}$$

$$w = w_0 e^{-x/\alpha} \left(\cos \frac{x}{\alpha} + \sin \frac{x}{\alpha}\right)$$

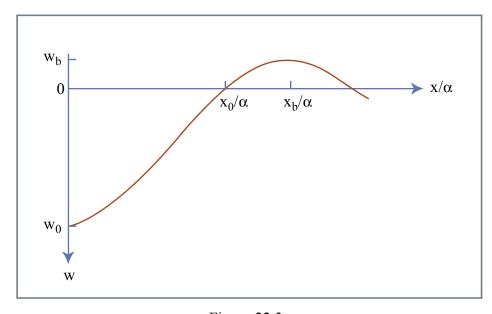


Figure 22.3 Figure by MIT OCW.

$$\frac{x_0}{\alpha} = \tan^{-1}(-1) = \frac{3\pi}{4}$$

$$\frac{x_b}{\alpha} = \sin^{-1}(0) = \pi$$

$$w_b = -w_0 e^{-\pi} = -0.0432 w_0$$

x;  $3^{\circ}$ ; 300 km

$$\alpha = \frac{314}{\pi} \text{km} ; 100 \text{km}$$

Suppose plate is fractured.

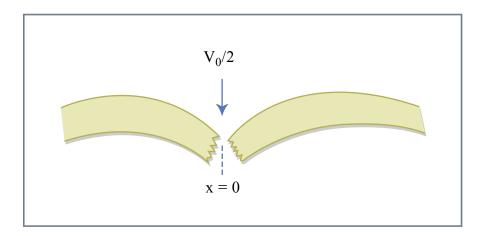


Figure 22.4 Figure by MIT OCW.

Same equation. Different boundary conditions  $\Rightarrow$  different profile.

$$M = 0$$
 at  $x = 0$  
$$\frac{d^2w}{dx^2} = 0$$

$$w = \frac{V_0 \alpha^3}{4D} e^{-x/\alpha} \cos \frac{x}{\alpha}$$

$$w_0 = \frac{V_0 \alpha^3}{4D}$$

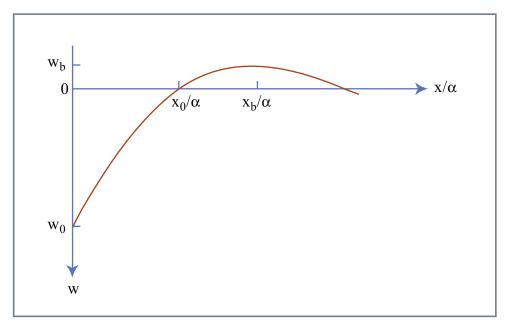


Figure 22.5 Figure by MIT OCW.

$$x_0 = \frac{\pi}{2}\alpha$$
,  $x_b = \frac{3\pi}{4}\alpha$ ,  $w_b = -0.067w_0$ 

h; 35km unbroken

h; 50km broken

Thickness of broken lithosphere is about 1.5 times thickness of the unbroken lithosphere.

Bending at a trench.

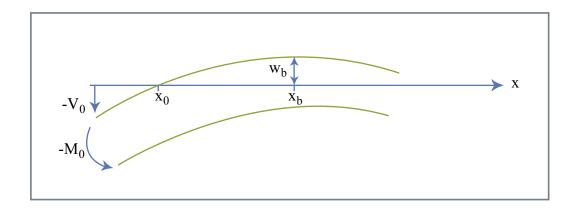


Figure 22.6 Figure by MIT OCW.

$$w = e^{-x/\alpha} \left( C_3 \cos \frac{x}{\alpha} + C_4 \sin \frac{x}{\alpha} \right)$$

$$C_4 = -\frac{M_0 \alpha^2}{2D}$$

$$C_3 = (V_0 \alpha + M_0) \frac{\alpha^2}{2D}$$
 (entire  $V_0$  supported)

$$w = \frac{\alpha^2 e^{-x/\alpha}}{2D} \left\{ -M_0 \sin \frac{x}{\alpha} + (V_0 \alpha + M_0) \cos \frac{x}{\alpha} \right\}$$

Observables --  $x_0, x_b, w_b$ 

$$\tan\frac{x_0}{\alpha} = 1 + \alpha V_0 / M_0$$

$$\tan\frac{x_b}{\alpha} = -1 - 2M_0 / \alpha V_0$$

$$x_b - x_0 = \frac{\pi}{4}\alpha$$

$$w_b = \frac{\alpha^2 e^{-x_b/\alpha}}{2D} \left\{ -M_0 \sin \frac{x_b}{\alpha} + (V_0 \alpha + M_0) \cos \frac{x_b}{\alpha} \right\}$$

$$w_{b} = -\frac{\alpha^{2} M_{0}}{2D} e^{-[(x_{b} - x_{0})/\alpha]} e^{-x_{0}/\alpha} \frac{\sin((x_{b} - x_{0})/\alpha)}{\cos(x_{0}/\alpha)}$$