Analytic Mechanics · generalized Coardinate · Constraint · Virtual disp · Virtual work  $\delta w = F. dr$ · Greneralized Force 8W = SW Pet SW non-pot -57 Cr = mg Cn 6

point 0 is an ideal Constraint and by definition it obesn't do work.

SW = 5W Ft SW frietion

SWF = F. Srp = F (Sin/gi-Con(gi) . 8 (L Sin (1 - L Con (1))

= Fl Sind 86 SWfriction = SW friction + SW friction Virtual of splacement

is 3000

FBD

S=MM Sign (r) what's N?

linear momentum principle Applied to Collar P=mrB=N+mg+5

(mrs). en = N-mg Sin 6

PB=rsinging coly ro = (r sing + zik Conk+r & Conp+r & sink) - ( i and 2 re sin 6 - re 20 - re and)

CIO. EN = 2ru+ru => N=m(ru+2ru+9sin() => 5=-mm 1ru+2ru+936/sign

$$\delta W = \left[ -g \sin \left( \frac{M_{2}^{L} + mr}{2} \right) + F \left( \frac{\sin x}{3} \right) \right] \delta v$$

$$+ \left[ \frac{mg \cos \left( \frac{m}{2} \right) - \int sign(r)}{2} \right] \delta r$$

$$Qr$$

Now we turn to deriving ean at mation using all those ingredients.

First let's formulate an extremum principle for the motion of a mechanical System

Consider a system of in particle (m., mm) subject to active forces Fi and Constrained forces Ki

Film: assume Constraints (via halonomic even without This assumption we have 
$$P_i = F_i + K_i$$

$$\sum_{i=1}^{n} F_i - P_i \cdot \delta r_i = e$$

$$D'Hembert's principle$$

NOTE: 
$$\sum_{i=1}^{n} F_{i} \cdot \delta r_{i} = \delta W$$

$$\sum_{i=1}^{n} P_{i} \cdot \delta r_{i} = \sum_{i=1}^{n} n_{i} r_{i} \cdot \delta r_{i} = \sum_{i=1}^{n} m_{i} \left[ \frac{d}{dt} \left[ r_{i} \cdot \delta r_{i} \right] - r_{i} \cdot \delta r_{i} \right]$$

$$= \sum_{i=1}^{n} \sum_{i=1}^{n} dt \cdot \left[ r_{i} \cdot \delta r_{i} \right] - \delta \sum_{i=1}^{n} \frac{1}{2} m_{i} \left( r_{i} \cdot r_{i} \right)$$

$$\Rightarrow \delta T + \delta W = \sum_{i=1}^{n} m_{i} \frac{d}{dt} \left[ r_{i} \cdot \delta r_{i} \right]$$

Integrate along the mation (victi, ..., vict+1))

$$\int_{t_{i}}^{t_{2}} S(T+W) dt = \int_{t_{i}}^{t_{2}} m_{i} dt \text{ Tri Sri J dt}$$
Variention

Creomethy

$$= \int_{t_1}^{t_2} \delta(7+w) \int_{r(t)} dt = \sum_{i} m_i \left[ \dot{r}_2 \cdot \delta \dot{r}_2 \right]_{t_i}^{t_2} = 0$$

$$\int_{t_{i}}^{t_{2}} \delta(T+w) \left| \frac{dt}{r(t)} \right| = 0$$
 Extended humilton Principle ( \*)

Assume all forces are (active forces) are patential forces

then define the Lagrangian L-T-V

$$= \Rightarrow (*) \text{ gives} \qquad \begin{cases} \begin{cases} t_2 \\ \delta \\ t_1 \end{cases} \text{ (E(t), } \dot{t}(t)) dt = 0 \end{cases} \text{ principle at least action} \\ \left( \text{ (Hamilton's principle}) \right) \end{cases}$$

In other words The function

$$I = \int_{t_1}^{t_2} L(\vec{r}_i(t), \vec{r}_i(t)) dt$$

defined for any kinematically admissible porth admittes an extremum along the actual mation of mechanical system. [SI-0] I is called the oction

Analogy g(x1,...,xn) (Function of n variables)

At points of extremo, clg = 0, indeed  $clg = \sum_{\partial x_i} \frac{\partial y}{\partial x_i} = 0$  $4 \rightarrow \frac{\partial Q}{\partial \Omega_{i}} = 0$  i=1,...,n