

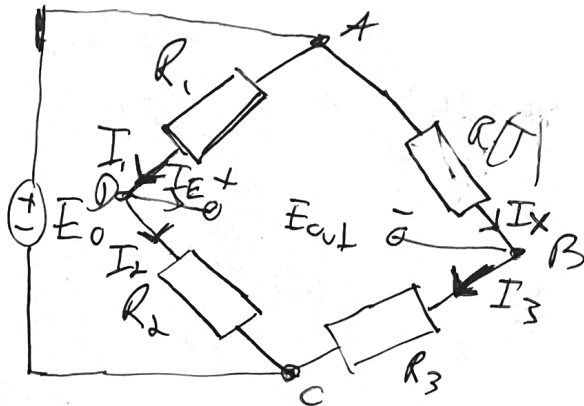
## Öving 2 - Karakterisering av sensorer

Wheatstone bro

$$R(T) = R_0 + \alpha \Delta T$$

$$\Delta T = T - T_0$$

$$E_{out} \propto \Delta T$$



Spänningsdelning över  
ADC vs ABC

$$\text{Från D: } V_D = \frac{R_2}{R_1 + R_2} E_0$$

$$\text{Från B: } V_B = \frac{R_3}{R_3 + R(T)} E_0$$

a)  $I_1 = I_2$ ,  $I_3 = I_x$ ,  $V_D = V_B$

$$\frac{V_{DC}}{V_{AD}} = \frac{V_{BC}}{V_{AB}} \Rightarrow \frac{I_2 R_2}{I_1 R_1} = \frac{I_3 R_3}{I_x R(T)}$$

$$\Rightarrow R(T) = R_3 \frac{R_1}{R_2}$$

$$E_{out} = \left( \frac{R_2}{R_1 + R_2} - \frac{R_3}{R_3 + R(T)} \right) E_0$$

$$E_{out} = E_0 \frac{R_2 \cdot R(T) - R_1 R_3}{(R_1 + R_2)(R_3 + R(T))}$$

V) se a)

$$F = \frac{R_1}{R_2} = \frac{R_0}{R_3} \quad \text{hvis } \alpha \Delta T \ll R_0$$

Siden  $I_1 = I_2$   $I_3 = I_x$

og at spændinger over branch ADC og ABC er den samme så

må

$$\frac{V_{AC}}{V_{AD}} = \frac{V_{BC}}{V_{AB}} \Leftrightarrow \frac{R_1}{R_2} = \frac{R(T)}{R_3} = \frac{R_0 + \alpha \Delta T}{R_3}$$

$$\alpha \Delta T \ll R_0 \Rightarrow \frac{R_1}{R_2} = \frac{R_0}{R_3}$$

$$\frac{E_{out}}{E_0} = \frac{R_2}{R_1 + R_2} - \frac{R_3}{R_3 + R(T)} \Rightarrow \frac{\frac{R_1}{F}}{\frac{R_1}{F} + R_1} = \frac{1}{1 + F}$$

$$\frac{R_3}{R_3 + R_0 + \alpha \Delta T} = \frac{\frac{R_0}{F}}{\frac{R_0}{F} + R_0 + \alpha \Delta T} = \frac{\frac{1}{F}}{\frac{1}{F} + 1 + \frac{\alpha \Delta T}{R_0}}$$

$$= \frac{1}{1 + F + \frac{\alpha \Delta T}{R_3}}$$

$$\boxed{\frac{1}{1+x} \approx 1-x}$$

$$\frac{E_{out}}{E_0} = \frac{1}{1+F} - \frac{1}{1+F + \frac{\alpha \Delta T}{R_3}}$$

$$E_{out} = \frac{E_0}{1+F} \left[ 1 - \frac{1}{1 + \frac{\alpha \Delta T}{R_3(1+F)}} \right]$$

$$= \frac{E_0}{1+F} \left[ 1 - \frac{1}{1 + \frac{\alpha \Delta T}{\frac{R_0}{F}(1+F)}} \right]$$

$$\frac{1}{1+x} \approx 1-x$$

$$= \frac{E_0}{1+F} \left[ 1 - \left( 1 - \frac{\alpha \Delta T}{\frac{R_0}{F} + R_0} \right) \right]$$

$$E_{out} = \frac{E_0}{(1+F) \left( \frac{1}{F} + 1 \right) R_0} \alpha \Delta T$$

$$\underline{E_{out} \propto \Delta T}$$

$$E_{out} = \frac{E_0 \propto \Delta T}{\frac{1}{F} + 1 + 1 + F} = \frac{E_0 \propto \Delta T}{2 + \frac{1}{F} + F} = E_0 \propto \Delta T \frac{F}{(1+F)^2}$$

$\downarrow$   
 $F^2 + 2F + 1$

$$\Rightarrow \quad \cancel{u = F^2 + 2F + 1} \quad | \quad u = \frac{1}{F} + 2 + F$$

$$\cancel{du = 2F + 2 dF} \quad | \quad du = -\frac{1}{F^2} + 1$$

$$u = \dots \quad u = 2 + F + \frac{1}{F}$$

$$= \frac{d}{du} \frac{1}{u} \frac{du}{dF} \quad u = 1 - F^2 \frac{dx}{dF}$$

$$\frac{\partial E_{out}}{\partial F} = E_0 \propto \Delta T \frac{d}{dF} \left[ \frac{1}{2 + F + \frac{1}{F}} \right] = \frac{1 - F}{(F + 1)^3} = 0$$

$$\underline{\underline{F = 1}}$$

d) Stille Temperaturspringe ( $\Delta T$ )

• da er immer  $\frac{1}{1+x} \approx 1-x$ , wenn

$$\frac{1}{1+x} = 1 - x - x^2 - x^3 - x^4 - \dots$$

$$\bar{E}_{out} = \frac{\bar{E}_0}{1+F} - \frac{1}{1 + \frac{\alpha \Delta T}{R_3}}$$

$$\bar{E}_{out} = A_1 \left( \frac{\alpha \Delta T}{R_3} \right) + A_2 \left( \frac{\alpha \Delta T}{R_3} \right)^2 + A_3 \left( \frac{\alpha \Delta T}{R_3} \right)^3 + \dots$$