

PVfit Performance Model

Model is based on the single-diode equation (SDE):

$$I = I_{ph} - I_{rs} \left(e^{\frac{q(V+IR_s)}{N_s n k_B T}} - 1 \right) - \frac{V + IR_s}{R_p},$$

with auxiliary equations formulated w.r.t.

$$\text{Effective Irradiance Ratio } F = \frac{I_{sc}}{I_{sc0}}$$

and Cell Temperature T .

I_{ph} is derived from the SDE at $V = 0$ and $I = I_{sc}$:

$$\begin{aligned} I_{ph} &= I_{rs} \left(e^{\frac{q I_{sc} R_s}{N_s n k_B T}} - 1 \right) + \frac{I_{sc} R_s}{R_p} + I_{sc} \\ &= I_{rs} \left(e^{\frac{q(F I_{sc0}) R_s}{N_s n k_B T}} - 1 \right) + \frac{F I_{sc0} R_s}{R_p} + F I_{sc0}. \end{aligned}$$

F may be determined several ways. A new method here uses spectral-irradiance, spectral-response, and MET-station data, including diffuse-angular effects.

PV Reference Device

$$F = \frac{I_{sc}}{I_{sc0}} = M(T, T_0) \frac{I_{sc,ref}}{I_{sc,ref0}} \quad \left(\begin{array}{l} \text{temperature and} \\ \text{IAM matched} \end{array} \right)$$

Sandia Array Performance Model

$$\begin{aligned} F &= \frac{I_{sc}}{I_{sc0}} = E_e (1 + \alpha_{sc0} (T - T_0)) \\ &= f_1 \frac{f_2 G_b + f_d G_d}{G_0} (1 + \alpha_{sc0} (T - T_0)) \end{aligned}$$

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Key Result

PVfit's single-diode model formulation, using the *effective irradiance ratio* $F = I_{sc}/I_{sc0}$, accommodates spectral and diffuse-angular corrections using device-spectral-response (equivalently, QE), spectral-irradiance, and MET-station data. This methodology complements F 's alternative determination by PV reference device or the Sandia Array Performance Model.

Derivation of Effective Irradiance Ratio using Spectral and Angular-Diffuse Corrected MET-Station Data

$$F = \frac{I_{sc}}{I_{sc0}} = \frac{I_{sc,T_0} (1 + \alpha_{sc0} (T - T_0))}{I_{sc0}} = \frac{A \int_{\lambda=0}^{\infty} S(\lambda, T_0) E_{eff}(\lambda) d\lambda (1 + \alpha_{sc0} (T - T_0))}{A \int_{\lambda=0}^{\infty} S(\lambda, T_0) E_0(\lambda) d\lambda} = \underbrace{\frac{\int_{\lambda=0}^{\infty} S(\lambda, T_0) E_{eff}(\lambda) d\lambda}{\int_{\lambda=0}^{\infty} S(\lambda, T_0) E_0(\lambda) d\lambda}}_{\text{spectral correction}} (1 + \alpha_{sc0} (T - T_0)),$$

where, by the assumption of current linearity w.r.t total irradiance, the effective spectral irradiance, E_{eff} , is scaled so that it equals the effective POA irradiance G_{eff} :

$$\int_{\lambda=0}^{\infty} E_{eff}(\lambda) d\lambda = G_{eff} = G_{dir,eff} + G_{cir,eff} + G_{sky,eff} + G_{hor,eff} + G_{grd,eff} = \underbrace{g_{dir}(\theta_{sun}) G_{dir}}_{\text{IAM correction}} + \underbrace{g_{cir}(\theta_{sun}) G_{cir} + g_{sky}(\theta_{tilt}) G_{sky} + g_{hor}(\theta_{tilt}) G_{hor} + g_{grd}(\theta_{tilt}) G_{grd}}_{\text{diffuse-angular correction [Marion, Solar Energy, 2017]}}.$$

- Irradiance components derived from, e.g., Perez model with MET-station measurement of GHI, DHI, and DNI, or a POA irradiance decomposition.
- Measured shape of $E_{eff}(\lambda)$ is assumed invariant w.r.t. incident angle. Missing “tails” must be extrapolated, here by $E_0(\lambda)$ scaled to match tail integrals.
- Short-circuit temperature coefficient at STC, α_{sc0} , approximates temperature dependence of spectral response $S(\lambda, T)$. More precisely, α_{sc} depends on spectrum.
- Relative measurement of PV device's spectral response at STC, $S(\lambda, T_0)$, is sufficient due to cancellation of any scalar multiplier, including active area A .

Demonstration of Spectral and Diffuse-Angular Corrections in PVfit

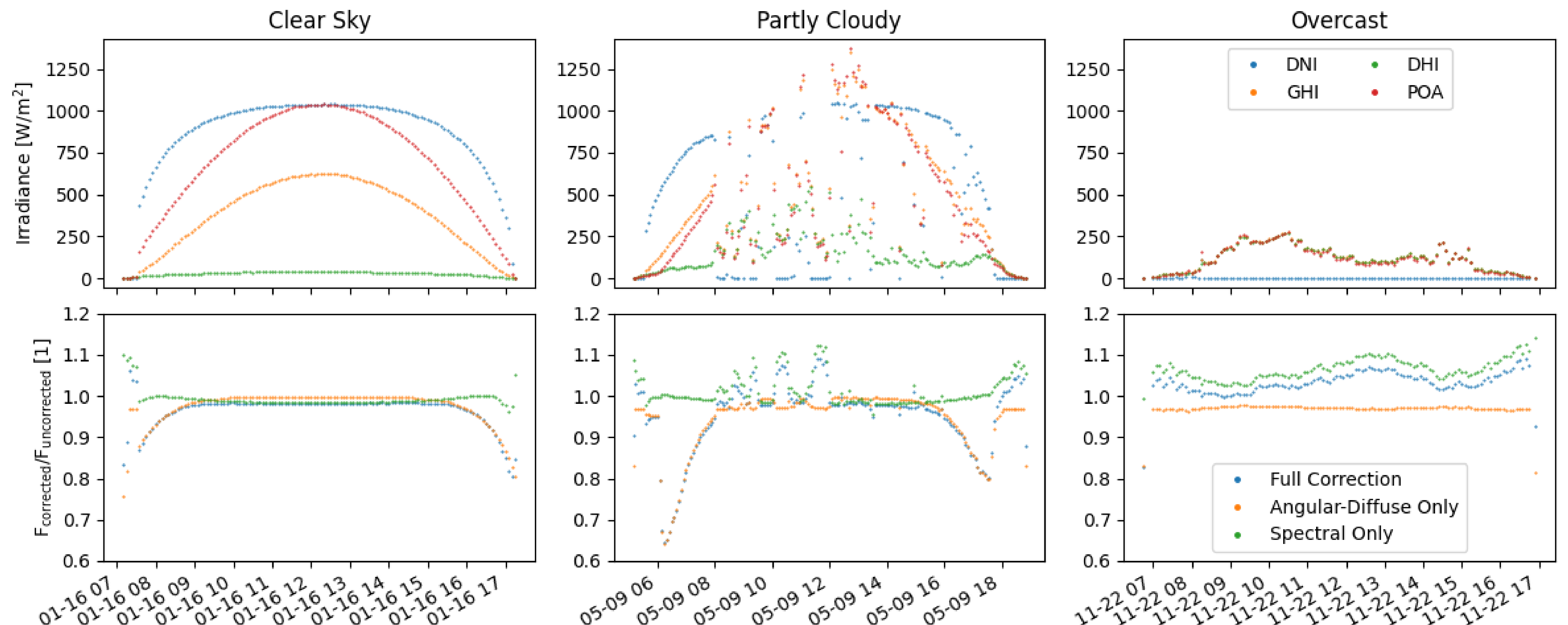


Figure 1: Irradiances and relative F corrections for a x-Si monofacial PV module tilted south 35°, using 5-min MET-station and global normal spectral irradiance measurements in Albuquerque, NM, USA.