Analysis of large plastic deformation of elasto-plastic solids

- Friction involves large plastic deformation.
- There are different ways of solving the deformation of elasto-plastic solids.
- Also upper- and lower-bound solutions, which are approximate solutions, can be very useful in engineering.
- One of the methods used is the slip-line field method, which gives a physical feel for the deformation process. It is an exact analysis for deformation of rigid-perfectly plastic solids.

- Three different types of pd equations:
 - Elliptic (elastic deformation)
 - Parabolic (heat transfer, mass transfer)
 - Hyperbolic equations (wave propagation, plastic deformation

• Consider the following second-order partial differential equation:

$$a \stackrel{\partial^2 z}{=} + b \stackrel{\partial^2 z}{=} + c \stackrel{\partial^2 z}{=} = e \square$$

Boundary conditions :

z,
$$\frac{\partial z}{\partial x}$$
, and $\frac{\partial z}{\partial y}$ are specified.

Then the variation of $\frac{\partial z}{\partial x} = \frac{\partial z}$

$$d(\frac{\partial z}{\partial x}) = \frac{\partial^2 z}{\partial x^2} dx \boxplus \frac{\partial^2 z}{\partial x \partial y} dy \square$$

$$d(\frac{\partial z}{\partial y}) = \frac{\partial^2 z}{\partial x \partial y} dx \boxplus \frac{\partial^2 z}{\partial y^2} dy \square$$

We have three equations and three unknowns $\frac{\partial^2 z}{\partial x^2}$, $\frac{\partial^2 z}{\partial x \partial y}$, and $\frac{\partial^2 z}{\partial y^2}$.

Solving for
$$\frac{\partial^2 z}{\partial x^2}$$
,

$$\frac{\partial^2 z}{\partial x^2} = \frac{|N|}{|D|}$$

Depending on whether |D| equal to orgreater than 0, the pde represents different physical phenomena.

 b^2 - 4ac < 0, elliptic equation.

 b^2 - 4ac > 0, hyperbolic equation.

 b^2 - 4ac = 0, parabolic equation.

The Upper- and the Lower-Bound Solutions

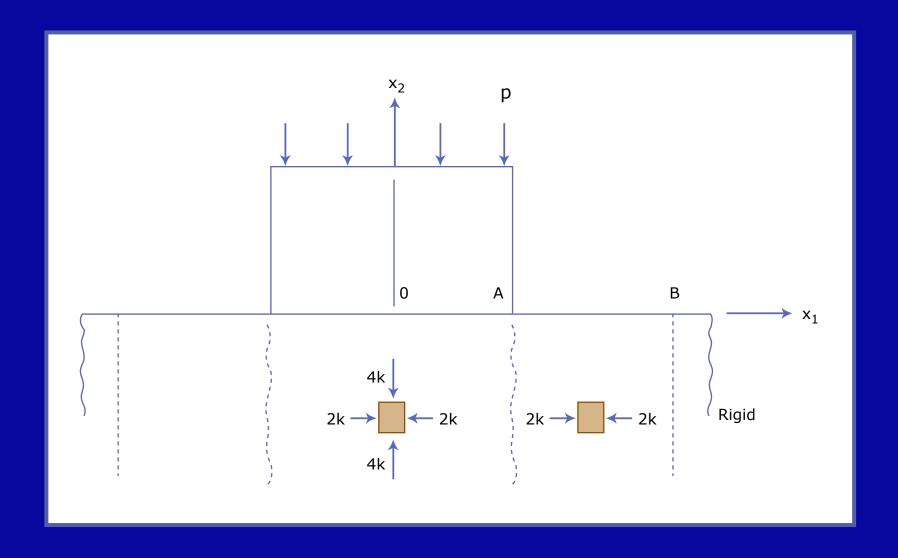
• We want to get approximation solutions for large deformation of rigid-perfectly plastic solid in plane strain.

- We have to satisfy
 - Equilibrium condition (F=ma)
 - Geometric compatibility
 - Stress-strain relationship (constitutive relationship)
 - Yield condition
 - Boundary conditions

The Upper- and the Lower-Bound Solutions

- Lower bound solutions are obtained if we satisfy
 - Equilibrium condition
 - Yield condition
 - Boundary conditions on stress
- Consider the punch indentation problem. The lower-bound can be obtained as

The Lower-Bound Solutions

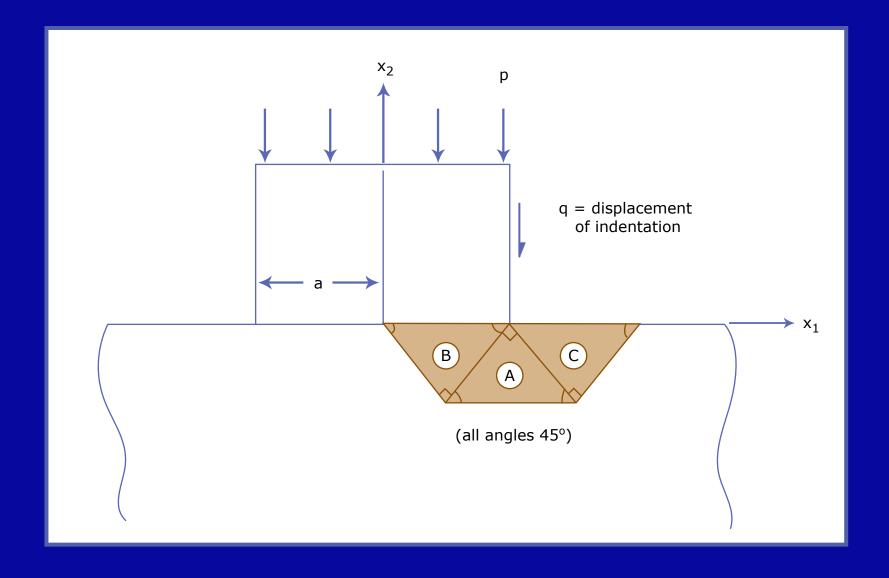


The Upper-Bound Solutions

The upper-bound-solutions are obtained by satisfying the following for an assumed displacement field:

- 1. Incompressibility condition
- 2. Geometric compatibility
- 3. Velocity boundary conditions.

The Upper-Bound Solutions



The Lower- and the Upper-Bound Solutions

The lower – bound solution

$$p \ge 4k$$

The upper — bound solution

$$p \le 6k$$

Equilibrium condition in plane strain:

$$\frac{\partial \sigma_{xx}}{\partial x} + \frac{\partial \sigma_{xy}}{\partial x} = 0$$
$$\frac{\partial \sigma_{yx}}{\partial x} + \frac{\partial \sigma_{yy}}{\partial x} = 0$$

The Tresca yield condition:

$$\sigma_I - \sigma_{III} = 2k$$

The stresses can be represented in terms of two invariants, p and k, as

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The Tresca yield condition:

$$\sigma_I - \sigma_{III} = 2k$$

The stresses can be represented in terms of two invariants, p and k, as

$$\sigma_{xx} = -p - k \sin \phi$$

$$\sigma_{yy} = -p + k \sin \phi$$

$$\sigma_{xy} = k \cos \phi$$

where

$$p = -\frac{\sigma_{xx} + \sigma_{yy}}{2}$$

Characteristic lines:

$$\frac{dy}{dx} = \tan \phi \qquad \qquad \alpha - \text{lines}$$

$$\frac{dy}{dx} = -\cot \phi \qquad \qquad \beta - \text{lines}$$

Characteristic equations:

$$p+2k\phi=$$
 constant $\alpha-$ lines $p-2k\phi=$ constant $\beta-$ lines

The Slip-line Field Solution for Asperity Deformation

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The Slip-line Field Solution for Asperity Deformation

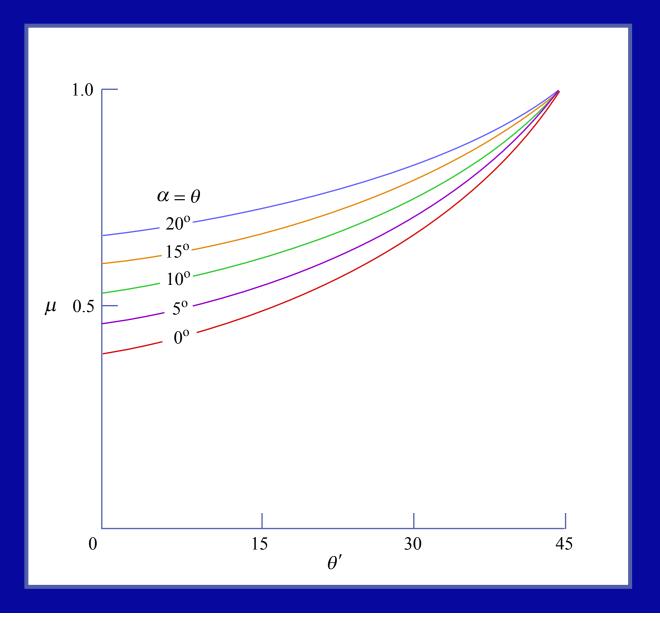


Figure by MIT OCW. After Suh, N. P., and H. C. Sin. "The Genesis of Friction." Wear 69 (1981): 91-114.