

Nonlinear control and aerospace applications

Attitude kinematics

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- 2 Kinematic equations
 - Vector derivative
 - Direction cosine matrix kinematics
 - Euler angle kinematics
 - Quaternion kinematics
- 3 Discussion
- 4 Appendix: Proofs

1 Introduction

2 Kinematic equations

- Vector derivative
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- Euler angle kinematics
- Quaternion kinematics

3 Discussion

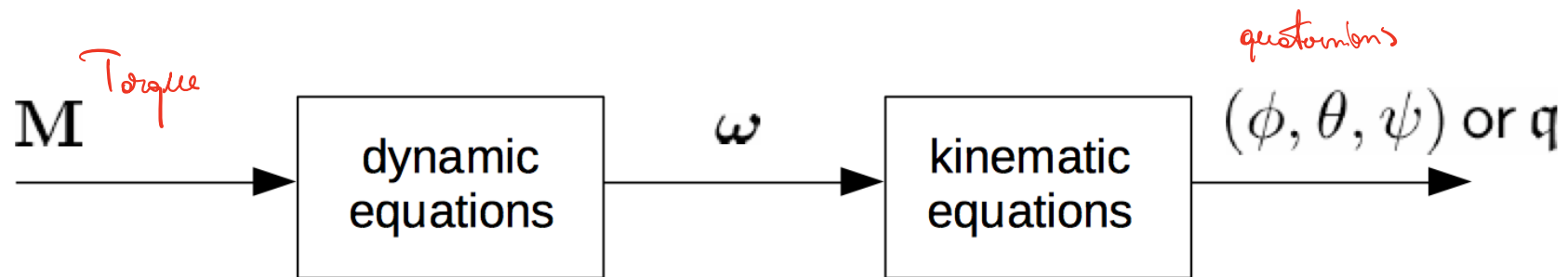
4 Appendix: Proofs

Introduction

- A spacecraft can be (approximately) described as a rigid body, which moves with respect to some inertial frame.
- The body movement is given by a combination of
 - ▶ a translation of the body center of mass (CoM);
 - ▶ a rotation of the body about an axis passing through the CoM.
- The study of both the translational and rotational motion is of paramount importance for spacecraft design and control.
- The objective here is to derive the *attitude kinematic equations* for a rigid body in rotational motion.
 - ▶ These equations, together with the dynamic equations, are fundamental for spacecraft attitude control.

Introduction

- The dynamic and kinematic equations can be seen as the **series connection of two nonlinear systems**:
 - ▶ the dynamic equations define a system from \mathbf{M} to ω , where \mathbf{M} is the moment applied to the body;
 - ▶ the kinematic equations define a system from ω to (ϕ, θ, ψ) or q .



- Overall, it is a nonlinear system with:
 - ▶ input \mathbf{M} , \rightarrow moment
 - ▶ output (ϕ, θ, ψ) , DCM or q . \leftarrow output to control.

Introduction

- Consider a rigid body rotating wrt some observer reference frame, with angular velocity $\omega = \omega_1 \mathbf{b}_1 + \omega_2 \mathbf{b}_2 + \omega_3 \mathbf{b}_3$.

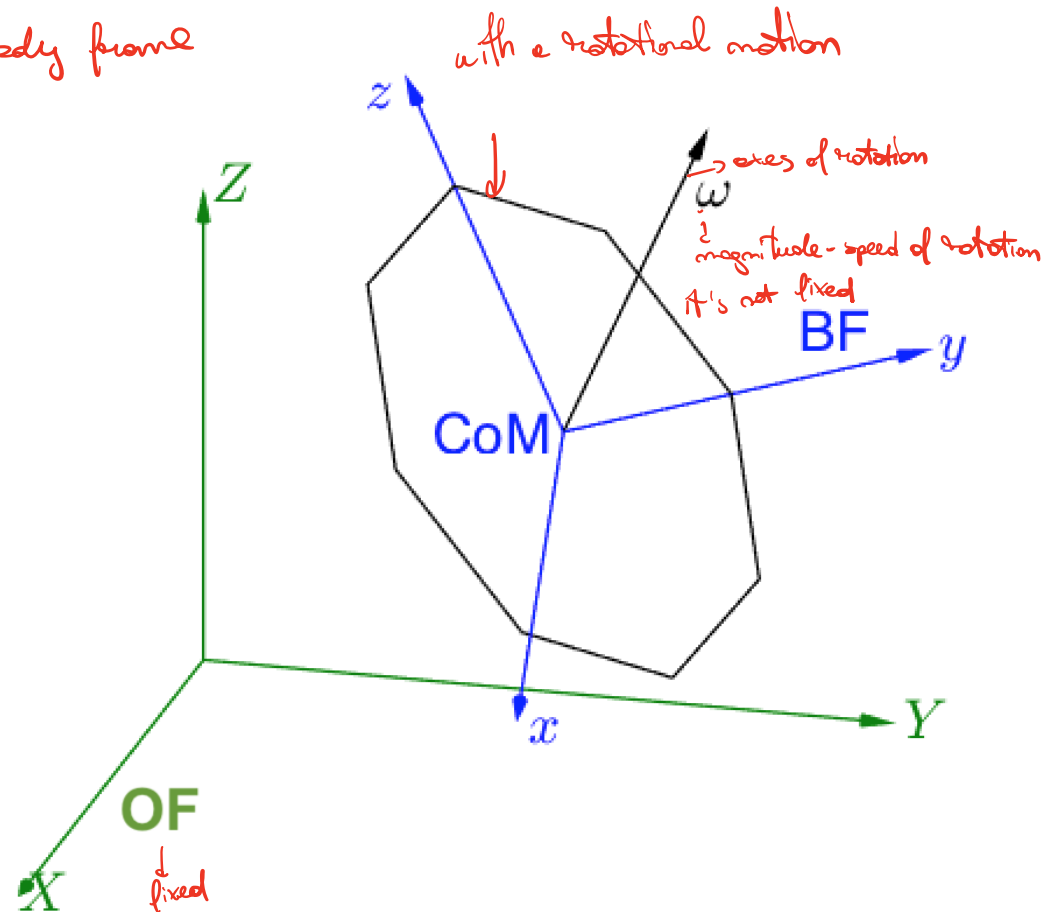
vector based on body frame

Observer frame (OF):

- origin: somewhere
- unit vectors: $\mathbf{i}_1, \mathbf{i}_2, \mathbf{i}_3$
- axes: X, Y, Z .

Body frame (BF):

- rotating with the body *attached to the body*
- origin: body CoM
- unit vectors: $\mathbf{b}_1, \mathbf{b}_2, \mathbf{b}_3$
- axes: x, y, z .



Introduction

- The representations of rotations we consider are:
 - ① Direction cosine matrix (DCM).
 - ② Euler angles.
 - ③ Quaternions.
- In the following, after a brief note about the derivative of a vector, we will present the kinematic equations for these three cases.
- The proofs/derivations of these equations are given in the Appendix.

1 Introduction

2 Kinematic equations

- Vector derivative
- Direction cosine matrix kinematics
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Vector derivative

- For any physical vector $\mathbf{r} = x\mathbf{b}_1 + y\mathbf{b}_2 + z\mathbf{b}_3$: *Combination of the vector in the body frame*

$$\dot{\mathbf{r}} = \dot{x}\mathbf{b}_1 + \dot{y}\mathbf{b}_2 + \dot{z}\mathbf{b}_3 + x\dot{\mathbf{b}}_1 + y\dot{\mathbf{b}}_2 + z\dot{\mathbf{b}}_3. \quad \text{-- derivatives respect to time}$$

- Consider the rotation

$$\delta\mathbf{b}_i = \delta\boldsymbol{\theta} \times \mathbf{b}_i$$

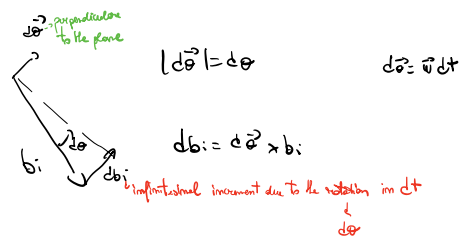
where $\delta\boldsymbol{\theta} = \boldsymbol{\omega}\delta t$ and $\delta t \rightarrow 0$. Then, $\dot{\mathbf{b}}_i = \boldsymbol{\omega} \times \mathbf{b}_i$.

- This implies the following relation:

$$\dot{\mathbf{r}} = \dot{\mathbf{r}}_B + \boldsymbol{\omega} \times \mathbf{r}. \quad (1)$$

due the fact that the body frame is rotating

- $\dot{\mathbf{r}}$ is the derivative in the observer frame
- $\dot{\mathbf{r}}_B \doteq \dot{x}\mathbf{b}_1 + \dot{y}\mathbf{b}_2 + \dot{z}\mathbf{b}_3$ is the derivative in the body frame.



We can write this relation in terms of coordinate vectors of a reference frame R :

$$r \rightarrow r_B = \begin{bmatrix} x \\ y \\ z \end{bmatrix} \quad \hat{r}_B = \begin{bmatrix} \hat{x} \\ \hat{y} \\ \hat{z} \end{bmatrix} \quad r \rightarrow (r_B) \rightarrow \begin{bmatrix} x \\ y \\ z \end{bmatrix}$$

$x, y, z \rightarrow r$ coordinates in R
 rotation of $R \rightarrow R'$
 Vector expressed in R' coordinates

DCM kinematics

- Define the matrix

$$\boldsymbol{\omega} \times \doteq \begin{bmatrix} 0 & -\omega_3 & \omega_2 \\ \omega_3 & 0 & -\omega_1 \\ -\omega_2 & \omega_1 & 0 \end{bmatrix}.$$

- The DCM kinematic equation is

$$\dot{\mathbf{T}} = \mathbf{T} \boldsymbol{\omega} \times .$$

- Also useful is the transpose kinematic equation

$$\dot{\mathbf{T}}^\top = -\boldsymbol{\omega} \times \mathbf{T}^\top.$$

A physical vector $\mathbf{r} = x\mathbf{b}_1 + y\mathbf{b}_2 + z\mathbf{b}_3 = x\mathbf{i}_1 + y\mathbf{i}_2 + z\mathbf{i}_3$ has coordinate vectors and derivatives given by:

$$\mathcal{B}: \mathbf{r}_B = (x, y, z)$$

$$\dot{\mathbf{r}}_B = (\dot{x}, \dot{y}, \dot{z})$$

$$\mathcal{B}^T: \mathbf{r}_O = (X, Y, Z)$$

$$\dot{\mathbf{r}}_O = (\dot{X}, \dot{Y}, \dot{Z})$$

T is the rotation matrix $\mathcal{O}^T \rightarrow \mathcal{B}^T$ (Transformation $\mathcal{B}^T \rightarrow \mathcal{O}^T$). So:

$$\mathbf{r}_O = T \mathbf{r}_B$$

$$\dot{\mathbf{r}}_O = \dot{T} \mathbf{r}_B + T \dot{\mathbf{r}}_B$$

We suppose that \mathbf{r}_O is an arbitrary constant vector. Then:

$$\dot{\mathbf{r}} = \dot{\mathbf{r}}_O + \boldsymbol{\omega} \times \mathbf{r} = \boldsymbol{\omega} \times \mathbf{r}$$

that in terms of coordinate vectors becomes: $(\dot{\mathbf{r}})_B = \boldsymbol{\omega} \times \mathbf{r}_B$
 \downarrow
 $\dot{\mathbf{r}}$ expressed in \mathcal{B}^T coordinates

Attention: $(\dot{\mathbf{r}})_B \neq \dot{\mathbf{r}}_B = 0$. So $(\dot{\mathbf{r}})_B = \dot{T} \mathbf{r}_O$

By substitution we obtain: $T \dot{\mathbf{r}}_O = \boldsymbol{\omega} \times \mathbf{r}_B \Rightarrow \dot{\mathbf{r}}_O = T \boldsymbol{\omega} \times \mathbf{r}_B$. But we know that $\dot{\mathbf{r}}_O = \dot{T} \mathbf{r}_O + T \dot{\mathbf{r}}_O = \dot{T} \mathbf{r}_O$. So

$$(\dot{T} - T \boldsymbol{\omega} \times) \mathbf{r}_O = 0$$

\downarrow
arbitrary \Rightarrow

$$\dot{T} = T \boldsymbol{\omega} \times$$

$$\dot{T}^T = -\boldsymbol{\omega} \times T^T$$

Euler angle kinematics

Tait-Bryan 321

- Tait-Bryan 321 rotation with angles (ψ, θ, ϕ) :

$$\begin{bmatrix} \omega_1 \\ \omega_2 \\ \omega_3 \end{bmatrix} = \begin{bmatrix} 1 & 0 & -s\theta \\ 0 & c\phi & s\phi c\theta \\ 0 & -s\phi & c\phi c\theta \end{bmatrix} \begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix}.$$

components of angular speed (pointing to the ω vector)

derivatives of angles (pointing to the $\dot{\phi}, \dot{\theta}, \dot{\psi}$ vector)

- Inverting the matrix, we obtain the Tait-Bryan 321 kinematic equation:

$$\begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix} = \frac{1}{c\theta} \begin{bmatrix} c\theta & s\phi s\theta & c\phi s\theta \\ 0 & c\phi c\theta & -s\phi c\theta \\ 0 & s\phi & c\phi \end{bmatrix} \begin{bmatrix} \omega_1 \\ \omega_2 \\ \omega_3 \end{bmatrix}.$$

- Singularity for $c\theta = 0$ (gimbal lock). *singularity* (pointing to $c\theta$)

The goal is to describe the time evolution of the rotation Euler angles in function of $\omega_1, \omega_2, \omega_3$.

The direct rotation from $O\vec{F}$ to $O\vec{F}$ can be seen as a sequence of 3 intrinsic elementary rotations:

- ① $O\vec{F} \rightarrow F_1$;
- ② $F_1 \rightarrow F_2$; \rightarrow intermediate frames
- ③ $F_2 \rightarrow O\vec{F}$

For example in Tat-Beyan as intrinsic rotation, the axes of F_1 are x', y', z' while those of F_2 are x'', y'', z'' with $x'' = x$

Euler angle kinematics

Tait-Bryan 123

- Tait-Bryan 123 rotation with angles (ϕ, θ, ψ) :

$$\begin{bmatrix} \omega_1 \\ \omega_2 \\ \omega_3 \end{bmatrix} = \begin{bmatrix} c\theta c\psi & s\psi & 0 \\ -c\theta s\psi & c\psi & 0 \\ s\theta & 0 & 1 \end{bmatrix} \begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix}$$

$$\begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix} = \frac{1}{c\theta} \begin{bmatrix} c\psi & -s\psi & 0 \\ c\theta s\psi & c\theta c\psi & 0 \\ -s\theta c\psi & s\theta s\psi & c\theta \end{bmatrix} \begin{bmatrix} \omega_1 \\ \omega_2 \\ \omega_3 \end{bmatrix}.$$

- Singularity for $c\theta = 0$ (gimbal lock).

Euler angle kinematics

Proper Euler 313

- Proper Euler 313 rotation with angles (ϕ, θ, ψ) :

$$\begin{bmatrix} \omega_1 \\ \omega_2 \\ \omega_3 \end{bmatrix} = \begin{bmatrix} s\theta s\psi & c\psi & 0 \\ s\theta c\psi & -s\psi & 0 \\ c\theta & 0 & 1 \end{bmatrix} \begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix}$$

$$\begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix} = \frac{1}{s\theta} \begin{bmatrix} s\psi & c\psi & 0 \\ s\theta c\psi & -s\theta s\psi & 0 \\ -c\theta s\psi & -c\theta c\psi & s\theta \end{bmatrix} \begin{bmatrix} \omega_1 \\ \omega_2 \\ \omega_3 \end{bmatrix}.$$

- Singularity for $s\theta = 0$ (gimbal lock).

Quaternion kinematics

- The quaternion kinematic equations can be written in different equivalent forms:

$$\dot{\mathbf{q}} = \frac{1}{2} \mathbf{q} \otimes (0, \boldsymbol{\omega})$$

$$\dot{\mathbf{q}} = \frac{1}{2} \boldsymbol{\Omega} \mathbf{q}$$

$$\dot{\mathbf{q}} = \frac{1}{2} \mathbf{Q} \boldsymbol{\omega}$$

where

$$\boldsymbol{\Omega} \doteq \begin{bmatrix} 0 & -\omega_1 & -\omega_2 & -\omega_3 \\ \omega_1 & 0 & \omega_3 & -\omega_2 \\ \omega_2 & -\omega_3 & 0 & \omega_1 \\ \omega_3 & \omega_2 & -\omega_1 & 0 \end{bmatrix}, \quad \mathbf{Q} \doteq \begin{bmatrix} -q_1 & -q_2 & -q_3 \\ q_0 & -q_3 & q_2 \\ q_3 & q_0 & -q_1 \\ -q_2 & q_1 & q_0 \end{bmatrix}.$$

- No singularities occur.

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Discussion

- We obtained the kinematics equations in the general form

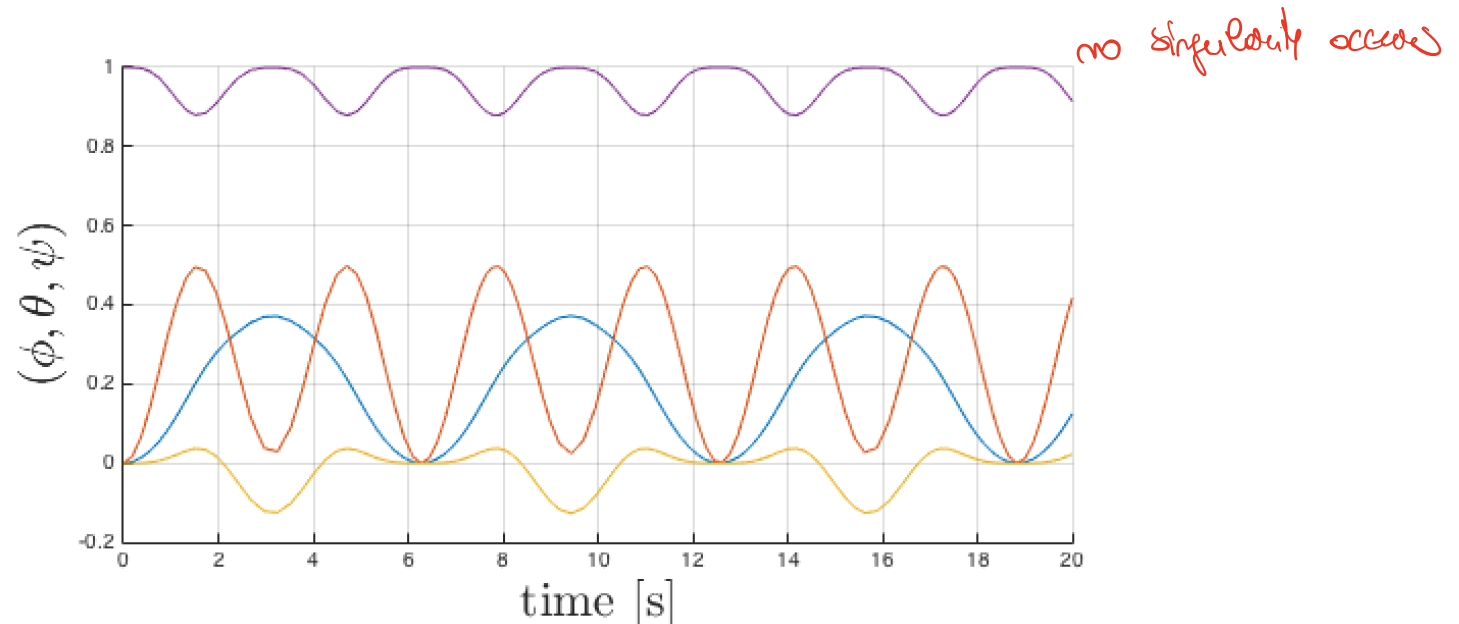
$$\dot{\mathbf{x}} = f(\mathbf{x}, \boldsymbol{\omega}) \text{ state equations}$$

where $\mathbf{x} = \mathbf{T}$, $\mathbf{x} = (\phi, \theta, \psi)$ or $\mathbf{x} = \mathbf{q}$.

- This is a *state equation*, with state \mathbf{x} and input $\boldsymbol{\omega}$.
- State equations allow us to predict the time evolution of a system:
 - ▶ Given an initial state $\mathbf{x}(0) = \mathbf{x}_0$ and an input $\boldsymbol{\omega}(t)$, $t \in [0, \infty)$, $\mathbf{x}(t)$ can be computed for any future time $t \in [0, \infty)$.
 - ▶ This computation is done by integration:
 - ★ analytical (possible only in very particular cases);
 - ★ numerical (always possible).

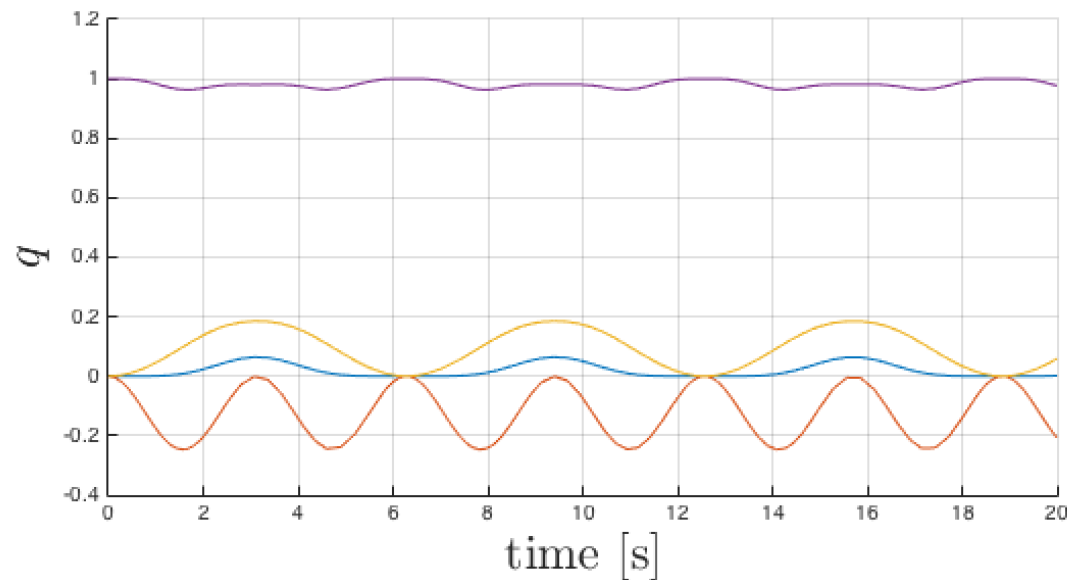
Example

- Consider the kinematic equation for the Tait-Bryan 321 rotation with angles (ψ, θ, ϕ) .
- Suppose that:
 - ▶ $\mathbf{x}(0) = (\phi(0), \theta(0), \psi(0)) = (0, 0, 0)$,
 - ▶ $\boldsymbol{\omega}(t) = (0.2 \sin(t), 0.5 \sin(2t), 0)$.
- The corresponding time evolution, obtained by integration of the kinematic equation is shown in the figure (magenta: $\cos(\theta)$).



Example

- Consider the quaternion kinematic equation.
- Suppose that:
 - ▶ $\mathbf{x}(0) = \mathbf{q}(0) = (0, 0, 0, 1)$,
 - ▶ $\boldsymbol{\omega}(t) = (0.2 \sin(t), 0.5 \sin(2t), 0)$.
- The corresponding time evolution, obtained by integration of the kinematic equation is shown in the figure.



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DCM kinematics

Preliminary considerations

- Equation (1) is a relation between physical vectors but it can be written in terms of coordinate vectors of a RF.
 - ▶ All vectors in an equation must be expressed in the same RF.
- In BF coordinates, the vectors are given by

$$\mathbf{r} \rightarrow \mathbf{r}_B = \begin{bmatrix} x \\ y \\ z \end{bmatrix}, \quad \dot{\mathbf{r}}_B = \begin{bmatrix} \dot{x} \\ \dot{y} \\ \dot{z} \end{bmatrix}, \quad \dot{\mathbf{r}} \rightarrow (\dot{\mathbf{r}})_B = \mathbf{T}^\top \begin{bmatrix} \dot{X} \\ \dot{Y} \\ \dot{Z} \end{bmatrix}$$

where $(\dot{\mathbf{r}})_B$ is the vector $\dot{\mathbf{r}}$ expressed in BF coordinates, T is the rotation $\text{OF} \rightarrow \text{BF}$, and X, Y, Z are the \mathbf{r} coordinates in OF.

DCM kinematics

- A physical vector $\mathbf{r} = x\mathbf{b}_1 + y\mathbf{b}_2 + z\mathbf{b}_3 = X\mathbf{i}_1 + Y\mathbf{i}_2 + Z\mathbf{i}_3$ has coordinate vectors and derivatives given by

$$\begin{aligned}\text{BF} : \quad \mathbf{r}_B &= (x, y, z) \\ \dot{\mathbf{r}}_B &= (\dot{x}, \dot{y}, \dot{z})\end{aligned}$$

$$\begin{aligned}\text{OF} : \quad \mathbf{r}_O &= (X, Y, Z) \\ \dot{\mathbf{r}}_O &= (\dot{X}, \dot{Y}, \dot{Z}).\end{aligned}$$

- Let \mathbf{T} be the rotation matrix $\text{OF} \rightarrow \text{BF}$ (transformation $\text{BF} \rightarrow \text{OF}$). The following relations hold:

$$\begin{aligned}\mathbf{r}_O &= \mathbf{T}\mathbf{r}_B \\ \dot{\mathbf{r}}_O &= \dot{\mathbf{T}}\mathbf{r}_B + \mathbf{T}\dot{\mathbf{r}}_B.\end{aligned}$$

DCM kinematics

- Suppose now that \mathbf{r}_B is an arbitrary constant vector. Then,

$$\dot{\mathbf{r}} = \dot{\mathbf{r}}_B + \boldsymbol{\omega} \times \mathbf{r} = \boldsymbol{\omega} \times \mathbf{r}.$$

- This equation is a relation between physical vectors but it can be expressed in terms of coordinate vectors:

$$(\dot{\mathbf{r}})_B = \boldsymbol{\omega} \times \mathbf{r}_B$$

where $(\dot{\mathbf{r}})_B$ is the vector $\dot{\mathbf{r}}$ expressed in BF coordinates.

- Note that $(\dot{\mathbf{r}})_B \neq \dot{\mathbf{r}}_B = 0$. The expression of $(\dot{\mathbf{r}})_B$ is

$$(\dot{\mathbf{r}})_B = \mathbf{T}^\top \dot{\mathbf{r}}_O.$$

DCM kinematics

- Hence,

$$\mathbf{T}^\top \dot{\mathbf{r}}_O = \boldsymbol{\omega} \times \mathbf{r}_B \quad \Rightarrow \quad \dot{\mathbf{r}}_O = \mathbf{T} \boldsymbol{\omega} \times \mathbf{r}_B.$$

- Since

$$\dot{\mathbf{r}}_O = \dot{\mathbf{T}} \mathbf{r}_B + \mathbf{T} \dot{\mathbf{r}}_B = \dot{\mathbf{T}} \mathbf{r}_B$$

we obtain

$$(\dot{\mathbf{T}} - \mathbf{T} \boldsymbol{\omega} \times) \mathbf{r}_B = 0.$$

- Considering that \mathbf{r}_B is arbitrary, we obtain the DCM kinematic equation

$$\dot{\mathbf{T}} = \mathbf{T} \boldsymbol{\omega} \times .$$

- The transpose kinematic equation directly follows:

$$\dot{\mathbf{T}}^\top = -\boldsymbol{\omega} \times \mathbf{T}^\top.$$

Euler angle kinematics

- The goal is to describe the time evolution of the rotation Euler angles in function of $\omega_1, \omega_2, \omega_3$.
- The overall rotation from OF to BF can be seen as a sequence of 3 intrinsic elementary rotations:
 - 1 OF \rightarrow F1;
 - 2 F1 \rightarrow F2;
 - 3 F2 \rightarrow BF.

where F1 and F2 are intermediate frames.

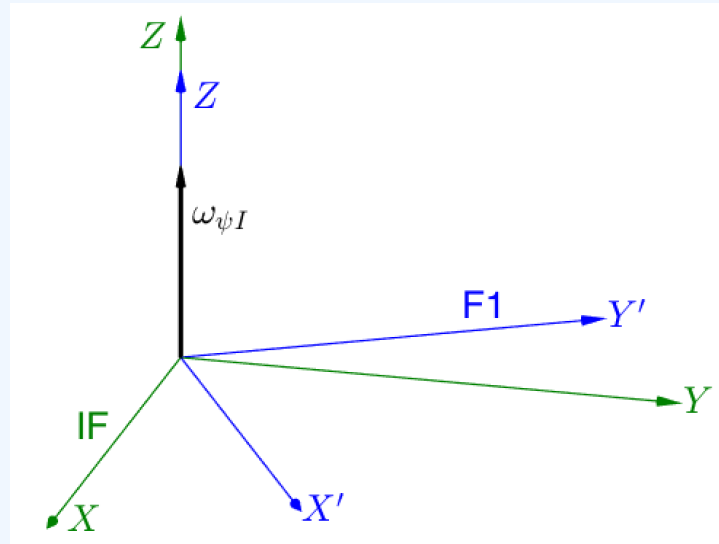
- We consider the Tait-Bryan 321 rotation. The proof for the other cases is similar.
- According to the intrinsic rotation interpretation, the axes of F1 are X', Y', Z , while the axes of F2 are X'', Y', Z' , with $X'' = x$.

Euler angle kinematics

Tait-Bryan 321

1 Rotation OF \rightarrow F1:

- ▶ F1 is rotated wrt OF of an angle ψ about the Z axis.
- ▶ In OF, the angular velocity due to the ψ rotation is $\omega_{\psi I} = [0 \ 0 \ \dot{\psi}]^T$.



- ▶ Coordinate transformations:
 - ★ $\mathbf{T}_3(\psi)$: F1 \rightarrow OF,
 - ★ $\mathbf{T}_3(\psi)^T = \mathbf{T}_3(-\psi)$: OF \rightarrow F1.
- ▶ In F1, the angular velocity is $\omega_{\psi 1} = \mathbf{T}_3(-\psi) \omega_{\psi I} = \omega_{\psi I}$.

Euler angle kinematics

Tait-Bryan 321

2 Rotation $F1 \rightarrow F2$; angle θ about the Y' axis:

- ▶ In $F1$, the angular velocity due to the θ rotation is

$$\boldsymbol{\omega}_{\theta 1} = [0 \ \dot{\theta} \ 0]^\top.$$

- ▶ In $F2$, the angular velocity due to the θ rotation is

$$\boldsymbol{\omega}_{\theta 2} = \mathbf{T}_2(-\theta) \boldsymbol{\omega}_{\theta 1} = \boldsymbol{\omega}_{\theta 1}.$$

- ▶ In $F2$, the angular velocity due to the ψ rotation is

$$\boldsymbol{\omega}_{\psi 2} = \mathbf{T}_2(-\theta) \boldsymbol{\omega}_{\psi 1} = \mathbf{T}_2(-\theta) \boldsymbol{\omega}_{\psi I}.$$

Euler angle kinematics

Tait-Bryan 321

3 Rotation $F2 \rightarrow BF$; angle ϕ about the X'' axis:

- ▶ In $F2$, the angular velocity due to the ϕ rotation is

$$\omega_{\phi 2} = [\dot{\phi} \ 0 \ 0]^T.$$

- ▶ In BF , the angular velocity due to the ϕ rotation is

$$\omega_{\phi B} = \mathbf{T}_1(-\phi) \omega_{\phi 2} = \omega_{\phi 2}.$$

- ▶ In BF , the angular velocity due to the θ rotation is

$$\omega_{\theta B} = \mathbf{T}_1(-\phi) \omega_{\theta 2} = \mathbf{T}_1(-\phi) \omega_{\theta 1}.$$

- ▶ In BF , the angular velocity due to the ψ rotation is

$$\omega_{\psi B} = \mathbf{T}_1(-\phi) \omega_{\psi 2} = \mathbf{T}_1(-\phi) \mathbf{T}_2(-\theta) \omega_{\psi I}.$$

Euler angle kinematics

Tait-Bryan 321

- In BF, the total angular velocity is

$$\begin{aligned}\boldsymbol{\omega} &= \boldsymbol{\omega}_{\phi B} + \boldsymbol{\omega}_{\theta B} + \boldsymbol{\omega}_{\psi B} \\&= \boldsymbol{\omega}_{\phi 2} + \mathbf{T}_1(-\phi) \boldsymbol{\omega}_{\theta 1} + \mathbf{T}_1(-\phi) \mathbf{T}_2(-\theta) \boldsymbol{\omega}_{\psi I} \\&= \begin{bmatrix} \dot{\phi} \\ 0 \\ 0 \end{bmatrix} + \mathbf{T}_1(-\phi) \begin{bmatrix} 0 \\ \dot{\theta} \\ 0 \end{bmatrix} + \mathbf{T}_1(-\phi) \mathbf{T}_2(-\theta) \begin{bmatrix} 0 \\ 0 \\ \dot{\psi} \end{bmatrix} \\&= \mathbf{I}_1 \dot{\phi} + \mathbf{A}_2 \dot{\theta} + \mathbf{B}_3 \dot{\psi} = \begin{bmatrix} \mathbf{I}_1 & \mathbf{A}_2 & \mathbf{B}_3 \end{bmatrix} \begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix}\end{aligned}$$

- ▶ \mathbf{I}_1 is the first column of the identity matrix,
- ▶ \mathbf{A}_2 is the second column of $\mathbf{A} \doteq \mathbf{T}_1(-\phi)$,
- ▶ \mathbf{B}_3 is the third column of $\mathbf{B} \doteq \mathbf{T}_1(-\phi) \mathbf{T}_2(-\theta)$.

Euler angle kinematics

Tait-Bryan 321

- For the Tait-Bryan 321 rotation with angles (ψ, θ, ϕ) , simple calculations yield

$$\begin{bmatrix} \omega_1 \\ \omega_2 \\ \omega_3 \end{bmatrix} = \begin{bmatrix} 1 & 0 & -s\theta \\ 0 & c\phi & s\phi c\theta \\ 0 & -s\phi & c\phi c\theta \end{bmatrix} \begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix}.$$

- Inverting the matrix, we obtain the kinematic equation

$$\begin{bmatrix} \dot{\phi} \\ \dot{\theta} \\ \dot{\psi} \end{bmatrix} = \frac{1}{c\theta} \begin{bmatrix} c\theta & s\phi s\theta & c\phi s\theta \\ 0 & c\phi c\theta & -s\phi c\theta \\ 0 & s\phi & c\phi \end{bmatrix} \begin{bmatrix} \omega_1 \\ \omega_2 \\ \omega_3 \end{bmatrix}.$$

Quaternion kinematics

- The goal is to describe the time evolution of the rotation quaternion \mathbf{q} in function of $\omega_1, \omega_2, \omega_3$.
- Note that both the quaternion and the angular velocity change in time:

$$\mathbf{q} \equiv \mathbf{q}(t)$$

$$\boldsymbol{\omega} = (\omega_1, \omega_2, \omega_3) \equiv \boldsymbol{\omega}(t).$$

- At time $t + \Delta t$, we have the rotation $\mathbf{q}(t)$ at time t composed with the rotation $\Delta\mathbf{q}(t)$ occurred from time t to time $t + \Delta t$.
- The quaternion at time $t + \Delta t$ is thus given by

$$\mathbf{q}(t + \Delta t) = \mathbf{q}(t) \otimes \Delta\mathbf{q}(t).$$

composition with quaternion multiplication

Quaternion kinematics

- The incremental quaternion $\Delta q(t)$ can be written as follows.
 - ▶ Let $\omega = |\boldsymbol{\omega}|$ be the angular speed magnitude;
 - ★ for a small Δt , the rotation angle is $\omega \Delta t$.
 - ▶ Let \mathbf{u} be the rotation axis, with $|\mathbf{u}| = 1$;
 - ★ it follows that $\boldsymbol{\omega} = \omega \mathbf{u}$.

Then, for small Δt , *components of quaternion in standard form*

$$\Delta q \cong \begin{bmatrix} \cos \frac{\omega \Delta t}{2} \\ \mathbf{u} \sin \frac{\omega \Delta t}{2} \end{bmatrix} \underset{\substack{\text{when } \Delta t \rightarrow 0}}{\cong} \begin{bmatrix} 1 \\ \mathbf{u} \frac{\omega \Delta t}{2} \end{bmatrix} = \begin{bmatrix} 1 \\ \frac{\boldsymbol{\omega} \Delta t}{2} \end{bmatrix}.$$

- The quaternion derivative is thus given by

$$\begin{aligned} \dot{q} &= \lim_{\Delta t \rightarrow 0} \frac{q(t+\Delta t) - q(t)}{\Delta t} = \lim_{\Delta t \rightarrow 0} \frac{q \otimes \Delta q - q}{\Delta t} \\ &= \lim_{\Delta t \rightarrow 0} \frac{q \otimes (\Delta q - (1, \mathbf{0}))}{\Delta t} = \lim_{\Delta t \rightarrow 0} \frac{q \otimes ((1, \boldsymbol{\omega} \Delta t / 2) - (1, \mathbf{0}))}{\Delta t}. \end{aligned}$$

Quaternion kinematics

- Consider that $(1, \frac{\omega \Delta t}{2}) - (1, \mathbf{0}) = (0, \frac{\omega \Delta t}{2})$. Then,

$$\dot{\mathbf{q}} = \lim_{\Delta t \rightarrow 0} \frac{\mathbf{q} \otimes (0, \frac{\omega \Delta t}{2})}{\Delta t} = \frac{1}{2} \mathbf{q} \otimes (0, \omega) \Rightarrow \dot{\mathbf{q}} = \frac{1}{2} \mathbf{q} \otimes (0, \omega).$$

- Equivalent equations are the following: *same equation*

$$\dot{\mathbf{q}} = \frac{1}{2} \Omega \mathbf{q}$$

$$\dot{\mathbf{q}} = \frac{1}{2} \mathbf{Q} \omega$$

$$\Omega \doteq \begin{bmatrix} 0 & -\omega_1 & -\omega_2 & -\omega_3 \\ \omega_1 & 0 & \omega_3 & -\omega_2 \\ \omega_2 & -\omega_3 & 0 & \omega_1 \\ \omega_3 & \omega_2 & -\omega_1 & 0 \end{bmatrix},$$

$$\mathbf{Q} \doteq \begin{bmatrix} -q_1 & -q_2 & -q_3 \\ q_0 & -q_3 & q_2 \\ q_3 & q_0 & -q_1 \\ -q_2 & q_1 & q_0 \end{bmatrix}.$$