#### 2.001 - MECHANICS AND MATERIALS I

Lecture #22 11/27/2006Prof. Carol Livermore

Beam in pure bending  $\rho = \text{radius of curvature}$   $\epsilon_{xx} = \frac{-y}{\rho} \ \sigma_{xx} = \frac{-Ey}{\rho}$ 

Locating the neutral axis  $\int_A \frac{Ey}{\rho} dA = 0$ 

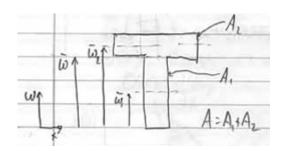
Moment-Curvature  $M = \int_A \frac{Ey^2}{\rho} dA$ 

Special Case: E = constantNeutral Axis:  $\int_A y dA = 0$ 

Moment-Curvature  $M = \frac{EI}{\rho} \; I = \int_A y^2 dA$ 

Neutral Axis Shortcut

1. Symmetric cross section  $\Rightarrow$  neutral axis in the center for E= constant For E= constant:



Area 1:

$$\int_{A_1} (w - \overline{w_1} dA_1 = 0$$

Area 2:

$$\int_{A_2} (w - \overline{w_2}) dA_2 = 0$$

Total:

$$\int_{A_1} (w - \overline{w_1} dA_1 + \int_{A_2} (w - \overline{w_2}) dA_2 = 0$$

$$\int_{A_1+A_2} w dA - \overline{w_1} \int_{A_1} dA_1 - \overline{w_2} \int_{A_2} dA_2 = 0$$

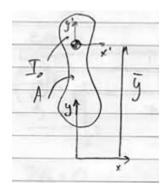
$$\overline{w} A = \overline{w_1} A_2 + \overline{w_2} A_2$$

$$\overline{w} = \frac{\sum_i \overline{w_i} A_i}{\sum_i A_i}$$

For a general beam:

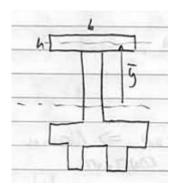
$$\overline{w} = \frac{\sum_{i} \overline{w_i} A_i E_0}{\sum_{i} A_i E_i}$$

## 3. Parallel Axis Theorem:



$$I_{y=0} = I_0 + \overline{y}^2 A$$

#### EXAMPLE:



$$I_{top} = \frac{bh^3}{12} + \overline{y}^2 bh$$
  
$$I_{totatl} = I_{top} + I_{mid} + \dots$$

Effective Bending Stiffness  $(EI)_{eff}$ 

$$(EI)_{eff} = \sum_{i} E_i I_i^{y=0}$$

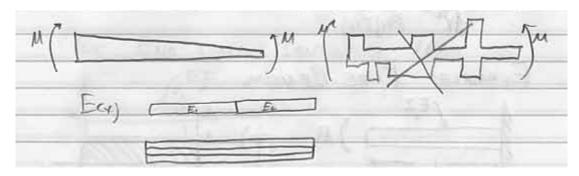
Beam Deflection (Displacement and slope) Recall for a one material beam

$$M(x) = EI \frac{1}{\rho(x)}$$

Note for  $E \neq \text{constant}$ :

$$M(x) = (EI)_{eff} \frac{1}{\rho(x)}$$

Note for gradual change in cross section, this works.

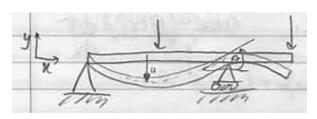


So:

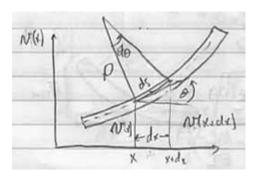
$$M(x) = \frac{E(x)I(x)}{\rho(x)}$$

### Example:

Draw what you think will happen.



u(x) - Beam deflection,  $\theta(x)$  - beam slope,  $\theta(x) = \frac{dv(x)}{dx}$ 



$$ds = \rho d\theta \Rightarrow d\theta = \frac{1}{\rho} ds, \ \theta = \frac{dv}{dx}, \ \frac{d\theta}{dx} = \frac{d^2v}{dx^2} \Rightarrow d\theta = \frac{d^2v}{dx^2} dx$$
  $\cos \theta = \frac{ds}{dx} \approx 1 \text{ so } ds \approx dx.$  So:

$$\frac{1}{\rho} = \frac{d^2v}{dx^2}$$

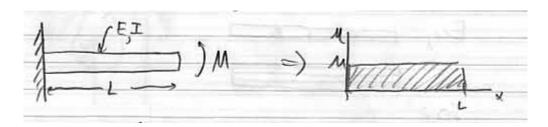
 ${\bf Recall:}$ 

$$\frac{1}{\rho} = \frac{M}{EI}$$

So:

$$\frac{d^2v}{dx^2} = \frac{M(x)}{E(x)I(x)}$$

Example: Pure Bending



$$M(x) = M$$

So:

$$\frac{d^2v}{dx^2} = \frac{M}{EI}$$

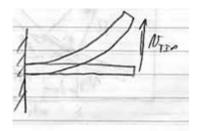
Integrate:

$$\frac{dv}{dx} = \frac{Mx}{EI} + c_1$$
$$v(x) = \frac{Mx^2}{2EI} + c_1x + c_2$$

Get  $c_1$  and  $c_2$  from BCs.

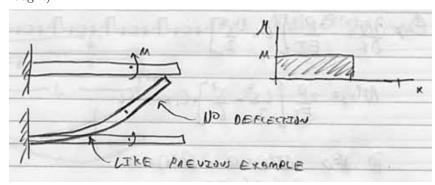
At x=0, v=0 due to fixed support. At  $x=0, \theta=\frac{dv}{dx}=0$  due to fixed support. So  $c_1=c_2=0$ Thus:

$$v(x) = \frac{Mx^2}{2EI}$$

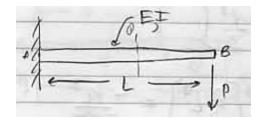


So, 
$$v_{tip} = \frac{ML}{2EI}$$
,  $\theta_{tip} = \frac{ML}{EI}$ .

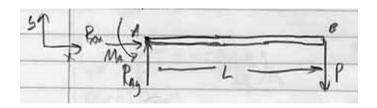
# Ex (Thought)



EX: End loaded cantilever beam



FBD



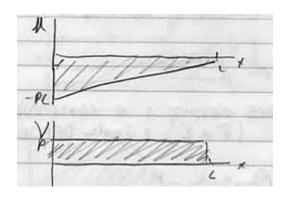
$$\sum F_x = 0 \Rightarrow R_{Ax} = 0$$
$$\sum F_y = 0 \Rightarrow R_{Ay} = P$$
$$\sum M_A = 0 \Rightarrow M_A = PL$$



$$\sum F_x = 0 \Rightarrow N = 0$$

$$\sum F_y = 0 \Rightarrow V_y = P$$

$$\sum M_* = 0 \Rightarrow M_* = -P(L - x)$$



So:

$$\frac{\partial^2 v(x)}{\partial x} = \frac{-P(L-x)}{EI}$$

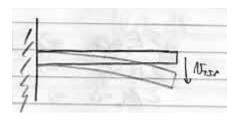
$$\theta_x = \frac{\partial v}{\partial x} = \frac{-P}{EI} \left[ Lx - \frac{x^2}{2} \right] + c_1$$

$$v(x) = \frac{-P}{EI} \left[ \frac{Lx^2}{2} - \frac{x^3}{6} \right] + c_1 x + c_2$$

 $0 x = 0, v(0) = 0, \theta(0) = 0 \Rightarrow c_1 = c_2 = 0$ 

So:

$$v(x) = \frac{-P}{2EI} \left[ Lx^2 - \frac{x^3}{3} \right]$$
$$v_{tip} = v(L) = \frac{-P}{2EI} \left[ \frac{2}{3} L^3 \right] = \frac{-PL^3}{3EI}$$



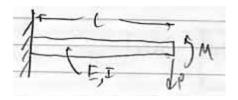
For this beam  $\Rightarrow$  stiffness "F=kx"

$$k = 3\frac{EI}{L^3}$$

Different configurations have different factors.

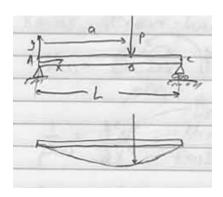
$$\theta_{tip} = \frac{-PL^2}{2EI}$$

Superpositions of these results: A consequence of linearity  $(\sigma \propto \epsilon)$  and small deformations

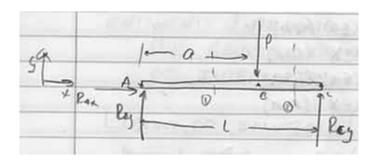


$$\theta_{tip} = \frac{ML}{EI} - \frac{PL^2}{2EI}$$

EX:



Find v(x),  $\theta(x)$ . FBD



$$\sum F_x = 0 \Rightarrow R_{Ax} = 0$$

$$\sum F_y = 0$$

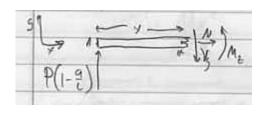
$$R_{Ay} + R_{Cy} - P = 0$$

$$\sum M_A = 0$$

$$-Pa + R_{Cy}L = 0$$

$$R_{Ay} = P(1 - \frac{a}{L})$$

FBD Cut 1  $0 \le x \le a$ 



$$\sum F_y = 0$$

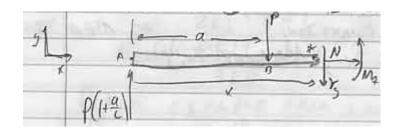
$$P(1 - \frac{a}{2}) = V_y$$

$$\sum M_* = 0$$

$$-P(1 - \frac{a}{L})x + M_z = 0$$

$$M_z = P(1 - \frac{a}{L})x$$

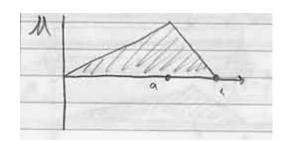
FBD Cut 2  $a \le x \le L$ 



$$\sum_{i} F_{y} = 0$$

$$P(1 + \frac{a}{L}) - P - V_{y} = 0$$

$$V_{y} = \frac{Pa}{L}$$

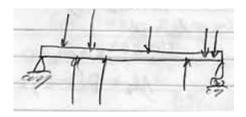


$$\sum M_* = 0$$

$$M_z + P(x - a) - P(1 + \frac{a}{L})x = 0$$

$$M_z = P(1 - \frac{a}{L})x - P(x - a)$$

- Solution Options
  1. Direct Integration
  - 2. But what about Use superposition.



# 3. Discontinuity Functions