Erosive Wear

- Several different kinds of erosive wear
 - Solid particle impingement
 - Impingement of liquid droplets
 - Flow of hot gases
 - Cavitation of liquid media due to collapsing bubbles

Erosive Wear Due to Solid Particle Impingement

- Useful Applications
 - Grit blasting
 - Abrasive cutting (typically with water)
 - Water jet cutting (demo in the lab)

Erosive Wear Due to Solid Particle Impingement

- Applications adversely affected by erosion
 - Polymer processing machines and others
 - Coal plants (transport of pulverized coal)
 - Gas turbines
 - Power plants
 - Pipelines
 - Ship propellers
 - Aircraft
 - Windshield
 - Wings
 - Propellers
 - Rotors

Erosive Wear Due to Solid Particle Impingement

Erosion as a function of the following variables:

Ductility of material being eroded

Microstructure

Velocity of particles

Impingement angle

Particle size

Hardness of particles

Strength of particles

Temperature

Erosive Wear Due to Solid Particle Impingement

- Roughly proportional to Vⁿ, where n can be 1.7 to 2.8 for ductile metals and 1.4 to 5.1 for brittle materials
- Erosion rate -(1/250) to (1/1000) by weight of abrasives
- Angle dependence around 20° for ductile materials and around 90° for brittle materials
- Particle size dependence -- Once it exceeds a certain size, it is independent of the particle size, similar to abrasive wear.
- Temperature dependence is different as a function of material properties. In general, the erosion rate of ductile metals decreases with increase in temperature.
- Erosion rate, in general, decreases with increase in hardness and toughness.

Model of Erosive Wear of Metals

• Cutting model of Finnie

$$m\ddot{x} + p\psi bx = 0$$
$$m\ddot{y} + pJ\psi by = 0$$
$$I\ddot{\phi} + p\psi b\phi = 0$$

$$\psi = \frac{\ell}{y_t}$$

J – ratio of vertical to horizontal force component p - constant horizontal component of contact stress

Erosion of Ductile Materials

• Erosive Wear Volume vs Velocity (Finnie Model)

$$W = \left(\frac{\rho}{p\psi} \frac{MU^2}{J}\right) \frac{J\cos^2\alpha}{6}$$

Erosion of Brittle Materials

- Transition from ring cracking to plastic indentation cracking
 - Yielding

$$a = \left(\frac{4kLR}{3E}\right)^{1/3}$$

$$\sigma_o = \frac{3L}{2\pi a^2}$$

$$L_y = B_2 \left(\frac{k}{E}\right)^2 H^3 R^2$$

Hertzian fracture load for large indentation
 L_f=B₁R_n

Erosion of Brittle Materials

• Critical Radius

$$R_c = B \left(\frac{E}{k}\right)^2 \frac{1}{H^3}$$

Erosion of Brittle Materials

• Loading due to Impact of Sphere

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See Sections 7.4 and 4.2 in [Suh 1986]: Suh, N. P. *Tribophysics*. Englewood Cliffs NJ: Prentice-Hall, 1986. ISBN: 0139309837.