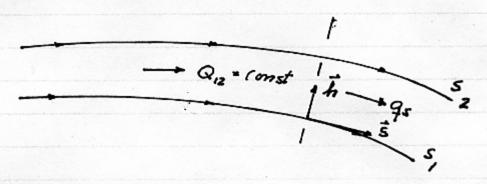
LECTURE #6

1.060 ENGINEERING MECHANICS I

Consorvation of Volume for a Sheamfube (2-D Plane Flow)



Streamline coordinates:

is local direction of sheamline h is local direction L sheamline

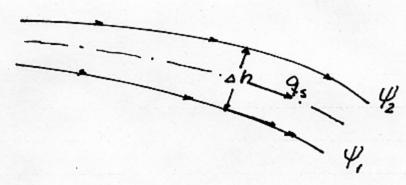
and

STREAM FUNCTION

Define a function 4 such that

4 = 4(s,h) = 4(h) = constant along \$

4 = sheam function is constant along a stream line.



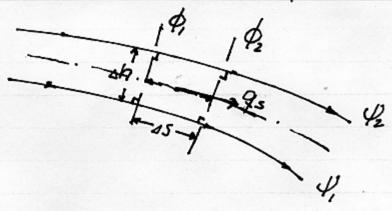
VELOCITY POTENTIAL

Define a function of such that

 $\frac{\partial \phi}{\partial s} = 9s$, $\frac{\partial \phi}{\partial h} = 0$

 $\phi = \phi(s,h) = \phi(s) = constant along$ lines $L \vec{s}$

p = velocity potential is constant along lines I streamlines (equipotential lines)



$$\frac{\partial \phi}{\partial s} = \lim_{\Delta s \to 0} \frac{\Delta \phi}{\Delta s} = \frac{\phi_z - \phi_z}{\Delta s} = \frac{q_s}{q_s}$$

$$\phi_{2} - \phi_{1} = q_{s} \Delta s = (q_{s} \Delta h) \frac{\Delta s}{\Delta h} = Q_{12}$$

if as/ah =1

FLOW NET

Lines of constant 4 (streamlines) and constant & (equipotential lines) form two Jamilies of cenves (s-lines and h-lines) that intersect each other at night angles, i.e. they form a rectangular" po Hern.

If the two families of curves one constructed (drawn) such that they form a pattern of squares", i.e. as = Ah, the discharge in stream tubes formed by adjacent stream lines, Q12, is constant (as it should be). This is a FLOW NET

If we know the discharge, Q12, in a stream tube, we can obtain an estimate of the velocity at the center of a "square from 95 = Que / sh , where sh (= DS) is the side length of the square.

Simple "Rules" to follow when Constructing Flow Nets

- " Use a pencil and bring an eraser.
- 21 Solid boundaries are streamlines
- Regions) where flow is uniform straight parallel streamline is a good place to start and end.
- 4) Sketch the streamlines and equipotential lines connecting regions) identified in (3) observing the following

 4-8 \$\phi\$-lines form a "square" pattern

 Streamlines can never cross

 Streamlines can start & end only at flow areas

 Sheamlines in the interior are quided by boundaries, but swoother (no kints).
- 5) Examine sketch and "repair" where needed (this is where the enaser comes in!)
- 6) Discharge = DQ is constant within a tube V = DQ/sh can be estimated at center of "squares". Directed along 4.
- Pressure is estimated from Bernoulli along a streamline.

STREAM FUNCTION & VELOCITY POTENTIAL

Their Generalized Definitions and Limitations

Differential form of Continuity Equation

$$y = \sigma + (\partial u/\partial y) \delta y$$
 $Volume Conservation:$

Rate in - Rate out =

Rate in - Rate out =

 $\sigma \times (u + (\partial u/\partial x)) \delta \times (u +$

Stream Function 4

defined by

u = 24/24; U = -24/2x

Continuity equation (in 2-D) is automatically

satisfied, since

au + au = a(ay) + a(-ay) = azy - azy = 0

Limitation of Sheam Function

Two-Dimensional Flows of an Incompressible Fluid

Velocity Potential P φ = φ(x,y,z,t) defined by U= 0\$/0x; U= 0\$/04; W= 0\$/02 $\vec{q} = (u, v, w) = grad \phi = \nabla \phi$ In terms of ϕ , the continuity equation is du + du + dw = a (dx) + a (dx) + d (db) = a (db) = ∂\$ + ∂\$\$ + ∂\$\$ = ∇²\$ = 0 (Laplace Eq.) V= V. V = 2x + 2y + 2 = Laplace Operator Limitation of Velocity Potential For \$ to make sense, we must have that $\frac{\partial^2 \phi}{\partial x \partial y} = \frac{\partial}{\partial x} \left(\frac{\partial \phi}{\partial y} \right) = \frac{\partial U}{\partial x} = \frac{\partial^2 \phi}{\partial y \partial x} = \frac{\partial}{\partial y} \left(\frac{\partial \phi}{\partial x} \right) = \frac{\partial U}{\partial y}$ Order of differentiation is immaterial! 4 1 24/24 +0 dulay=0 At solid boundary U=0, i.e. 20/2x =0 So, for \$ to exist, du/dy = 0 1 no-slip velocity which cannot be the case solid boundary unless fluid is inviscid (V=0)

FLOW NET LIMITATIONS

Since flow nets are based on Stream Function and Velocity Potential concepts they are limited to:

Two-Dimensional Flows of an Incompressible and Inviscial Fluid,

Two-Dimensional Flows of an Ideal Fluid

- · We can still sketch flow nets for 3-D flows and get a very good physical picture of the nature of the flow, e.g. ugions where velocities are large or small may be identified.
- The flow net allows fluid to have a slip-velocity along solid boundaries (they become streamlines!). Since There is no such thing as an ideal fluid the flow net features very close to solid boundaries donies are unreliable.
- Flow nets are useful when the bulk of the flow may be considered minimally affected by boundary shear stresses, and the flow is "converging", i.e. velocity is increasing along a streamline.

$$\frac{\partial \psi}{\partial s} = \frac{\partial \psi}{\partial x} \delta x + \frac{\partial \psi}{\partial y} \delta y = \frac{\partial \psi}{\partial x} (u_s \delta t) + \frac{\partial \psi}{\partial y} (v_s \delta t) =$$

$$\left[\frac{\partial \psi}{\partial x} \frac{\partial \psi}{\partial y} + \frac{\partial \psi}{\partial y} (-\frac{\partial \psi}{\partial x}) \right] \delta t = 0$$
e.
$$\frac{\partial \psi}{\partial s} = 0 \quad \text{along sheamlines}$$

In the direction L s, i.e. the "h'-direction $\frac{\partial \psi}{\partial h} = \frac{\partial \psi}{\partial h} \left(u_s^2 + v_s^2\right)^{1/2} \delta t = \frac{\partial \psi}{\partial x} \left(-v_s \delta t\right) + \frac{\partial \psi}{\partial y} \left(u_s \delta t\right) = \left[\frac{\partial \psi}{\partial x} \left(-\left(-\frac{\partial \psi}{\partial x}\right)\right) + \frac{\partial \psi}{\partial y} \left(\frac{\partial \psi}{\partial y}\right)\right] \delta t = \left(v_s^2 + u_s^2\right) \delta t$ $\frac{\partial \psi}{\partial x} \left(-\left(-\frac{\partial \psi}{\partial x}\right)\right) + \frac{\partial \psi}{\partial y} \left(\frac{\partial \psi}{\partial y}\right) = \frac{\partial \psi}{\partial x} \left$

Similarly,

$$\frac{\partial \phi}{\partial s} \delta s = \frac{\partial \phi}{\partial s} (u_s^2 + u_s^2)^{1/2} \delta t = \frac{\partial \phi}{\partial x} \delta x + \frac{\partial \phi}{\partial y} \delta y = (u_s^2 + u_s^2) \delta t$$

$$\frac{\partial \phi}{\partial s} \delta s = \frac{\partial \phi}{\partial s} (u_s^2 + u_s^2)^{1/2} \delta t = \frac{\partial \phi}{\partial s} \delta s = \frac{\partial \phi}{\partial s} \delta s$$

and $\frac{\partial \phi}{\partial h} \delta h = \frac{\partial \phi}{\partial x} (-\upsilon_s \delta t) + \frac{\partial \phi}{\partial y} (\upsilon_s \delta t) = (-\upsilon_s \upsilon_s + \upsilon_s \upsilon_s) \delta t = 0$ $\frac{\partial \phi}{\partial h} (\partial h) = 0$