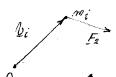
2 [a-V(t-ts)] (dn-Vdt) + 2ydy=0

(dm, dy, dt) true in finitesimal displacement

(4) Virtual Work



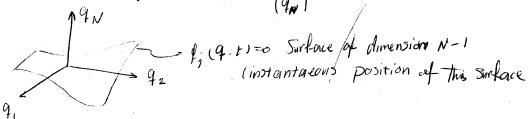
 $\delta W_{F_i} = F_i \cdot \delta_{F_i}$

Definition: A Constraint is Control ideal if The associated ideal force does zono cirtual work

Consider Specifically halonomic Constraints

$$f_{j}(q,t)=0$$
 $q=\begin{cases} q_{1}\\ q_{2} \end{cases}$

 $f_{j}(q_{j}t)=0$ $q=\begin{cases} q_{j}\\ q_{p} \end{cases}$ Space at q_{i} 's are Called Configuration space



NOTE: the Constraint force Ki (corresponding to F; (4, +)=0 must be or theyonal to the above surface)

$$= D \quad K_j = Q \nabla f_j \quad (\nabla = \nabla g) \qquad (a)$$

On the other hand, by definition, This . 59 = 0 (2)

Any halonomic Constraint is ideal

Example:
$$J = V$$
 because $f_1(q_1t) = 0$
 $T = V$
 $T =$

wark done by the Consistaint is non-goro but virtual wark is zero (ideal

General Result

true infinitesimal of the Constraint is only equal to the virtual work for schronomic Constraint

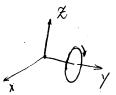
(2) Rolling in 2D

$$\begin{array}{ccc} & & & & & & & \\ & & & & & \\ & & & & \\ & & & & \\ & & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ &$$

ideal Constraint

(3) 3D rolling

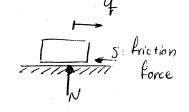
truly non halonomic



Creneral argument
given for halonomic Systems does not apply.
But One Can Still Show that this

Constraint is ideal.

(4) Stiding over rough Surface



Milly Scleronomic System

dWs = 5 Ws 70

Constraint is not ideal

Trick: Consider 5 as an active force that is not part of the Constraint 75 sliding be ames an ideal ansymmetry, and 5=5(41N, 9.9...)

is just another active force

(5) Creneralized Forces & forces expressed acting in the direction of generalize

 $\begin{cases} R_i = F_{i+1}K_i \\ \text{Cirtual work on } its particle \\ SW' = P_i \cdot Sr_i = (F_{i+1}K_i)Sr_i \end{cases}$ Total virtual work closs on System SW= \sum_{i=1}^n \in Ei. \Sri + \sum_{i=1}^n \in K: \Sr; $= \sum_{i} F_{i} \cdot \sum_{j} \frac{\partial r_{i}}{\partial q_{j}} \delta q_{j}$ if all Constraints are ideal $=\sum_{i=1}^{N}\left(\sum_{i=1}^{n}F_{i}\cdot\underbrace{\partial r_{i}}_{\partial q_{i}}\right)\delta q_{i}$ Q; the generalized force associated with 4; Special case: generalized forces in the Case when Ei's one all potential forces. $\delta W = \sum_{i} F_{i} \delta r_{i} = \sum_{i} (-\frac{\partial \vec{V}}{\partial r_{i}}) \cdot \delta r_{j}$ $= -\delta V = \sum_{i=1}^{N} - \frac{\delta V}{\delta q_i} \delta q_i$ =D for potential forces by definition a; = - 27 Example: Stiding Collar on a rough beam
Subjected to a tollower force # DOF: 3+3-2-2=9-D 2 generalized Coardinates Question: Cheneral, zeel Porces Car, & Qp 8W=8W +8W compotential $SW = -\delta V = -\delta \left(Mg + Co (-mgrCo) \right)$ $= Mg + (-\sin \theta) \delta \theta + mgr(-\sin \theta) \delta \theta + mg Co (6) \delta r$

Grotential - (My 1 + mgr) Jin 6

G potential = mg Con &