Fracture - Griffith Energy Balance

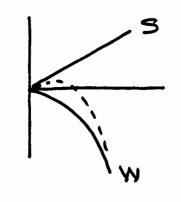
· Strain energy released by crack extension

energy por unit volume = Jode = 100 = 02 volume

$$= 2 \times \frac{1}{2} (a) (\beta a) = \beta a^{2}$$
Inglis: $\beta = \pi$

$$\longrightarrow W = -\frac{\sigma^{2}}{zE} \cdot \pi a^{2}$$

· Equate to surface energy 5= 2a.8



$$E = 5+W$$

catastrophe when

 $O = \frac{dE}{d\alpha} = -\frac{o_{\xi}^{2}}{2E} \cdot 2\pi\alpha + 2\%$

• | rwin / 0 sowan: use U = 28 + Wp

Compliance Calibration

$$C = \frac{\delta}{P}, \quad U = \frac{1}{2}P\delta = \frac{1}{2}CP^{2}$$

$$M = \frac{\partial U}{\partial a} = \frac{1}{2}P^{2}\frac{\partial C}{\partial a}$$

$$\Phi_{P,\delta}$$

$$\frac{1}{|a_c|} = \frac{1}{|a_c|} \frac{2c}{|a_c|} = \frac{1}{|a_c|} = \frac{1}{|a_c|} \frac{2c}{|a_c|} = \frac{1}{|a_c|} = \frac{1}{$$

eg DC13:

$$\frac{S}{Z} = \frac{Pa^{3}}{3ET}, T = \frac{bk^{3}}{17}$$

$$C = \frac{S}{P} = \frac{2a^{3}}{3ET}$$

$$C = \frac{S}{P} = \frac{7a^{3}}{3ET}$$

$$\mathcal{L}_{c} = \frac{1}{2}P_{c}^{2} \cdot \frac{2a^{2}}{EI} = \frac{12P_{c}^{2}a^{2}}{b^{2}h^{3}E}$$

Fracture - Stross luteusity • Singular stress field $O_{y} = \frac{\sqrt{2\pi x}}{\sqrt{2\pi x}} f_{y}(e)$ KI = { 1.10/TTA, edge concle fracture when KI & KIC

· Relation to ewsqy approach of = KIC = NEE - KIC = NEE

· Plane stross us plane strain - KIC = Wet for plane strain - elastic constraint: 02>0 -> T smaller -> less plastic flow

-> smaller ils -> less tough

of applicability

$$V = \frac{K_{\pm}}{\sqrt{2\pi \kappa_{p}}} \rightarrow \kappa_{p} = \frac{K_{\pm}}{2\pi V^{2}}$$

$$\rightarrow \text{ keep B, (W-a) > 2.5 (\frac{K_{\pm}c}{V})^{2}}$$