Final Presentation: Boat Crew

Professor: Franz Hover

Lab Instructor: Harrison Chin

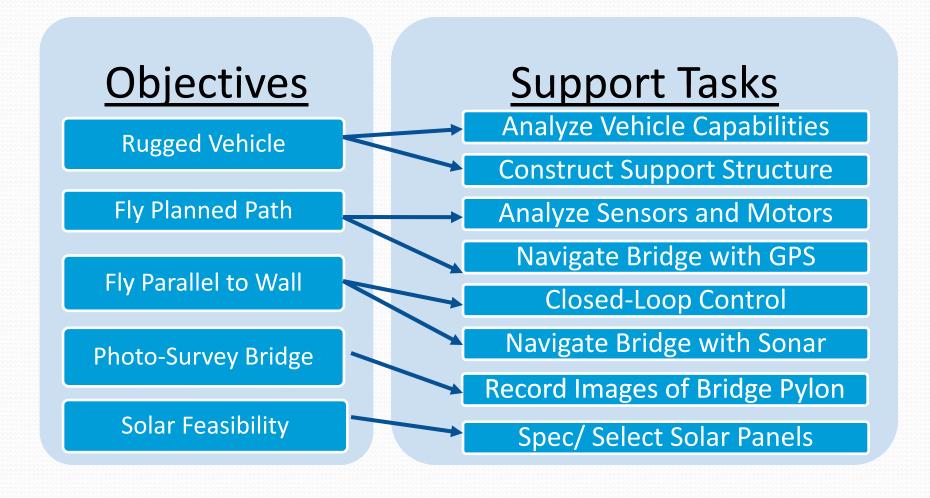
2.017 Fall 2009

December 10, 2009

Group 2

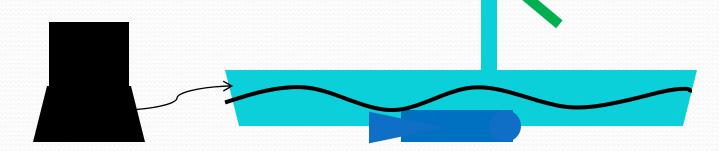
Mission Objective Tree

Goal: Autonomously travel to and survey Harvard Bridge Pylons.



Project Division

- Vessel Structure Physical Components
- Sensors GPS, Sonar, etc.
- Propulsion Motors
- Control Data Collection, Commands
- Solar Panel Selection/Integration
- Environment Waves



Vessel Design

Student D

- Vessel Modifications
- Buoyancy
- Weight and Trim
- Final Design

Vessel Modifications

Motivation: needed survivable & rugged vessel

- Functional Requirements:
 - Stable
 - Maneuverable
 - Sensor mounts
 - Rugged design

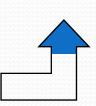


PT 2017

Photo of the Pro Boat Miss Elam 1/12 Brushless RTR removed due to copyright restrictions.





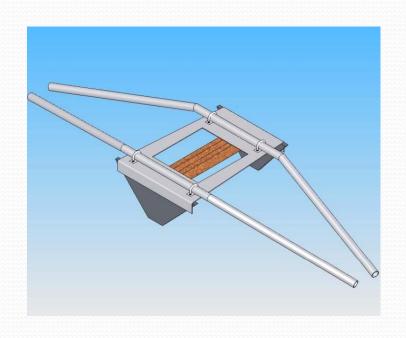


Pro Boat Miss Elam

Spirit of the Challenge

Final Design

- Trimaran
 - Stability pontoons
 - Maneuverability = motors mounted outboard
 - Sensor mounts = metal sheet + hull structure



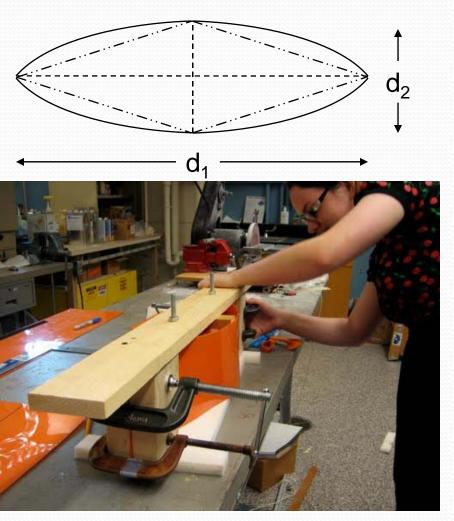


Pontoon Size Calculations

$$V = A_{\text{waterline}} \cdot h \sim A_{\text{kite}} \cdot h$$

Streamline : $d_1/d_2 \sim 3$

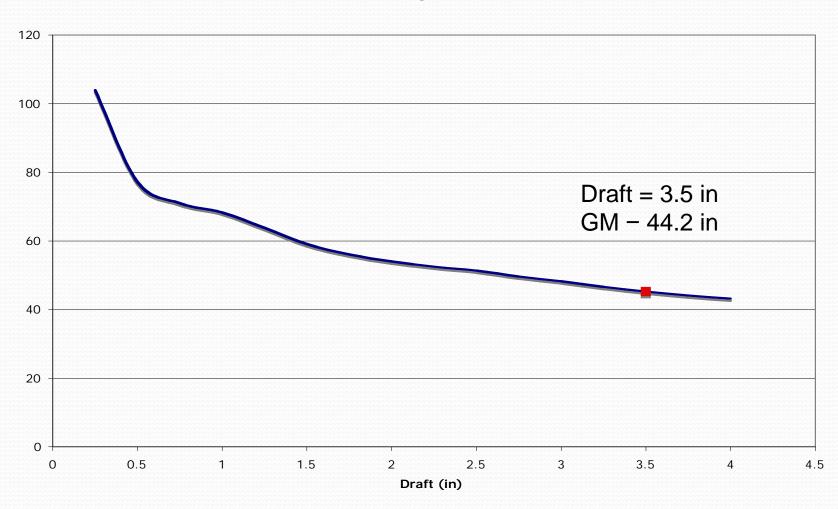
$$V = .5(d_1)(d_2)(h)$$
= .5(6")(18")(5.75")
= **310.5** in³ > 303 in³



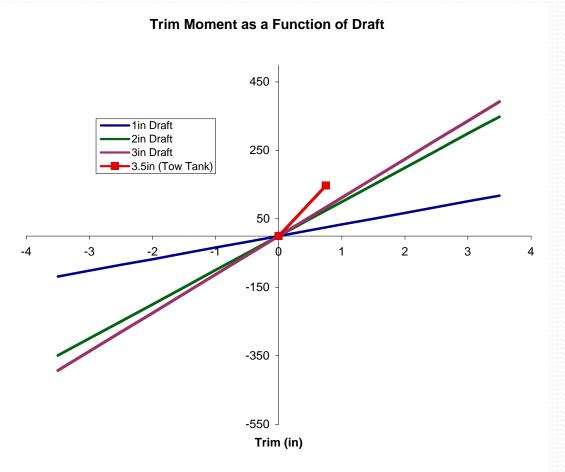
Mold to shape pontoons

Hull Stability

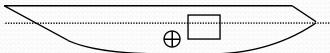
Metacentric height v. Draft



Hull Trim



Port-Starboard trim with symmetry



- Loaded with battery and pontoon assembly only:
- Freeboard = 0 in !



- Loaded with extra 3.5 lbs at bow:
- Freeboard = 0.75 in

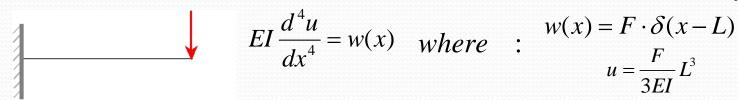
Stress Analysis

Student B

- Pontoon Wave Forcing
- Wave –Frequency Resonance
- Transportation Stress Hazards
- Crashworthiness-

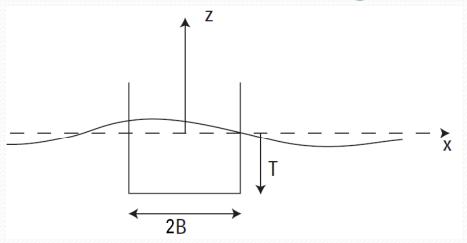
Spring-Mass Resonance Model

Single cantilever beam w/point loading : Euler Bernoulli Equation



- Mass –Spring System: $F = -k \cdot u$ $k = \frac{3EI}{L^3}$
- Resonant frequency: $\omega = \sqrt{\frac{k}{m}}$
- Vessel Natural Frequency: ω = 83Hz
- Far higher than frequency of water waves!
- Near frequency of transportation vibrations
 - Switch bolt attachments to delrin wingnuts

Wave Forcing on Pontoon



$$\overrightarrow{F}_{FK} = -\iint_{Sw} \overrightarrow{pnds}$$

$$F_Z = \frac{l2\rho age^{-kT}\cos(\omega t)\sin(kb)}{k}$$

$$F_{zMax} = \frac{L2\rho age^{-kT}\sin(kb)}{k} = 166N$$

• B =
$$0.075$$
m, T = 0.1 m

• Worst-case waves : ω = 1Hz A= 0.3m

• Deep water waves:

$$k = \frac{\omega^2}{m} \sim 0.1$$

• Surface pressure integration:

$$F_x - 2L\rho ag(1 - e^{-kt})\sin(\omega t)\sin(kb)$$

$$F_{xMax} = 2L\rho ag(1 - e^{-kt})\sin(kb)$$

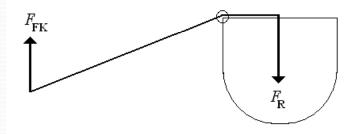
$$F_{xMax} = 0.44N$$

Implications of wave forcing

- Forcing moment: 50Nm
 - Horizontal force on pontoon is negligible
 - Vertical force causes moment
- Reaction force on boat structure: 277.8N
- Bend in pipes
 - Stress calculated using $\sigma = \frac{MR}{I}$
 - Max stress: 8.8 x 10⁶ Pa
 - Yield stress of aluminum: 4 x 10⁸ Pa
- Force on bolts
 - Originally, load distributed over 6 bolts
 - Total force on each bolt is 46.3N

Danger zones:

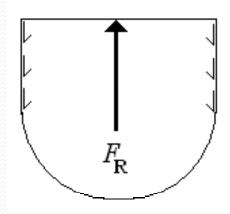
- Strut bend
- Structural bolts



If stress is too high, the internal structure could be ripped completely out of the boat!

Failure of internal boat structure

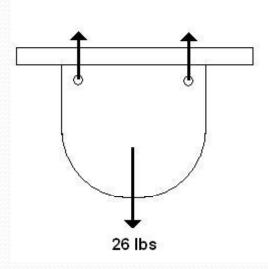
- Internal structure to which pontoons are mounted is held onto hull with epoxy
- Approximate that most stress on epoxy is in the shear direction



- Epoxy much weaker in 'peel' forcing
- Peel forcing unlikely: hull not pulled outwards independent of plate
 - Shear force per unit area of epoxy contact: 1.5 x 10⁴ Pa
 - Shear strength of epoxy: 1.4 x 10⁷ Pa

Transportation and Handling

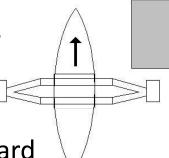
- Most likely transportation method is to carry by frame
- Potential problems due to weight of boat:



- Total weight of boat hull and components: 26lbs
- •Stress on epoxy << than rated shear stress (8,000 PSI)</p>
- •Original 6-bolt design: 19.3N per attachment point
 - Internal boat structure failure possible
- Design modified to reduce these issues
 - Number of bolts increased to 12

Pontoon Arm Collision

- Impact creates moment around central attachments
 - U-bolts on plate act as moment constraint
 - Peel forces on epoxy
- Crash 1 pontoon while boat travelling at 1 ms⁻¹ forward
 - Relevant for mission and for vessel transportation
- Results:
 - Moment around center 15.87 Nm
 - Force per U-bolt 31.24 N (U-bolt max. rating: 1935 N)
 - Average force on epoxy 89.25 N
 - Total peel strength of epoxy 91.44 N/mm epoxy peeled



GPS, Compass, and Sonar

Student E

- Reading GPS Data
- GPS Test Results
- Reading Compass Data
- Reading Sonar Data

Global Positioning System

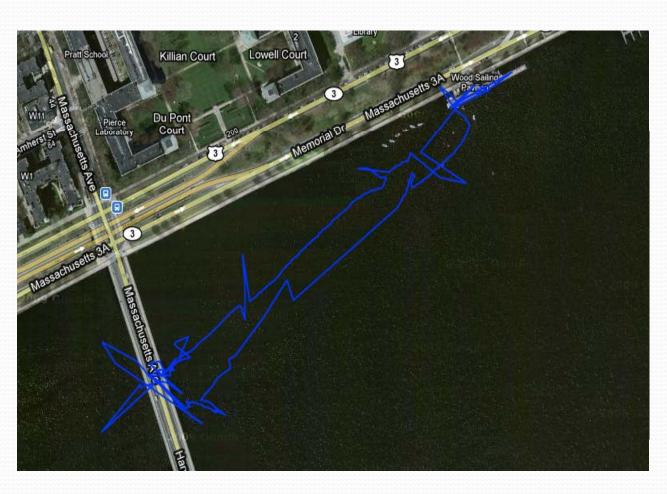
• Standard Format:

GPRMC,135713.000,A,4221.4955,N,07105.5817,W,4.29,258.17,310809,,*16

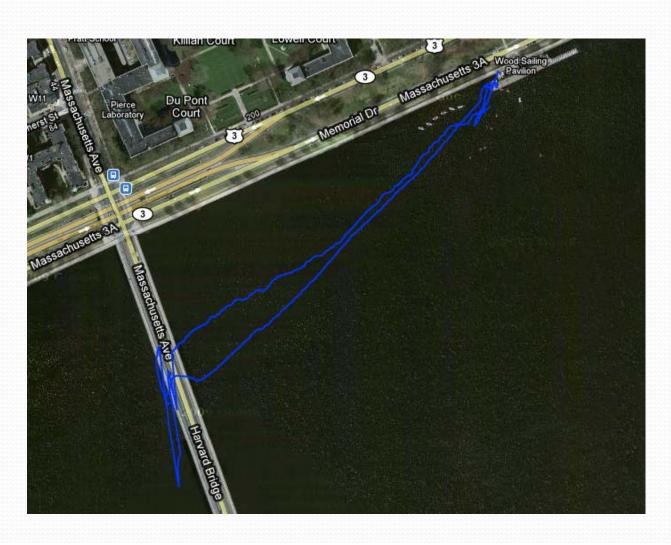
- GPS shield is used on Arduino MEGA
 - 1 signal hit/second



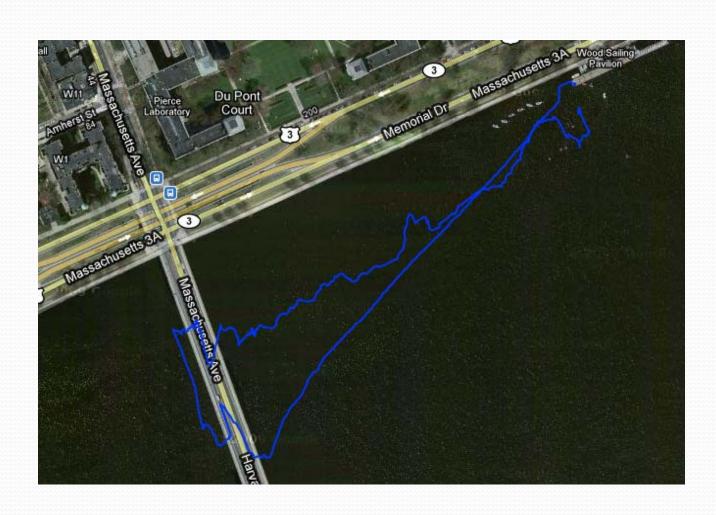
Trial 1



Trial-2

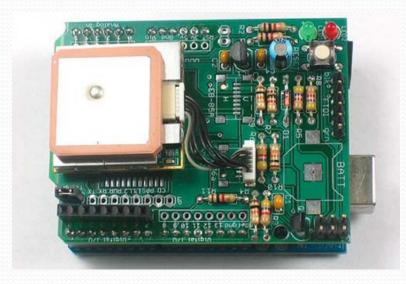


Trial-3



GPS Output

- Imaginary X-Y coordinate system
 - Sailing pavilion as the origin
- GPS latitude and longitude processing:
 - Decoded into x-y coordinates
 - Sent as an input to control system



OS5000 3-Axis Compass

- Primary Navigation
 - Low Noise
 - Works under the bridge
 - Faster refresh rate than GPS
- Outputs to Control System
 - Heading: 0 to 360 degrees
 - Pitch: -90 to +90 degrees
 - Roll: -180 to +180 degrees

LV MaxSonar WR-1

Range 0-255 inches

Photo of the MaxSonar WR1

http://www.active-robots.com/products/sensors/maxbotix/WR1-large.jpg removed due to copyright restrictions.

- Analog and serial output
 - Analog accurate 1" of serial output
 - Maintain moving average of analog output
- Fully waterproofed
- Mounted to servo
- Run at pre-set heading until wall is detected
- Wall detection @ 3.05 m,
- Accurate reliable readings @ 2.13 m
- Safety buffer of 1.52 m from wall

Mission Planning and Data Logging

Student A

- Selected Sonar
- Wall Finding
- Wall Following
- Control Architecture

Mission Planning

- Mission stored as an array of way points
 - Sample way point: { x, y, heading, speed, range, mode }
- Modes describe behavior of boat

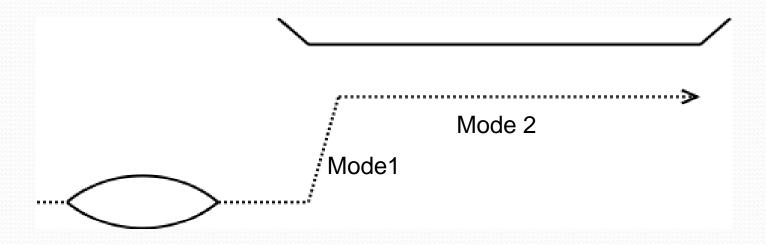


Test Mission

- Unreliable GPS and sonar data
- Reliable compass data
- Internal clock, counting time
- Mission composed of target headings, and times at which to change way points

Wall Finding and Following

- Two modes:
 - Mode 1: Travel at set heading until wall is detected
 - Mode 2: Hold constant distance from wall, assumed to face a known heading



Data Collection

- Serial
 - GPS: Position
 - Compass: Heading, Pitch and Roll
- Analog
 - Sonar: Range
 - Solar: Voltage Output
- Internal
 - Time: Since program start up
 - Way point and error



Data Logging

- Logging constrained to <1 Hz
 - Higher speed causes serial buffers to fill
- Logged to an onboard netbook
 - Data stored via Realterm
 - Formatted for MATLAB importing
- External GPS data stored on SD card





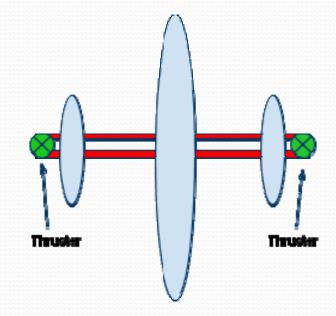
Propulsion and Control

Student C

- Propulsion and Speed Control
- Thrust Tests
- MATLAB Simulations
- Real-World Tests

Propulsion System Design

- 2 Thrusters
 - 1 per outer hull
 - Differential thrust for yaw
- PWM control with Arduino and Speed Controllers
- 12V DC Trolling Motors



Speed Controller Selection

- Pro Boat 40A Waterproof ESC
 - Limited PWM frequency range
 - Incompatible with Arduino PWM
- Victor 884 ESC
 - Compatible with Arduino
 - Not Waterproof

Photos removed due to copyright restrictions.

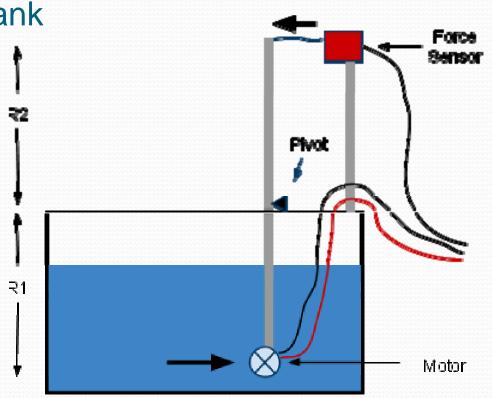
Please see:

Pro Boat Waterproof ESC with Reverse 5-12V 40A

VEX Robotics Victor 884 + 12V Fan

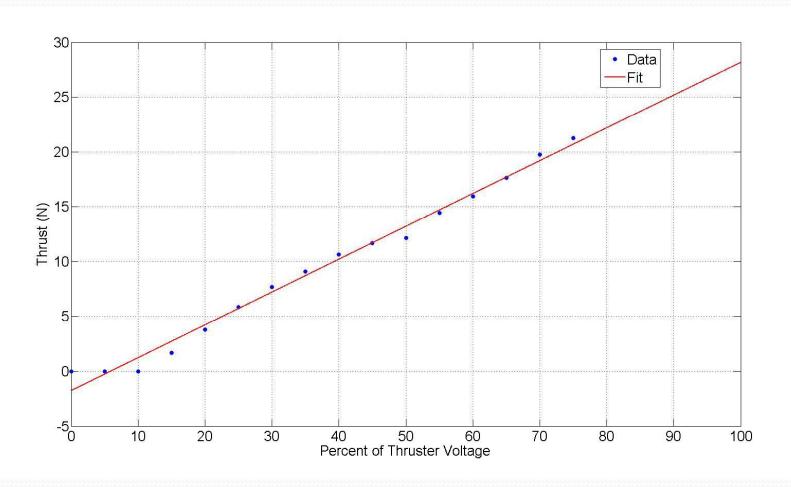
Thrust Test

- Test conducted in water tank
- Thrust was measured at different motor voltages
- Data fit to linear curve
- Maximum vehicle thrust=2X28.17N=56.3N
- Minimum voltage=1.5V



Force=Sensor Force X R2/R1

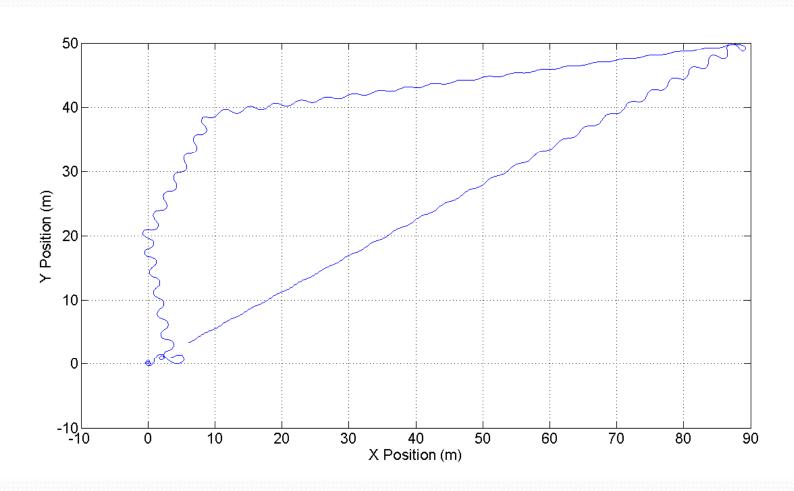
Thrust Test Data



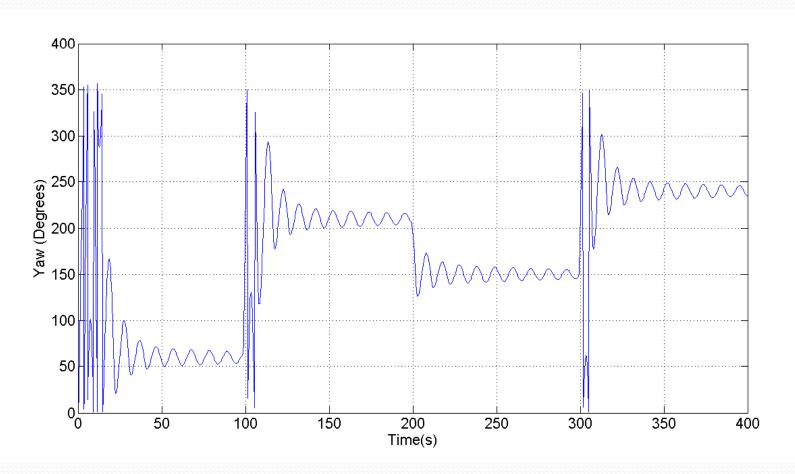
Control System and MATLAB Simulation

- Closed-loop proportional control
 - heading and speed using sonar, GPS, and compass
- Mission set-points determine control behavior
 - Way-point Traveling
 - Static Heading Following
 - Wall Following
- Boat and control system modeled in MATLAB using ODE45
 - M, J, B(lateral), B(rotational)
- Various set-points were used as inputs to adjust the gains

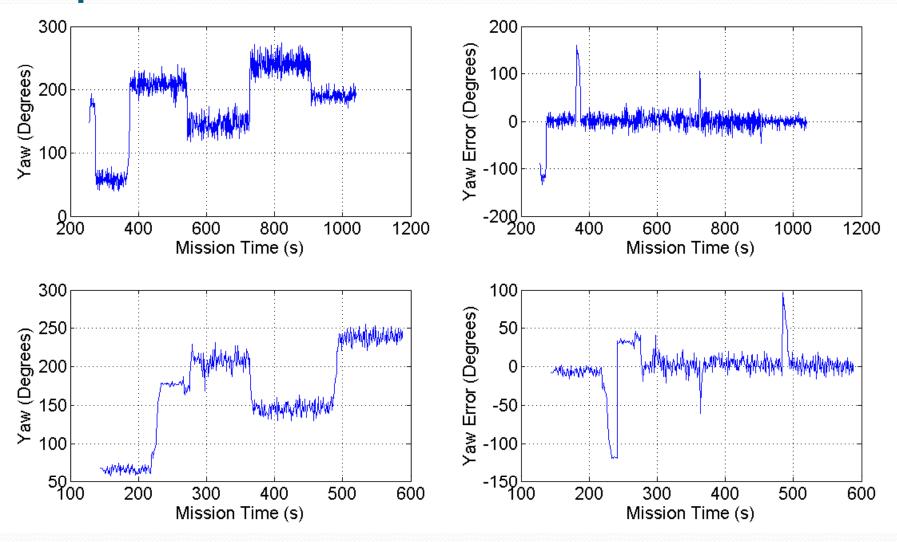
Simulations



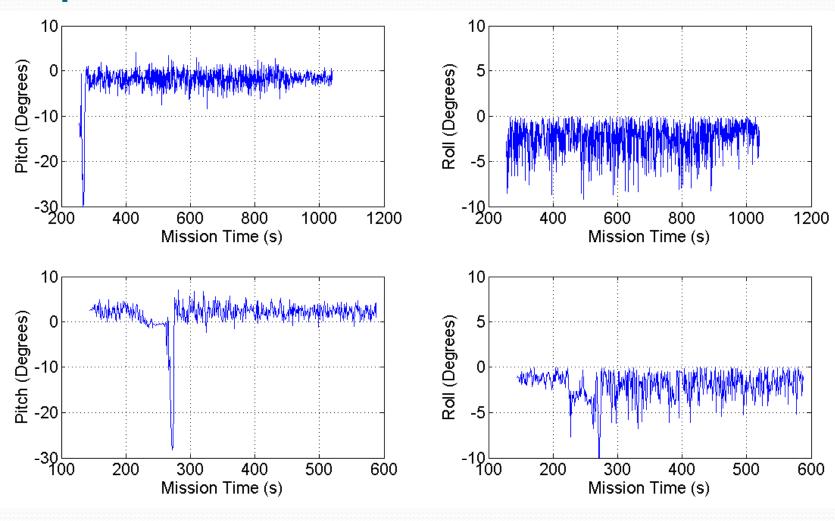
Simulations



Experiments



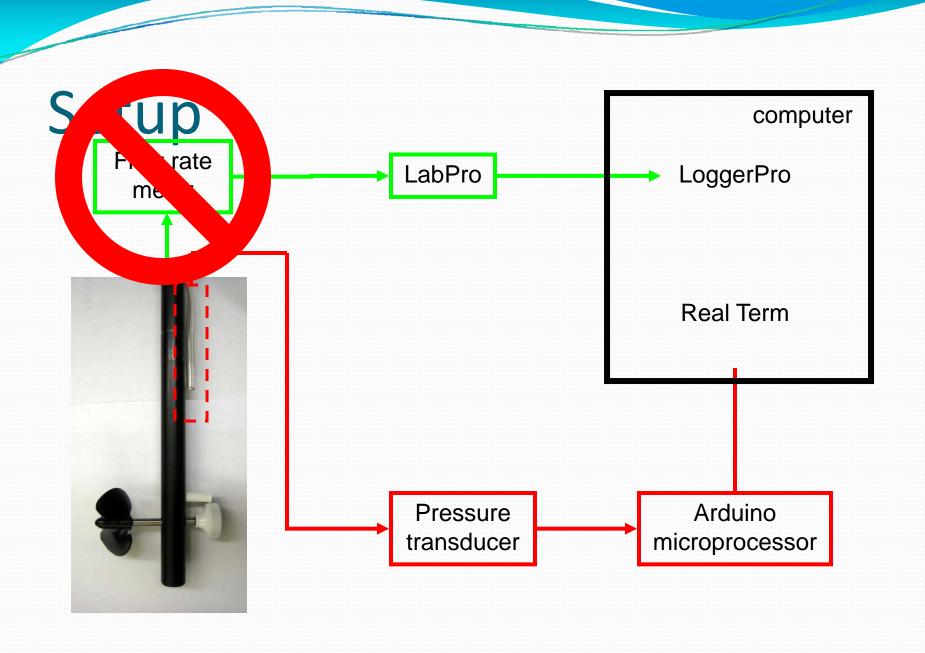
Experiments



Wave Environment

Student F

Characterize wave spectrum of Charles River



River Wave Data

Case 1

- Fair weather
- No Wind
- No river activity

Case 2

- Raining
- Steady wind
- No river activity

- Case 3
- Fair weather
- Slight wind
- High boat traffic

Case 4

- Raining
- High winds
- No river activity
- Test Day

River Wave Data

Case 1

- Fair weather
- No Wind
- No river activity

Case 2

Raining

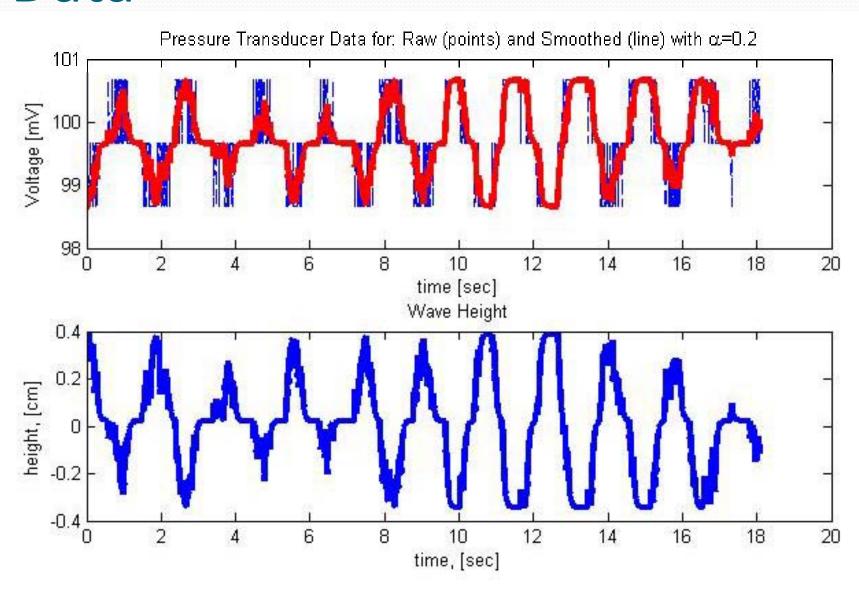
Steady wind

No river activity

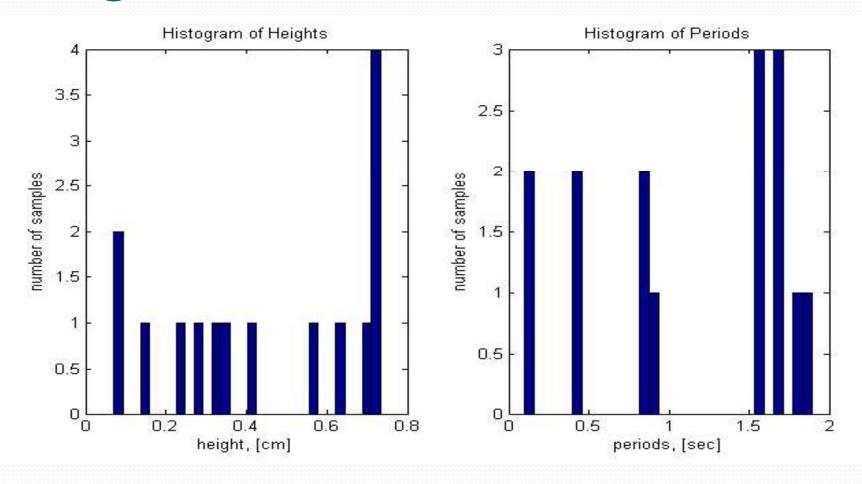
Case 3
Fair weather
Slight wind
High boat traffic

Case 4
Raining
High winds
No river activity
Test Day

Data



Heights and Wave Periods



Average 1/3 wave height = 0.7174 cm

Average period length = 1.1487 s

River Wave Data

Case

Fair weather

No Wind

No river activity

Case 2

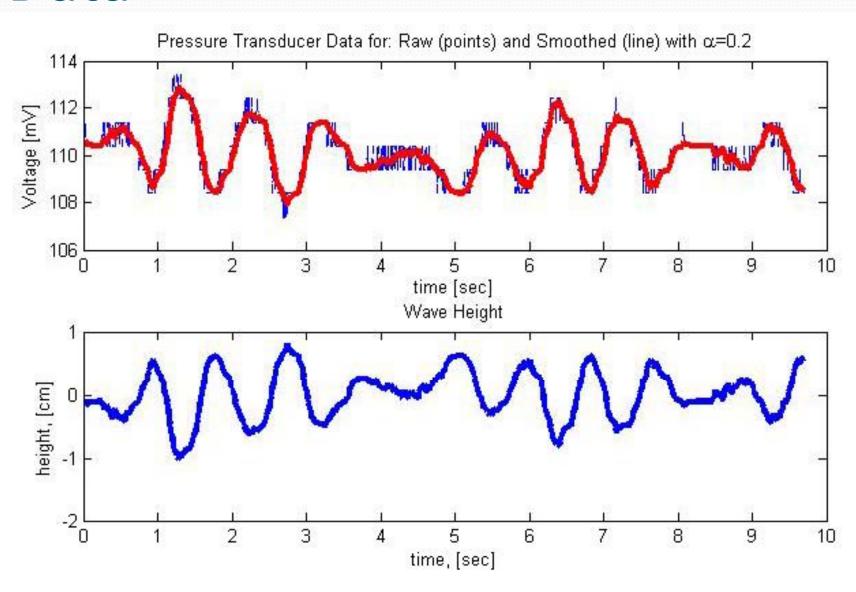
- Raining
- Steady wind
- No river activity

Case 3
Fair weather
Slight wind
High boat traffic

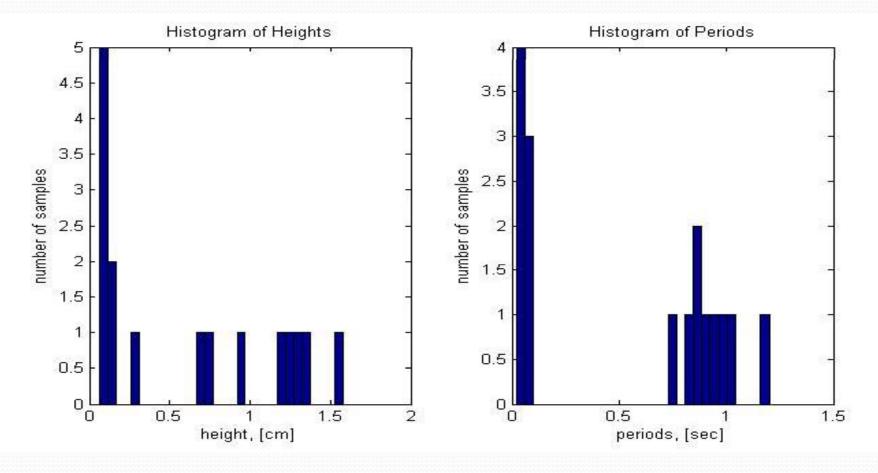
Case 4
Raining
High winds
No river activity

Test Day

Data



Heights and Periods



Average 1/3 wave height = 1.3295 cm

Average period length = 0.5450 s

River Wave Data

Case

Fair weather

No Wind

No river activity

Case 2

Rair

Moderate wind

No river activity

- Case 3
- Fair weather
- Moderate wind
- High boat traffic

Case 4

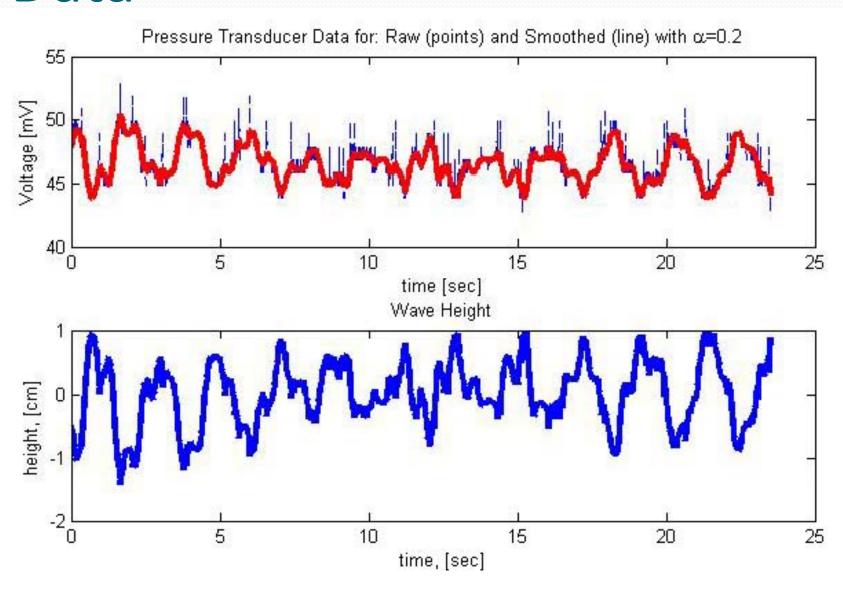
Rain

High winds

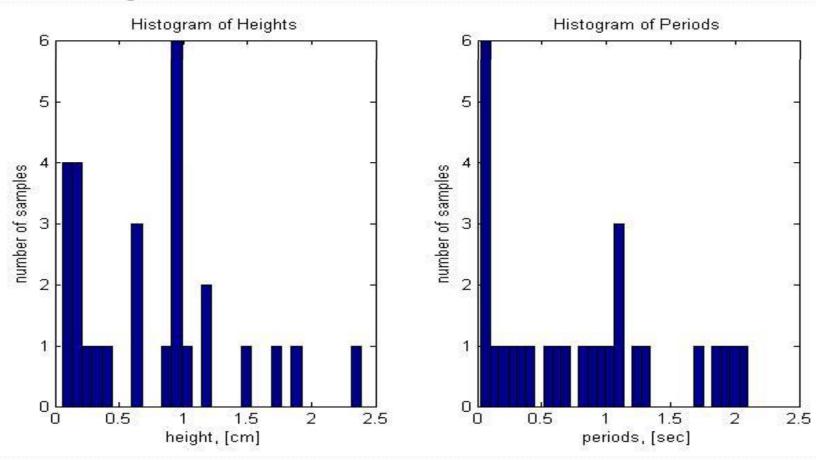
No river activity

Test Day

Data



Heights and Periods



Average 1/3 wave height = 1.4242 cm

Average period length = 0.8082 s

River Wave Data

Case

Fair weather

No Wind

No river activity

Case 2

Rain

Steady wind

No river activity

Case 3

Fair weather

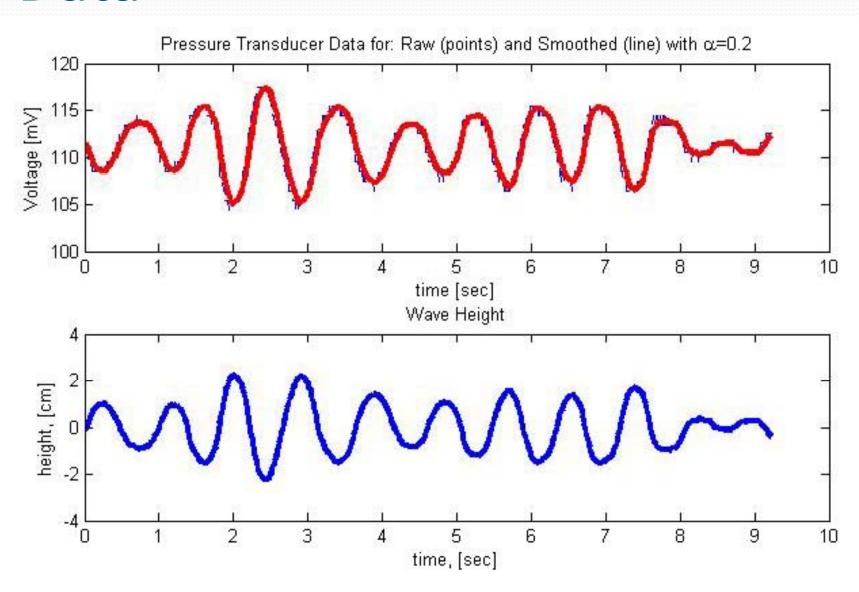
Slight wind

High boat traffic

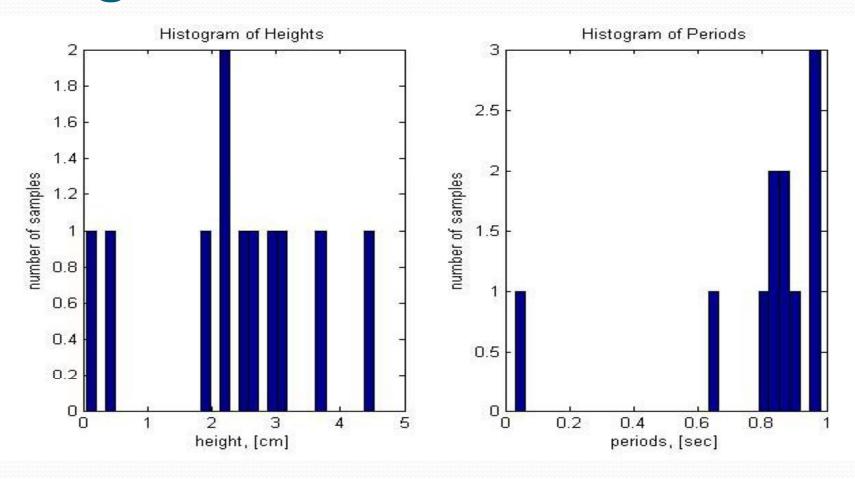
Case 4

- Rain
- High winds
- No river activity
- Test Day

Data



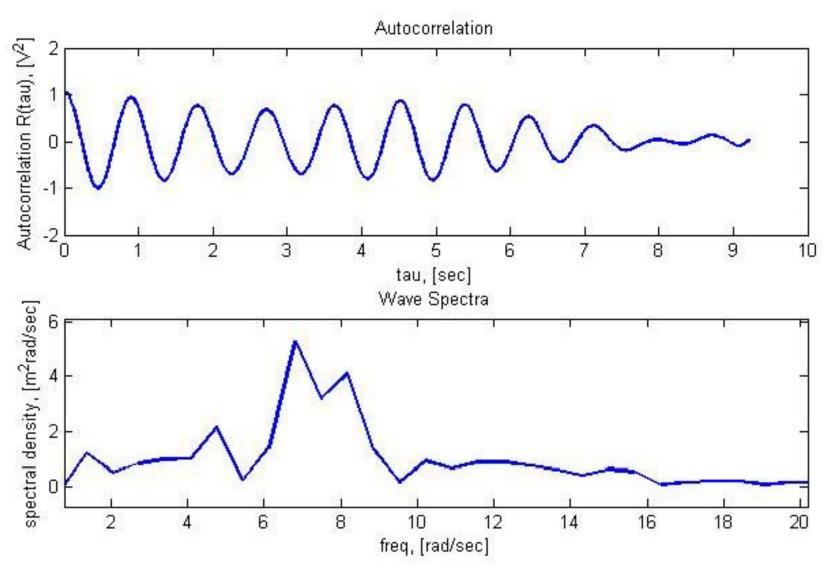
Heights and Periods



Average 1/3 wave height = 3.5856 cm

Average period length = 0.7936 s

Wave Spectra



Conclusions

- No real current
- Waves driven by two sources
 - Wind
 - River activity
- Frequency faster in presence of wind source
- Need more data!

Solar Energy

Student G

- Vehicle Requirements
 Power Output Test
- System Integration
- Feasibility Comparison

Project Overview

- Tasked with feasibility assessment for solar power use
- Desired quantitative data

Assess Vehicle Requirements Select Panels Check Panel Specifications

Integrate System Full System Test

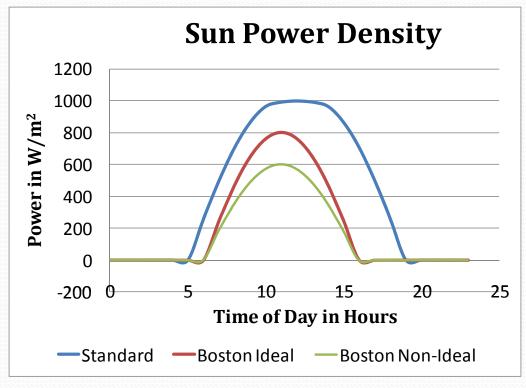
Vehicle Requirements

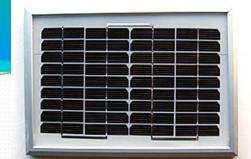
| Component | Voltage | Current | Power | | | | | | |
|---------------|------------------------------|---------|---------|--|--|--|--|--|--|
| Accelerometer | 6 V | 50 mA | 0.300 W | | | | | | |
| Sonar | 5 V | 50 mA | 0.250 W | | | | | | |
| GPS | 3.3 V | 50 mA | 0.165 W | | | | | | |
| Arduino Mega | 5 V | 50 mA | 0.25 W | | | | | | |
| | Electronics Total: | | | | | | | | |
| Motors (Min) | 12 V | 0.25 A | 3 W | | | | | | |
| Motors (Max) | 12 V | 2.50 A | 30 W | | | | | | |
| | Vehicle Minimum Total: | | | | | | | | |
| | Vehicle Maximum Total Total: | | | | | | | | |

Correcting Specifications

- Panel output: $P_{out} = \eta_{panel} E_{density} A_{panel}$
- Standard Peak E_{density}: 1000 W/m² (noon @ equator)
- Boston Dec. Peak E_{density}: 800 W/m²
- Ideal: 10am on sunny day
 - 600 W/m²
- Non-ideal: 10am Cloudy
 - 200 W/m²
- Power through day:

$$P(t) = P \cdot \sin(t - t_{dawn} / t_{dusk} - t_{dawn} \cdot \Pi)$$





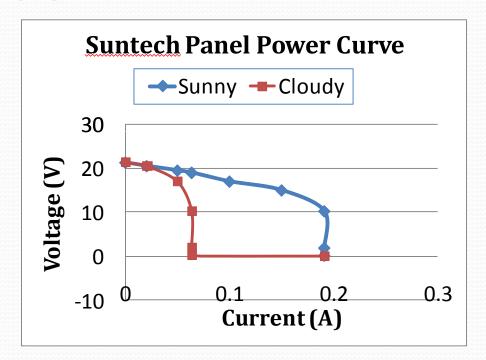
Suntech STP0055-12

Estimated Capabilities

- Peak Rated Power = 5W
- Peak Power (sunny)= 3W
- Peak Power (rainy) = 1W

Measured Capabilities

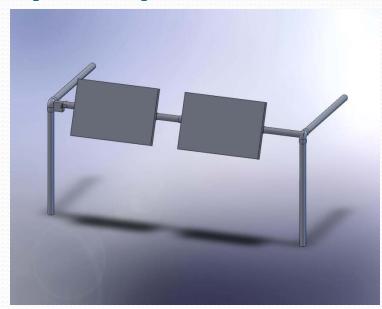
- Sunny:
 - Short Circuit Current : 0.21 A
 - Measured Output: 2.8 W
- Cloudy
 - Short Circuit Current: 0.065 A
 - Measured Output: 0.933 W



$$P = VI + \frac{V^2}{R}$$

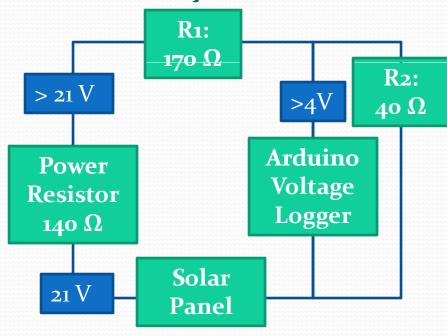
System Integration

Physical System



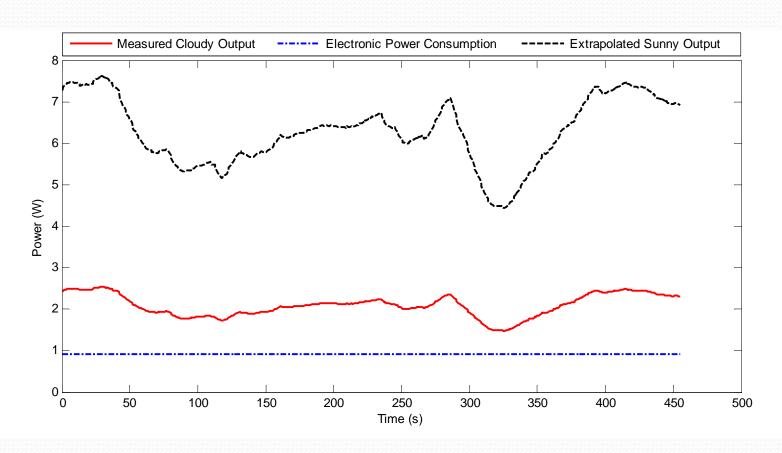
- Panels sit on motor mounting
- Servo available for optimization

Electronic System

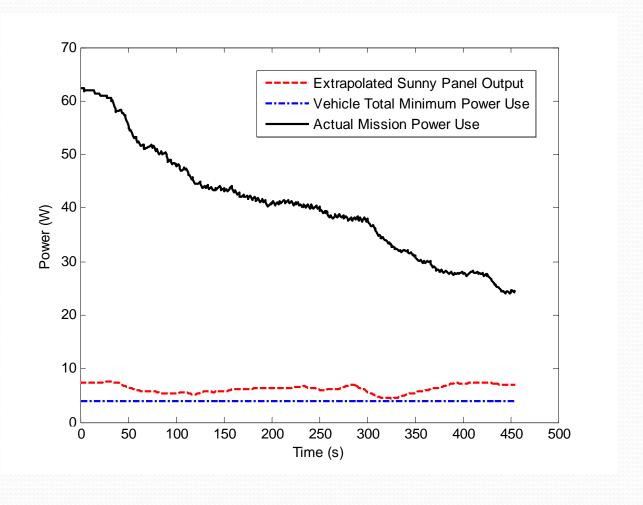


$$V_{out} = \frac{R_2}{R_1 + R_2} V_{in}$$

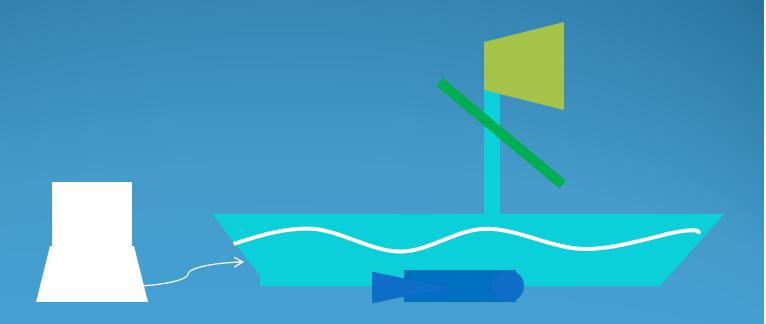
Feasibility- Electronics



Full Vehicle Feasibility



Summary and Next Steps

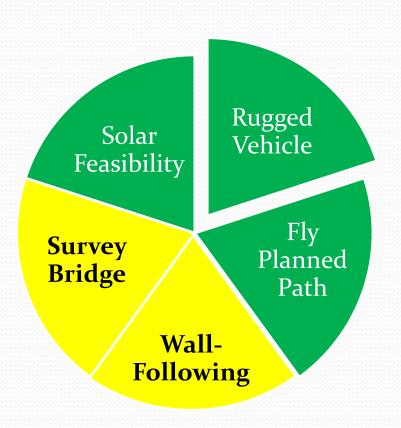


Mission Video

- View from vessel
- View from shore



Final Evaluation



- Vehicle survived well
 - Deployment & leaks
- Path followed
- Solar power sufficient
- No time for bridge test
 - Capability Present
- Wall following untested

Future Mission Objectives

- Add full GPS navigation capabilities
- Use Sonar for wall following
- Remote data logging abilities
- Actively control solar panel angle
- Test in warmer drier weather!!



Special Thanks to:

Franz Hover Harrison Chin

Josh Leighton Charlie Ambler

MIT Sailing Pavilion MIT Towing Tank

Mechanical Engineering Department Center for Ocean Engineering

Chevron Schlumberger

Questions?

Naval Architecture Spreadsheet

• Displacement v. draft

| | | | | | | | Draft | s (in) | | | | | | | | | | |
|-------------------------|-------------------|--|----------|----------|----------|---|-----------|--------------|----------|----------|----------|----------|----------|----------|----------|----------|----------|----------|
| Simpson's Aultipier: | | 0.25 | 0.5 | 0.75 | 1 | 1.25 | 1.5 | 1.75 | 2 | 2.25 | 2.5 | 2.75 | 3 | 3.25 | 3.5 | 3.75 | 4 | |
| | 1 Does | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| - 1 | 2 Section | 0 | 0 | 0 | 0 | 0 | 0.25 | 0.5 | 0.75 | 1 | 1.25 | 1.5 | 1.75 | 2 | 2.25 | 2.5 | 2.75 | |
| | 4 Matterfor | 0 | 0.25 | 0.5 | 0.75 | 1 | 1.25 | 1.5 | 1.75 | 2 | 2.25 | 2.5 | 2.75 | 3 | 3.25 | 3.5 | 3.75 | |
| - 1 | 2 Draft? | 0 | 0.25 | 0.5 | 0.75 | 1 | 1.25 | 1.5 | 1.75 | 2 | 2.25 | 2.5 | 2.75 | 3 | 3.25 | 3.5 | 3.75 | |
| | 4 | 0.25 | 0.5 | 0.75 | 1 | 1.25 | 1.5 | 1.75 | 2 | 2.25 | 2.5 | 2.75 | 3 | 3.25 | 3.5 | 3.75 | 4 | |
| - 1 | 2 | 0.25 | 0.5 | 0.75 | 1 | 1.25 | 1.5 | 1.75 | 2 | 2.25 | 2.5 | 2.75 | 3 | 3.25 | 3.5 | 3.75 | 4 | |
| | 4 | 0.25 | 0.5 | 0.75 | 1 | 1.25 | 1.5 | 1.75 | 2 | 2.25 | 2.5 | 2.75 | 3 | 3.25 | 3.5 | 3.75 | 4 | |
| 1 | 2 | 0 | 0 | 0 | 0 | 0.25 | 0.5 | 0.75 | 1 | 1.25 | 1.5 | 1.75 | 2 | 2.25 | 2.5 | 2.75 | 3 | |
| | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.25 | 0.5 | 0.75 | 1 | 1.25 | 1.5 | |
| - 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | . 0 | 0 | 0 | 0 | 0 | 0 | 0.25 | 0.5 | 0.75 | 1 | |
| | | | | | | As | sumed B(1 |) = sqrt(T/C | (x) | | | | | | | | | |
| | | 4.082483 | 5.773503 | 7.071068 | 8.164966 | | | | | 12.24745 | 12.90994 | 13.54006 | 14.14214 | 14.7196 | 15.27525 | 15.81139 | 16.32993 | |
| | Station Number | Integrand : B(T) Draft * Section Coefficient | | | | | | | | | | | | | | | | |
| | 1 | 0 | 0 | 0 | 0 | provide the law | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| | 2 | | . 0 | 0 | 0 | . 0 | 4.5 | 9.721111 | 15.58846 | 22.04541 | 29.04738 | 36,55817 | 44.54773 | 52,99057 | 61.86477 | 71.15125 | 80.83316 | |
| | 3 | 0 | 2.598076 | 6.363961 | 11.0227 | 16,43168 | 22.5 | 29.16333 | 36.37307 | 44.09082 | 52.28528 | 60.93029 | 70.00357 | 79,48585 | 89.36023 | 99,61175 | 110.227 | |
| | 4 | 0 | 2.598076 | 6.363961 | 11.0227 | 16,43168 | 22.5 | 29.16333 | 36,37307 | 44.09082 | 52,28528 | 60.93029 | 70.00357 | 79,48585 | 89.36023 | 99.61175 | 110.227 | |
| | 5 | 1.837117 | 5.196152 | 9.545942 | 14.69694 | 20.5396 | 27 | 34.02389 | 41.56922 | 49.60217 | 58.09475 | 67.02332 | 76.36753 | 86.10967 | 96.23409 | 106.7269 | 117.5755 | |
| | 6 | 1.837117 | 5.196152 | 9.545942 | 14.69694 | 20.5396 | 27 | 34.02389 | 41,56922 | 49.60217 | 58.09475 | 67.02332 | 76.36753 | 86,10967 | 96.23409 | 106,7269 | 117,5755 | |
| | 7 | | 5.196152 | | | 20.5396 | 27 | 34.02389 | 41.56922 | 49.60217 | 58.09475 | | | 86,10967 | | 106,7269 | 117.5755 | |
| | 8 | | 0 | | | 4.107919 | 9 | 14.58167 | 20.78461 | 27.55676 | 34.85685 | 42.6512 | 50.91169 | 59.61439 | 68.73864 | 78.26637 | 88.18163 | |
| | 9 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | | 6.093029 | | | | | | |
| | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | | | | 13.74773 | | | |
| | | | | | | | Sum Ove | Sections | | | | | | | | | | |
| | | 5.511352 | 20.78461 | 41.36575 | 66.13622 | 98.59006 | 139.5 | 184.7011 | 233.8269 | 286.5903 | 342.759 | 408.2329 | 477.2971 | 556.4009 | 639.2693 | 725.7427 | 815.6801 | |
| | Multiplier: | 2.906667 | 2.906667 | 2.906667 | 2.906667 | 2.906667 | 2.906667 | 2.906667 | 2.906667 | 2.906667 | 2.906667 | 2.906667 | 2.906667 | 2.906667 | 2.906667 | 2.906667 | 2.906667 | |
| Submerged ' | Volume: | 16.01966 | 60.41393 | 120.2364 | 192.236 | 286.5684 | 405.48 | 536.8646 | 679.6567 | 833.0225 | 996.2862 | 1186.597 | 1387.344 | 1617.272 | 1858.143 | 2109.492 | 2370.91 | in^3 |
| - | | | | | | | | | | | | | | | | | | |
| Density of W | | 62.4 | 62.4 | 62.4 | 62.4 | 62.4 | 62.4 | 62.4 | 62.4 | 62.4 | 62.4 | 62.4 | 62.4 | 63.4 | 64.4 | 65.4 | | Ib(f)/ft |
| Density of W | | 0.036111 | | | 0.036111 | 0.036111 | 0.036111 | | 0.036111 | | 0.036111 | | | | 0.037269 | | | |
| isplacemen | nt: | 0.578488 | 2.181614 | 4.3418/1 | 6.941854 | 10.3483 | 14.64233 | 19.38678 | 24.54316 | 30.08137 | 35.977 | 42.84934 | 50.09852 | 59.33741 | 69.25023 | 79.83842 | 91.10442 | IDS (f) |

Naval Architecture Spreadsheet

GM calculation

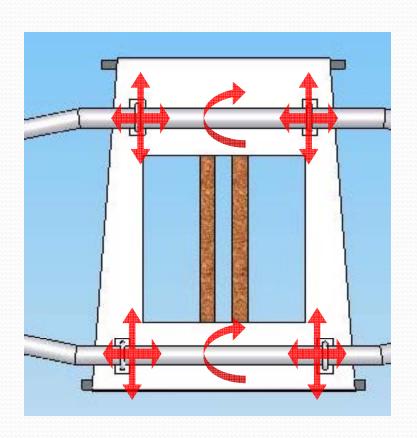
| KG Local | tion | | No. 10 | - San Lancon | F. 27.00 | 20.120-2 | | | | | | | | | | |
|----------|----------|----------------|--------------------|--------------|-------------|--------------|-----------|----------|----------|---------------------------------|----------|-----------|----------|--|--|---------|
| (GT = | 3.090909 | 9 | Element: | Weight: | Approx KG | Multiply: | | | | | | | | | | |
| | | | Solar Panels | 1.8 | 10.5 | | | | | | | | | | | |
| | | | Motors | 4 | -6.5 | -26 | | | | | | | | | | |
| | | | Main Hull | 5.2 | 3 | 15.6 | | | | | | | | | | |
| | | | Mounting Structure | 4.2 | 5.5 | 23.1 | | | | | | | | | | |
| | | | Solar Panel Mounts | 2.4 | 9.5 | 22.8 | | | | | | | | | | |
| | 1 | | | 700 | | | | | | | | | | | | |
| | | | Total Structure: | 17.6 | 3.090909091 | 54.4 | | | | | | | | | | |
| | | | Battery | 13.4 | | 100000 | | | | | | | | | | |
| | | | Ballast | 3.5 | | | | | | | | | | | | |
| | | | Sensors | 1 | | | | | | | | | | | | |
| | | | | 35.5 | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | |
| | | | | | Draft | | | | | | | | | | | |
| | | | | | 0.25 | 0.5 | 0.75 | - 1 | 1.25 | 1.5 | 1.75 | 2 | 2.25 | 2.5 | 2.75 | |
| | | | | | B(T) | 0.5 | 0.75 | | 1.23 | 1.5 | 1.75 | | 2.23 | 2.3 | 2.73 | |
| BM Loca | tion | | | | 4.082482905 | E 772E02 | 7.074000 | D 464066 | 0.420700 | 10 | 10.80123 | 44 E4704 | 40 04745 | 42 00004 | 40 E4000 | 44 4424 |
| DIN LUCA | uon | | | Simpson's | 4.002402803 | 3.773303 | 7.07 1000 | 0.104300 | 3.120703 | 10 | 10.00123 | 11.547.01 | 12.24143 | 12.50554 | 13.34000 | 14,1421 |
| BMT = | It/disp | Station Number | | Multipier: | Integrand: | | | | | | | | | | | |
| DIVIT - | itroisp | Station Number | 0 | | 22.68046058 | C4 4E002 | 447 DE44 | 101 4427 | 252 5752 | 222 2222 | 420.040 | E42 2002 | 612.3724 | 747 9494 | 027 4404 | 942.80 |
| | - | | | | | | | | | | | | | | | |
| | - | 2 | | | 45.36092116 | | | | 507.1505 | | 840.096 | | 1224.745 | | | |
| | | 3 | | | | | | | | | | | | 2868.877 | | |
| | | 4 | 26.16 | | 45.36092116 | | | | | | | | 1224.745 | | | |
| | | 5 | | | 90.72184233 | | | | | | | 2052.801 | | 2868.877 | | |
| | | 6 | 37.50 | | | | | | | | | | 1224.745 | The second secon | The second secon | |
| | | 7 | 32.32 | | | | | | | and the same of the same of the | | 2052.801 | | 2868.877 | | |
| | | 8 | | | | | | | | | | | 1224.745 | | | |
| | | 9 | | | | | | | | | | | | 2868.877 | | |
| | | 10 | 78.5 | | 22.68046058 | | | | | | | | 612.3724 | | 827.4484 | 942.80 |
| | | | | Sum: | 589.6919751 | 1667.901 | 3064.129 | 4717.536 | 6592.957 | 8666.667 | 10921.25 | 13343.21 | 15921.68 | 18647.7 | 21513.66 | 24513.0 |
| | | | Multiplying Term: | | 2.906666667 | 2.906667 | 2.906667 | 2.906667 | 2.906667 | 2.906667 | 2.906667 | 2.906667 | 2.906667 | 2.906667 | 2.906667 | 2.90666 |
| | | | | It: | 1714.038008 | 4848.032 | 8906.403 | 13712.3 | 19163.53 | 25191.11 | 31744.43 | 38784.25 | 46279.03 | 54202.64 | 62533.03 | 71251.2 |
| | | | Displacement: | | 16.01966292 | 60.41393 | 120.2364 | 192.236 | 286.5684 | 405.48 | 536.8646 | 679.6567 | 833.0225 | 996.2862 | 1186.597 | 1387.34 |
| | | | | BMt | 106.9958848 | 80.24691 | 74.07407 | 71.33059 | 66.87243 | 62.12664 | 59.1293 | 57.06447 | 55.55556 | 54.40469 | 52.69947 | 51.3580 |
| | | | | | | | | | | | | | | | | |
| KB Locat | tion | | | | | | | | | | | | | | | |
| KBt= | | 2 | | KBt | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 |
| | | | | | | | | | | | | | | | | |
| KM Loca | tion | | | | | | | | | | | | | | | |
| KM = KB | + BM | | | KMt | 106.9958848 | 80.24691 | 74.07407 | 71.33059 | 66.87243 | 62.12664 | 59.1293 | 57.06447 | 55.55556 | 54.40469 | 52.69947 | 51.3580 |
| | | | | | | 251100000000 | | | | | | | | | | |
| GM Loca | tion | | | | | | | | | | | | | | | |
| GM = KM | | | | GMt | 103.9049757 | 77.156 | 70.98316 | 68.23968 | 63.78152 | 59.03573 | 56.0384 | 53,97356 | 52,46465 | 51,31378 | 49,60856 | 48.2671 |

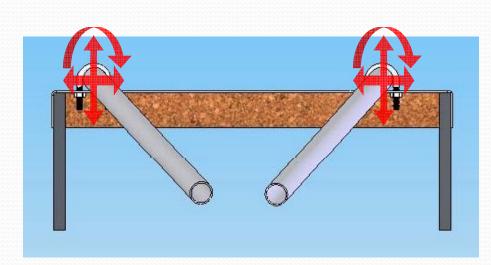
Naval Architecture Spreadsheet

• Trim Calculation

| Draft (in) | | 0.25 | 0.5 | 0.75 | - 1 | 1.25 | 1.5 | 1.75 | 2 | 2.25 | 2.5 | 2.75 | |
|--------------------|---------------------|---------------------|----------------|----------|-----------------|----------|----------|----------|----------------|----------|----------|----------|----------|
| | | | | | | | | | | | | | |
| GM Location (in) | | | | | discount of the | | | | Action Company | | | | |
| GM = KM-KG | | 103.9049757 | 77.156 | 70.98316 | 68.23968 | 63.78152 | 59.03573 | 56.0384 | 53.97356 | 52.46465 | 51.31378 | 49.60856 | 48.2671 |
| Change in GM | | 26.74897119 | 6.17284 | 2.743484 | 4.458162 | 4.745785 | 2.997338 | 2.064833 | 1.508916 | 1.150868 | 1.705222 | 1.341441 | |
| Estimated MT1 (lb) | | 0.028395935 | 0.006553 | 0.002912 | 0.004733 | 0.005038 | 0.003182 | 0.002192 | 0.001602 | 0.001222 | 0.00181 | 0.001424 | |
| Trim | Trim Angle (rad) | Trim Angle (deg) | Trim Moment | | | | | | | | | | |
| -3.5 | -0.08893674 | -0.558806026 | -19.6791 | -85.276 | -191.871 | -118.075 | -110.918 | -175.621 | -254.934 | -348.857 | -457.39 | -308.696 | -392.4 |
| -3 | -0.0762848 | -0.47931153 | -16.8796 | -73.1449 | -164.576 | -101.277 | -95.1395 | -150.637 | -218.667 | -299.229 | -392,322 | -264.782 | -336.58 |
| -2.5 | -0.06360834 | -0.399662997 | -14.0747 | -60.9902 | -137.228 | -84.4479 | -79.3299 | -125.606 | -182.331 | -249.505 | -327.129 | -220.782 | -280.65 |
| -2 | -0.05091138 | -0.319885644 | -11.2652 | -48.8158 | -109.836 | -67.5911 | -63.4947 | -100.533 | -145.935 | -199.701 | -261.83 | -176.712 | -224.63 |
| -1.5 | -0.03819797 | -0.240004934 | -8.45209 | -36.6257 | -82.4079 | -50.7125 | -47.639 | -75.4285 | -109.493 | -149.832 | -196.447 | -132.584 | -168.53 |
| -1 | -0.0254722 | -0.160046531 | -5.63625 | -24.4237 | -54.9534 | -33.8175 | -31.7679 | -50.2992 | -73.015 | -99.9153 | -131 | -88.413 | -112.389 |
| -0.5 | -0.01273816 | -0.080036248 | -2.81858 | -12.2139 | -27.4812 | -16.9115 | -15.8865 | -25.1537 | -36.5134 | -49.9658 | -65.5107 | -44.2137 | -56.2039 |
| 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | (|
| 0.5 | 0.01273816 | 0.080036248 | 2.818581 | | | | 15.88655 | 25.1537 | 36.51344 | 49.96576 | 65.51066 | 44.2137 | 56.20385 |
| 1 | 0.0254722 | 0.160046531 | | | 54.95342 | | 31.76794 | 50.29924 | 73.01503 | 99.9153 | | 88.41305 | |
| 1.5 | 0.03819797 | 0.240004934 | | | 82.40785 | | 47.63904 | 75.42848 | 109.493 | 149.8325 | 196.447 | 132.5837 | |
| 2 | 0.05091138 | 0.319885644 | | | | | | 100.5333 | 145.9354 | 199.7011 | 261.8304 | 176.7115 | |
| 2.5 | 0.06360834 | 0.399662997 | 14.07466 | 60.99017 | 137.2279 | | | 125.6056 | 182.3308 | 249.5052 | | 220.7822 | |
| 3 | 0.0762848 | 0.47931153 | | | | | | 150.6375 | | 299.229 | | 264.7817 | 336.5869 |
| 3.5 | 0.08893674 | 0.558806026 | 19.67908 | 85.27603 | 191.8711 | 118.0745 | 110.9185 | 175.6209 | 254.9336 | 348.8565 | 457.3896 | 308.6961 | 392.4103 |

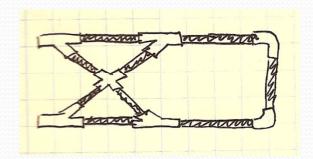
Fully Constrained Pontoon Attachments

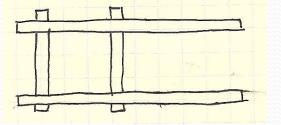


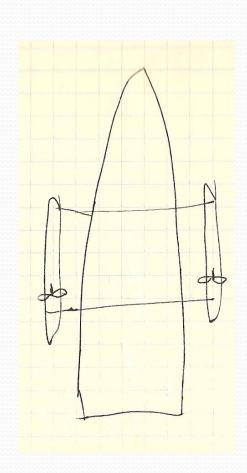


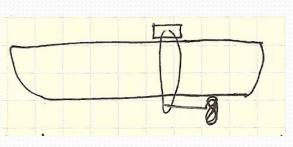
Leads to stress concentrations at joints

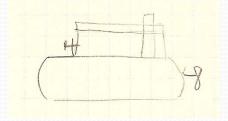
Previous Designs

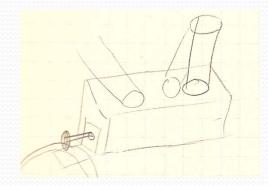




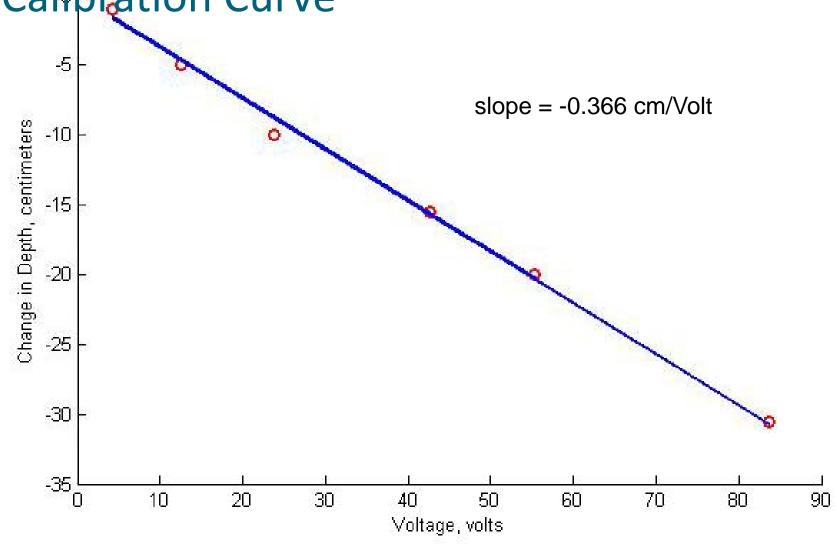








Pressure Transducer: Calibration Curve



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