

EGR 550 Mechatronics

PROJECT – 3 | MIMO LAB

MANOHAR AKULA | ASU ID: 1223335191

CEP-550: Project 3 (M/M LAB)

Student name: Manohar Akula

ASU - ID: 1223335191

Aim: To derive a nonlinear transient model for two heaters and compare model predictions using the Arduino TC lab.

Procedure:

1. Connect the TC lab kit to the monitor through USB and open MATLAB.
2. Download the TClab-mimo files and run the test_models.m script.
3. The script to describe the dynamic temperature response of two temperature sensors given the heat inputs uses the following energy balance equations.

$$mC_p \frac{dT_1}{dt} = UA(T_b T_1) + \epsilon \sigma A (T_b^4 - T_1^4) + Q_{c12} + Q_{r12} + Q_1$$

$$mC_p \frac{dT_2}{dt} = UA(T_b T_2) + \epsilon \sigma A (T_b^4 - T_2^4) + Q_{c12} + Q_{r12} + Q_2$$

* Output;

* Observational

* The heater are operated for ten-minute

* Initially heater was turned on and this had effect on temperature even with the absence of heater 2.

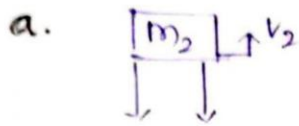
* At 300sec, heater 2 was turned on & the increase in the temperature values can be observed.

* As this system is a first order system, there is a time lag b/w the input and the result.

* It is clear that due to the disturbances experienced by the sensors the output response curve is not smooth.

* The accuracy of the model can be improved by tuning both the internal and external parameters.

2.26 Drawing the free body diagram of the given system.

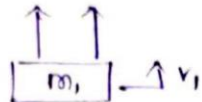


lets assume, $v_2 = \text{output}$

$$u(t) = \text{input} \quad G(s) = v_2(s)/u(s)$$

$k_2(v_2 - v_1)$ $b_2(\dot{v}_2 - \dot{v}_1)$ For mass 1, using law of conservation

$$\sum \vec{F} = m\vec{a}$$



$$\Rightarrow k_2(v_2 - v_1) + b_2(\dot{v}_2 - \dot{v}_1) - k_1v_1 - m_1\ddot{v}_1 = u(t)$$

$$\textcircled{1} \Rightarrow u(t) = k_2v_2 - k_2v_1 + b_2\dot{v}_2 - b_2\dot{v}_1 - k_1v_1 - m_1\ddot{v}_1$$

For mass 2, $k_2(v_2 - v_1) + b_2(\dot{v}_2 - \dot{v}_1) + k_1v_2 - m_2\ddot{v}_2 = 0$

$$\Rightarrow k_2v_2 - k_2v_1 + b_2\dot{v}_2 - b_2\dot{v}_1 + k_1v_2 - m_2\ddot{v}_2 = 0 \textcircled{2}$$

writing eq ① & ② in matrix form, $[m]\ddot{v} = [b]\dot{v} + [k]v = u(t)$

$$\textcircled{3} \begin{bmatrix} u(t) \\ v_2 \end{bmatrix} = \begin{bmatrix} m_1 & 0 \\ 0 & m_2 \end{bmatrix} \begin{bmatrix} \ddot{v}_1 \\ \ddot{v}_2 \end{bmatrix} + \begin{bmatrix} b_2 & -b_2 \\ -b_2 & b_2 \end{bmatrix} \begin{bmatrix} \dot{v}_1 \\ \dot{v}_2 \end{bmatrix} + \begin{bmatrix} -k_1+k_2 & -k_2 \\ -k_2 & k_1+k_2 \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \end{bmatrix}$$

c. ~~Constitutive~~ equations;

$$v_1 = \frac{1}{m_1} \int F_1' dt \textcircled{a} \quad \dot{v}_1 = \frac{1}{m_1} F_1'$$

$$F_1 = k_1 \int v_1' dt \textcircled{a} \quad F_1' = k_1 v_1'$$

$$F_2 = k_2 \int v_2' dt \textcircled{a} \quad F_2' = k_2 v_2'$$

$$-v_1' = -v_1(t) + v_2 \textcircled{a} \quad v_1' = v_1(t) - v_2$$

$$v_2 = \frac{1}{m_2} \int F_2' dt \textcircled{b} \quad \dot{v}_2 = \frac{1}{m_2} F_2'$$

$$-v_2' = -v_2 + v_1 \textcircled{b} \quad v_2' = v_2 - v_1$$

$$F_1' = F_1 + F_1''$$

$$\therefore \dot{v}_1 = \frac{1}{m_1} [F_2 + F_1 - b_1 (v_2 - v_1)]$$

$$F_1' = F_2 - F_1$$

$$v_2' = \frac{1}{m_2} [F_1 + b_1 (v_2 - v_1)]$$

$$F_1'' = b_1 v_1'$$

$$F_1 = k_1 (v_1(t) - v_2)$$

$$F_2 = k_2 (v_2 - v_1)$$

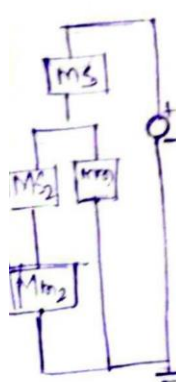
writing as $A\dot{x} = Bx$, $A = \begin{bmatrix} -b_1/m_2 & b_1/m_2 & 1/m_2 & 0 \\ b_1/m_1 & -b_1/m_1 & -1/m_1 & 1/m_1 \\ -k_2 & k_1 & 0 & 0 \\ 0 & -k_1 & 0 & 0 \end{bmatrix}$

$$B = \begin{bmatrix} 0 \\ 0 \\ 0 \\ k_1 \end{bmatrix} \therefore x = [v_1, v_2, F_1, F_2]^T$$

The system is a second order system.

d. Solving 1, 2 eq, rearranging as matrix form (3), we get.

$$\begin{bmatrix} m_1 & 0 \\ 0 & m_2 \end{bmatrix} \begin{bmatrix} \ddot{v}_1 \\ \ddot{v}_2 \end{bmatrix} + \begin{bmatrix} b_2 - b_1 & b_1 \\ -b_1 & b_1 \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \end{bmatrix} + \begin{bmatrix} k_1 + k_2 & -k_2 \\ -k_2 & k_1 + k_2 \end{bmatrix} \begin{bmatrix} v_1 \\ v_2 \end{bmatrix} = \begin{bmatrix} u(t) \\ 0 \end{bmatrix}$$



$$Z = \frac{1}{sm_1} + \frac{1}{ms + 1/2}, \quad V' = \begin{bmatrix} 1/2 \\ ms + 1/2 \end{bmatrix}, \quad V = \begin{bmatrix} 1 \\ ms + 1 \end{bmatrix} V$$

$$v_m = \begin{bmatrix} mm_2 \\ ms + 1/2 \end{bmatrix} \cdot V'; \quad T_m = \frac{v_m}{V} = \begin{bmatrix} 1 \\ 1 + ms \end{bmatrix} \begin{bmatrix} mm_2 \\ ms + 1/2 \end{bmatrix}$$

$$\therefore T_m = \begin{bmatrix} \frac{zs}{z + z_s} \end{bmatrix} \begin{bmatrix} mm_2 \\ ms + 1/2 \end{bmatrix} \quad \left(\text{here } z = \frac{1}{ms + 1/2} + z_{m1} \right)$$

$$\therefore T_m = \begin{bmatrix} \frac{1}{zm_2 \left[\frac{1}{zm_1 z_s} + \frac{1}{z_s} \right]} + 1 \end{bmatrix} \begin{bmatrix} \frac{zs}{zm_1 z_s} \end{bmatrix}$$

This is a first order system.

2.28 From the given mechanical model, $J_m \dot{\omega}_m = T_m - b_m \omega_m - T_k$

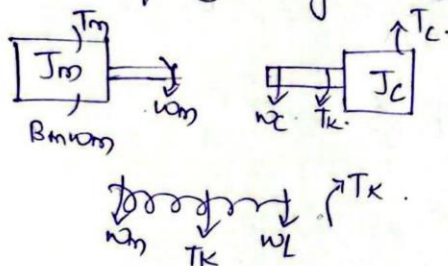
$$\dot{T}_k = K(\omega_m - \omega_c) \Rightarrow J_m \dot{\omega}_m = T_m - b_m \omega_m - K(\omega_m - \omega_c)$$

$$\Rightarrow J_c \dot{\omega}_c = T_k - b_c \omega_c - c / \omega_c / \omega_c$$

$$\Rightarrow J_c \dot{\omega}_c = K(\omega_m - \omega_c) - b_c \omega_c - c / \omega_c / \omega_c$$

$$T_c = -c / \omega_c / \omega_c$$

The FBD of given system is as shown.



State space equations

$$\frac{d\omega_m}{dt} = -\frac{b_m}{J_m} \omega_m - \frac{1}{J_m} T_k + \frac{1}{J_m} T_m$$

$$\frac{d\omega_c}{dt} = -\frac{c}{J_c} \omega_c / \omega_c + \frac{1}{J_c} T_c + \frac{1}{J_c} T_k$$

$$\frac{dT_k}{dt} = K_c \omega_m - K_c \omega_c$$

Assuming of $c \cdot \frac{1}{K_c} T$, also if $\omega_m = \omega_c$ using linearization $\omega_c = \omega_m = \bar{\omega}$
 $\dot{\omega}_m = \dot{\omega}_c = 0$
 $T_m = \bar{T}_m \cdot \omega_m - \omega_c$
 $= \Delta \bar{\omega}$

$$\therefore T_m - b_m \bar{\omega} = K_c \Delta \bar{\omega} = 0$$

$$K_c \Delta \bar{\omega} - (\bar{\omega})^2 - T_c = 0$$

Let $q_1 \rightarrow$ variation of ω_m steady state value.

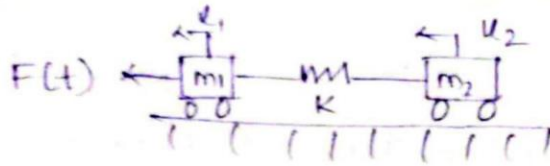
$q_2 \rightarrow$ variation of ω_c steady state value Applying Taylor series

$$J_m \ddot{\omega}_m + J_m \dot{q}_1 = T_m + u + b_m \bar{\omega} - b_m \dot{q}_1 - K_c \Delta \bar{\omega} - K_c (q_1 - q_2)$$

$$J_c \ddot{\omega}_c + J_c \dot{q}_2 = K_c \Delta \bar{\omega} + K_c (q_1 - q_2) - c \bar{\omega} - z c \bar{\omega} \dot{q}_2 + T$$

$$\therefore \begin{cases} J_m \ddot{q}_1 = u + b_m \dot{q}_1 - K_c (q_1 - q_2) \\ J_c \ddot{q}_2 = K_c (q_1 - q_2) - 2 \omega \dot{q}_2 \end{cases} \rightarrow \text{System linear model}$$

P2.73



a) $F(s)$ for the given system :

$$F(s) = m_1 s^2 x_1(s) + k [x_1(s) - x_2(s)] \rightarrow (1)$$

$$0 = m_2 s^2 x_2(s) + k [x_2(s) - x_1(s)] \rightarrow (2)$$

$$\frac{x_2(s)}{x_1(s)} = \frac{k}{m_2 s^2 + k} \Rightarrow x_2(s) = \frac{k x_1(s)}{k + m_2 s^2} \rightarrow (3)$$

substituting eq (3) in eq (1)

$$\frac{x_1(s)}{F(s)} = \frac{m_2 s^2 + k}{(m_1 s^2 + k)(m_2 s^2 + k) - k^2}$$

② If T.F is zero, m_1 will be motionless, $\therefore m_2 s^2 + k = 0$

$$s = j \sqrt{\frac{k}{m_2}} = j\omega$$

$$\therefore \boxed{\omega = \sqrt{\frac{k}{m_2}}}$$

Output: (Question -1)

