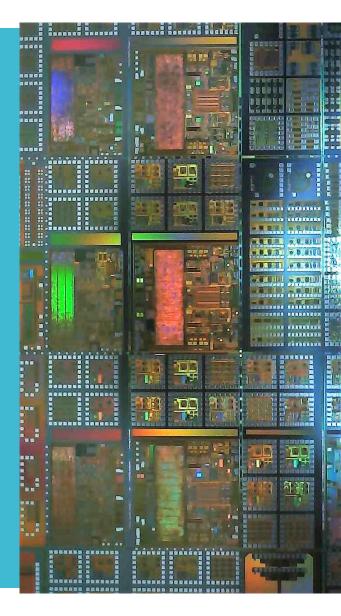


# Diseño Analógico

2024







# Calendario

#### Capítulo 1: Introducción

- · Clase 1: Transistores Bipolar y MOS. Pequeña señal. Circuitos monoetapas
- · Clase 2: Cadence Introducción y Circuitos monoetapas
- · Clase 3: Par diferencial. Amplificador diferencial. Implementación básica

## Capítulo 2: Respuesta en Frecuencia y Estabilización

- Clase 4: Amplificador operacional: Respuesta en frecuencia, estabilidad.
   Capacidades asociadas al transistor MOS
- Clase 5: Cadence Amplificador operacional. Operación en DC, offset sistemático, ganancia
- · Clase 6: Estabilización, Miller, cero asociado, compensaciones avanzadas
- Clase 7: Cadence Amplificador operacional. Respuesta en frecuencia, estabilidad





# Capítulo 3: Amplificadores Avanzados

- Clase 8: Amplificadores avanzados. Current mirror opamp, cascode, folded amplifier, folded cascode.
- · Clase 9: Amplificadores avanzados. Push-pull output, Diff-diff, CMFB
- Clase 10: Cadence Amplificadores avanzados

### Capítulo 4: Ruido, offset

- Clase 11: Offset
- · Clase 12: Ruido
- · Clase 13: Cadence Diseño con offset y ruido

## Capítulo 5: Circuitos auxiliares

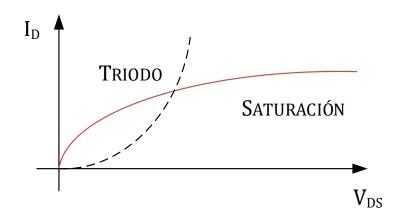
- · Clase 14: Circuitos auxiliares. Referencias, bandgap, osciladores
- Clases 15/16: Extra. Diseño físico de semiconductores (layout)

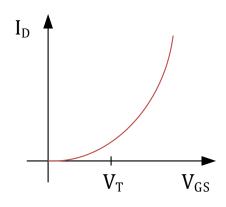
# Calendario



#### • 1.1 Transistor MOS

#### 1.1.1 Transferencias





## 1.1.2 Modos de Operación

Subthreshold

Triodo

$$VGS > VT$$
 ,  $VDS < VGS - VT$ 

$$ID = Kp \frac{W}{L} \left[ (VGS - VT)VDS - \frac{VDS^2}{2} \right]$$

#### Saturación

$$VGS > VT$$
 ,  $VDS > VGS - VT$ 

$$ID = \frac{1}{2} Kp \frac{W}{L} (VGS - VT)^{2} (1 + \lambda VDS)$$

Si 
$$\lambda VDS \ll 1 \Rightarrow$$

$$ID = \frac{1}{2} Kp \frac{W}{L} (VGS - VT)^2$$

## $Kp = \mu o. Cox$

μο: Zero field mobility

Cox: Gate oxide capacitance per unit area

$$Cox = \frac{\varepsilon ox}{tox}$$

tox: Gate oxide thickness

εοχ: Oxide permittivity

$$\epsilon ox = \epsilon o. \epsilon r$$

$$\varepsilon o = 8.85 \times 10^{-12} \text{ F/m}$$

$$\varepsilon r = 3.9 \text{ para SiO}_2$$

$$VT = VT0 + \gamma \left[ \sqrt{2\varphi f + VSB} - \sqrt{2\varphi f} \right]$$

VT0: Zero bias threshold voltage [V]

 $\gamma$ : Bulk threshold parameter [ $\sqrt{V}$ ]

 $2\phi f$ : Strong inversion surface potential [V]

VSB: Source to Body voltage [V]

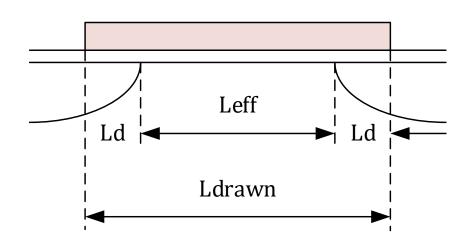
$$\lambda = \frac{1}{VA}$$
 VA: Early voltage [V]

$$\lambda = \frac{1}{\text{Leff}} \frac{dXd}{dVDS}$$

Leff = Ldrawn - 2Ld - Xd

Ld: Lateral diffusion

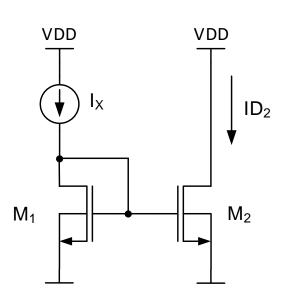
Xd: Depletion layer width



La variación de Xd con el voltaje VDS es compleja, por el hecho de que la distribución del campo en la región desierta del drain no es unidimensional. Por consiguiente, el cálculo de  $\lambda$  a partir de la estructura del dispositivo es difícil.

El valor de  $\lambda$  se suele obtener de datos experimentales.

Ejemplo: Espejo de corriente



$$VGS1 = VGS2$$

VDS1 = VGS1 → VGS1 será tal que ID1 = IX

$$\frac{\text{ID1}}{\text{ID1}} = \frac{1}{2} \text{Kp} \frac{\text{W1}}{\text{L1}} (\text{VGS1} - \text{VT})^2 \quad \Rightarrow \quad \text{VGS1} = \sqrt{\frac{2. \text{ID1}}{\text{Kp} \frac{\text{W1}}{\text{L1}}}} + \text{VT}$$

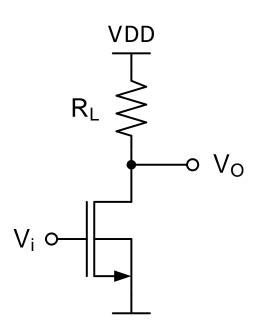
$$\frac{\text{ID2}}{\text{ID2}} = \frac{1}{2} \text{Kp} \frac{\text{W2}}{\text{L2}} \left( \sqrt{\frac{2. \text{ID1}}{\text{Kp} \frac{\text{W1}}{\text{L1}}}} + \text{VT} - \text{VT} \right)^2$$

$$\frac{\text{ID2}}{\text{ID2}} = \frac{1}{2} \text{Kp} \frac{\text{W2}}{\text{L2}} \left( \sqrt{\frac{2. \text{ID1}}{\text{Kp} \frac{\text{W1}}{\text{L1}}}} + \text{VT} - \text{VT} \right)^{2}$$

$$ID2 = \frac{W2}{L2} \frac{L1}{W1} ID1$$

Si L1 = L2 
$$\rightarrow$$
 ID2 =  $\frac{W2}{W1}$ ID1

Ejemplo: Ganancia de señal



$$Kp=120\mu A/V^2\,,\ RL=100k\Omega\,,\ ID=10\mu A$$
 
$$VDD=3V\,,\ W=10\mu m\,,\ L=5\mu m\,,\ VT=0.7V$$

$$\frac{\Delta Vo}{\Delta Vi} = ?$$

Vi = ?

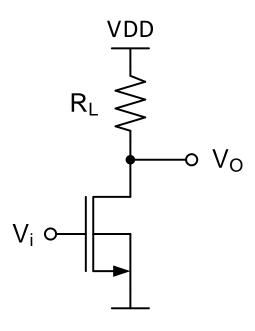
Primero es necesario calcular el punto Q

$$Vo = VDD - ID. RL$$

$$Vo = VDD - RL. \frac{1}{2} Kp \frac{W}{L} (Vi - VT)^{2}$$

$$Vi = VT + \sqrt{\frac{2.ID}{Kp W/L}}$$

Ejemplo: Ganancia de señal



$$Kp=120\mu A/V^2\,,\ RL=100k\Omega\,,\ ID=10\mu A$$
 
$$VDD=3V\,,\ W=10\mu m\,,\ L=5\mu m\,,\ VT=0.7V$$

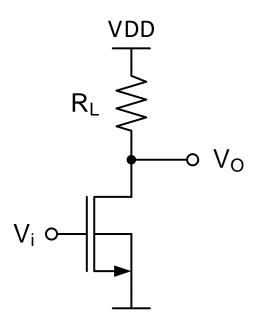
$$Vi = 0.7V + \sqrt{\frac{2x10\mu A}{120\mu A/V^2 \frac{10\mu m}{5\mu m}}}$$

$$Vi = 0.7V + 0.289V = 0.989V$$

$$Vo = 3V - 100k\Omega \cdot \frac{1}{2}120\mu A/V^2 \frac{10\mu m}{5\mu m}(0.989V - 0.7V)^2$$

$$Vo = 1.998V$$

Ejemplo: Ganancia de señal



$$Kp = 120\mu A/V^2 \,, \quad RL = 100k\Omega \,, \quad ID = 10\mu A$$
 
$$VDD = 3V \,, \quad W = 10\mu m \,, \quad L = 5\mu m \,, \quad VT = 0.7V$$

Defino: 
$$\Delta Vi = 10 \text{mV} \rightarrow$$

$$Vi2 = 0.999V \rightarrow$$

$$Vo2 = 1.927V$$

$$\frac{\Delta Vo}{\Delta Vi} = \frac{1.927V - 1.998V}{0.999V - 0.989V}$$

$$\frac{\Delta Vo}{\Delta Vi} = -7.1 \, V/V$$

Ejemplo: Ganancia de señal

$$Kp=120\mu A/V^2\,,\ RL=100k\Omega\,,\ ID=10\mu A$$
 
$$VDD=3V\,,\ W=10\mu m\,,\ L=5\mu m\,,\ VT=0.7V$$

Defino: 
$$\Delta Vi = 1mV \rightarrow$$

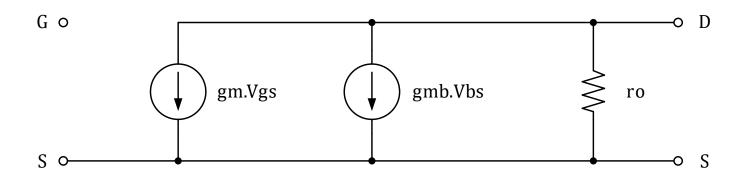
$$Vi2 = 0.99V \rightarrow$$

$$Vo2 = 1.991V$$

$$\frac{\Delta Vo}{\Delta Vi} = \frac{1.991V - 1.998V}{0.99V - 0.989V}$$

$$\frac{\Delta \text{Vo}}{\Delta \text{Vi}} = -7.0 \text{ V/V}$$

#### 1.1.3 Pequeña Señal



gm = 
$$\frac{dID}{dVGS}$$
 = Kp $\frac{W}{L}$ (VGS - VT)(1 +  $\lambda$ VDS)

Si 
$$\lambda VDS \ll 1 \Rightarrow$$

$$gm = kp \frac{w}{L} (VGS - VT) = \sqrt{2Kp \frac{w}{L}} ID$$

gmb = 
$$\frac{dID}{dVBS}$$
 =  $-Kp\frac{W}{L}(VGS - VT)(1 + \lambda VDS)\frac{dVT}{dVBS}$ 

$$\frac{dVT}{dVBS} = -\frac{\gamma}{2\sqrt{2\varphi f + VSB}} = -\chi$$

gmb = 
$$\gamma$$
. Kp  $\frac{W}{L} \frac{VGS - VT}{2\sqrt{2\phi f + VSB}} (1 + \lambda VDS)$ 

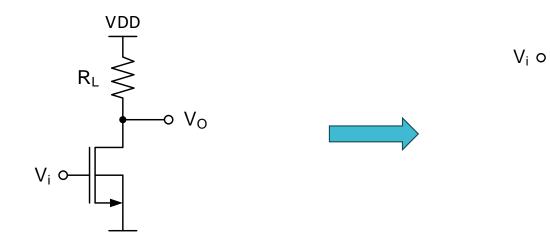
$$\frac{\text{gmb}}{\text{gm}} = \frac{\gamma}{2\sqrt{2\phi f + \text{VSB}}} = \chi$$

*Típicamente*  $\chi$  *vale* 0.1 a 0.3  $\Rightarrow$  *gm es* 3 a 10 *veces más grande que gmb* 

$$ro = \frac{VA}{ID} = \frac{1}{\lambda ID}$$

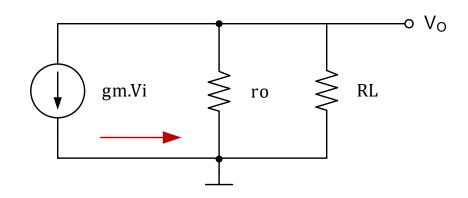
ro α Leff

Ejemplo de Ganancia - Continuación



gm = 
$$\sqrt{2Kp \frac{W}{L} ID}$$
 =  $\sqrt{2x120\mu A/V^2 \frac{10\mu m}{5\mu m}} 10\mu A$ 

$$gm = 69.36 \mu S$$



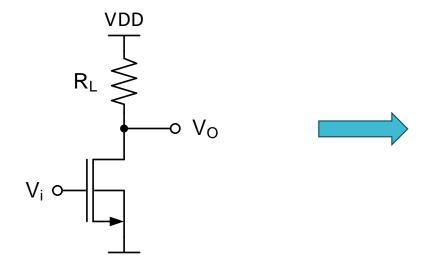
$$\frac{\Delta Vo}{\Delta Vi} = -gm. (ro // RL)$$

$$ro = \frac{1}{\lambda ID}$$

$$\lambda = 0.01 1/V$$

$$ro = 10M\Omega$$

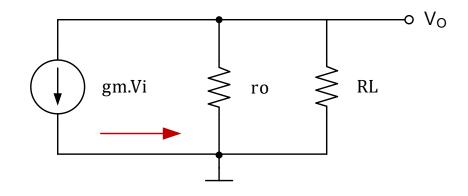
Ejemplo de Ganancia - Continuación



$$\frac{\Delta Vo}{\Delta Vi} = -69.36\mu S. (10M\Omega//100k\Omega)$$

$$\frac{\Delta Vo}{\Delta Vi} = -6.9 \, \text{V/V}$$

 $V_i$  o



$$\frac{\Delta Vo}{\Delta Vi} = -7.1 \, \text{V/}_{\text{V}} \quad (\Delta Vi = 10 \,\text{mV})$$

$$\frac{\Delta Vo}{\Delta Vi} = -7.0 \text{ V/}_{V} \quad (\Delta Vi = 1 \text{mV})$$

Valores típicos, NMOS

$$Kp = 100 \mu A/V^2$$
,  $ID = 10 \mu A$ 

$$W = 10 \mu m$$
,  $L = 5 \mu m$ ,  $\lambda = 0.01 1/V$ 

$$gm = \sqrt{2Kp \frac{W}{L} ID} = 63.25 \mu S$$

$$\frac{1}{\text{gm}} = 15.81 \text{k}\Omega$$

$$ro = \frac{1}{\lambda ID} = 10M\Omega$$

$$ro \gg \frac{1}{gm}$$

gm. ro = 
$$632.5 \gg 1$$

Valores típicos, PMOS

$$Kp = 30\mu A/V^2$$
,  $ID = 10\mu A$ 

$$W = 10 \mu m$$
,  $L = 5 \mu m$ ,  $\lambda = 0.02 1/V$ 

$$gm = \sqrt{2Kp \frac{W}{L} ID} = 34.64\mu S$$

$$\frac{1}{\text{gm}} = 28.87 \text{k}\Omega$$

$$ro = \frac{1}{\lambda ID} = 5M\Omega$$

$$ro \gg \frac{1}{gm}$$

gm. ro = 
$$173.2 \gg 1$$

#### • 1.2 Transistor Bipolar

#### 1.2.1 Operación en DC

$$IC = IS.e^{\frac{VBE}{VT}} \left( 1 + \frac{VCE}{VA} \right)$$

$$IS = \frac{q. A. D_n. ni^2}{W_B. NA} \qquad (NPN) \qquad IS típico de 10^{-16} a 10^{-14} A$$

A: Cross-sectional emitter area

N<sub>A</sub>: Base doping density

ni: Silicon intrinsic carrier concentration

D<sub>n</sub>: Electron diffusion parameter in the base

W<sub>B</sub>: Base width

$$VT = \frac{k.T}{q}$$

Si 
$$\frac{\text{VCE}}{\text{VA}} \ll 1 \rightarrow \text{IC} = \text{IS.e} \frac{\text{VBE}}{\text{VT}}$$

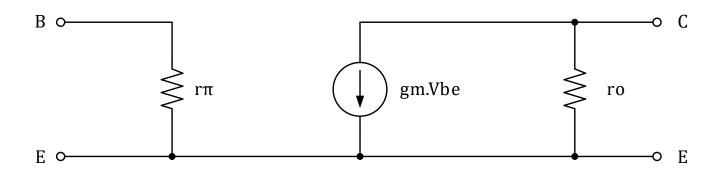
$$\beta_{\rm F} = \frac{\rm IC}{\rm IB}$$

$$|IE| = IC + IB$$

$$|IE| = \frac{IC}{\alpha_F}$$

$$\alpha_{\rm F} = \frac{\beta_{\rm F}}{1 + \beta_{\rm F}} \quad \rightarrow \quad \alpha_{\rm F} < 1 \qquad (IC < IE)$$

## 1.2.2 Pequeña Señal



$$gm = \frac{dIC}{dVBE}$$

$$gm = \frac{IC}{VT}$$

$$r\pi = \frac{vi}{ib} = \frac{vi}{ic}\beta c$$

βo: Small signal current gain

Si  $\beta$ F es constante  $\rightarrow$   $\beta_F = \beta$ o En general  $\beta_F \approx \beta_F \approx \beta$ 

$$r\pi = \frac{vi}{ib} = \frac{vi}{ic}\beta = \frac{\beta}{gm}$$

$$r\pi = \frac{\beta.VT}{IC}$$

$$\beta = r\pi$$
. gm

$$ro = \frac{VA}{IC}$$

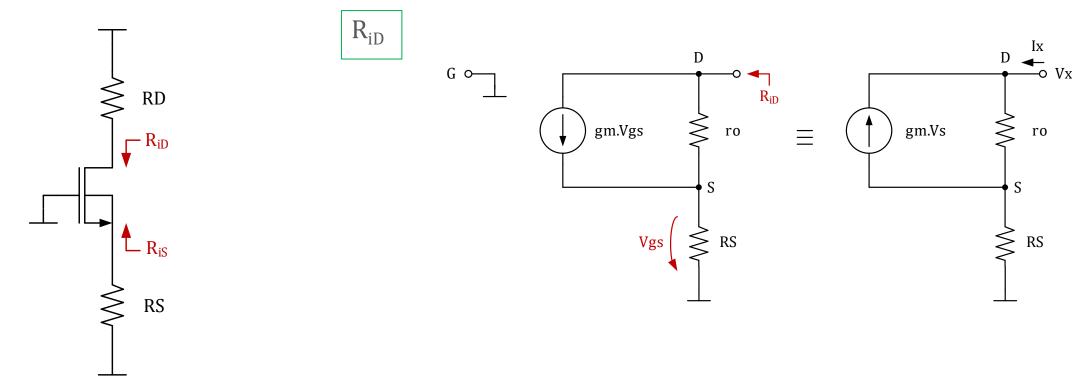
VA: Early voltage

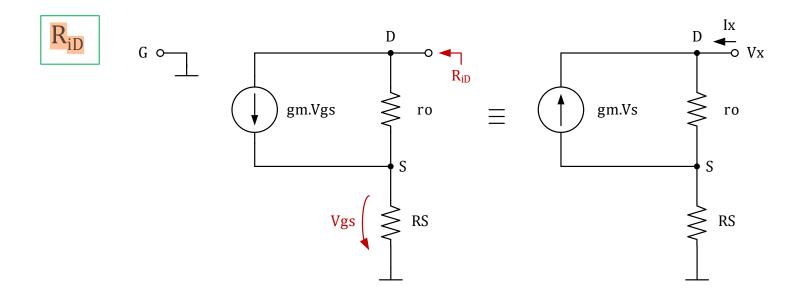
$$ro = \frac{1}{\eta \cdot gm}$$
  $\eta = \frac{k \cdot T}{q \cdot VA}$ 

#### • 1.3 Cálculo de Parámetros de Pequeña Señal en Transistores MOS

El objetivo de esta sección es definir una metodología para simplificar el cálculo de transferencias de pequeña señal. Para eso obtendremos las impedancias y ganancias típicas del transistor MOS

## 1.3.1 Impedancias





$$Vx = Ix.RS + (Ix + gm.VS)$$
. ro

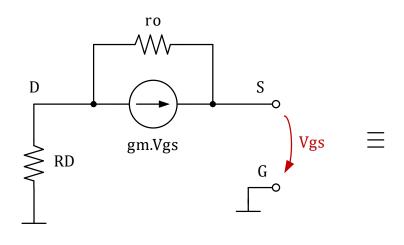
$$VS = Ix.RS$$

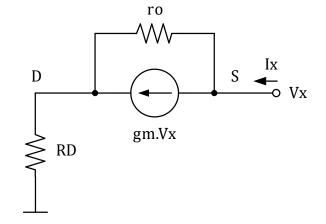
$$Vx = Ix.RS + Ix.ro + Ix.gm.ro.RS$$

$$R_{iD}$$
= gm.ro.RS + ro + RS

Si 
$$RS = 0 \rightarrow R_{iD} = rc$$







$$Vx = Ix.RD + (Ix - gm.Vx) . ro$$

$$Vx.(1+gm.ro) = Ix.(RD + ro)$$

$$R_{IS} = \frac{RD + ro}{1 + gm.ro}$$

$$R_{IS} \approx \frac{RD + ro}{gm. ro}$$

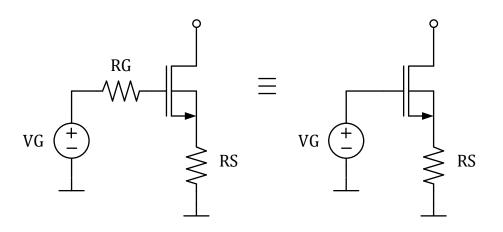
$$RD = 0$$

$$R_{iS} = 1 / gm$$

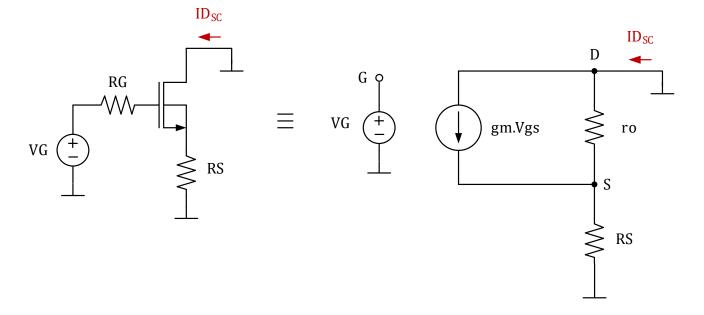
## 1.3.2 Ganancias

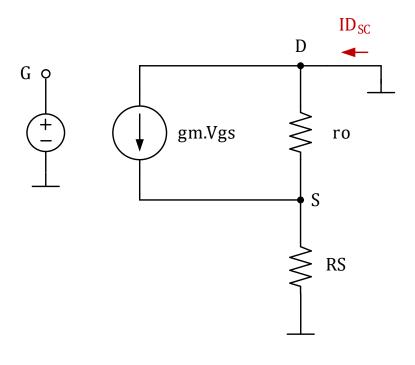


(Corriente de drain de cortocircuito)



## Equivalente de Norton

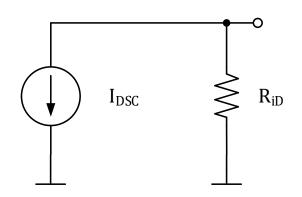




$$Vgs = VG - ID_{SC}.RS$$
 
$$ID_{SC}.RS + (IDSC - gm.Vgs) \cdot ro = 0$$
 
$$ID_{SC}.RS + ID_{SC}.ro = gm.VG.ro - ID_{SC}.RS.gm.ro$$

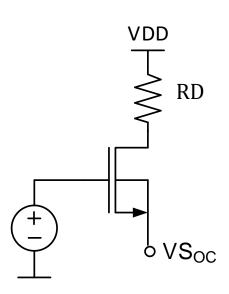
$$ID_{SC} = VG \frac{gm. ro}{gm. ro. RS + RS}$$

Si 
$$RS = 0 \rightarrow ID_{SC} = VG.gm$$

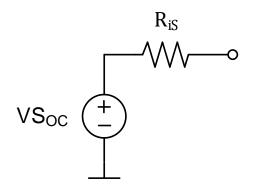




(Tensión de source de circuito abierto)

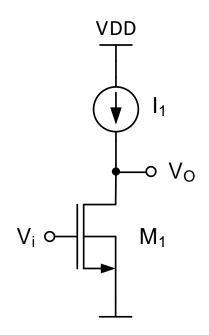


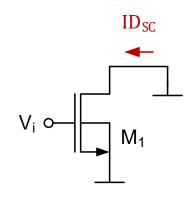
$$VS_{SC} = VG \frac{gm. ro}{1 + gm. ro}$$
  $\rightarrow$   $VS_{OC} \approx VG$ 



## 1.4 Circuitos Monoetapas

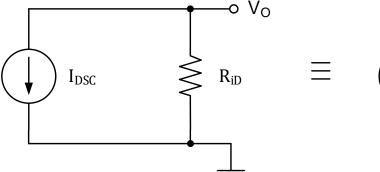
## 1.4.1 Carga Ideal

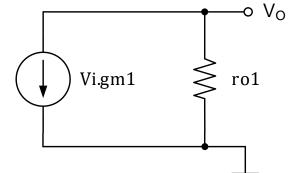






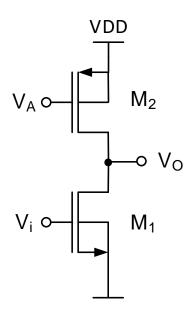
$$R_{iD} = ro1$$

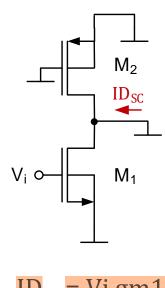




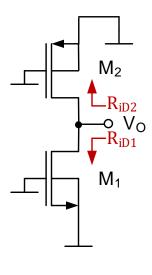
Vo = - Vi.gm1.ro1

## 1.4.2 Carga Activa

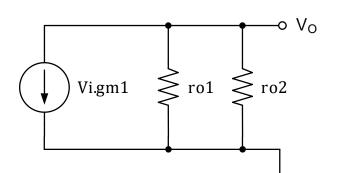




$$ID_{SC} = Vi.gm1$$

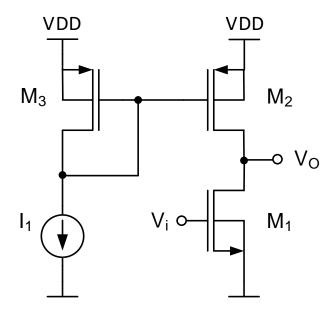


$$R_{iD} = ro1 // ro2$$



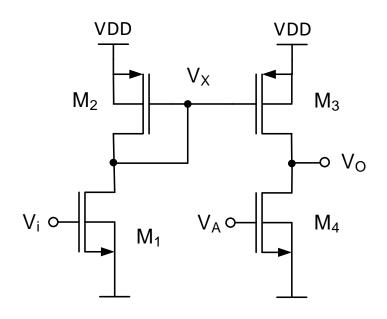
Vo = - Vi.gm1.(ro1//ro2)

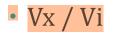
## 1.4.3 Carga Activa v2

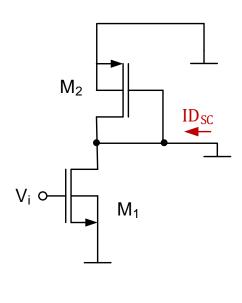


Vo = - Vi.gm1.(ro1//ro2)

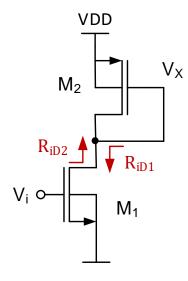
## 1.4.4 Carga Activa v3





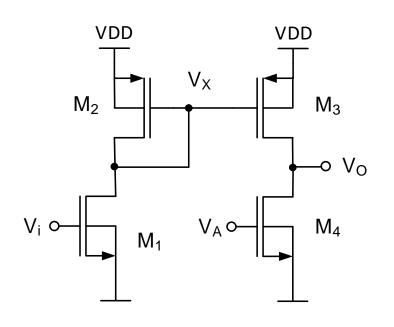


$$ID_{SC} = Vi.gm1$$



$$R_{iD} = ro1 // (1/gm2) \approx 1/gm2$$

$$Vx = -Vi \frac{gm1}{gm2}$$



Vo / Vx

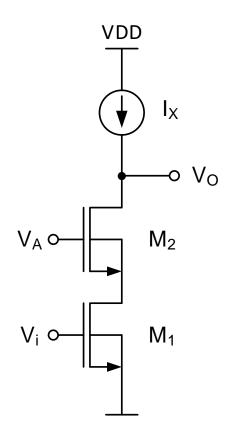
$$Vo = - Vx.gm3.(ro3//ro4)$$

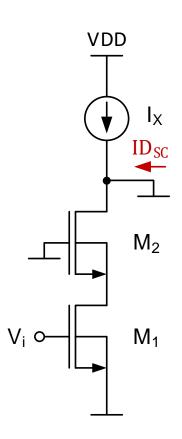
Vo / Vi

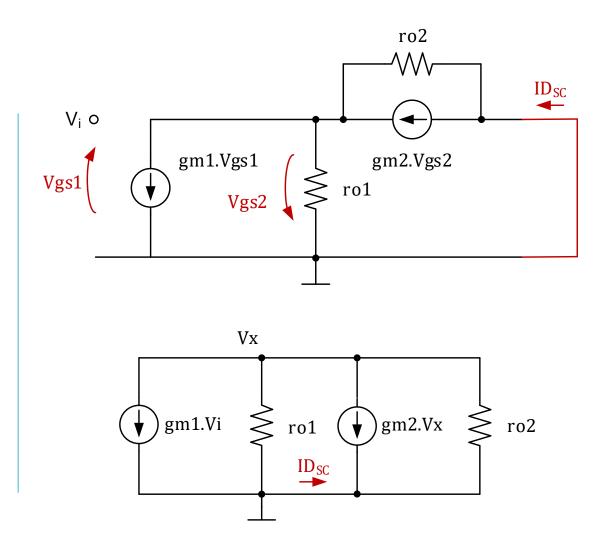
$$Vo = Vi \frac{gm3}{gm2} gm1(ro3//ro4)$$
 (Cambio de signo)

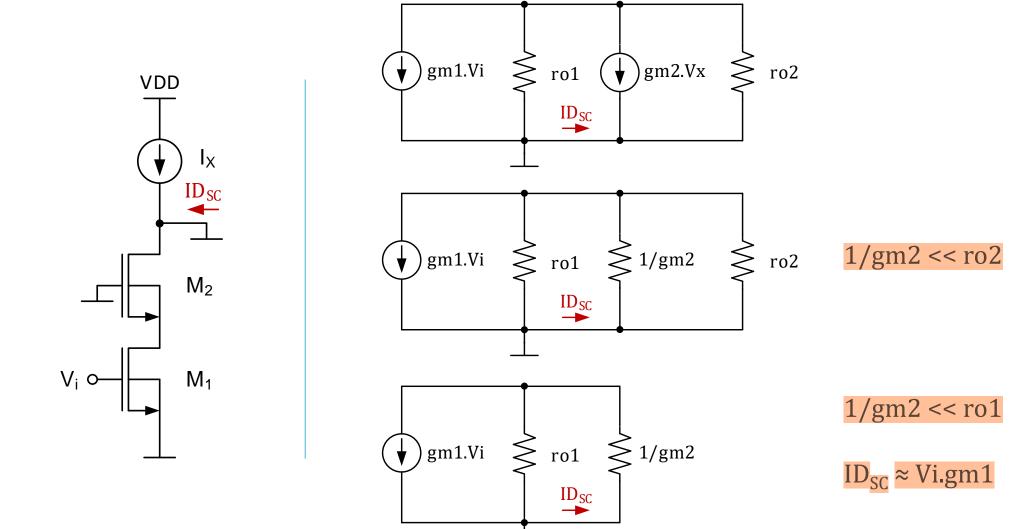
Si 
$$M2 = M3 \rightarrow Vo = Vi.gm1.(ro3//ro4)$$

## 1.4.5 Cascode



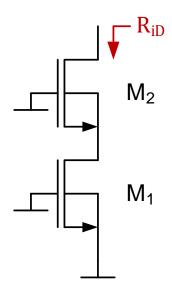




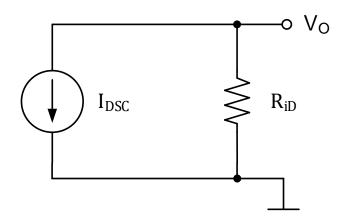


 $\rightarrow$ 

Vx

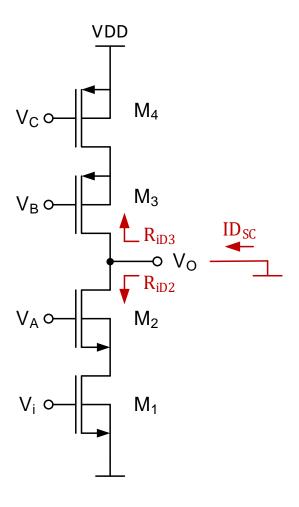


 $R_{iD} = gm2.ro2.ro1 + ro2 + ro1 \approx gm2.ro2.ro1$ 



Vo = - Vi.gm1.ro1.gm2.ro2

## 1.4.6 Cascode con carga activa



$$ID_{SC} = Vi.gm1$$

$$R_{iD2} = gm2.ro2.ro1$$

$$R_{iD3} = gm3.ro3.ro4$$

Vo = - Vi.gm1.(gm2.ro2.ro1)//(gm3.ro3.ro4)