

Plant Stems with Radial Density Gradients



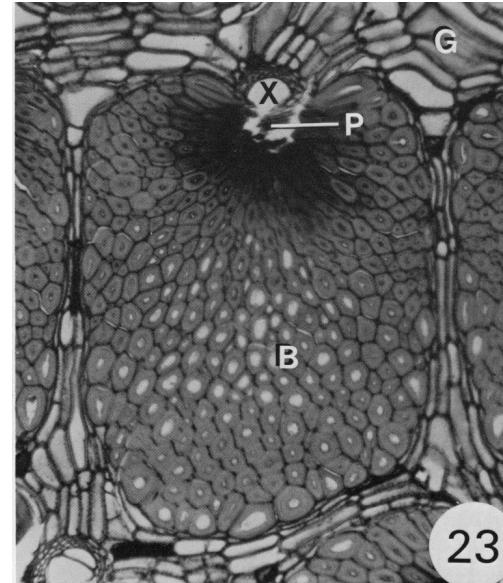
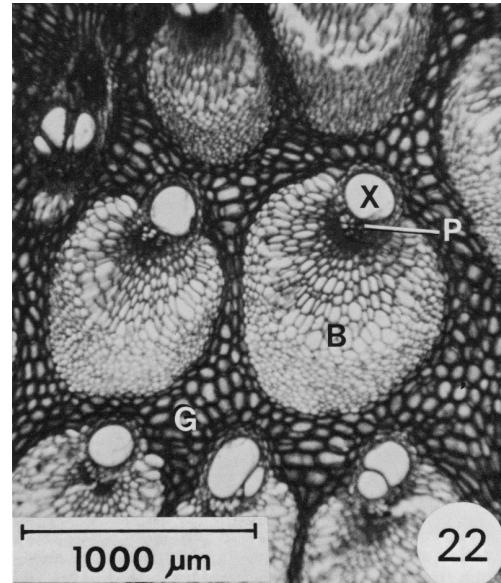
Coconut Palm

[http://en.wikipedia.org/wiki/
Image:Palmtree_Curacao.jpg](http://en.wikipedia.org/wiki/Image:Palmtree_Curacao.jpg)

Palm: Density Gradient

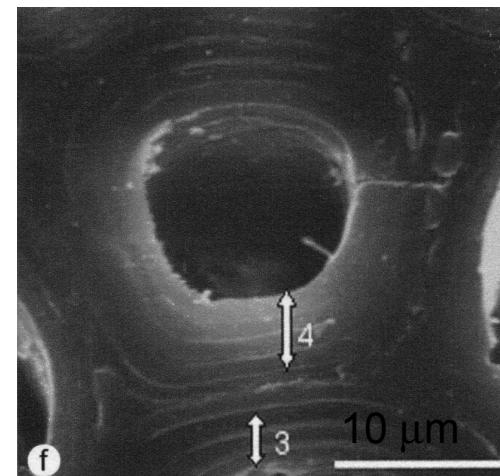
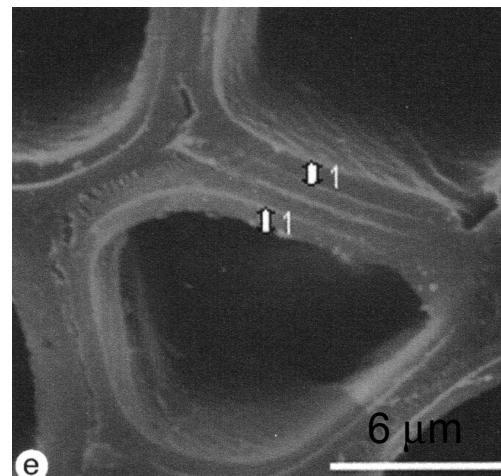
Vascular
bundles:
Honeycomb

Ground tissue
(Parenchyma):
Foam



Peripheral
Stem
Tissue

Rich, 1987

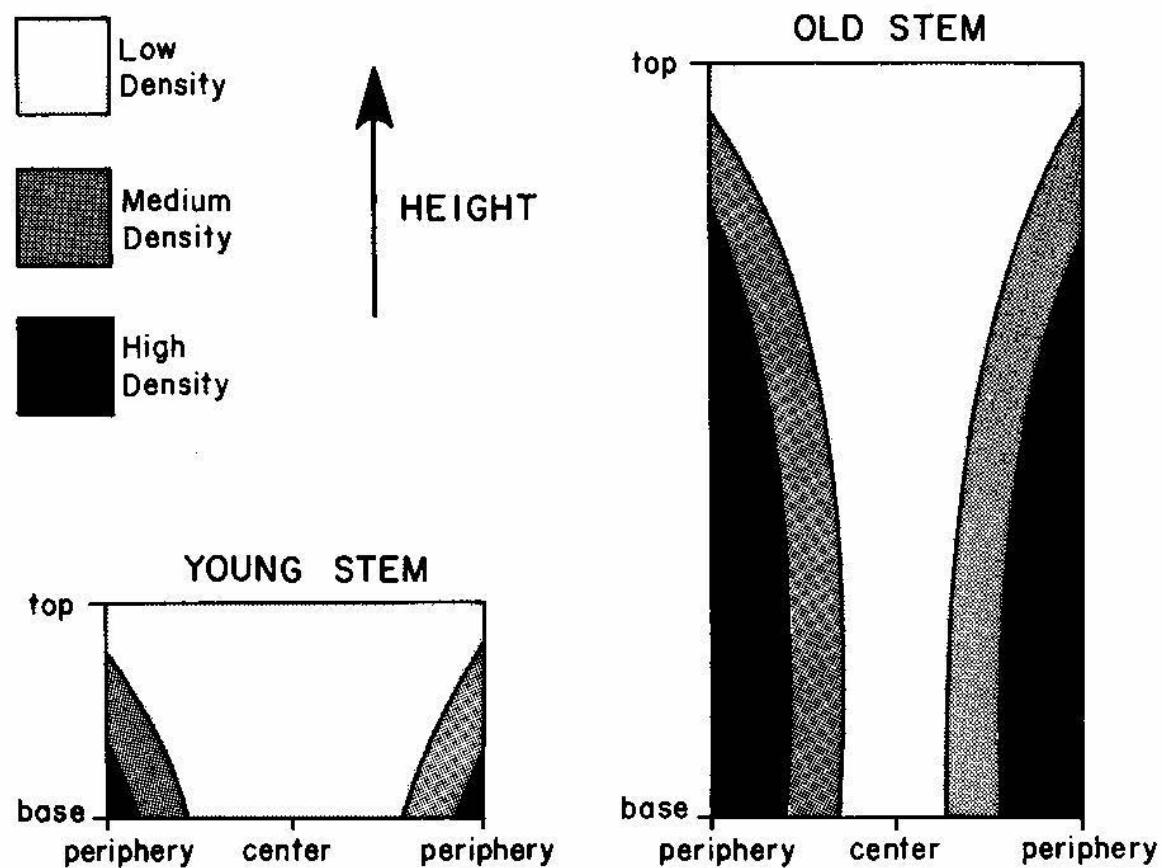


Young

Old

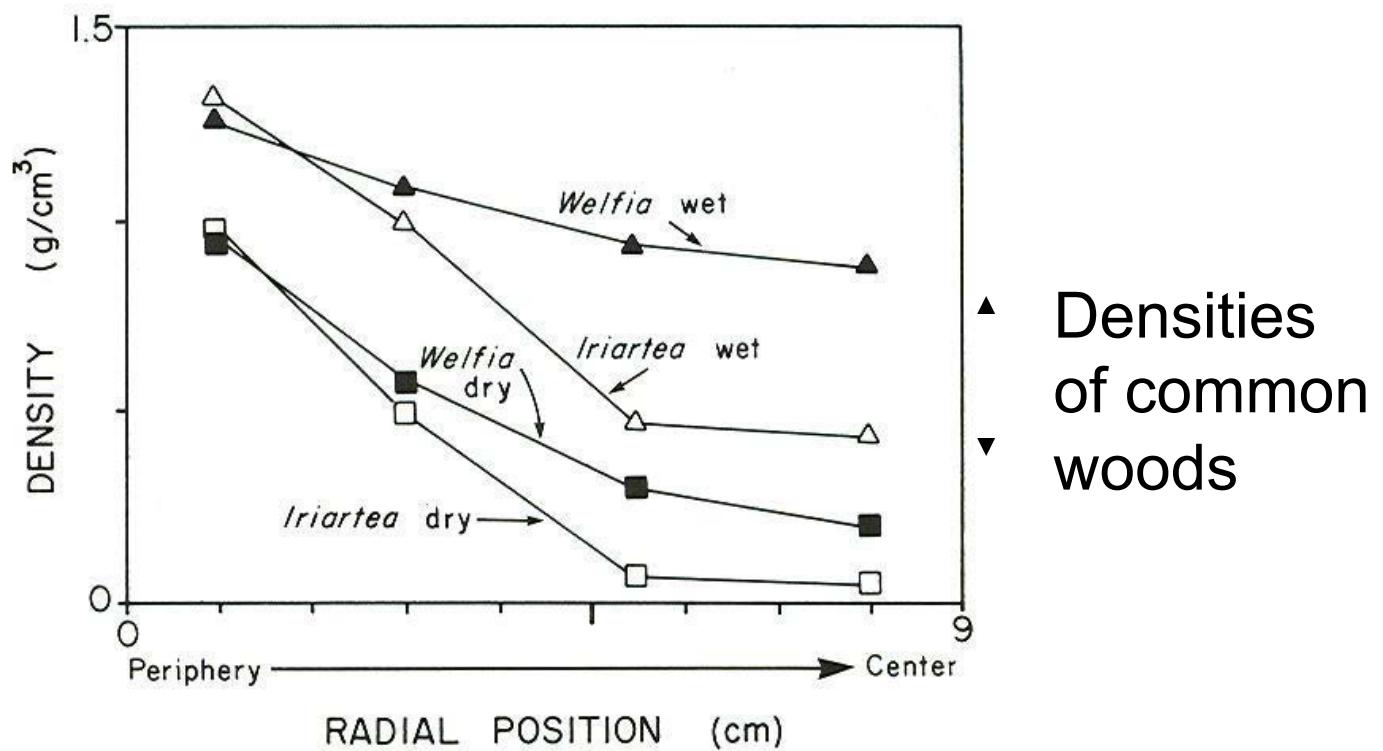
Kuo-Huang
et al., 2004

Palm Stem: Density Gradient



Rich, PM (1987) Bot.Gazette 148, 42-50.

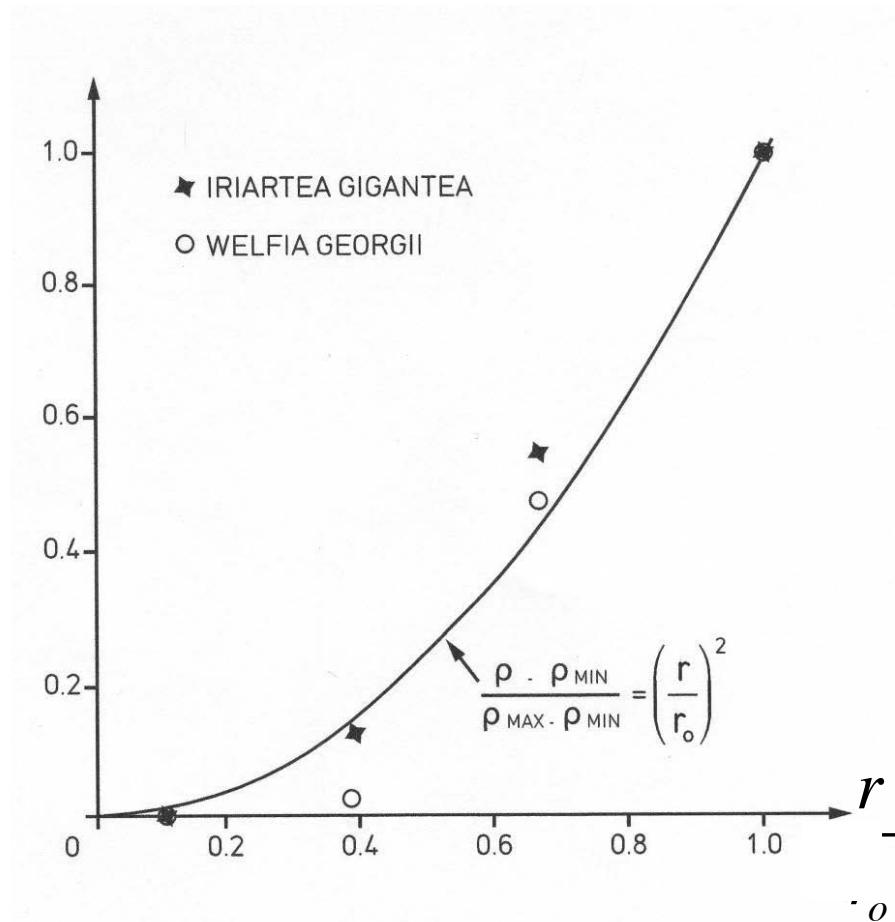
Palm Stem: Density at Breast Height



A single mature palm has a similar range of density as nearly all species of wood combined

Palm Stem: Density Gradient

$$\frac{\rho - \rho_{\min}}{\rho_{\max} - \rho_{\min}}$$

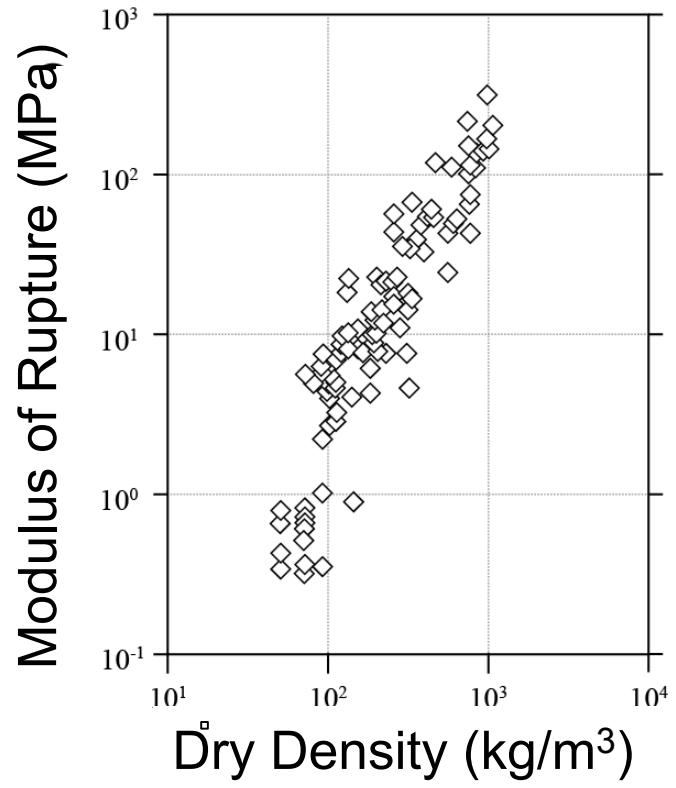
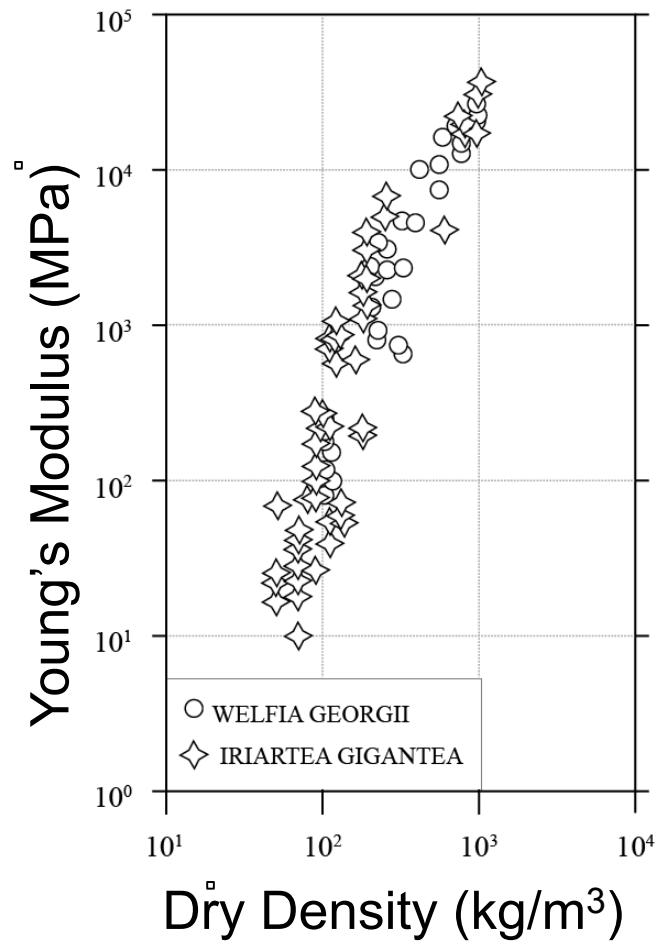


*Iriartea
gigantea:*

$$\rho_{\min} \approx 0$$

$$\frac{\rho^*}{\rho_{\max}} = \left(\frac{r}{r_o} \right)^2$$

r_o is the outer radius



Along Grain

*Iriartea
gigantea*

$$E^* = C \left(\frac{\rho^*}{\rho_{\max}} \right)^{2.5}$$

$$\sigma^* = C \left(\frac{\rho^*}{\rho_{\max}} \right)^2$$

Palm Properties

- Prismatic cells in palm deform axially (like wood loaded along the grain)
- If E_s was constant, would expect: $E^* = E_s (\rho^* / \rho_s)$
- But measure: $E^* = C (\rho^* / \rho_{\max})^{2.5}$
- Similarly with strength

Palm Properties

- $E_s = 0.1\text{-}3.0 \text{ GPa}$ in low density palm tissue from *Washingtonia robusta* (Rueggeberg et al., 2008)
- Estimate in dense tissue ($E^* = 30 \text{ GPa}$; $\rho^* = 1000 \text{ kg/m}^3$) $E_s = 45 \text{ GPa}$
- Large variation in E_s due to additional secondary layers in cell walls of denser tissue and increased alignment of cellulose microfibrils in those layers

Palm: Mechanical Efficiency Bending Stiffness

$$\rho = \left(\frac{r}{r_o} \right)^n \rho_{\max}$$

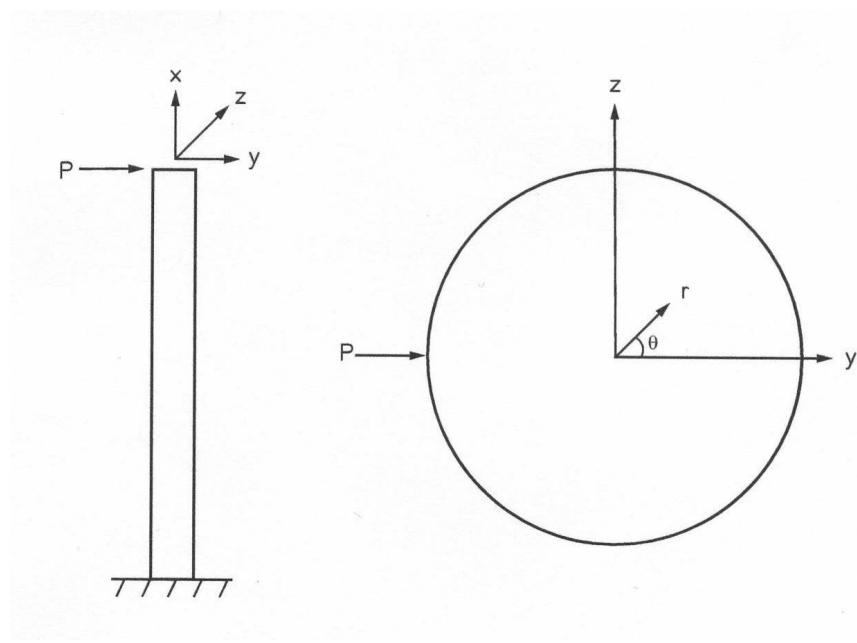
$$(EI)_{gradient} = \frac{C\pi r_o^4}{mn + 4}$$

$$E = C \left(\frac{\rho}{\rho_{\max}} \right)^m = C \left(\frac{r}{r_o} \right)^{mn} \quad \frac{(EI)_{gradient}}{(EI)_{uniform}} = \frac{4}{mn + 4} \left(\frac{n + 2}{2} \right)^m$$

Iriartea gigantea: n = 2, m = 2.5

$$(EI)_{gradient}/(EI)_{uniform} = 2.5$$

Palm: Mechanical Efficiency Bending Stress Distribution



$$\sigma(y) = E\varepsilon = E\kappa y$$

$$\sigma(r, \theta) = C \left(\frac{r}{r_o} \right)^{mn} \kappa r \cos \theta \propto r^{mn+1}$$

I. gigantea: $n = 2$, $m = 2.5$

$$\sigma \propto r^6$$

Palm: Mechanical Efficiency Bending *Strength* Distribution

$$\sigma^* \propto \left(\frac{\rho}{\rho_{\max}} \right)^q \propto \left(\frac{r}{r_o} \right)^{nq}$$

Iriartea gigantea: n = 2, q = 2

$$\sigma^* \propto r^4$$

Palm bending stress, strength

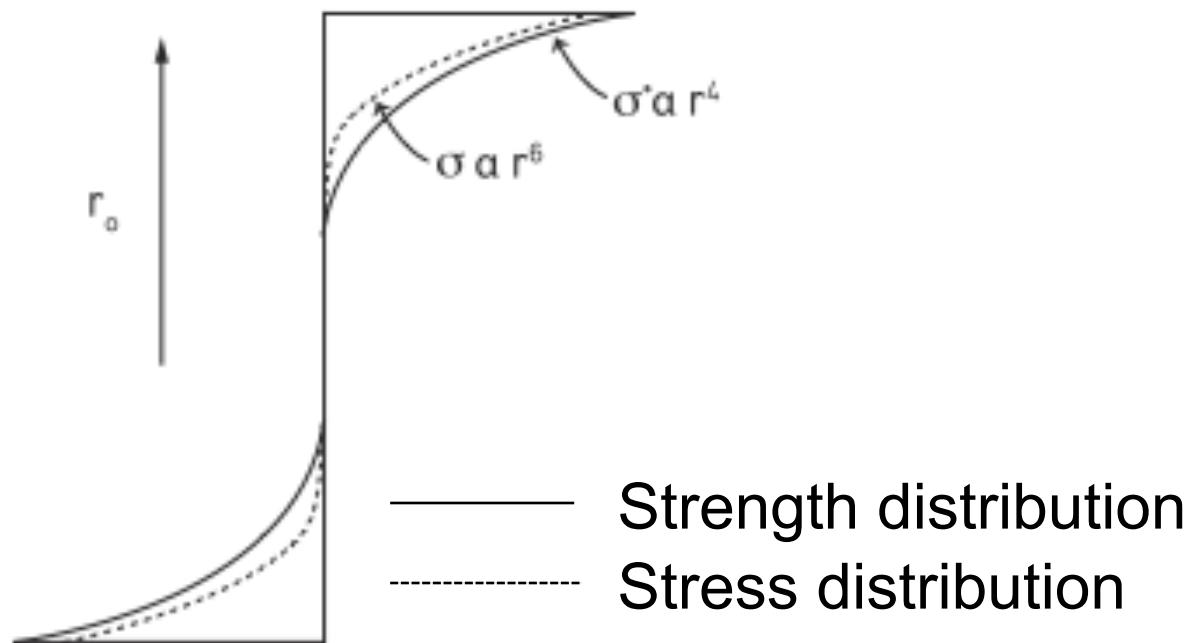


Figure sources

Sources for all figures in:
Cellular Materials in Nature and Medicine (2010)

Circular sections with radial density gradients: Palm Stems

- Palms can grow up to 20-40m - largest stresses from hurricane winds
- Unlike trees, palms do not have a cambium layer at the periphery, with dividing cells to allow increase in diameter as palm grows in height
- Instead, diameter of palm roughly constant as it grows in height
- Increasing stress resisted by cell walls increasing in thickness
- Add additional layers of secondary cell wall
- Produces radial density gradient
 - Density higher at periphery and at base of stem
 - A single stem can have densities from 100-1000 kg/m³, nearly spanning the density range of all woods (balsa \sim 200 kg/m³ \rightarrow lignum vitae \sim 1300 kg/m³)
- Specimen of palm taken from different radial positions tested in bending (Paul Rich, 1980s)
- Found $E_{\text{axial}}^* = C' \rho^{* 2.46}$
- Might expect $E_{\text{axial}}^* \propto \rho$ - vascular bundles honeycomb-like

- But additional cell wall layers change E_s : data $E_s=0.1\text{-}3 \text{ GPa}$
- Also: lower density palm has more ground tissue (parenchyma) with $E \propto \rho$ if at high turgor, but $E \propto \rho^2$ if at low turgor. (bending specimens dry)
- Modulus of rupture $\sigma^* = C'' \rho^{*2.05}$
- Radial density gradient increases flexural rigidity
- Compare (EI) with density gradient to (EI) of section of same mass+radius but uniform density
- For Iriartea gigantea:

$$\left(\frac{\rho^*}{\rho_{\max}}\right) = \left(\frac{r}{r_0}\right)^n \quad r_0 = \text{outer radius}$$

$$n = 2$$

$$E = C \left(\frac{\rho}{\rho_{\max}}\right)^m = C \left(\frac{r}{r_0}\right)^{mn}$$

$$\begin{aligned} (EI)_{\text{gradient}} &= \int_0^{r_0} = C \left(\frac{\rho}{\rho_{\max}}\right)^m \frac{2\pi r r^2 dr}{2} \\ &= \int_0^{r_0} C \left(\frac{r}{r_0}\right)^{mn} \pi r^3 dr \end{aligned}$$



$$\int r^2 2\pi r dr = J = 2I$$

$$\begin{aligned}
(EI)_{gradient} &= \frac{C\pi}{r_0^{mn}} \int_0^{r_0} r^{mn+3} dr \\
&= \frac{C\pi}{r_0^{mn}} \frac{r_0^{mn+4}}{mn+4} \\
&= \frac{C\pi r_0^4}{mn+4}
\end{aligned}$$

Equivalent mass, r_0 , uniform density $\bar{\rho}$:

$$\frac{\bar{\rho}}{\rho_{max}} = \frac{1}{\pi r_0^2} \int_0^{r_0} \left(\frac{r}{r_0}\right)^n 2\pi r dr = \frac{1}{\pi r_0^2} \frac{2\pi}{r_0^n} \frac{r_0^{n+2}}{n+2} = \frac{2}{n+2}$$

$$\begin{aligned}
(EI)_{\substack{\text{uniform} \\ \text{density}}} &= C \left(\frac{\bar{\rho}}{\rho_{max}} \right)^m \frac{\pi r_0^4}{4} \\
&= C \left(\frac{2}{n+2} \right)^m \frac{\pi r_0^4}{4}
\end{aligned}$$

$$\frac{(EI)_{gradient}}{(EI)_{\text{uniform}}} = \frac{C\pi r_0^4}{mn+4} \frac{4}{C\pi r_0^4} \left(\frac{n+2}{2} \right)^m = \frac{4}{mn+4} \left(\frac{n+2}{2} \right)^m$$

I.gigantea $m = 2.5$ $n = 2$	$\frac{(EI)_{gradient}}{(EI)_{\text{uniform}}} = 2.5$
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Stress and Strength distribution

$$\frac{\rho}{\rho_{\max}} = \left(\frac{r}{r_0}\right)^n$$

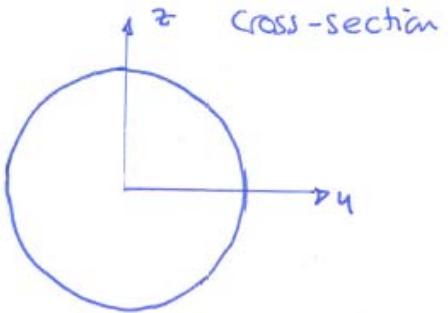
Stress $\sigma(y) = E \epsilon = E \mathcal{K} y$

$$= C \left(\frac{\rho}{\rho_{\max}}\right)^m \mathcal{K} y$$

$$= C \left(\frac{r}{r_0}\right)^{mn} \mathcal{K} r$$

$$\sigma(r) \propto r^{mn+1}$$

I. gigantea m=2.5 n=2 $\sigma(r) \propto r^6$



\mathcal{K} =curvature at the cross-section

y=distance from neutral axis
 $E = C \left(\frac{\rho}{\rho_{\max}}\right)^m$

Strength $\sigma^*(r) = C' \left(\frac{\rho}{\rho_{\max}}\right)^q = C \left(\frac{r}{r_0}\right)^{nq}$

$$\sigma^* r \propto r^{nq}$$

I. gigantea q=2 n=2 $\sigma^*(r) \propto r^4$

Figure: if max normal stress at $r = r_0$ is $\sigma = \sigma^*$ then bending stress distribution closely follows strength distribution!

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3.054 / 3.36 Cellular Solids: Structure, Properties and Applications

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